(Revision of ASME B31.3-2016)

ASME Code for Pressure Piping, B31

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Process Piping

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FOREWORD

Responding to evident need and at the request of The American Society of Mechanical Engineers (ASME), the American Standards Association initiated Project B31 in March 1926, with ASME as sole administrative sponsor. The breadth of the field involved required that membership of the Sectional Committee be drawn from some 40 engineering societies, industries, government bureaus, institutes, and trade associations.

Initial publication in 1935 was as the American Tentative Standard Code for Pressure Piping. Revisions from 1942 through 1955 were published as American Standard Code for Pressure Piping, ASA B31.1. It was then decided to publish as separate documents the various industry Sections, beginning with ASA B31.8-1955, Gas Transmission and Distribution Piping Systems. The first Petroleum Refinery Piping Code Section was designated ASA B31.3-1959, ASA B31.3 revisions were published in 1962 and 1966.

In 1967–1969, the American Standards Association became first the United States of America Standards Institute, then the American National Standards Institute (ANSI). The Sectional Committee became American National Standards Committee B31 and the Code was renamed the American National Standard Code for Pressure Piping. The next B31.3 revision was designated ANSI B31.3-1973. Addenda were published through 1975.

A draft Code Section for Chemical Plant Piping, prepared by Section Committee B316, was ready for approval in 1974. It was decided, rather than have two closely related Code Sections, to merge the Section Committees and develop a joint Code Section, titled Chemical Plant and Petroleum Refinery Piping. The first edition was published as ANSI B31.3-1976.

In this Code, responsibility for piping design was conceptually integrated with that for the overall processing facility, with safeguarding recognized as an effective safety measure. Three categories of Fluid Service were identified, with a separate Chapter for Category M Fluid Service. Coverage for nonmetallic piping was introduced. New concepts were better defined in five Addenda, the fourth of which added Appendix M, a graphic aid to selection of the proper Fluid Service category.

The Standards Committee was reorganized in 1978 as a Committee operating under ASME procedures with ANSI accreditation. It is now the ASME Code for Pressure Piping B31 Committee. Section committee structure remains essentially unchanged.

The second edition of Chemical Plant and Petroleum Refinery Piping was compiled from the 1976 Edition and its five Addenda, with nonmetal requirements editorially relocated to a separate Chapter. Its new designation was ANSI/ASME R31 3-1980

Section Committee B31.10 had a draft Code for Cryogenic Piping ready for approval in 1981. Again, it was decided to merge the two Section Committees and develop a more inclusive Code with the same title. The work of consolidation was partially completed in the ANSI/ASME B31.3-1984 Edition.

Significant changes were made in Addenda to the 1984 Edition: integration of cryogenic requirements was completed; a new stand-alone Chapter on high-pressure piping was added; and coverage of fabrication, inspection, testing, and allowable stresses was reorganized. The new Edition was designated as ASME/ANSI B31.3-1987 Edition.

Addenda to the subsequent five Editions, published at three-year intervals, were primarily used to keep the Code up to date. New Appendices were added, however, on requirements for bellows expansion joints, estimating service life, submittal of Inquiries, aluminum flanges, and quality control in the 1990, 1993, 1999, and 2002 Editions, all designated as ASME B31.3.

In a program to clarify the application of all Sections of the Code for Pressure Piping, changes were made in the Introduction and Scope statements of the 1996 Edition, and its title was changed to Process Piping.

Under direction of ASME Codes and Standards management, SI (metric) units of measurement were emphasized. With certain exceptions, SI units were listed first in the 1996 Edition and were designated as the standard. Instructions for conversion were given where SI units data were not available. U.S. Customary units also were given. By agreement, either system may have been used.

Beginning with the 2004 Edition, the publication cycle of ASME B31.3 was changed to biennial. Other changes made in the 2004 Edition included the introduction of the weld joint strength reduction factor, W, and the additions of Appendix P, Alternative Rules for Evaluating Stress Range, and Appendix S, Piping System Stress Analysis Examples.

Changes that were made to the 2006 and 2008 Editions of ASME B31.3 included the requirement that valves have blowout-proof stems and the addition of a definition for elevated temperature fluid service, respectively. The most significant change that was made to the 2010 Edition of ASME B31.3 was the addition of Chapter X, High Purity

Piping. In the 2012 Edition, Tables A-1M and A-2M were added to Appendix A that give allowable design values in SI units, and Appendix N, Application of ASME B31.3 Internationally, was also added.

For the 2016 Edition, the allowable design values in SI units as shown in Tables A-1M and A-2M were changed from for information only to values that may be used to meet the requirements of the Code.

In this Edition, SI units are given first, with U.S. Customary units in parentheses. Table K-1 in Appendix K is an exception, containing only U.S. Customary units. The allowable design values in Tables A-1 and A-2 are given in U.S. Customary units, and the SI values are given in Tables A-1M and A-2M. Either the U.S. Customary units or the SI units for these allowable design values may be used. Except for Tables A-1, A-1M, A-2, A-2M, C-1, C-1M, C-6, C-6M, and K-1, values in SI units are to be regarded as the standard, unless otherwise agreed between the contracting parties. Instructions are given in Table K-1 for converting tabular data in U.S. Customary units to appropriate SI units.

Interpretations, Code Cases, and errata to the B31.3 Code on Process Piping are published on the following large: https://cstools.ame.org/csconnect/CommitteePages.fm?Committee=N10020400.

ASME B31.3-2018 was approved by the American National Standards Institute on August 8, 2018. Interpretations, Code Cases, and errata to the B31.3 Code on Process Piping are published on the following ASME web page: https://cstools.asme.org/csconnect/CommitteePages.cfm?Committee=N10020400.

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INTRODUCTION

The ASME B31 Code for Pressure Piping consists of a number of individually published Sections, each an American National Standard, under the direction of ASME Committee B31, Code for Pressure Piping.

Rules for each Section reflect the kinds of piping installations considered during its development, as follows:

- B31.1 Power Piping: piping typically found in electric power generating stations, in industrial and institutional plants, geothermal heating systems, and central and district heating and cooling systems
- B31.3 Process Piping: piping typically found in petroleum refineries; onshore and offshore petroleum and natural gas production facilities; chemical, pharmaceutical, textile, paper, ore processing, semiconductor, and cryogenic plants; food and beverage processing facilities; and related processing plants and terminals
- B31.4 Pipeline Transportation Systems for Liquids and Slurries: piping transporting products that are predominately liquid between plants and terminals and within terminals, pumping, regulating, and metering stations
- B31.5 Refrigeration Piping and Heat Transfer
 Components: piping for refrigerants and secondary coolants
- B31.8 Gas Transmission and Distribution Piping
 Systems: piping transporting products
 that are predominately gas between
 sources and terminals, including
 compressor, regulating, and metering
 stations; gas gathering pipelines
- B31.9 Building Services Piping: piping typically found in industrial, institutional, commercial, and public buildings, and in multi-unit residences, which does not require the range of sizes, pressures, and temperatures covered in B31.1
- B31.12 Hydrogen Piping and Pipelines: piping in gaseous and liquid hydrogen service and pipelines in gaseous hydrogen service

This is the B31.3 Process Piping Code Section. Hereafter, in this Introduction and in the text of this Code Section B31.3, where the word *Code* is used without specific identification, it means this Code Section.

It is the owner's responsibility to select the Code Section that most nearly applies to a proposed piping installation. Factors to be considered by the owner include limitations of the Code Section; jurisdictional requirements; and the applicability of other codes and standards. All applicable requirements of the selected Code Section shall be met. For some installations, more than one Code Section may apply to different parts of the installation. The owner is also responsible for imposing requirements supplementary to those of the Code if necessary to assure safe piping for the proposed installation.

Certain piping within a facility may be subject to other codes and standards, including but not limited to

- ANSI 2223.1 National Fuel Gas Code: piping for fuel gas from the point of delivery to the connection of each fuel utilization device
- NFPA Fire Protection Standards: fire protection Systems using water, carbon dioxide, halon, foam, dry chemicals, and wet chemicals
- NFPA 99 Health Care Facilities: medical and laboratory gas systems
- building and plumbing codes, as applicable, for potable hot and cold water, and for sewer and drain systems

The Code specifies engineering requirements deemed necessary for safe design and construction of pressure piping. While safety is the primary consideration, this factor alone will not necessarily govern the final specifications for any piping installation. The Code is not a design handbook. Many decisions that must be made to produce a sound piping installation are not specified in detail within this Code. The Code does not serve as a substitute for sound engineering judgments by the owner and the designer.

To the greatest possible extent, Code requirements for design are stated in terms of basic design principles and formulas. These are supplemented as necessary with specific requirements to ensure uniform application of principles and to guide selection and application of piping elements. The Code prohibits designs and practices known to be unsafe and contains warnings where caution, but not prohibition, is warranted.

This Code Section includes the following:

- (a) references to acceptable material specifications and component standards, including dimensional requirements and pressure–temperature ratings
- (b) requirements for design of components and assemblies, including piping supports
- (c) requirements and data for evaluation and limitation of stresses, reactions, and movements associated with pressure, temperature changes, and other forces
- (d) guidance and limitations on the selection and application of materials, components, and joining methods
- (e) requirements for the fabrication, assembly, and erection of piping
- (f) requirements for examination, inspection, and testing of piping

ASME Committee B31 is organized and operates under procedures of The American Society of Mechanical Engineers that have been accredited by the American National Standards Institute. The Committee is a continuing one, and keeps all Code Sections current with new developments in materials, construction, and industrial practice. New editions are published at intervals of two years.

Code users will note that paragraphs in the Code are not necessarily numbered consecutively. Such discontinuities result from following a common outline, insofar as practical, for all Code Sections. In this way, corresponding material is correspondingly numbered in most Code Sections, thus facilitating reference by those who have occasion to use more than one Section.

This edition of Code Section B31.3 is not retroactive Normally, agreement is made between contracting parties to use a specific edition, considering requirements of the authority having jurisdiction. When specified as the latest edition and when no edition is specified, the specific edition is the one issued at least 6 months prior to the original contract date for the first design activity.

Users of this Code are cautioned against making use of Code revisions without assurance that they are acceptable to the proper authorities in the jurisdiction where the piping is to be installed.

The B31 Committee has established an orderly procedure to consider requests for interpretation and revision of Code requirements. To receive consideration, such request must be in writing and must give full particulars in accordance with Appendix Z.

The approved reply to an inquiry will be sent directly to the inquirer. In addition, the question and reply will be published as part of an Interpretation supplement.

A Case is the prescribed form of reply when study indicates that the Code wording needs clarification, or when the reply modifies existing requirements of the Code or grants permission to use new materials or alternative constructions. The Case will be published as part of a Case supplement.

Code Cases remain available for use until annulled by the ASME B31 Standards Committee.

A request for revision of the Code will be placed on the Committee's agenda. Further information or active participation on the part of the proponent may be requested during consideration of a proposed revision.

Materials ordinarily are listed in the stress tables only when sufficient usage in piping within the scope of the Code has been shown. Requests for listing shall include evidence of satisfactory usage and specific data to permit establishment of allowable stresses, maximum and minimum temperature limits, and other restrictions. Additional criteria can be found in the guidelines for addition of new materials in the ASME Boiler and Pressure Vessel Code, Section II. (To develop usage and gain experience, unlisted materials may be used in accordance with para. 323.1.2.)

ASME B31.3-2018 SUMMARY OF CHANGES

Following approval by the ASME B31 Committee and ASME, and after public review, ASME B31.3-2018 was approved by the American National Standards Institute on August 8, 2018.

ASME B31.3-2018 includes the following changes identified by a margin note, (18).

		15
Page	Location	Change Revised Subparagraphs (b)(1) and (c)(4) revised Revised Footnote 2 revised
XX	Introduction	Revised
1	300	Subparagraphs (b)(1) and (c)(4) revised Revised Footnote 2 revised Revised (1) Footnote 3 revised
2	300.1	Revised
2	300.1.3	Footnote 2 revised
2	300.1.4	Revised
3	300.2	(1) Footnote 3 revised
		(2) indication, linear; indication, rounded; and stress ratio revised
		(3) owner, readily accessible (for visual examination), and representative added
9	Table 300.4	Entry for Warded
11	301.5	First paragraph deleted
11	301.5.1	Revised
11	301.5.4	Revised
12	302.2.3	Revised in its entirety
12	302.2.4 302.3.2 302.3.5 302.3.6 Table 302.3.5	First paragraph and subpara. (c) revised
14	302.3.2	Revised in its entirety
15	302.3.5	Subparagraphs (c), (e), and (f) revised
18	302.3.6	Subparagraph (a) revised
20	Table 302.3.5	(1) Second column head revised
		(2) First row added
	QN.	(3) General Note (b) and Notes (2), (3), and (9) revised
29	304.5.1	Subparagraph (b) revised
32	306.3.2	Revised
32	306.3.3	Revised
33	306.4.4	Subparagraph (b) revised
33	306.5.2	Revised
33	Table 308.2.1	General Note revised
34	308.3	Revised
34	308.4	Revised
34	309.2.3	First paragraph revised
35	310	Revised
35	311.1	Revised
35	311.2	Paragraphs 311.2.1, 311.2.2, and 311.2.3 deleted, and subsequent paragraphs redesignated

35	312	First paragraph added
36	Table 314.2.1	Revised in its entirety
36	314.2.1	Subparagraphs (a) and (b) revised
36	315.2	Subparagraph (a) revised
36	315.3	Revised
37	318.2.3	Revised
39	319.3.6	Second paragraph revised
40	319.4.4	Subparagraph (c) revised
43	320.2	Second paragraph revised
45	321.3.2	(1) First paragraph revised
		(2) Last paragraph and footnote 10 added
47	323.2.2	Revised in its entirety
48	Table 323.2.2	(1) Last two column heads revised
		(2) Under Type of Material, third entry revised
		(3) Notes (1), (3), (4), (6), and (7) revised
50	Figure 323.2.2A	Previous Note (6) redesignated as (1) and revised; other Notes renumbered
51	Table 323.2.2A	In seventh group of rows, in fourth row, entries under Nominal Thickness revised
52	Figure 323.2.2B	(1) Fahrenheit values corrected by errata and moved to bottom of illustration
		(2) General Notes replaced by one General Note
54	323.3.5	Subparagraphs (b) and (c) revised
57	Table 323.3.5	In first column, last entry revised
60	Table 326.1	(1) ASME B18.31.2 added
	*	(2) Notes (4) and (5) revised
72	Table 330.1.1	For P-No. 5B, first two entries in third row revised
72	331.1.1 335.3.1 340.4	Subparagraph (a) revised
79	335.3.1	Revised
81	340.4	Subparagraph (b)(3) revised
82	341.4.1	Subparagraphs (a)(2) and (a)(3) revised
84	Table 341.3.2	(1) Under Weld Imperfection, fifth entry revised
		(2) For Criteria F and G, main entry under Measure revised
85	Criterion Value Notes for Table 341.3.2	Note (2) [formerly Note (10)] revised
89	344.2.1	Revised
89	344.2.2	Revised
89	344.5.1	Revised
90	344.6.2	Subparagraph (b) corrected by errata
91	345.2.1	Subparagraph (a) revised
91	345.2.5	Revised
93	345.8	(1) Paragraph 345.8.1 added
		(2) Existing text moved to new para. 345.8.2 and subpara. (a) revised
95	A302.2.3	Revised
96	A302.3.2	Footnote 1 revised

97	A302.3.4	Subparagraph (a) revised
101	A319.2.1	Revised in its entirety
102	A319.2.2	Subparagraph (a) revised
107	Table A326.1	(1) ASTM F1545 and AWWA C900 revised
		(2) Note (4) added
114	Table A341.3.2	Revised
119	M323.2	Revised
120	M335.1.1	First cross-reference corrected by errata to read 335.1
124	K300	Subparagraphs (a), (b)(1), and (e) revised
124	K300.1	Revised in its entirety
124	K300.4	Revised
124	K301	Subparagraphs (a), (b)(1), and (e) revised Revised in its entirety Revised (1) First paragraph revised (2) Paragraph K301.1 deleted (3) Paragraph K301.2.1 revised
		(2) Paragraph K301.1 deleted
		(3) Paragraph K301.2.1 revised
		(4) Paragraphs K301.4.2 and K301.73 added
125	K302.2.3	Revised in its entirety
125	K302.2.4	Revised
126	K302.3.3	First paragraph revised
127	K302.3.5	Subparagraph (c) revised
127	K302.3.6	Subparagraph (a) revised
128	K304.1.2	(1) Equations (34a), (34b), (34c), and (34d) revised
		(2) Footnote 3 deleted and subsequent footnotes renumbered
130	K304.7.4	Revised
131	K306.1.1	Revised
133	K314	Revised in its entirety
133	K315	Revised in its entirety
134	K318	Revised
134	K319	Revised
134	K320	Added
135	K323.2	Revised
135	K323.2.1	Revised
136	K323.2.4	Subparagraph (a) revised
139	K326.4	Revised in its entirety
144	Table K341.3.2	Under Type of Imperfection, fifth entry revised
145	Criterion Value Notes for Table K341.3.2	For Symbol C, Measure revised
146	K344.6.3	Subparagraph (b) revised
148	K346.2	Subparagraph (d) revised
151	U328.4	Revised
152	U341.3.2	Revised
157	Specification Index for Appendix A	
161	-	(1) General Note (a) and Notes (6), (30), and (65) revised
	A-1B, A-2, and A-2M	(2) Note (79) added
165	Table A-1	(1) All Note (2) references deleted

- (2) Under Carbon Steel Forgings and Fittings, A694 F42, F46, F52, F56, F60, F65, and F70; A707 L1, L2, and L3; and A860 WPHY 42, WPHY 46, WPHY 52, WPHY 60, WPHY 65, and WPHY 70 added
- (3) Under Low and Intermediate Alloy Steel Pipes, for A671 CFB70 and CFE70, Type/Grade revised
- (4) Under Low and Intermediate Alloy Steel Plates, for A387 9, P-No. revised
- (5) Under Stainless Steel Pipes and Tubes, A312 TP321, A312 TP321H, A376 TP321, and A376 TP321H revised
- (6) A270 TP304L and TP316L added
- (7) A358 321 and A409 TP321 revised
- (8) A358 321H added
- (9) A270 TP316 added
- (10) A270 TP304 added
- (11) A789 and A790 S82441 added
- (12) A789 and A790 S32003 revised
- (13) For A928 S32003, Size revised
- (14) A789 and A790 \$32760 revised
- (15) Under Stainless Steel Plates and Sheets, A240 321 and 321H revised
- (16) A240 S82441 added
- (17) For A240 S32003, Size revised
- (18) A240 S32760 revised
- (19) Under Stainless Steel Forgings and Fittings, A182 F321 and F321H revised
- (20) A403 WP321 and WP321H revised
- (21) Under Stainless Steel Bar, for A479 304, 304H, 304L, 316, 316H, and 316L, Notes revised
- (22) For A479 321 and 321H, stress value for 650°F and font for stress values revised
- (23) A479 S82441 added
- (24) Under Stainless Steel Castings, for A351 CF8C, Notes and stress values revised
- (25) Under Nickel and Nickel Alloy Pipes and Tubes, N08825 B163, B474, and B704 added
- (26) For N08825 B423 and B705, fonts for stress values corrected by errata
- (27) N06690 B163 and B167 added
- (28) N08120 B163, B407, B514, and B515 added
- (29) Under Nickel and Nickel Alloy Plates and Sheets, for N08825 B424, fonts for stress values corrected by errata
- (30) N06690 B168 added
- (31) N08120 B409 added
- (32) Under Nickel and Nickel Alloy Forgings and Fittings, for N02200 B366, stress value revised
- (33) N02200 B564 deleted

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- (34) For N08825 B366 and B564, fonts for stress values corrected by errata
- (35) N06690 B564 added
- (36) N08120 B366 and B564 added
- (37) Under Nickel and Nickel Alloy Rod and Bar, for N08825 B425, fonts for stress values corrected by errata
- (38) N06690 B166 added
- (39) N08120 B408 added
- (40) For the titanium and titanium alloys, Product Form and Class/Condition/Temper entries added, and stress values revised
- (41) Under Titanium and Titanium Alloy Pipes and Tubes, R50250, R50400, R50550, R52400, and R53400 B338 added
- (42) R53400 B861 and B862 added
- (43) Under Titanium and Titanium Allow Plates, Sheet, and Strips (formerly Plates and Sheets), for R50250 B265, Specified Min. Yield Strength revised
- (44) R52400 and R53400 B265 added
- (45) Under Titanium and Titanium Alloy Forgings and Fittings (formerly Forgings), R50250, R50400, R50550, R52400, and R53400 B363 added
- (46) For R50250 B381, Type/Grade and Specified Min. Yield Strength revised
- (47) For R50400 and R50550 B381, Type/Grade revised
- (48) R52400 and R53400 B381 added
- (49) Under Titanium and Titanium Alloy Bars, R50250, R50400, R50550, R52400, and R53400 B348 added
- (50) Under Titanium and Titanium Alloy Castings, R52550 and R52700 B367 added
- (51) Under Aluminum Alloy Seamless Pipes and Tubes, A83003, A91060, A93003, A95083, A95086, A96061, and A96063 B345 deleted
- (52) Under Aluminum Alloy Castings, for A03560 B26, P-Nos. added
- (1) All Note (2) references deleted
- (2) A694 F42, F46, F52, F56, F60, F65, and F70; A707 L1, L2, and L3; and A860 WPHY 42, WPHY 46, WPHY 52, WPHY 60, WPHY 65, and WPHY 70 added
- (3) For A671 CFB70 and CFE70, Type/Grade revised
- (4) For A387 9, P-No. revised
- (5) A270 TP304L and TP316L added
- (6) A312 TP321, A312 TP321H, A358 321, A376 TP321, A376 TP321H, and A409 TP321 revised
- (7) A358 321H added
- (8) A270 TP304, TP304L, TP316, and TP316L added
- (9) A789 and A790 S82441 added
- (10) A789 and A790 S32003 revised
- (11) For A928 S32003, Size revised
- (12) A789 and A790 S32760 revised

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- (13) A358 S34565 revised
- (14) A240 321 and 321H revised
- (15) A240 S82441 added
- (16) For A240 S32003, Size revised
- (17) A240 S32760 revised
- (18) A182 F321 and F321H revised
- (19) A403 WP321 and WP321H revised
- (20) A182 and A815 S32760 revised
- (21) For A479 304, 304H, 304L, 316, 316H, and 316L, Notes revised
- (22) A479 321 and 321H revised
- (23) A479 S82441 added
- (24) A351 CF8C revised
- (25) N08825 B163 added
- (26) For N08825 B423, Notes revised
- (27) N08825 B474 and B704 added
- (28) N08825 B705 revised
- (29) N06690 B163 and B167 added
- (30) N08120 B163, B407, B514, and B515 added
- (31) For N06230 B619, B622, and B626, font for stress values

- (34) For N06230 B435, font for stress values revised

- (40) For N06230 B366, font for stress values revised

- (43) For N06230 B572, font for stress values revised
- (44) For titanium and titanium alloy materials, Product Form and Class/Condition/Temper entries added; and Min. Tensile Strength, Min. Yield Strength, and stress values revised
- (45) R50250, R50400, R50550, R52400, and R53400 B338 added
- (47) R52400 and R53400 B265 added
- (48) R50250, R50400, R50550, R52400, and R53400 B363 and B381 added
- (49) R50250, R50400, R50550, R52400, and R53400 B348 added
- (50) R52550 and R52700 B367 added
- (51) A83003, A91060, A93003, A95083, A95086, A96061, and A96063 B345 deleted
- (52) For A03560 B26, P-Nos. added

351 Table A-1B (1) A105, A181, A350, A182, A487, B160, B164, B564, B247, and B345 deleted (2) A813, A814, B517, and B862 revised (3) A270, B163, B515, B704, and B338 added (3) A356 deleted (2) F3125 A325 added (3) A354 BC and BD lines revised and new BC line added (4) For last B150 HR50, Size Range corrected by errata (2) A325 deleted (3) F3125 A325 added (4) A354 BC and BD lines revised and new BC line added (4) A354 BC and BD lines revised and new BC line added (5) For last B150 HR50, Size Range corrected by errata (2) A325 deleted (3) F3125 A325 added (4) A354 BC and BD lines revised and new BC line added (5) For last B150 HR50, Size Range corrected by errata 396 Table C-1M Table C-2 redesignated as Table C-1M 403 Table C-6 Revised in its entirety 407 Table C-6M Added 413 Table D300 General Note (b) added 417 Appendix E Revised in its entirety 423 F300.1.4 Added (2) Paragraph F391.5.1 added (2) Paragraph F301.11 deleted 424 F308.4	350	Table A-1A	B367 added
(2) A813, A814, B517, and B862 revised (3) A270, B163, B515, B704, and B338 added (1) A325 deleted (2) F3125 A325 added (3) A354 BC and BD lines revised and new BC line added (4) For last B150 HR50, Size Range corrected by errata (2) A325 deleted (3) F3125 A325 added (4) For A307 B, Min. Yield Strength deleted by errata (2) A325 deleted (3) F3125 A325 added (4) A354 BC and BD lines revised and new BC line added (5) For last B150 HR50, Size Range corrected by errata Table C-2 redesignated as Table C-1M Table C-6 Revised in its entirety Added Table D300 General Note (b) added F300.1.4 Added C3 Paragraph F301.5.1 added (2) Paragraph F301.11 deleted Revised Revised Revised Revised	351	Table A-1B	(1) A105, A181, A350, A182, A487, B160, B164, B564, B247, and
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(2) Paragraph F301.11 deleted 424 F308.4 Revised			XV.
424 F308.4 Revised	423	F301	
425 F312.1 Subparagraph (b) revised			
426 F323.2.2 Revised			
426 F323.4 Subparagraphs (a) and (c)(4) revised			
428 FK300 Added		•	
439 Appendix J (1) Entry for X deleted by errata	439	Appendix J	
(2) Appendix revised 455 Appendix K ASTM A789, A790, and A815 added to Specification Index	4.55	Appendix K	
457 Notes for Table K- (1) General Note (b) revised	457	Notes for Table K	•
(2) Notes (9) and (10) deleted	107	Notes for Tuble 154	
(3) Notes (19) and (20) added			
458 Table K-1 (1) Under Carbon Steel — Pipes and Tubes, API 5L lines revised	458	Table K-1	
(2) Under Carbon Steel — Forgings and Fittings, for A694 F42			•
457 Notes for Table K-1 (1) General Note (b) revised (2) Notes (9) and (10) deleted (3) Notes (19) and (20) added (1) Under Carbon Steel — Pipes and Tubes, API 5L lines revised (2) Under Carbon Steel — Forgings and Fittings, for A694 F42 through F70, stress values for highest temperatures deleted (3) For Stainless Steel entries, UNS Nos. added (4) Under Stainless Steel — Pipes and Tubes, A789 and A790		alk	
(3) For Stainless Steel entries, UNS Nos. added		Si	(3) For Stainless Steel entries, UNS Nos. added
(4) Under Stainless Steel — Pipes and Tubes, A789 and A790 S32750 added		Y	
(5) Under Stainless Steel — Forgings and Fittings, A182 and A815 S32750 added			
(6) Titanium and Titanium Alloy entries revised, and entries in columns for 350°C, 450°F, and 550°F added			
Figure M300 Cross-references in Col. 1 revised	474	Figure M300	Cross-references in Col. 1 revised
476 Appendix Q Footnote 1 revised	476	Appendix Q	Footnote 1 revised
477 R300 Subparagraph (a) corrected by errata	477	R300	Subparagraph (a) corrected by errata

480	Appendix S	Footnote 1 added			
482	S301.6	First paragraph revised			
492	V303.1.1	Subparagraph (b) revised			
493	V303.1.3	Revised			
495	Appendix W	Added			
502		In subparagraph (d), last cross-reference corrected by errata to read Table 331.1.1			
502	X302.2.3	Subparagraph (a) revised			
504	Appendix Z	Revised in its entirety			
In subparagraph (d), last cross-reference corrected by errata to read Table 331.1.1 502 X302.2.3 Subparagraph (a) revised Subparagraph (a) revised Revised in its entirety NOTES: (1) The ASME B31.3 Interpretations Volume will no longer be published with the Code. (2) The B31.3 Code Cases will no longer be published with the Code.					

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Chapter I Scope and Definitions

(18) 300 GENERAL STATEMENTS

(a) Identification. This Process Piping Code is a Section of The American Society of Mechanical Engineers Code for Pressure Piping, ASME B31, an American National Standard. It is published as a separate document for convenience of Code users.

(b) Responsibilities

- (1) Owner. The owner of a piping installation shall have overall responsibility for compliance with this Code, and for establishing the requirements for design, construction, examination, inspection, and testing that will govern the entire fluid handling or process installation of which the piping is a part. The owner is also responsible for designating piping in Category D, Category M, High Pressure, and High Purity Fluid Services, and for determining if a specific Quality System is to be employed. [See paras. 300(d)(4) through (7) and Appendix Q.] Where applicable, the owner shall consider requirements? imposed by the authority having jurisdiction regarding the piping installation. The owner may designate a representative to carry out selected responsibilities required by this Code, but the owner retains ultimate responsibility for the actions of the representative.
- (2) Designer. The designer is responsible to the owner for assurance that the engineering design of piping complies with the requirements of this Code and with any additional requirements established by the owner.
- (3) Manufacturer, Fabricator, and Erector. The manufacturer, fabricator, and erector of piping are responsible for providing materials, components, and workmanship in compliance with the requirements of this Code and of the engineering design.
- (4) Owner's Inspector. The owner's Inspector (see para. 340) is responsible to the owner for ensuring that the requirements of this Code for inspection, examination, and testing are met. If a Quality System is specified by the owner to be employed, the owner's Inspector is responsible for verifying that it is implemented.

(c) Intent of the Code

- (1) It is the intent of this Code to set forth engineering requirements deemed necessary for safe design and construction of piping installations.
- (2) This Code is not intended to apply to the operation, examination, inspection, testing, maintenance, or repair of piping that has been placed in service. See

para. F300.1 for examples of standards that may apply in these situations. The provisions of this Code may optionally be applied for those purposes, although other considerations may also be necessary.

- (3) The Code generally specifies a simplified approach for many of its requirements. A designer may choose to use a more rigorous analysis to develop design and construction requirements. When the designer decides to take this approach, the designer shall provide to the owner details and calculations demonstrating that design, construction, examination, and testing are consistent with the design criteria of this Code. These details shall be adequate for the owner to verify the validity and shall be approved by the owner. The details shall be documented in the engineering design.
- (4) Piping elements shall conform to the specifications and standards listed in this Code or, if not prohibited by this Code, shall be qualified for use as set forth in applicable Chapters of this Code.
- (5) The engineering design shall specify any unusual requirements for a particular service. Where service requirements necessitate measures beyond those required by this Code, such measures shall be specified by the engineering design. Where so specified, the Code requires that they be accomplished.
- (6) Compatibility of materials with the service and hazards from instability of contained fluids are not within the scope of this Code. See para. F323.

(d) Determining Code Requirements

- (1) Code requirements for design and construction include fluid service requirements, which affect selection and application of materials, components, and joints. Fluid service requirements include prohibitions, limitations, and conditions, such as temperature limits or a requirement for safeguarding (see Appendix G). Code requirements for a piping system are the most restrictive of those that apply to any of its elements.
- (2) For metallic piping not designated by the owner as Category M, High Pressure, or High Purity Fluid Service (see para. 300.2 and Appendix M), Code requirements are found in Chapters I through VI (the base Code) and fluid service requirements are found in
 - (-a) Chapter III for materials
 - (-b) Chapter II, Part 3, for components
 - (-c) Chapter II, Part 4, for joints

- (3) For nonmetallic piping and piping lined with nonmetals, all requirements are found in Chapter VII. Paragraph designations begin with "A."
- (4) For piping in a fluid service designated as Category M, all requirements are found in Chapter VIII. Paragraph designations begin with "M."
- (5) For piping in a fluid service designated as Category D, piping elements restricted to Category D Fluid Service in Chapters I through VII, as well as elements suitable for other fluid services, may be used.
- (6) For piping designated as High Pressure Fluid Service, all requirements are found in Chapter IX. These rules apply only when specified by the owner. Paragraph designations begin with "K."
- (7) For piping designated as High Purity Fluid Service, all requirements are found in Chapter X. Paragraph designations begin with "U."
- (8) Requirements for Normal Fluid Service in Chapters I through VI are applicable under severe cyclic conditions unless alternative requirements for severe cyclic conditions are stated.
- (9) Requirements for Normal Fluid Service in Chapters I through VI are applicable for Elevated Temperature Fluid Service unless alternative requirements for Elevated Temperature Fluid Service are invoked.
- (e) Appendices. Appendices of this Code contain Code requirements, supplementary guidance, or other information. See para. 300.4 for a description of the status of each Appendix.
- (f) Code Cases. ASME issues Code Cases that are applicable to this Code. The Code Cases
 - (1) modify the requirements of this Code
- (2) are applicable from the issue date until the Cases are annulled
- (3) may be used only when approved by the owner. When so approved, the Code Cases shall be specified in the engineering design and become requirements of this Code.

(18) **300.1 Scope**

Rules for the Process Piping Code Section B31.3¹ have been developed considering piping typically found in petroleum refineries; onshore and offshore petroleum and natural gas production facilities; chemical, pharmaceutical, textile, paper, ore processing, semiconductor, and cryogenic plants; food and beverage processing facilities; and related processing plants and terminals.

300.1.1 Content and Coverage

- (a) This Code prescribes requirements for materials and components, design, fabrication, assembly, erection, examination, inspection, and testing of piping.
 - (b) This Code applies to piping for all fluids, including

- (1) raw, intermediate, and finished chemicals
- (2) petroleum products
- (3) gas, steam, air, and water
- (4) fluidized solids
- (5) refrigerants
- (6) cryogenic fluids
- (c) See Figure 300.1.1 for a diagram illustrating the application of B31.3 piping at equipment. The joint connecting piping to equipment is within the scope of B31.3.
- **300.1.2 Packaged Equipment Piping.** Also included within the scope of this Code is piping that interconnects pieces or stages within a packaged equipment assembly.
 - **300.1.3 Exclusions.** This Code excludes the following: (18)
- (a) piping systems designed for internal gage pressures at or above zero but less than 105 kPa (15 psi), provided the fluid handled is nonflammable, nontoxic, and not damaging to human tissues as defined in 300.2, and its design temperature is from -29°C (-20°F) through 186°C (366°F)
- (b) power boilers in accordance with ASME BPVC,² Section I and boiler external piping that is required to conform to ASME B31.1
- (c) tubes, tube headers, crossovers, and manifolds of fired heaters that are internal to the heater enclosure
- (d) pressure vessels, heat exchangers, pumps, compressors, and other fluid handling or processing equipment, including internal piping and connections for external piping
 - **300.1.4 Rounding.** The rules described in this paragraph apply unless otherwise specified in the Code or the engineering design. For purposes of determining conformance with specified limits in this Code, an observed value or a calculated value shall be rounded "to the nearest unit" in the last right-hand significant digit used in expressing the requirement, in accordance with the rounding method of ASTM E29, Using Significant Digits in Test Data to Determine Conformance with Specifications. ASTM E29 requires that when rounding a number to one having a specified number of significant digits, choose that which is nearest. If two choices are possible, as when the digits dropped are exactly a 5 or a 5 followed only by zeros, choose that ending in an even digit. See Appendix F, para. F300.1.4.

¹ B31 references here and elsewhere in this Code are to the ASME B31 Code for Pressure Piping and its various Sections, which are identified and briefly described in the Introduction.

² ASME BPVC references here and elsewhere in this Code are to the ASME Boiler and Pressure Vessel Code and its various Sections as follows:

Section I, Rules for Construction of Power Boilers

Section II, Materials, Parts C and D

Section III, Rules for Construction of Nuclear Facility Components, Division 1, Subsection NH

Section V. Nondestructive Examination

Section VIII, Rules for Construction of Pressure Vessels, Divisions 1, 2, and 3

Section IX, Welding, Brazing, and Fusing Qualifications

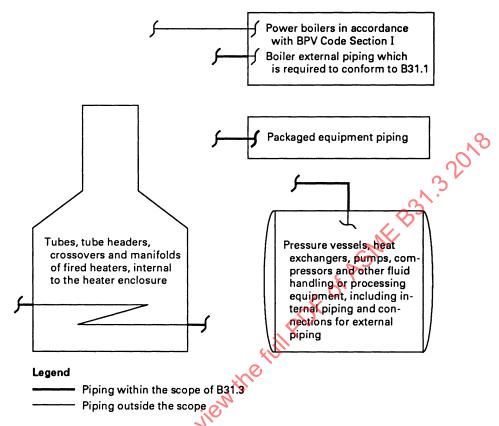


Figure 300.1.1 Diagram Illustrating Application of B31.3 Piping at Equipment

GENERAL NOTE: The means by which piping is attached to equipment is within the scope of the applicable piping code.

(18) 300.2 Definitions

Some of the terms relating to piping are defined below. For welding, brazing, and soldering terms not shown here, definitions in accordance with AWS Standard A3.0³ apply. *air-hardened steel:* a steel that hardens during cooling in air from a temperature above its transformation range. *anneal heat treatment:* see *heat treatment*.

arc cutting: a group of cutting processes wherein the severing or removing of metals is effected by melting with the heat of an arc between an electrode and the base metal. (Includes carbon-arc cutting, metal-arc cutting, gas metal-arc cutting, gas tungsten-arc cutting, plasma-arc cutting, and air carbon-arc cutting.) See also oxygen-arc cutting.

arc welding (AW): a group of welding processes that produces coalescence of metals by heating them with an arc or arcs, with or without the application of pressure and with or without the use of filler metal.

assembly: the joining together of two or more piping components by bolting, welding, bonding, screwing, brazing, soldering, cementing, or use of packing devices as specified by the engineering design.

autogenous weld: a weld made by fusion of the base metal without the addition of filler metal [see also gas tungstenarc welding (GTAW)].

automatic welding: welding with equipment that performs the welding operation without adjustment of the controls by an operator. The equipment may or may not perform the loading and unloading of the work.

backing filler metal: see consumable insert.

backing ring: material in the form of a ring used to support molten weld metal.

balanced piping system: see para. 319.2.2(a).

base material: the material to be brazed, soldered, welded, or otherwise fused.

basic allowable stress: see stress terms frequently used. bolt design stress: see stress terms frequently used.

 $^{^3}$ AWS A3.0M/A3.0, Standard Welding Terms and Definitions, Including Terms for Adhesive Bonding, Brazing, Soldering, Thermal Cutting and Thermal Spraying

bonded joint: a permanent joint in nonmetallic piping made by one of the following methods:

- (a) adhesive joint: a joint made by applying an adhesive to the surfaces to be joined and pressing them together
- (b) butt-and-wrapped joint: a joint made by butting together the joining surfaces and wrapping the joint with plies of reinforcing fabric saturated with resin
- (c) heat fusion joint: a joint made by heating the surfaces to be joined and pressing them together to achieve fusion
- (d) hot gas welded joint: a joint made by simultaneously heating the surfaces to be joined and a filler material with a stream of hot air or hot inert gas, then pressing the surfaces together and applying the filler material to achieve fusion
- (e) solvent cemented joint: a joint made by using a solvent cement to soften the surfaces to be joined and pressing them together
- (f) electrofusion joint: a joint made by heating the surfaces to be joined using an electrical resistance wire coil that remains embedded in the joint.

bonder: one who performs a manual or semiautomatic bonding operation.

bonding operator: one who operates machine or automatic bonding equipment.

bonding procedure: the detailed methods and practices involved in the production of a bonded joint.

bonding procedure specification (BPS): the document that lists the parameters to be used in the construction of bonded joints in accordance with the requirements of this Code.

borescopic examination: a visual examination aided by a mechanical or electromechanical device to examine the inside diameter of inaccessible welds.

branch connection fitting: an integrally reinforced fitting welded to a run pipe and connected to a branch pipe by a buttwelding, socket welding, threaded, or flanged joint; includes a branch outlet fitting conforming to MSS SP-97.

brazing: a metal joining process wherein coalescence is produced by use of a nonferrous filler metal having a melting point above 427°C (800°F), but lower than that of the base metals being joined. The filler metal is distributed between the closely fitted surfaces of the joint by capillary attraction.

butt joint: a joint between two members aligned approximately in the same plane.

Category D: see fluid service.

Category M: see fluid service.

caulked joint: a joint in which suitable material (or materials) is either poured or compressed by the use of tools into the annular space between a bell (or hub) and spigot (or plain end), thus comprising the joint seal.

chemical plant: an industrial plant for the manufacture or processing of chemicals, or of raw materials or intermediates for such chemicals. A chemical plant may include supporting and service facilities, such as storage, utility, and waste treatment units.

cold spring: see para. 319.2.4.

compression type tube fittings: tube fittings consisting of a flareless, mechanical grip connection, including a body, nut, and single or dual ferrules. See also para. U306.6.

connections for external piping: those integral parts of individual pieces of equipment that are designed for attachment of external piping.

consumable insert: preplaced filler metal that is completely fused into the root of the joint and becomes part of the weld.

damaging to human tissues: for the purposes of this Code, this phrase describes a fluid service in which exposure to the fluid, caused by leakage under expected operating conditions, can harm skin, eyes, or exposed mucous membranes so that irreversible damage may result unless prompt restorative measures are taken. (Restorative measures may include flushing with water, administration of antidotes, or medication.)

design minimum temperature: see para. 301.3.1.

design pressure: see para. 301.2.

design temperature: see para. 301.3.

designer: the person or organization in responsible charge of the engineering design.

displacement stress range: see para. 319.2.3.

elements: see piping elements.

engineering design: the detailed design governing a piping system, developed from process and mechanical requirements, conforming to Code requirements, and including all necessary specifications, drawings, and supporting documents.

equipment connection: see connections for external piping.

erection: the complete installation of a piping system in the locations and on the supports designated by the engineering design including any field assembly, fabrication, examination, inspection, and testing of the system as required by this Code.

examination, examiner: see paras. 341.1 and 341.2.

examination, types of: see para. 344.1.3 for the following:

- (a) 100% examination
- (b) random examination
- (c) spot examination
- (d) random spot examination

extruded outlet header: see para. 304.3.4.

fabrication: the preparation of piping for assembly, including cutting, threading, grooving, forming, bending, and joining of components into subassemblies. Fabrication may be performed in the shop or in the field.

face of weld: the exposed surface of a weld on the side from which the welding was done.

face seal fitting: a High Purity Fluid Service fitting that incorporates two machined faces and a metallic gasket within an external/internal nut configuration to attain a high leak integrity seal. See also para. U315.3(b).

filler material: the material to be added in making metallic or nonmetallic joints.

fillet weld: a weld of approximately triangular cross section joining two surfaces approximately at right angles to each other in a lap joint, tee joint, or corner joint. (See also size of weld and throat of a fillet weld.)

flammable: for the purposes of this Code, describes a fluid that under ambient or expected operating conditions is a vapor or produces vapors that can be ignited and continue to burn in air. The term thus may apply, depending on service conditions, to fluids defined for other purposes as flammable or combustible.

fluid service: a general term concerning the application of a piping system, considering the combination of fluid properties, operating conditions, and other factors that establish the basis for design of the piping system. See Appendix M.

- (a) Category D Fluid Service: a fluid service in which all of the following apply:
- (1) the fluid handled is nonflammable, nontoxic, and not damaging to human tissues as defined in para. 300.2
- (2) the design gage pressure does not exceed 1 035 kPa (150 psi)
- (3) the design temperature is not greater than 186°C (366°F)
- (4) the fluid temperature caused by anything other than atmospheric conditions is not less than -29°C (-20°F)
- (b) Category M Fluid Service: a fluid service in which both of the following apply:
- (1) the fluid is so highly toxic that a single exposure to a very small quantity of the fluid, caused by leakage, can produce serious irreversible harm to persons on breathing or bodily contact, even when prompt restorative measures are taken
- (2) after consideration of piping design, experience, service conditions, and location, the owner determines that the requirements for Normal Fluid Service do not sufficiently provide the leak tightness required to protect personnel from exposure
- (c) Elevated Temperature Fluid Service: a fluid service in which the piping metal temperature is sustained equal to or greater than T_{cr} as defined in Table 302.3.5, General Note (b).

- (d) High Pressure Fluid Service: a fluid service for which the owner specifies the use of Chapter IX for piping design and construction; see also para. K300.
- (e) High Purity Fluid Service: a fluid service that requires alternative methods of fabrication, inspection, examination, and testing not covered elsewhere in the Code, with the intent to produce a controlled level of cleanness. The term thus applies to piping systems defined for other purposes as high purity, ultra high purity, hygienic, or aseptic.
- (f) Normal Fluid Service: a fluid service pertaining to most piping covered by this Code, i.e., not subject to the rules for Category D, Category M, Elevated Temperature, High Pressure, or High Purity Fluid Service.

full fillet weld: a fillet weld whose size is equal to the thickness of the thinner member joined.

fusion: the melting together of filler material and base material, or of base material only, that results in coalescence.

gas metal-arc welding (GMAW): an arc-welding process that produces coalescence of metals by heating them with an arc between a continuous filler metal (consumable) electrode and the work. Shielding is obtained entirely from an externally supplied gas, or gas mixture. Some variations of this process are called MIG or CO_2 welding (nonpreferred terms).

gas tungsten-arc welding (GTAW): an arc-welding process that produces coalescence of metals by heating them with an arc between a single tungsten (nonconsumable) electrode and the work. Shielding is obtained from a gas or gas mixture. Pressure may or may not be used and filler metal may or may not be used. (This process has sometimes been called TIG welding.)

gas welding: a group of welding processes wherein coalescence is produced by heating with a gas flame or flames, with or without the application of pressure, and with or without the use of filler material.

groove weld: a weld made in the groove between two members to be joined.

heat affected zone: that portion of the base material which has not been melted, but whose mechanical properties or microstructure have been altered by the heat of welding, brazing, soldering, forming, or cutting.

heat treatment: the following terms describe various types and processes of heat treatment:

- (a) annealing: heating to and holding at a suitable temperature above the transformation temperature range, followed by slow cooling to well below the transformation temperature range.
- (b) normalizing: heating a ferrous metal to a temperature above the transformation temperature range, followed by cooling in room-temperature still air to well below the transformation temperature range.

- (c) quenching: when used as a part of a heat-treating operation, a rapid cooling process that results in microstructural stabilization or changes in material properties that would not have occurred without rapid cooling.
- (d) recommended or required heat treatment: the application of heat to a metal section subsequent to a cutting, forming, or welding operation, as provided in para. 331.
- (e) solution heat treatment: heating an alloy to a suitable temperature, holding at that temperature long enough to allow one or more constituents to enter into solid solution, and then cooling rapidly enough to hold the constituents in solution.
- (f) stress-relief: uniform heating of a structure or portion thereof to a sufficient temperature below the transformation temperature range to relieve the major portion of the residual stresses, followed by uniform cooling slowly enough to minimize development of new residual stresses.
- (g) tempering: reheating a hardened metal to a temperature below the transformation range to improve toughness.
- (h) transformation range: the temperature range over which a phase change occurs.
- (i) transformation temperature: the temperature at which a phase change begins or ends. In metals, phase changes can be solid-state changes.

High Pressure Fluid Service: see fluid service.

High Purity Fluid Service: see fluid service.

hygienic clamp joint: a tube outside-diameter union consisting of two neutered ferrules having flat faces with a concentric groove and mating gasket that is secured with a clamp, providing a nonprotruding, recessless product contact surface. See also para. U3(153(b).

indication, linear: in nondestructive examination, an indication having a length greater than 3 times its width.

indication, rounded: in nondestructive examination, an indication with a length equal to or less than 3 times its width. These indications may be circular, elliptical, conical, or irregular in shape and may have tails.

inline portions of instruments: pressure-containing portions of instruments that are in direct contact with the fluid when installed in a piping system. Permanently sealed fluid-filled tubing systems furnished with instruments as temperature- or pressure-responsive devices, e.g., pressure gages, pressure transmitters, and transducers, are excluded.

in-process examination: see para. 344.7.

inspection, Inspector: see para. 340.

integrally reinforced branch connection fitting: see branch connection fitting.

joint design: the joint geometry together with the required dimensions of the welded joint.

listed: for the purposes of this Code, describes a material or component that conforms to a specification in Appendix A, Appendix B, or Appendix K or to a standard in Table 326.1, A326.1, or K326.1.

manual welding: a welding operation performed and controlled completely by hand.

may: a term that indicates a provision is neither required nor prohibited.

mechanical joint: a joint for the purpose of mechanical strength or leak resistance, or both, in which the mechanical strength is developed by threaded, grooved, rolled, flared, or flanged pipe ends; or by bolts, pins, toggles, or rings; and the leak resistance is developed by threads and compounds, gaskets, rolled ends, caulking, or machined and mated surfaces.

miter or miter bend: for the purposes of this Code, two or more straight sections of pipe matched and joined in a plane bisecting the angle of junction so as to produce a change in direction greater than 3 deg.

nominal: a numerical identification of dimension, capacity, rating, or other characteristic used as a designation, not as an exact measurement.

Normal Fluid Service: see fluid service.

normalizing: see heat treatment.

notch-sensitive: describes a metal subject to reduction in strength in the presence of stress concentration. The degree of notch sensitivity is usually expressed as the strength determined in a notched specimen divided by the strength determined in an unnotched specimen, and can be obtained from either static or dynamic tests.

NPS: nominal pipe size (followed, when appropriate, by the specific size designation number without an inch symbol).

orbital welding: automatic or machine welding in which the electrode rotates (orbits) around the circumference of a stationary pipe or tube.

owner: the person, partnership, organization, or business ultimately responsible for design, construction, operation, and maintenance of a facility.

oxygen-arc cutting (OAC): an oxygen-cutting process that uses an arc between the workpiece and a consumable electrode, through which oxygen is directed to the workpiece. For oxidation-resistant metals, a chemical flux or metal powder is used to facilitate the reaction.

oxygen cutting (OC): a group of thermal cutting processes that severs or removes metal by means of the chemical reaction between oxygen and the base metal at elevated temperature. The necessary temperature is maintained by the heat from an arc, an oxyfuel gas flame, or other source.

oxygen gouging: thermal gouging that uses an oxygen cutting process variation to form a bevel or groove.

packaged equipment: an assembly of individual pieces or stages of equipment, complete with interconnecting piping and connections for external piping. The assembly may be mounted on a skid or other structure prior to delivery.

petroleum refinery: an industrial plant for processing or handling of petroleum and products derived directly from petroleum. Such a plant may be an individual gasoline recovery plant, a treating plant, a gas processing plant (including liquefaction), or an integrated refinery having various process units and attendant facilities.

pipe: a pressure-tight cylinder used to convey a fluid or to transmit a fluid pressure, ordinarily designated "pipe" in applicable material specifications. Materials designated "tube" or "tubing" in the specifications are treated as pipe when intended for pressure service. Types of pipe, according to the method of manufacture, are defined as follows:

- (a) electric resistance-welded pipe: pipe produced in individual lengths or in continuous lengths from coiled skelp and subsequently cut into individual lengths, having a longitudinal butt joint wherein coalescence is produced by the heat obtained from resistance of the pipe to the flow of electric current in a circuit of which the pipe is a part, and by the application of pressure.
- (b) furnace butt welded pipe, continuous welded: pipe produced in continuous lengths from coiled skelp and subsequently cut into individual lengths, having its longitudinal butt joint forge welded by the mechanical pressure developed in passing the hot-formed and edgeheated skelp through a set of round pass welding rolls.
- (c) electric-fusion welded pipe: pipe having a longitudinal butt joint wherein coalescence is produced in the preformed tube by manual or automatic electric-arc welding. The weld may be single (welded from one side) or double (welded from inside and outside) and may be made with or without the addition of filler metal.
- (d) double submerged-arc welded pipe: pipe having a longitudinal buttjoint produced by at least two passes, one of which is on the inside of the pipe. Coalescence is produced by heating with an electric arc or arcs between the bare metal electrode or electrodes and the work. The welding is shielded by a blanket of granular fusible material on the work. Pressure is not used and filler metal for the inside and outside welds is obtained from the electrode or electrodes.
- (e) seamless pipe: pipe produced by piercing a billet followed by rolling or drawing, or both.
- (f) spiral (helical seam) welded pipe: pipe having a helical seam with a butt, lap, or lock-seam joint that is welded using an electrical resistance, electric fusion, or double-submerged arc welding process.

pipe-supporting elements: pipe-supporting elements consist of fixtures and structural attachments as follows:

(a) fixtures: fixtures include elements that transfer the load from the pipe or structural attachment to the supporting structure or equipment. They include hanging type fixtures, such as hanger rods, spring hangers, sway braces, counterweights, turnbuckles, struts, chains, guides, and anchors; and bearing type fixtures, such as saddles, bases, rollers, brackets, and sliding supports.

(b) structural attachments: structural attachments include elements that are welded, bolted, or clamped to the pipe, such as clips, lugs, rings, clamps, clevises, straps, and skirts.

piping: assemblies of piping components used to convey, distribute, mix, separate, discharge, meter, control, or snub fluid flows. Piping also includes pipe-supporting elements, but does not include support structures, such as building frames, bents, foundations, or any equipment excluded from this Code (see para. 300.1.3).

piping components: mechanical elements suitable for joining or assembly into pressure-tight fluid-containing piping systems. Components include pipe, tubing, fittings, flanges, gaskets, bolting, valves, and devices such as expansion joints, flexible joints, pressure hoses, traps, strainers, inline portions of instruments, and separators.

piping elements: any material or work required to plan and install a piping system. Elements of piping include design specifications, materials, components, supports, fabrication, examination, inspection, and testing.

piping installation: designed piping systems to which a selected Code edition and addenda apply.

piping Wbassembly: a portion of a piping system that consists of one or more piping components.

piping system: interconnected piping subject to the same set or sets of design conditions.

welding. The weld may be single (welded from one side) or double (welded from inside and outside) and uses a constricted arc and removes molten metal with may be made with or without the addition of filler metal a high velocity jet of ionized gas issuing from the constricting orifice.

postweld heat treatment: see heat treatment.

preheating: the application of heat to the base material immediately before or during a forming, welding, or cutting process. See para. 330.

procedure qualification record (PQR): a document listing all pertinent data, including the essential variables employed and the test results, used in qualifying the procedure specification.

process unit: an area whose boundaries are designated by the engineering design within which reactions, separations, and other processes are carried out. Examples of installations that are *not* classified as process units are loading areas or terminals, bulk plants, compounding plants, and tank farms and storage yards.

quench annealing: see solution heat treatment under heat treatment.

quenching: see heat treatment.

readily accessible (for visual examination): those surfaces that can be examined from a distance of not more than 600 mm (24 in.) and at an angle of not less than 30 deg to the surface to be examined.

reinforcement: see paras. 304.3 and A304.3. See also weld reinforcement.

representative: a person, partnership, organization, or business designated by the owner to carry out selected responsibilities on the owner's behalf. room temperature: temperature between 10°C and 38°C (50°F and 100°F).

root opening: the separation between the members to be joined, at the root of the joint.

safeguarding: provision of protective measures of the types outlined in Appendix G, where deemed necessary. See Appendix G for detailed discussion.

seal bond: a bond intended primarily to provide joint tightness against leakage in nonmetallic piping.

seal weld: a weld intended primarily to provide joint tightness against leakage in metallic piping.

semiautomatic arc welding: arc welding with equipment that controls only the filler metal feed. The advance of the welding is manually controlled.

severe cyclic conditions: conditions applying to specific piping components or joints for which the owner or the designer determines that construction to better resist fatigue loading is warranted. See Appendix F, para. F301.10.3 for guidance on designating piping as being under severe cyclic conditions.

shall: a term that indicates a provision is a Code requirement.

shielded metal-arc welding (SMAW): an arc welding process that produces coalescence of metals by heating them with an arc between a covered metal electrode and the work. Shielding is obtained from decomposition of the electrode covering. Pressure is not used and filler metal is obtained from the electrode.

should: a term that indicates a provision is recommended as good practice but is not a Code requirement.

size of weld:

(a) fillet weld: the leg lengths (the leg length for equalleg welds) of the sides, adjoining the members welded, of the largest triangle that can be inscribed within the weld cross section. For welds between perpendicular members, the definitions in Figure 328.5.2A apply.

NOTE: When the angle between members exceeds 105 deg, size is of less significance than effective throat (see also *throat of a fillet weld*).

(b) groove weld: the joint penetration (depth of bevel plus the root penetration when specified). The size of a groove weld and its effective throat are the same.

slag inclusion: nonmetallic solid material entrapped in weld metal or between weld metal and base metal.

soldering: a metal joining process wherein coalescence is produced by heating to suitable temperatures and by using a nonferrous alloy fusible at temperatures below 427°C (800°F) and having a melting point below that of the base metals being joined. The filler metal is distributed between closely fitted surfaces of the joint by capillary attraction. In general, solders are lead-tin alloys and may contain antimony, bismuth, and other elements.

solution heat treatment: see heat treatment.

stress ratio: see para. 323.2.2(b). stress relief: see heat treatment. stress terms frequently used:

- (a) basic allowable stress: this term, symbol *S*, represents the stress value for any material determined by the appropriate stress basis in para. 302.3.2
- (b) bolt design stress: this term represents the design stress used to determine the required cross-sectional area of bolts in a bolted joint
- (c) hydrostatic design basis: selected properties of plastic piping materials to be used in accordance with ASTM D2837 or D2992 to determine the HDS [see (d) below] for the material
- (d) hydrostatic design stress (HDS): the maximum continuous stress due to internal pressure to be used in the design of plastic piping, determined from the hydrostatic design basis by use of a service (design) factor

submerged arc welding (SAW): an arc welding process that produces coalescence of metals by heating them with an arc or arcs between a bare metal electrode or electrodes and the work. The arc is shielded by a blanket of granular, fusible material on the work. Pressure is not used and filler metal is obtained from the electrode and sometimes from a supplemental source (welding rod, flux, or metal granules).

tack weld: a weld made to hold parts of a weldment in proper alignment until the final welds are made.

tempering: see heat treatment.

thermoplastic: a plastic that is capable of being repeatedly softened by increase of temperature and hardened by decrease of temperature.

thermosetting resin: a resin capable of being changed into a substantially infusible or insoluble product when cured at room temperature, or by application of heat, or by chemical means.

throat of a fillet weld:

- (a) theoretical throat: the perpendicular distance from the hypotenuse of the largest right triangle that can be inscribed in the weld cross section to the root of the joint
- (b) actual throat: the shortest distance from the root of a fillet weld to its face
- (c) effective throat: the minimum distance, minus any reinforcement (convexity), between the weld root and the face of a fillet weld

toe of weld: the junction between the face of a weld and the base material.

tube: see pipe.

tungsten electrode: a nonfiller-metal electrode used in arc welding or cutting, made principally of tungsten.

unbalanced piping system: see para. 319.2.2(b).

undercut: a groove melted into the base material adjacent to the toe or root of a weld and left unfilled by weld material.

visual examination: see para. 344.2.1.

weld: a localized coalescence of material wherein coalescence is produced either by heating to suitable temperatures, with or without the application of pressure, or by application of pressure alone, and with or without the use of filler material.

Table 300.4 Status of Appendices in B31.3

Appendix	Title	Status
Α	Allowable Stresses and Quality Factors for Metallic Piping and Bolting Materials	Requirements
В	Stress Tables and Allowable Pressure Tables for Nonmetals	Requirements
С	Physical Properties of Piping Materials	Requirements (1)
D	Flexibility and Stress Intensification Factors	Requirements (1)
E	Reference Standards	Requirements
F	Guidance and Precautionary Considerations	Guidance (2)
G	Safeguarding	Guidance 😢
Н	Sample Calculations for Branch Reinforcement	Guidance
J	Nomenclature	Information
K	Allowable Stresses for High Pressure Piping	Requirements (3)
L	Aluminum Alloy Pipe Flanges	Specification (4)
M	Guide to Classifying Fluid Services	Guidance (2)
N	Application of ASME B31.3 Internationally	Guidance (2)
Q	Quality System Program	Guidance (2)
R	Allowable Stresses for High Pressure Piping Aluminum Alloy Pipe Flanges Guide to Classifying Fluid Services Application of ASME B31.3 Internationally Quality System Program Use of Alternative Ultrasonic Acceptance Criteria Piping System Stress Analysis Examples	Requirements (5)
S	Piping System Stress Analysis Examples	Guidance (2)
V	Allowable Variations in Elevated Temperature Service	Guidance (2)
W	High-Cycle Fatigue Assessment of Piping Systems	Requirements
X	Metallic Bellows Expansion Joints	Requirements
Z	Preparation of Technical Inquiries	Requirements (5)

NOTES:

- (1) Contains default requirements, to be used unless more directly applicable data are available.
- (2) Contains no requirements but Code user is responsible for considering applicable items.
- (3) Contains requirements applicable only when use of Chapter IX is specified.
- (4) Contains pressure-temperature ratings, materials, dimensions, and markings of forged aluminum alloy flanges.
- (5) Contains administrative requirements.

weld coupon: a sample weld used to determine weld acceptance. Types of weld coupons are defined as follows:

- (a) primary weld coupon; made prior to the start of production welding to establish a benchmark of weld acceptance
- (b) production weld coupon: made when any of the conditions in para, U341.4.5 exist and used to compare against a corresponding primary weld coupon to demonstrate continued acceptability of welds during production welding

weld coupon examination: see para. U344.8.1.

weld reinforcement: weld material in excess of the specified weld size.

welder: one who performs a manual or semi-automatic welding operation. (This term is sometimes erroneously used to denote a welding machine.)

welding operator: one who operates machine or automatic welding equipment.

welding procedure: the detailed methods and practices involved in the production of a weldment.

welding procedure specification (WPS): the document that lists the parameters to be used in construction of weldments in accordance with requirements of this Code. weldment: an assembly whose component parts are joined by welding.

300.3 Nomenclature

Dimensional and mathematical symbols used in this Code are listed in Appendix J, with definitions and location references to each. Uppercase and lowercase English letters are listed alphabetically, followed by Greek letters.

300.4 Status of Appendices

Table 300.4 indicates for each Appendix of this Code whether it contains Code requirements, guidance, or supplemental information. See the first page of each Appendix for details.

Chapter II Design

PART 1 CONDITIONS AND CRITERIA

301 DESIGN CONDITIONS

Paragraph 301 states the qualifications of the Designer, defines the temperatures, pressures, and forces applicable to the design of piping, and states the consideration that shall be given to various effects and their consequent loadings. See also Appendix F, para. F301.

301.1 Qualifications of the Designer

The Designer is the person(s) in charge of the engineering design of a piping system and shall be experienced in the use of this Code. The qualifications and experience required of the Designer will depend on the complexity and criticality of the system and the nature of the individual's experience. The owner's approval is required if the individual does not meet at least one of the following criteria:

- (a) Completion of a degree, accredited by an independent agency [such as ABET (U.S. and international) NBA (India), CTI (France), and CNAP (Chile)], in engineering, science, or technology, requiring the equivalent of at least 4 years of full-time study that provides exposure to fundamental subject matter relevant to the design of piping systems, plus a minimum of 5 years experience in the design of related pressure piping.
- (b) Professional Engineering registration, recognized by the local jurisdiction, and experience in the design of related pressure piping
- (c) Completion of an accredited engineering technician or associates degree, requiring the equivalent of at least 2 years of study, plus a minimum of 10 years experience in the design of related pressure piping.
- (d) Fifteen years experience in the design of related pressure piping.

Experience in the design of related pressure piping is satisfied by piping design experience that includes design calculations for pressure, sustained and occasional loads, and piping flexibility.

301.2 Design Pressure

301.2.1 General

- (a) The design pressure of each component in a piping system shall be not less than the pressure at the most severe condition of coincident internal or external pressure and temperature (minimum or maximum) expected during service, except as provided in para. 302.2.4.
- (b) The most severe condition is that which results in the greatest required component thickness and the highest component rating.
- (c) When more than one set of pressure-temperature conditions exist for a piping system, the conditions governing the rating of components conforming to listed standards may differ from the conditions governing the rating of components designed in accordance with para 304.
- (minimum or maximum) and differential pressure between the adjoining chambers expected during service, except as provided in para. 302.2.4.

301.2.2 Required Pressure Containment or Relief

- (a) Provision shall be made to safely contain or relieve (see para. 322.6.3) any expected pressure to which the piping may be subjected. Piping not protected by a pressure-relieving device, or that can be isolated from a pressure-relieving device, shall be designed for at least the highest expected pressure.
- (b) Sources of pressure to be considered include ambient influences, pressure oscillations and surges, improper operation, decomposition of unstable fluids, static head, and failure of control devices.
- (c) The allowances of para. 302.2.4(f) are permitted, provided that the other requirements of para. 302.2.4 are also met.

301.3 Design Temperature

The design temperature of each component in a piping system is the temperature at which, under the coincident pressure, the greatest thickness or highest component rating is required in accordance with para. 301.2. (To satisfy the requirements of para. 301.2, different

components in the same piping system may have different design temperatures.)

In establishing design temperatures, consider at least the fluid temperatures, ambient temperatures, solar radiation, heating or cooling medium temperatures, and the applicable provisions of paras. 301.3.2, 301.3.3, and 301.3.4.

301.3.1 Design Minimum Temperature. The design minimum temperature is the lowest component temperature expected in service. This temperature may establish special design requirements and material qualification requirements. See also paras. 301.4.4 and 323.2.2.

301.3.2 Uninsulated Components

- (a) For fluid temperatures below 65°C (150°F), the component temperature shall be taken as the fluid temperature unless solar radiation or other effects result in a higher temperature.
- (b) For fluid temperatures 65°C (150°F) and above, unless a lower average wall temperature is determined by test or heat transfer calculation, the temperature for uninsulated components shall be no less than the following values:
- (1) valves, pipe, lapped ends, welding fittings, and other components having wall thickness comparable to that of the pipe 95% of the fluid temperature
- (2) flanges (except lap joint) including those on fittings and valves 90% of the fluid temperature
 - (3) lap joint flanges 85% of the fluid temperature
 - (4) bolting 80% of the fluid temperature
- **301.3.3 Externally Insulated Piping.** The component design temperature shall be the fluid temperature unless calculations, tests, or service experience based on measurements support the use of another temperature. Where piping is heated or cooled by tracing or jacketing, this effect shall be considered in establishing component design temperatures.
- **301.3.4 Internally Insulated Piping.** The component design temperature shall be based on heat transfer calculations or tests.

301.4 Ambient Effects

See Appendix F, para. F301.4.

- **301.4.1 Cooling Effects on Pressure.** The cooling of a gas or vapor in a piping system may reduce the pressure sufficiently to create an internal vacuum. In such a case, the piping shall be capable of withstanding the external pressure at the lower temperature, or provision shall be made to break the vacuum.
- **301.4.2 Fluid Expansion Effects.** Provision shall be made in the design either to withstand or to relieve increased pressure caused by the heating of static fluid in a piping component. See also para. 322.6.3(b)(2).

- **301.4.3 Atmospheric lcing.** Where the design minimum temperature of a piping system is below 0°C (32°F), the possibility of moisture condensation and buildup of ice shall be considered and provisions made in the design to avoid resultant malfunctions. This applies to surfaces of moving parts of shutoff valves, control valves, pressure-relief devices including discharge piping, and other components.
- **301.4.4 Low Ambient Temperature.** Consideration shall be given to low ambient temperature conditions for displacement stress analysis.

301.5 Dynamic Effects

(18)

- **301.5.1 Impact.** Impact forces caused by external or (18) internal conditions (including changes in flow rate, hydraulic shock, liquid or solid slugging, flashing, and geysering) shall be taken into account in the design of piping. See Appendix F, para. F301.5.1.
- **301.5.2 Wind.** The effect of wind loading shall be taken into account in the design of exposed piping. The analysis considerations and loads may be as described in ASCE 7. Authoritative local meteorological data may also be used to define or refine the design wind loads.
- **301.5.3 Earthquake.** The effect of earthquake loading shall be taken into account in the design of piping. The analysis considerations and loads may be as described in ASCE 7. Authoritative local seismological data may also be used to define or refine the design earthquake loads
 - **301.5.4 Vibration.** Piping shall be designed, arranged, (18) and supported to eliminate excessive and harmful effects of vibration that may arise from such sources as impact, pressure pulsation, turbulent flow vortices, resonance in compressors, external vortex shedding (e.g., wind), and acoustically induced vibration.
 - **301.5.5 Discharge Reactions.** Piping shall be designed, arranged, and supported so as to withstand reaction forces due to let-down or discharge of fluids.

301.6 Weight Effects

The following weight effects, combined with loads and forces from other causes, shall be taken into account in the design of piping.

- **301.6.1 Live Loads.** These loads include the weight of the medium transported or the medium used for test. Snow and ice loads due to both environmental and operating conditions shall be considered.
- **301.6.2 Dead Loads.** These loads consist of the weight of piping components, insulation, and other superimposed permanent loads supported by the piping.

301.7 Thermal Expansion and Contraction Effects

The following thermal effects, combined with loads and forces from other causes, shall be taken into account in the design of piping. See also Appendix F, para. F301.7.

- **301.7.1 Thermal Loads Due to Restraints.** These loads consist of thrusts and moments that arise when free thermal expansion and contraction of the piping are prevented by restraints or anchors.
- **301.7.2 Loads Due to Temperature Gradients.** These loads arise from stresses in pipe walls resulting from large rapid temperature changes or from unequal temperature distribution as may result from a high heat flux through a comparatively thick pipe or stratified two-phase flow causing bowing of the line.
- **301.7.3 Loads Due to Differences in Expansion Characteristics.** These loads result from differences in thermal expansion where materials with different thermal expansion coefficients are combined, as in bimetallic, lined, jacketed, or metallic-nonmetallic piping.

301.8 Effects of Support, Anchor, and Terminal Movements

The effects of movements of piping supports, anchors, and connected equipment shall be taken into account in the design of piping. These movements may result from the flexibility and/or thermal expansion of equipment, supports, or anchors; and from settlement, tidal movements, or wind sway.

301.9 Reduced Ductility Effects

The harmful effects of reduced ductility shall be taken into account in the design of piping. The effects may, for example, result from welding, heat treatment, forming, bending, or low operating temperatures, including the chilling effect of sudden loss of pressure on highly volatile fluids. Low ambient temperatures expected during operation shall be considered.

301.10 Cyclic Effects

Fatigue due to pressure cycling, thermal cycling, and other cyclic loadings shall be considered in the design of piping. See Appendix F, para. F301.10.

301.11 Air Condensation Effects

At operating temperatures below -191°C (-312°F) in ambient air, condensation and oxygen enrichment occur. These shall be considered in selecting materials, including insulation, and adequate shielding and/or disposal shall be provided.

302 DESIGN CRITERIA

302.1 General

Paragraph 302 states pressure-temperature ratings, stress criteria, design allowances, and minimum design values together with permissible variations of these factors as applied to the design of piping.

302.2 Pressure-Temperature Design Criteria

302.2.1 Listed Components Having Established Ratings. Except as limited elsewhere in the Code, pressure-temperature ratings contained in standards for piping components listed in Table 326. Dare acceptable for design pressures and temperatures in accordance with this Code. When the owner approves, provisions of this Code may be used to extend the pressure-temperature ratings of a component beyond the ratings contained in the listed standard.

302.2.2 Listed Components Not Having Specific Ratings

- (a) Some of the standards for fittings in Table 326.1 (e.g., ASME B16.9 and B16.11) state that pressure-temperature ratings are based on straight seamless pipe. Such fittings shall be rated as calculated for straight seamless pipe with the same allowable stresses as the fitting and the nominal thickness corresponding to the wall thickness or class designation of the fitting, less all applicable allowances (e.g., thread depth and corrosion allowance), and considering the manufacturing undertolerances of the fittings and the pipe.
- (b) For components with straight or spiral (helical seam) longitudinal welded joints, the pressure rating as determined for seamless pipe shall be multiplied by the weld joint strength reduction factor, *W*, as defined in para. 302.3.5(e).
- (c) Other listed components not addressed in para. 302.2.1 or 302.2.2(a) shall have their pressure-temperature ratings established in accordance with the rules in para. 304.
- **302.2.3 Unlisted Components.** Piping components not (18) listed in Table 326.1 may be used subject to all of the following requirements:
 - (a) The material shall comply with para. 323.
- (b) The designer shall be satisfied that the design is suitable for the intended service.
- (c) Pressure–temperature ratings shall be established in accordance with the rules in para. 304.

302.2.4 Allowances for Pressure and Temperature (18) **Variations.** Occasional variations of pressure, temperature, or both may occur in a piping system. Such variations shall be considered in selecting design pressure (para. 301.2) and design temperature (para. 301.3). The most severe coincident pressure and temperature

shall determine the design conditions unless all of the following criteria are met:

- (a) The piping system shall have no pressurecontaining components of gray iron or other nonductile metal.
- (b) Circumferential pressure stresses (based on minimum pipe wall thickness, less allowances) shall not exceed the yield strength at temperature (see para. 302.3 of this Code and S_y data in ASME BPVC, Section II, Part D, Table Y-1).
- (c) Combined stresses shall not exceed the limits established in para. 302.3.6.
- (d) The total number of pressure–temperature variations above the design conditions shall not exceed 1000 during the life of the piping system.
- (e) In no case shall the increased pressure exceed the test pressure used under para. 345 for the piping system.
- (f) Occasional variations above design conditions shall remain within one of the following limits for pressure design.
- (1) Subject to the owner's approval, it is permissible to exceed the pressure rating or the allowable stress for pressure design at the temperature of the increased condition by not more than
- (-a) 33% for no more than 10 h at any one time and no more than 100 h/y, or
- (-b) 20% for no more than 50 h at any one time and no more than 500 h/y

The effects of such variations shall be determined by the designer to be safe over the service life of the piping system by methods acceptable to the owner. (See Appendix V.)

- (2) When the variation is self-limiting (e.g., due to a pressure-relieving event), and lasts no more than 50 h at any one time and not more than 500 h/y, it is permissible to exceed the pressure rating or the allowable stress for pressure design at the temperature of the increased condition by not more than 20%
- (g) The combined effects of the sustained and cyclic variations on the serviceability of all components in the system shall have been evaluated.
- (h) Temperature variations below the minimum temperature shown in Appendix A are not permitted unless the requirements of para. 323.2.2 are met for the lowest temperature during the variation.
- (i) The application of pressures exceeding pressuretemperature ratings of valves may under certain conditions cause loss of seat tightness or difficulty of operation. The differential pressure on the valve closure element should not exceed the maximum differential pressure rating established by the valve manufacturer. Such applications are the owner's responsibility.

302.2.5 Ratings at Junction of Different Services.

When two services that operate at different pressuretemperature conditions are connected, the valve segregating the two services shall be rated for the more severe service condition. Where multiple valves are used (e.g., in a double block and bleed arrangement), all of the valves shall be rated for the more severe service condition. If the valve(s) will operate at a different temperature due to remoteness from a header or piece of equipment, the valve(s) (and any mating flanges) may be selected on the basis of the different temperature. For piping on either side of the valve, however, each system shall be designed for the conditions of the service to which it is connected.

302.3 Allowable Stresses and Other Stress Limits

- **302.3.1 General.** The allowable stresses defined in paras. 302.3.1(a), (b), and (c) shall be used in design calculations unless modified by other provisions of this Code.
- (a) Tension. Basic allowable stresses, *S*, in tension for metals listed in Tables A-1 and A-1M, and design stresses, *S*, for bolting materials listed in Tables A-2 and A-2M were determined in accordance with para. 302.3.2.

In equations elsewhere in the Code where the product *SE* appears, the value *S* is multiplied by one of the following quality factors:¹

- (1) casting quality factor E_c as defined in para, 302:3.3 and tabulated for various material specifications in Table A-1A, and for various levels of supplementary examination in Table 302.3.3C, or
- (2) longitudinal weld joint factor E_j as defined in 302.3.4 and tabulated for various material specifications and classes in Table A-1B, and for various types of joints and supplementary examinations in Table 302.3.4

The stress values in Tables A-1, A-1M, A-2, and A-2M are grouped by materials and product forms, and are for stated temperatures up to the limit provided in para. 323.2.1(a). Straight-line interpolation between temperatures is permissible. The temperature intended is the design temperature (see para. 301.3).

- (b) Shear and Bearing. Allowable stresses in shear shall be 0.80 times the basic allowable stress in tension tabulated in Appendix A. Allowable stress in bearing shall be 1.60 times that value.
- (c) Compression. Allowable stresses in compression shall be no greater than the basic allowable stresses in tension as tabulated in Appendix A. Consideration shall be given to structural stability.

 $^{^{1}}$ If a component is made of castings joined by longitudinal welds, both a casting and a weld joint quality factor shall be applied. The equivalent quality factor E is the product of E_{C} Table A-1A, and E_{B} Table A-1B.

(18) **302.3.2 Bases for Design Stresses.** The bases for establishing design stress values for bolting materials and basic allowable stress values for other metallic materials in this Code are specified in (a), (b), (c), and (d). In the application of these criteria, the yield strength at temperature is considered to be $S_Y R_Y$ and the tensile strength at temperature is considered to be $1.1S_T R_T$, where

 R_T = ratio of the average temperature-dependent trend curve value of tensile strength to the room temperature tensile strength

 R_Y = ratio of the average temperature-dependent trend curve value of yield strength to the room temperature yield strength

 S_T = specified minimum tensile strength at room temperature

 S_Y = specified minimum yield strength at room temperature

- (a) Bolting Materials. Design stress values at temperature for bolting materials shall not exceed the lowest of the following:
- (1) at temperatures below the creep range, for bolting materials whose strength has not been enhanced by heat treatment or strain hardening, the lowest of one-fourth of S_T , one-fourth of tensile strength at temperature, two-thirds of S_Y , and two-thirds of yield strength at temperature
- (2) at temperatures below the creep range, for bolting materials whose strength has been enhanced by heat treatment or strain hardening, the lowest of one-fifth of S_T , one-fourth of the tensile strength at temperature, one-fourth of S_Y , and two-thirds of the yield strength at temperature (unless these values are lower than corresponding values for annealed material, in which case the annealed values shall be used) slope, n, of the plot at $100\,000$ not exceed 0.67. (7) 80% of $100\,000$ h. For structural stress shall be 0 in (d)(1) through
- (3) 100% of the average stress for a creep rate of 0.01% per 1000 h
- (4) 67% of the average stress for rupture at the end of 100 000 h
- (5) 80% of minimum stress for rupture at the end of 100 000 h
- (b) Gray Iron. Basic allowable stress values at temperature for gray iron shall not exceed the lower of the following:
 - (1) one-tenth of S_T
 - (2) one-tenth of the tensile strength at temperature

- (c) Malleable Iron. Basic allowable stress values at temperature for malleable iron shall not exceed the lower of the following:
 - (1) one-fifth of S_T
 - (2) one-fifth of the tensile strength at temperature
- (d) Other Materials. Basic allowable stress values at temperature for materials other than bolting materials, gray iron, and malleable iron shall not exceed the lowest of the following:
- (1) the lower of one-third of S_T and one-third of tensile strength at temperature.
- (2) except as provided in (3) below, the lower of two-thirds of S_Y and two-thirds of yield strength at temperature
- (3) for austenitic stainless steels and nickel alloys having similar stress-strain behavior, the lower of two-thirds of S_Y and 90% of yield strength at temperature [see (e)].
- (4) 100% of the average stress for a creep rate of 0.01% per 1000 h.
- (5) for temperatures up to and including 815°C (1,500°F), 67% of the average stress for rupture at the end of 100000 h.
- (6) for temperatures higher than 815°C (1,500°F), $(100 \times F_{\rm avg})\%$ times the average stress for rupture at the end of 100000 h. $F_{\rm avg}$ is determined from the slope, n, of the log time-to-rupture versus log stress plot at 100000 h such that log $F_{\rm avg} = 1/n$. $F_{\rm avg}$ shall not exceed 0.67.
- (7) 80% of the minimum stress for rupture at the end of $100\,000\,h$.

For structural grade materials, the basic allowable stress shall be 0.92 times the lowest value determined in (d)(1) through (7).

- (e) Application Limits. Application of stress values determined in accordance with (d)(3) is not recommended for flanged joints and other components in which slight deformation can cause leakage or malfunction.
- (1) These values are shown in italics or boldface in Table A-1, as explained in Note (4a) to Appendix A Tables. Instead, either 75% of the stress value in Table A-1 or two-thirds of the yield strength at temperature listed in ASME BPVC, Section II, Part D, Table Y-1 should be used.
- (2) Stress values determined in accordance with (d)(3) are not identified in Table A-1M. See Note (4b) to Appendix A. When using Table A-1M, two-thirds of the yield strength at temperature listed in ASME BPVC, Section II, Part D, Table Y-1 should be used.

302.3.3 Casting Quality Factor, E_c

(a) General. The casting quality factors, E_c , defined herein shall be used for cast components not having pressure–temperature ratings established by standards in Table 326.1.

² These bases are the same as those for ASME BPVC, Section III, Class 1 materials, given in ASME BPVC, Section II, Part D. Stress values in B31.3, Appendix A, at temperatures below the creep range generally are the same as those listed in ASME BPVC, Section II, Part D, Tables 2A and 2B, and in Table 3 for bolting, corresponding to those bases. They have been adjusted as necessary to exclude casting quality factors and longitudinal weld joint quality factors. Stress values at temperatures in the creep range generally are the same as those in ASME BPVC, Section II, Part D, Tables 1A and 1B, corresponding to the bases for ASME BPVC, Section VIII, Division 1.

Table 302.3.3C Increased Casting Quality Factors, E_c

Supplementary Examination in Accordance With Note(s)	Factor, E_c
(1)	0.85
(2)(a) or (2)(b)	0.85
(3)(a) or (3)(b)	0.95
(1) and (2)(a) or (2)(b)	0.90
(1) and (3)(a) or (3)(b)	1.00
(2)(a) or (2)(b) and (3)(a) or (3)(b)	1.00

GENERAL NOTE: Titles of standards referenced in this Table's Notes are as follows:

ASME B46.1	Surface Texture (Surface Roughness, Waviness and Lay)
ASTM E94	Guide for Radiographic Examination
ASTM E114	Practice for Ultrasonic Pulse-Echo Straight-Beam Contact Testing
ASTM E125	Reference Photographs for Magnetic Particle Indications on Ferrous Castings
ASTM E165	Practice for Liquid Penetrant Examination for General Industry
ASTM E709	Guide for Magnetic Particle Testing
MSS SP-53	Quality Standard for Steel Castings and Forgings for Valves, Flanges, Fittings, and Other Piping Components — Magnetic Particle Examination Method
MSS SP-93	Quality Standard for Steel Castings and Forgings for Valves, Flanges, Fittings, and Other Piping Components — Liquid Penetrant Examination Method

NOTES:

- (1) Machine all surfaces to a finish of $6.3 \mu m R_a$ (250 μ in. R_a in accordance with ASME B46.1), thus increasing the effectiveness of surface examination.
- (a) Examine all surfaces of each casting (ferromagnetic material only) by the magnetic particle method in accordance with ASTM E709. Judge acceptability in accordance with MSS SP-53, Table 1.
- (b) Examine all surfaces of each casting by the liquid penetrant method, in accordance with ASTM E165. Judge acceptability in accordance with SP-93, Table 1.
- (a) Fully examine each casting ultrasonically in accordance with ASTM E114, accepting a casting only if there is no evidence of depth of defects in excess of 5% of wall thickness.
- (b) Fully radiograph each casting in accordance with ASTM E94. Judge in accordance with the stated acceptance levels in Table 302.3.3D.

- (b) Basic Quality Factors. Castings of gray and malleable iron, conforming to listed specifications, are assigned a basic casting quality factor, E_c , of 1.00 (due to their conservative allowable stress basis). For most other metals, static castings that conform to the material specification and have been visually examined as required by MSS SP-55, Quality Standard for Steel Castings for Valves, Flanges and Fittings and Other Piping Components Visual Method, are assigned a basic casting quality factor, E_c , of 0.80. Centrifugal castings that meet specification requirements only for chemical analysis, tensile, hydrostatic, and flattening tests, and visual examination are assigned a basic casting quality factor of 0.80. Basic casting quality factors are tabulated for listed specifications in Table A-1A.
- (c) Increased Quality Factors. Casting quality factors may be increased when supplementary examinations are performed on each casting. Table 302.3.3C states the increased casting quality factors, E_c , that may be used for various combinations of supplementary examination. Table 302.3.3D states the acceptance criteria for the examination methods specified in the Notes to Table 302.3.3C. Quality factors higher than those shown in Table 302.3.3C do not result from combining tests (2)(a) and (2)(b), or (3)(a) and (3)(b). In no case shall the quality factor exceed 1.00.

Several of the specifications in Appendix A require machining of all surfaces and/or one or more of these supplementary examinations. In such cases, the appropriate increased quality factor is shown in Table A-1A.

302.3.4 Weld Joint Quality Factor, E_i

- (a) Basic Quality Factors. The weld joint quality factors, E_j , tabulated in Table A-1B are basic factors for straight or spiral (helical seam) welded joints for pressure-containing components as shown in Table 302.3.4.
- (b) Increased Quality Factors. Table 302.3.4 also indicates higher joint quality factors that may be substituted for those in Table A-1B for certain kinds of welds if additional examination is performed beyond that required by the product specification.

302.3.5 Limits of Calculated Stresses Due to (18) Sustained Loads and Displacement Strains

- (a) Internal Pressure Stresses. Stresses due to internal pressure shall be considered safe when the wall thickness of the piping component, including any reinforcement, meets the requirements of para. 304.
- (b) External Pressure Stresses. Stresses due to external pressure shall be considered safe when the wall thickness of the piping component, and its means of stiffening, meet the requirements of para. 304.
- (c) Stresses Due to Sustained Loads, S_L . The stresses due to sustained loads, S_L , in any component in a piping system (see para. 320), shall not exceed S_h , where S_h is the basic allowable stress provided in Table A-1 or Table A-1M at

Table 302.3.3D Acceptance Levels for Castings

	-		
Material Examined Thickness, T	Applicable Standard	Acceptance Level (or Class)	Acceptable Discontinuities
Steel	ASTM E446	1	Types A, B, C
$T \le 25 \text{ mm}$ (1 in.)			
Steel	ASTM E446	2	Types A, B, C
T > 25 mm, $\leq 51 \text{ mm}$ (2 in.)			
Steel	ASTM E186	2	Categories A, B, C
T > 51 mm, $\leq 114 \text{ mm}$ $(4\frac{1}{2} \text{ in.})$			
Steel	ASTM E280	2	Categories A, B, C
<i>T</i> > 114 mm, ≤ 305 mm (12 in.)			
Aluminum and magnesium	ASTM E155		Shown in reference radiographs
Copper, Ni-Cu	ASTM E272	2	Codes A, Ba, Bb
Bronze	ASTM E310	2	Codes A and B

GENERAL NOTE: Titles of ASTM standards referenced in this Table are as follows:

- E155 Reference Radiographs for Inspection of Aluminum and Magnesium Castings
- E186 Reference Radiographs for Heavy-Walled (2 to $4-\frac{1}{2}$ -in. (50.8 to 114 mm)) Steel Castings
- E272 Reference Radiographs for High-Strength Copper-Base and Nickel-Copper Alloy Castings
- E280 Reference Radiographs for Heavy-Walled (4-½ to 12 in. (114 to 305 mm)) Steel Castings
- E310 Reference Radiographs for Tin Bronze Castings
- E446 Reference Radiographs for Steel Castings Up to 2 in. (50.8 mm) in Thickness

the metal temperature for the operating condition being considered.

(d) Allowable Displacement Stress Range, S_A . The computed displacement stress range, S_E , in a piping system (see para. 319.4.4) shall not exceed the allowable displacement stress range, S_A (see paras. 319.2.3 and 319.3.4), calculated by eq. (1a)

$$S_A = f(1.25S_c + 0.25S_h)$$
 (1a)

When S_h is greater than S_L , the difference between them may be added to the term $0.25S_h$ in eq. (1a). In that case, the allowable stress range is calculated by eq. (1b)

$$S_A = f[1.25(S_c + S_h) - S_L]$$
 (1b)

For eqs. (1a) and (1b)

 $f = \text{stress range factor,}^3 \text{ calculated by eq. } (1c)^4$

$$f ext{ (see Fig. 302.3.5)} = 6.0(N)^{-0.2} \le f_m$$
 (1c)

- f_m = maximum value of stress range factor; 1.2 for ferrous materials with specified minimum tensile strengths \leq 517 MPa (75 ksi) and at metal temperatures \leq 371°C (700°F); otherwise $f_m = 1.0$
- N = equivalent number of full displacement cycles during the expected service life of the piping system⁵
- S_c = basic allowable stress⁶ at minimum metal temperature expected during the displacement cycle under analysis
 - = 138 MPa (20 ksi) maximum
- S_h = basic allowable stress⁶ at maximum metal temperature expected during the displacement cycle under analysis
 - = 138 MPa (20 ksi) maximum
- S_L = stress due to sustained loads; in systems where supports may be active in some conditions and inactive in others, the maximum value of sustained stress, considering all support conditions, shall be used

When the computed stress range varies, whether from thermal expansion or other conditions, S_E is defined as the greatest computed displacement stress range. The value of N in such cases can be calculated by eq. (1d)

$$N = N_E + \sum_i (r_i^5 N_i) \text{ for } i = 1, 2, ..., n$$
 (1d)

where

 N_E = number of cycles of maximum computed displacement stress range, S_E

 N_i = number of cycles associated with displacement stress range, S_i

 $r_i = S_i/S_E$

 S_i = any computed displacement stress range smaller than S_E

When the total number of significant stress cycles due to all causes exceeds 100 000, and with the owner's approval, the designer may elect to apply the alternative fatigue assessment rules in Appendix W to satisfy the displacement stress range requirements of this paragraph and of

³ Applies to essentially noncorroded piping. Corrosion can sharply decrease cyclic life; therefore, corrosion resistant materials should be considered where a large number of major stress cycles is anticipated.

⁴ The minimum value for f is 0.15, which results in an allowable displacement stress range, $S_{A^{\prime}}$ for an indefinitely large number of cycles.

placement stress range, S_A , for an indefinitely large number of cycles.

⁵ The designer is cautioned that the fatigue life of materials operated at elevated temperature may be reduced.

⁶ For castings, the basic allowable stress shall be multiplied by the applicable casting quality factor, E_c . For longitudinal welds, the basic allowable stress need not be multiplied by the weld quality factor, E_f .

No.	Туре о	of Joint	Type of Seam	Examination	Factor, <i>E_j</i>
1	Furnace butt weld, continuous weld		Straight	As required by listed specification	0.60 [Note (1)]
2	Electric resistance weld		Straight or spiral (helical seam)	As required by listed specification	0.85 [Note (1)]
3	Electric fusion weld				
	(a) Single butt weld		Straight or spiral (helical seam)	As required by listed specification or this Code	0.80
	(with or without filler metal)			Additionally spot radiographed in accordance with para. 341.5.1	0.90
				Additionally 100% radiographed in accordance with para. 344.5.1 and Table 341.3.2	1.00
	(b) Double butt weld		Straight or spiral (helical seam) (except as provided in 4 below)	As required by listed specification or this Code	0.85
	(with or without filler metal)			Additionally spot radiographed in accordance with para. 341.5.1	0.90

Straight (with one or two

seams) or spiral (helical seam)

Table 302.3.4 Longitudinal Weld Joint Quality Factor, E_i

NOTE: (1) It is not permitted to increase the joint quality factor by additional examination for joint 1 or 2.

para. 319. A significant stress cycle is defined in para. W300. When the alternative rules of Appendix W are applied, the calculations shall be documented in the engineering design.

Specific specification

API 5L, electric fusion

weld, double butt

seam

(e) Weld Joint Strength Reduction Factor, W. At elevated temperatures, the long-term strength of weld joints may be lower than the long-term strength of the base material.

The weld joint strength reduction factor, *W*, is the ratio of the nominal stress to cause failure of a weld joint to that of the corresponding base material for an elevated temperature condition of the same duration. It only applies at weld locations in longitudinal or spiral (helical seam) welded piping components. The designer is responsible for the application of weld joint strength reduction factors to other welds (e.g., circumferential).

When determining the required wall thickness for internal pressure in accordance with para. 304, for each coincident operating pressure–temperature condition under consideration, the product of the *basic* allowable stress and the applicable weld quality factor, *SE*, shall be multiplied by *W*.

W is equal to 1.0 when evaluating occasional loads, e.g., wind and earthquake, or when evaluating permissible variations in accordance with para. 302.2.4. Application of *W* is not required when determining the pressure rating

for the occasional load or *permissible* variation condition. It is also not required when calculating the allowable stress range for displacement stresses, S_A , in (d).

Additionally 100% radiographed in accordance with para. 344.5.1 and

Additionally 100% radiographed in

accordance with para. 344.5.1

As required by specification

and Table 341.3.2

Table 341.3.2

1.00

0.95

1.00

For other than occasional loads or permissible variations, *W* shall be in accordance with Table 302.3.5 except as provided in (f).

- (f) Alternative Weld Strength Reduction Factors. A weld strength reduction factor other than that listed in Table 302.3.5 may be used in accordance with one of the following criteria:
- (1) Creep test data may be used to determine the weld joint strength reduction factor, W. However, the use of creep test data to increase the factor W above that shown in Table 302.3.5 is not permitted for the CrMo and Creep Strength Enhanced Ferritic (CSEF) steels materials, as defined in Table 302.3.5. Creep testing of weld joints to determine weld joint strength reduction factors, when permitted, should be full thickness cross-weld specimens with test durations of at least 1000 h. Full thickness tests shall be used unless the designer otherwise considers effects such as stress redistribution across the weld.
- (2) With the owner's approval, extensive successful experience may be used to justify the factor *W* above that shown in Table 302.3.5. Successful experience must

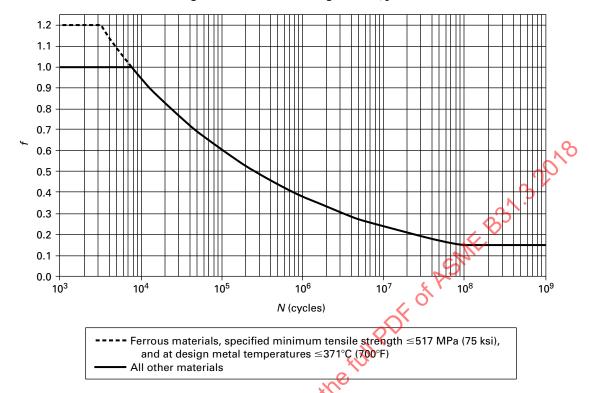


Figure 302.3.5 Stress Range Factor, f

include same or like material, weld metal composition, and welding process under equivalent, or more severes sustained operating conditions.

(18) 302.3.6 Limits of Calculated Stresses Due to Occasional Loads

- (a) Operation. Stresses due to occasional loads may be calculated using the equations for stress due to sustained loads in para. 320.2.
- (1) Subject to the limits of para. 302.2.4, the sum of the stresses due to sustained loads, such as pressure and weight, S_L , and of the stresses produced by occasional loads, such as wind and earthquake, may be as much as 1.33 times the basic allowable stress provided in Table A-1 or Table A-1M at the metal temperature for the occasional condition being considered. Wind and earthquake forces need not be considered as acting concurrently.
- (2) For Elevated Temperature Fluid Service (see definition in para. 300.2) of materials having ductile behavior, as an alternative to the use of 1.33 times the basic allowable stress provided in Table A-1 or Table A-1M, the allowable stress for occasional loads of short duration, e.g., surge, extreme wind, or earthquake, may be taken as the lowest of the following:

- (-a) the weld strength reduction factor times 90% of the yield strength at the metal temperature for the occasional condition being considered
- (-b) four times the basic allowable stress provided in Appendix A
- (-c) for occasional loads that exceed 10 h over the life of the piping system, the stress resulting in a 20% creep usage factor in accordance with Appendix V

For (-a), the yield strength shall be as listed in ASME BPVC, Section II, Part D, Table Y-1 or determined in accordance with para. 302.3.2. The strength reduction factor represents the reduction in yield strength with long-term exposure of the material to elevated temperatures and, in the absence of more-applicable data, shall be taken as 1.0 for austenitic stainless steel and 0.8 for other materials.

For (-b), the basic allowable stress for castings shall also be multiplied by the casting quality factor, E_c . Where the allowable stress value exceeds two-thirds of yield strength at temperature, the allowable stress value must be reduced as specified in para. 302.3.2(e).

(b) Test. Stresses due to test conditions are not subject to the limitations in para. 302.3. It is not necessary to consider other occasional loads, e.g., wind and earthquake, as occurring concurrently with test loads.

302.4 Allowances

In determining the minimum required thickness of a piping component, allowances shall be included for corrosion, erosion, and thread depth or groove depth. See definition for c in para. 304.1.1(b).

302.5 Mechanical Strength

- (a) Designs shall be checked for adequacy of mechanical strength under applicable loadings. When necessary, the wall thickness shall be increased to prevent overstress, damage, collapse, or buckling due to superimposed loads from supports, ice formation, backfill, transportation, handling, or other loads enumerated in para. 301.
- (b) Where increasing the thickness would excessively increase local stresses or the risk of brittle fracture, or is otherwise impracticable, the impact of applied loads may be mitigated through additional supports, braces, or other means without requiring an increased wall thickness. Particular consideration should be given to the mechanical strength of small pipe connections to piping or equipment.

303 GENERAL

O3 GENERALComponents manufactured in accordance with standards listed in Table 326.1 shall be considered switchlard use at pressure-temperature ration in the para. 302.2.1 \circ dards listed in Table 326.1 shall be considered suitable for use at pressure-temperature ratings in accordance with para. 302.2.1 or para. 302.2.2, as applicable. The rules in para. 304 are intended for pressure design of components not covered in Table 326.1, but may be used for a special or more-rigorous design of such components, or to satisfy requirements of para. 302.2.2. Designs shall be checked for adequacy of mechanical strength as described in para. 302.5.

304 PRESSURE DESIGN OF COMPONENTS

304.1 Straight Pipe

304.1.1 General

(a) The required thickness of straight sections of pipe shall be determined in accordance with eq. (2)

$$t_m = t + c \tag{2}$$

The minimum thickness, *T*, for the pipe selected, considering manufacturer's minus tolerance, shall be not less than t_m .

- (b) The following nomenclature is used in the equations for pressure design of straight pipe:
 - c = sum of the mechanical allowances (thread or c = sum of the mechanical allowances)groove depth) plus corrosion and erosion allowances. For threaded components, the nominal

thread depth (dimension h of ASME B1.20.1, or equivalent) shall apply. For machined surfaces or grooves where the tolerance is not specified, the tolerance shall be assumed to be 0.5 mm (0.02 in.) in addition to the specified depth of the cut.

D = outside diameter of pipe as listed in tables of standards or specifications or as measured

d = inside diameter of pipe. For pressure design calculation, the inside diameter of the pipe is the maximum value allowable under the purchase specification.

E = quality factor from Table A-1A or Table A-1B

P = internal design gage pressure

S = stress value for material from Table A-1 or Table A-1M

T = pipe wall thickness measured or minimum in accordance with the purchase specification)

t =pressure design thickness, as calculated in accordance with para 304.1.2 for internal pressure or as determined in accordance with para. 304.1.3 for external pressure

 t_m = minimum required thickness, including mechan-

$$Y = \frac{d + 2c}{D + d + 2c}$$

304.1.2 Straight Pipe Under Internal Pressure

(a) For t < D/6, the internal pressure design thickness for straight pipe shall be not less than that calculated in accordance with either eq. (3a) or eq. (3b)

$$t = \frac{PD}{2(SEW + PY)} \tag{3a}$$

$$t = \frac{P(d+2c)}{2[SEW - P(1-Y)]}$$
 (3b)

(b) For $t \ge D/6$ or for P/SE > 0.385, calculation of pressure design thickness for straight pipe requires special consideration of factors such as theory of failure, effects of fatigue, and thermal stress.

304.1.3 Straight Pipe Under External Pressure. To determine wall thickness and stiffening requirements for straight pipe under external pressure, the procedure outlined in ASME BPVC, Section VIII, Division 1, UG-28 through UG-30 shall be followed, using as the design length, L, the running centerline length between any two sections stiffened in accordance with UG-29. As an exception, for pipe with $D_o/t < 10$, the value of S to be

Table 302.3.5 Weld Joint Strength Reduction Factor, W

							Compone	Component Temperature, T_h °C (°F)	ature, T _i ,	°C (°F)					
Steel Group	<427 (≤800)	<pre><427 454 482 (<800) (850) (900)</pre>	482 (900)	510 (950)	538 (1,000)	566 (1,050)	593 (1,100)	621 (1,150)	649 (1,200)	677 (1,250)	704 (1,300)	732 (1,350)	760 (1,400)	788 (1,450)	816 (1,500)
Carbon Steel	(C)	1	1	1	1	1	1	:	:	:	:	:	:	:	: :
CrMo [Notes (1)-(3)]	AF	0.95	0.91	0.86	0.82	0.77	0.73	89.0	0.64	i	i	:	i	i	ŧ
CSEF $(N + T)$ [Notes (3)-(5)]	:	70X	:	\vdash	0.95	0.91	0.86	0.82	0.77	:	:	:	÷	÷	:
CSEF [Notes (3) and (4)] (Subcritical PWHT)	:	574	TOC	0.5	0.5	0.5	0.5	0.5	0.5	÷	÷	÷	÷	÷	:
Autogenous welds in austenitic stainless grade 3xx, and N088xx and N066xx nickel alloys [Note (6)]	i	i		-,cO/	1	1	1	1	1	1	1	1	1	1	1
Austenitic stainless grade 3xx and N088xx nickel alloys [Notes (7) and (8)]	i	ŧ	ŧ	1	26:0	0.91	0.86	0.82	0.77	0.73	89.0	0.64	0.59	0.55	0.5
Other materials [Note (9)]	:	÷	÷	i	:	ή. .×	:	i	÷	÷	÷	i	i	÷	÷

GENERAL NOTES:

- (a) Weld joint strength reduction factors at temperatures above the upper temperature limitalisted in Appendix A for the base metal or outside of the applicable range in Table 302.3.5 are the responsibility of the designer. At temperatures below those where weld joint strength reducton are tabulated, a value of 1.0 shall be used for the factor W where required; however, the additional rules of this Table and Notes do not apply.
 - T_{cr} = temperature 25°C (50°F) below the temperature identifying the start of time-dependent properties listed under "NOTES TIME-DEPENDENT PROPERTIES" (Txx) in the Notes to ASME criteria in paras. 302.3.2(d)(4), (5), (6), and (7) governs the basic allowable stress value of the metals joined by welding. When the base metals differ, the lower value of T_{cr}shall be used for the BPVC, Section II, Part D, Tables 1A and 1B for the base metals joined by welding. For materials not listed in Section II, Part D, T_{cr} shall be the temperature where the creep rate or stress rupture **(**P)
- T_i = temperature, °C (°F), of the component for the coincident operating pressure–temperature condition, Y_i and Y_i
- factors. For example, fabrication issues such as the deviation from a true circular form in pipe (e.g., "peaking" at longitudinal weld seams) or offset at the weld joint can cause an increase in stress CAUTIONARY NOTE: There are many factors that may affect the life of a welded joint at elevated temperature and an of those factors cannot be addressed in a table of weld strength reduction that may result in reduced service life and control of these deviations is recommended. <u>a</u>
- (e) The weld joint strength reduction factor, W, may be determined using linear interpolation for intermediate temperature values.

- (1) The Cr-Mo Steels include: $\frac{1}{2}$ Cr- $\frac{1}{2}$ Mo, $1\frac{1}{4}$ Cr- $\frac{1}{2}$ Mo, -5i, $2\frac{1}{4}$ Cr-1Mo, 3Cr-1Mo, 5Cr- $\frac{1}{2}$ Mo. 9Cr-1Mo. Longitudinal and 5Minal seam) welds shall be normalized, normalized and tempered, or subjected to proper subcritical postweld heat treatment (PWHT) for the alloy. Required examination is in accordance with para. 341.4.4 or 305.2.4.
 - Longitudinal and spiral (helical seam) seam fusion welded construction is not permitted for C^{-1} 2Mo steel above 454° C (850° F).
- The required carbon content of the weld filler metal shall be >0.05 C wt. %. See para. 341.4.4(b) for examination requirements. The basicity index of SAW flux shall be >1.0.
 - The CSEF (Creep Strength Enhanced Ferritic) steels include grades 91, 92, 911, 122, and 23.
 - N + T = Normalizing + Tempering PWHT.
- Autogenous welds without filler metal in austenitic stainless steel (grade 3xx) and austenitic nickel alloys UNS Nos. N066xx and N088xx. A solution and after welding is required for use of the factors in the Table. See para. 341.4.3(b) for examination requirements. 2646
 - Alternatively, the 100,000 hr Stress Rupture Factors listed in ASME BPVC, Section III, Division 1, Subsection NH, Tables I-14.10 A-xx, B-xx, and C-xx may be used as the weld joint strength reduction factor for the materials and welding consumables specified.

Table 302.3.5 Weld Joint Strength Reduction Factor, W (Cont'd)

NOTES: (Cont'd)

from an embrittlement condition in the weld heat affected zone that can lead to premature failure of welded components operating at elevated temperatures. A solution annealing heat (8) Certain heats of the austenitic standers steels, particularly for those grades whose creep strength is enhanced by the precipitation of temper-resistant carbides and carbonitrides, can suffer treatment of the weld area mitigates this susceptibility.

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				Tempera	ture, °C (°F)		
Material	482 (900) and Below	510 (950)	538 (1,000)	566 (1,050)	593 (1,100)	621 (1,150)	649 (1,200)	677 (1,250) and Above
Ferritic steels	0.4	0.5	0.7	0.7	0.7	0.7	0.7	0.7
Austenitic steels	0.4	0.4	0.4	0.4	0.5	0.7	0.7	0.7
Nickel alloys UNS Nos. N06617, N08800, N08810, and N08825	0.4	0.4	0.4	0.4	0.4	0.4	0.5	0.7
Gray iron	0.0							2
Other ductile metals	0.4	0.4	0.4	0.4	0.4	0.4	0.4	0.4

Table 304.1.1 Values of Coefficient Y for t < D/6

used in determining P_{a2} shall be the lesser of the following values for pipe material at design temperature:

- (a) 1.5 times the stress value from Table A-1 or Table A-1M of this Code, or
- (b) 0.9 times the yield strength tabulated in ASME BPVC, Section II, Part D, Table Y-1 for materials listed therein

(The symbol D_o in ASME BPVC, Section VIII is equivalent to D in this Code.)

304.2 Curved and Mitered Segments of Pipe

304.2.1 Pipe Bends. The minimum required thickness, t_m , of a bend, after bending, in its finished form, shall be determined in accordance with eqs. (2) and (3c)

$$t = \frac{PD}{2[(SEW/I) + PY]} \tag{3c}$$

where at the intrados (inside bend radius)

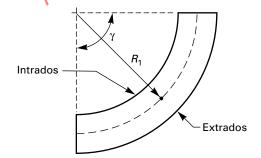
$$I = \frac{4(R_1/D) - 1}{4(R_1/D) - 2} \tag{3d}$$

and at the extrados (outside bend radius)

$$I = \frac{4(R_1/D) + 1}{4(R_1/D) + 2}$$
 (3e)

and at the sidewall on the bend centerline radius, I = 1.0, and where

Figure 304.2.1 Nomenclature for Pipe Bends



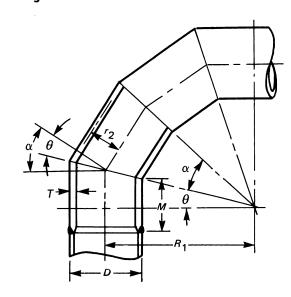
 R_1 = bend radius of welding elbow or pipe bend

Thickness variations from the intrados to the extrados and along the length of the bend shall be gradual. The thickness requirements apply at the mid-span of the bend, $\gamma/2$, at the intrados, extrados, and bend centerline radius. The minimum thickness at the end tangents shall not be less than the requirements of para. 304.1 for straight pipe (see Figure 304.2.1).

304.2.2 Elbows. Manufactured elbows not in accordance with para. 303 shall be qualified as required by para. 304.7.2 or designed in accordance with para. 304.2.1, except as provided in para. 328.4.2(b)(6).

304.2.3 Miter Bends. An angular offset of 3 deg or less (angle α in Figure 304.2.3) does not require design consideration as a miter bend. Acceptable methods for pressure design of multiple and single miter bends are given in (a) and (b) below.

Figure 304.2.3 Nomenclature for Miter Bends



(a) Multiple Miter Bends. The maximum allowable internal pressure shall be the lesser value calculated from eqs. (4a) and (4b). These equations are not applicable when θ exceeds 22.5 deg.

$$P_{m} = \frac{SEW(T-c)}{r_{2}} \left(\frac{T-c}{(T-c) + 0.643 \tan \theta \sqrt{r_{2}(T-c)}} \right)$$
(4a)

$$P_m = \frac{SEW(T-c)}{r_2} \left(\frac{R_1 - r_2}{R_1 - 0.5r_2} \right)$$
 (4b)

- (b) Sinale Miter Bends
- (1) The maximum allowable internal pressure for a single miter bend with angle θ not greater than 22.5 deg shall be calculated by eq. (4a).
- (2) The maximum allowable internal pressure for a single miter bend with angle θ greater than 22.5 deg shall be calculated by eq. (4c)

$$P_{m} = \frac{SEW(T-c)}{r_{2}} \left(\frac{T-c}{(T-c) + 1.25 \tan \theta \sqrt{r_{2}(T-c)}} \right)$$
(4c)

(c) The miter pipe wall thickness, T_1 , used in eqs. (4a), (4b), and (4c) shall extend a distance not less than M from the inside crotch of the end miter welds where

M =the larger of $2.5(r_2T)^{0.5}$ or tan θ ($R_1 - r_2$)

The length of taper at the end of the miter pipe may be included in the distance, M.

- (d) The following nomenclature is used in eqs. (4a), (4b), and (4c) for the pressure design of miter bends:
 - c = same as defined in para. 304.1.1
 - E = same as defined in para. 304.1.1
 - P_m = maximum allowable internal pressure for miter bends
 - R_1 = effective radius of miter bend, defined as the shortest distance from the pipe centerline to the intersection of the planes of adjacent miter joints miter joints r_2 = mean radius of pipe using nominal wall \overline{T}

 - S = same as defined in para. 304.1.1
 - T = miter pipe wall thickness (measured or minimum)in accordance with the purchase specification)
 - W = same as defined in para. 304.1.1
 - α = angle of change in direction at miter joint
 - θ = angle of miter cut

For compliance with this Code, the value of R_1 shall be not less than that given by eq. (5)

$$R_1 = \frac{A}{\tan \theta} + \frac{D}{2} \tag{5}$$

where *A* has the following empirical values:

(1) For SI units

$$\frac{(T-c), \text{ mm}}{\leq 13} \qquad \frac{A}{25} \\
13 < (T-c) < 22 \qquad 2(T-c) \\
\geq 22 \qquad [2(T-c)/3] + 30$$

(2) For U.S. Customary units

$$\frac{(T-c), \text{ in.}}{\leq 0.5} \qquad \frac{A}{1.0}$$

$$0.5 < (T-c) < 0.88 \qquad 2(T-c)$$

$$\geq 0.88 \qquad [2(T-c)/3] + 1.17$$

304.2.4 Curved and Mitered Segments of Pipe Under **External Pressure.** The wall thickness of curved and mitered segments of pipe subjected to external pressure may be determined as specified for straight pipe in para. 304.1.3.

304.3 Branch Connections

304.3.1 General

- (a) Except as provided in (b) below, the requirements in paras. 304.3.2 through 304.3.4 are applicable to branch connections made in accordance with the following
- (1) fittings (tees, extruded outlets, branch outlet fittings in accordance with MSS SP-97, laterals, crosses)
- (2) unlisted cast or forged branch connection fittings (see para. 300.2), and couplings not over DN 80 (NPS 3), attached to the run pipe by welding
- (3) welding the branch pipe directly to the run pipe. with or without added reinforcement, as covered in para. 328.5.4
- (b) The rules in paras. 304.3.2 through 304.3.4 are minimum requirements, valid only for branch connections in which (using the nomenclature of Figure 304.3.3)
- (1) the run pipe diameter-to-thickness ratio (D_h/T_h) is less than 100 and the branch-to-run diameter ratio (D_b / D_h) is not greater than 1.0
- (2) for run pipe with $D_h/T_h \ge 100$, the branch diameter, D_h , is less than one-half the run diameter, D_h
 - (3) angle β is at least 45 deg
 - (4) the axis of the branch intersects the axis of the run
- (c) Where the provisions of (a) and (b) above are not met, pressure design shall be qualified as required by para. 304.7.2.
- (d) Other design considerations relating to branch connections are stated in para. 304.3.5.

304.3.2 Strength of Branch Connections. A pipe having a branch connection is weakened by the opening that must be made in it and, unless the wall thickness of the pipe is sufficiently in excess of that required to sustain the pressure, it is necessary to provide added reinforcement. The amount of reinforcement required to sustain the pressure shall be determined in accordance with para. 304.3.3 or 304.3.4. There are, however, certain branch connections that have adequate pressure strength or reinforcement as constructed. It may be assumed without calculation that a branch connection has adequate strength to sustain the internal and external pressure that will be applied to it if

- (a) the branch connection is made with a listed branch type fitting such as an ASME B16.9 or ASME B16.11 tee, or MSS SP-97 branch connection fitting. See para. 303.
- (b) the branch connection is made by welding a listed threaded or socket welding coupling or listed half coupling directly to the run in accordance with para. 328.5.4, provided the size of the branch does not exceed DN 50 (NPS 2) nor one-fourth the nominal size of the run. The minimum wall thickness of the coupling anywhere in the reinforcement zone (if threads are in the zone, wall thickness is measured from root of thread to minimum outside diameter) shall be not less than that of the unthreaded branch pipe. In no case shall a coupling or half coupling have a rating less than Class 3000 in accordance with ASME B16.11.
- (c) the branch connection utilizes an unlisted branch connection fitting (see para. 300.2), provided the fitting is made from materials listed in Table A-1 or Table A-1M and provided that the branch connection is qualified as required by para. 304.7.2.

304.3.3 Reinforcement of Welded Branch Connections. Added reinforcement is required to meet the criteria in (b) and (c) when it is not inherent in the components of the branch connection. Sample problems illustrating the calculations for branch reinforcement are shown in Appendix H.

(a) Nomenclature. The nomenclature below is used in the pressure design of branch connections. It is illustrated in Figure 304.3.3, which does not indicate details for construction or welding. Some of the terms defined in Appendix J are subject to further definitions or variations,

b = subscript referring to branch

 d_1 = effective length removed from pipe at branch. For branch intersections where the branch opening is a projection of the branch pipe inside diameter (e.g., pipe-to-pipe fabricated branch), $d_1 = [D_h]$ $-2(T_b-c)]/\sin\beta$

 d_2 = "half width" of reinforcement zone = d_1 or $(T_h - c) + (T_h - c) + d_1/2$, whichever is greater, but in any case not more than D_h

h =subscript referring to run or header

 L_4 = height of reinforcement zone outside of run pipe = $2.5(T_h - c)$ or $2.5(T_b - c) + T_r$, whichever is less

 T_b = branch pipe thickness (measured or minimum in accordance with the purchase specification) except for branch connection fittings (see para. 300.2). For such connections the value of T_b for use in calculating L_4 , d_2 , and A_3 is the thickness of the reinforcing barrel (minimum per purchase specification), provided that the barrel thickness is uniform (see

Figure K328.5.4) and extends at least to the L_4 limit (see Figure 304.3.3).

- T_r = minimum thickness of reinforcing ring or saddle made from pipe (use nominal thickness if made from plate)
 - = 0 if there is no reinforcing ring or saddle
- t =pressure design thickness of pipe, according to the appropriate wall thickness equation or procedure in para. 304.1. For welded pipe, when the branch does not intersect the longitudinal weld of the run, the basic allowable stress, S, for the pipe may be used in determining t_h for the purpose of reinforcement calculation only. When the branch does intersect the longitudinal weld of the run, the product SEW (of the stress value, S; the appropriate weld joint quality factor, E_{ij} from Table A-1B; and the weld joint strength reduction factor, W; see para. 302.3.5) for the run pipe shall be used in the calculation. The product SEW of the branch shall be used in calculating t_h .

 β = smaller angle between axes of branch and run

(b) Required Reinforcement Area. The reinforcement area, A_1 , required for a branch connection under internal pressure

$$A_1 = t_h d_1 (2 - \sin \beta) \tag{6}$$

For a branch connection under external pressure, area A_1 \checkmark s one-half the area calculated by eq. (6), using as t_h the thickness required for external pressure.

(c) Available Area. The area available for reinforcement is defined as

$$A_2 + A_3 + A_4 \ge A_1 \tag{6a}$$

These areas are all within the reinforcement zone and are further defined below.

(1) Area A_2 is the area resulting from excess thickness in the run pipe wall

$$A_2 = (2d_2 - d_1)(T_h - t_h - c)$$
(7)

(2) Area A_3 is the area resulting from excess thickness in the branch pipe wall

$$A_3 = 2L_4(T_b - t_b - c)/\sin\beta$$
 (8)

If the allowable stress for the branch pipe wall is less than that for the run pipe, its calculated area must be reduced in the ratio of allowable stress values of the branch to the run in determining its contributions to area A_3 .

(3) Area A_4 is the area of other metal provided by welds and properly attached reinforcement. [See (f).] Weld areas shall be based on the minimum dimensions specified in para. 328.5.4, except that larger dimensions may be used if the welder has been specifically instructed to make the welds to those dimensions.

- (d) Reinforcement Zone. The reinforcement zone is a parallelogram whose length extends a distance, d_2 , on each side of the centerline of the branch pipe and whose width starts at the inside surface of the run pipe (in its corroded condition) and extends beyond the outside surface of the run pipe a perpendicular distance, L_4 .
- (e) Multiple Branches. When two or more branch connections are so closely spaced that their reinforcement zones overlap, the distance between centers of the openings should be at least $1\frac{1}{2}$ times their average diameter, and the area of reinforcement between any two openings shall be not less than 50% of the total that both require. Each opening shall have adequate reinforcement in accordance with (b) and (c). No part of the metal cross section may apply to more than one opening or be evaluated more than once in any combined area. (Consult PFI Standard ES-7, Minimum Length and Spacing for Branch Connections, for detailed recommendations on spacing of welded nozzles.)
 - (f) Added Reinforcement
- (1) Reinforcement added in the form of a ring or saddle as part of area A_4 shall be of reasonably constant width.
- (2) Material used for reinforcement may differ from that of the run pipe provided it is compatible with run and branch pipes with respect to weldability, heat treatment requirements, galvanic corrosion, thermal expansion, etc.
- (3) If the allowable stress for the reinforcement material is less than that for the run pipe, its calculated area must be reduced in the ratio of allowable stress values in determining its contribution to area A₄.
- (4) No additional credit may be taken for a material having higher allowable stress value than the run pipe.

304.3.4 Reinforcement of Extruded Outlet Headers

- (a) The principles of reinforcement stated in para. 304.3.3 are essentially applicable to extruded outlet headers. An extruded outlet header is a length of pipe in which one or more outlets for branch connection have been formed by extrusion, using a die or dies to control the radii of the extrusion. The extruded outlet projects above the surface of the header a distance h_x at least equal to the external radius of the outlet r_x (i.e., $h_x \ge r_x$).
- (b) The rules in this paragraph are minimum requirements, valid only within the limits of geometry shown in Figure 304.3.4, and only where the axis of the outlet intersects and is perpendicular to the axis of the header. Where these requirements are not met, or where nonintegral material such as a ring, pad, or saddle has been added to the outlet, pressure design shall be qualified as required by para. 304.7.2.

- (c) Nomenclature. The nomenclature used herein is illustrated in Figure 304.3.4. Note the use of subscript *x* signifying extruded. Refer to para. 304.3.3(a) for nomenclature not listed here.
 - d_x = the design inside diameter of the extruded outlet, measured at the level of the outside surface of the header. This dimension is taken after removal of all mechanical and corrosion allowances, and all thickness tolerances.
 - d_2 = half width of reinforcement zone (equal to d_x)
 - h_x = height of the extruded outlet. This must be equal to or greater than r_x [except as shown in illustration (b) in Figure 304.3.4].
 - L_5 = height of reinforcement zone
 - $= 0.7\sqrt{D_hT_x}$
 - r_x = radius of curvature of external contoured portion of outlet, measured in the plane containing the axes of the header and branch
 - T_x = corroded finished thickness of extruded outlet, measured at a height equal to r_x above the outside surface of the header
- (d) Limitations on Radius r_x . The external contour radius, r_x is subject to the following limitations:
- (1) minimum r_x the lesser of $0.05D_b$ or 38 mm (1.50 in.)
 - (2) maximum r_x shall not exceed
 - (a) for D_b < DN 200 (NPS 8), 32 mm (1.25 in.)
 - (b) for $D_b \ge DN 200$, $0.1D_b + 13 \text{ mm } (0.50 \text{ in.})$
- (3) for an external contour with multiple radii, the requirements of (1) and (2) above apply, considering the best-fit radius over a 45-deg arc as the maximum radius
- (4) machining shall not be employed in order to meet the above requirements
- (e) Required Reinforcement Area. The required area of reinforcement is defined by

$$A_1 = Kt_h d_x \tag{9}$$

where K is determined as follows:

- (1) For $D_b/D_h > 0.60$, K = 1.00.
- (2) For $0.60 \ge D_b/D_h > 0.15$, $K = 0.6 + \frac{2}{3}(D_b/D_h)$.
- (3) For $D_b/D_h \le 0.15$, K = 0.70.
- (f) Available Area. The area available for reinforcement is defined as

$$A_2 + A_3 + A_4 \ge A_1 \tag{9a}$$

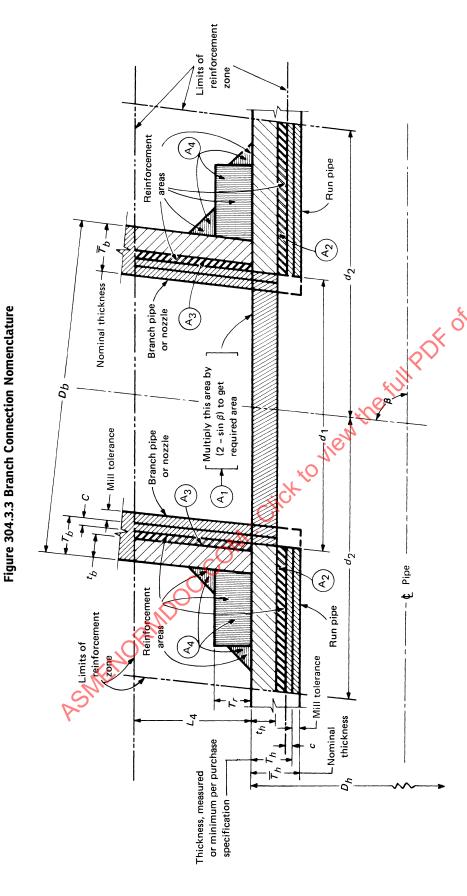
These areas are all within the reinforcement zone and are further defined below.

(1) Area A_2 is the area resulting from excess thickness in the header wall

$$A_2 = (2d_2 - d_x)(T_h - t_h - c)$$
(10)

(2) Area A_3 is the area resulting from excess thickness in the branch pipe wall

$$A_3 = 2L_5(T_h - t_h - c) (11)$$



GENERAL NOTE: This Figure 328.5.4D and Figure 328.5.4F.

Figure 328.5.4D and Figure 328.5.4F.

(3) Area A_4 is the area resulting from excess thickness in the extruded outlet lip

$$A_4 = 2r_x[T_x - (T_h - c)]$$
 (12)

- (g) Reinforcement of Multiple Openings. The rules of para. 304.3.3(e) shall be followed, except that the required area and reinforcement area shall be as given in this paragraph.
- (h) Identification. The manufacturer shall establish the design pressure and temperature for each extruded outlet header and shall mark the header with this information, together with the symbol "B31.3" (indicating the applicable Code Section) and the manufacturer's name or trademark.
- **304.3.5 Additional Design Considerations.** The requirements of paras. 304.3.1 through 304.3.4 are intended to ensure satisfactory performance of a branch connection subject only to pressure. The designer shall also consider the following:
- (a) In addition to pressure loadings, external forces and movements are applied to a branch connection by thermal expansion and contraction, dead and live loads, and movement of piping terminals and supports. Special consideration shall be given to the design of a branch connection to withstand these forces and movements.
- (b) Branch connections made by welding the branch pipe directly to the run pipe should be avoided under the following circumstances:
- (1) when branch size approaches run size, particularly if pipe formed by more than 1.5% cold expansion, or expanded pipe of a material subject to work hardening, is used as the run pipe
- (2) where repetitive stresses may be imposed on the connection by vibration, pulsating pressure, temperature cycling, etc.

In such cases, it is recommended that the design be conservative and that consideration be given to the use of tee fittings or complete engineement types of reinforcement

- (c) Adequate flexibility shall be provided in a small line that branches from a large run, to accommodate thermal expansion and other movements of the larger line (see para. 319.6).
- (d) If ribs, gussets, or clamps are used to stiffen the branch connection, their areas cannot be counted as contributing to the reinforcement area determined in para. 304.3.3(c) or 304.3.4(f). However, ribs or gussets may be used for pressure-strengthening a branch connection in lieu of reinforcement covered in paras. 304.3.3 and 304.3.4 if the design is qualified as required by para. 304.7.2.
- (e) For branch connections that do not meet the requirements of para. 304.3.1(b), integral reinforcement, complete encirclement reinforcement, or other means of reinforcement should be considered.

304.3.6 Branch Connections Under External Pressure. Pressure design for a branch connection subjected to external pressure may be determined in accordance with para. 304.3.1, using the reinforcement area requirement stated in para. 304.3.3(b).

304.4 Closures

304.4.1 General

- (a) Closures not in accordance with para. 303 or (b) shall be qualified as required by para. 3040.2.
- (b) For materials and design conditions covered therein, closures may be designed in accordance with rules in ASME BPVC, Section VIII, Division 1, calculated from eq. (13)

$$t_m = t + Q^2 \tag{13}$$

where

c = sum of allowances defined in para. 304.1.1

t = pressure design thickness, calculated for the type of closure and direction of loading, shown in Table 304.4.1, except that the symbols used to determine t shall be as follows:

🏗 = same as defined in para. 304.1.1

P = design gage pressure

S = S times W, with S and W as defined in para. 304.1.1

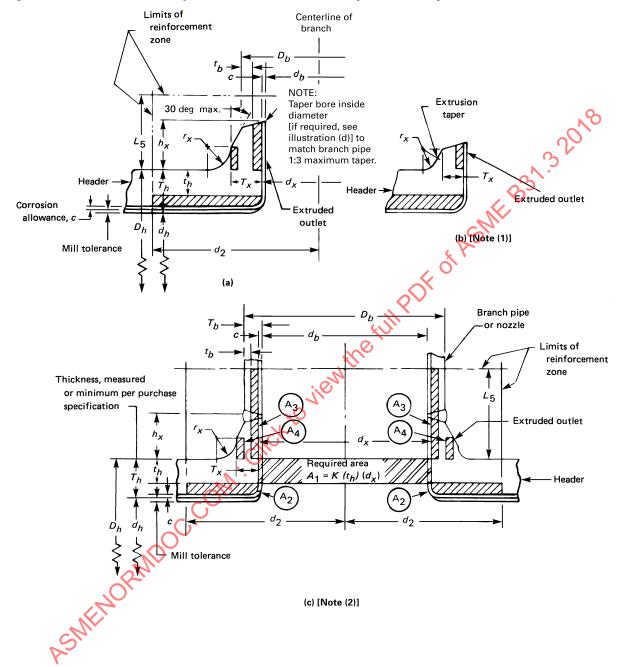
 t_m = minimum required thickness, including mechanical, corrosion, and erosion allowance

304.4.2 Openings in Closures

- (a) The rules in (b) through (g) apply to openings not larger than one-half the inside diameter of the closure as defined in the ASME BPVC, Section VIII, Division 1, UG-36. A closure with a larger opening should be designed as a reducer in accordance with para. 304.6 or, if the closure is flat, as a flange in accordance with para. 304.5.
- (b) A closure is weakened by an opening and, unless the thickness of the closure is sufficiently in excess of that required to sustain pressure, it is necessary to provide added reinforcement. The need for and amount of reinforcement required shall be determined in accordance with the subparagraphs below except that it shall be considered that the opening has adequate reinforcement if the outlet connection meets the requirements in para. 304.3.2(b) or (c).
- (c) Reinforcement for an opening in a closure shall be so distributed that reinforcement area on each side of an opening (considering any plane through the center of the opening normal to the surface of the closure) will equal at least one-half the required area in that plane.
- (d) The total cross-sectional area required for reinforcement in any given plane passing through the center of the opening shall not be less than that defined in ASME BPVC, Section VIII, Division 1, UG-37 (b), UG-38, and UG-39.

Figure 304.3.4 Extruded Outlet Header Nomenclature

This Figure illustrates the nomenclature of para. 304.3.4. It does not indicate complete details or a preferred method of construction.



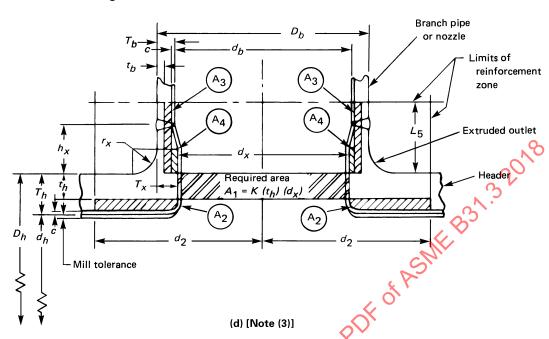


Figure 304.3.4 Extruded Outlet Header Nomenclature (Cont'd)

NOTES:

- (1) Illustration to show method of establishing T_x when the taper encroaches on the crotch radius.
- (2) Illustration is drawn for condition where K = 1.00.
- (3) Illustration is drawn for condition where K = 1.00 and $d_x < d_b$

Table 304.4.1 ASME BPVC References for Closures

Type of Closure	Concave to Pressure	Convex to Pressure
Ellipsoidal	UG-32(d)	UG-33(d)
Torispherical	UG-32(e)	UG-33(e)
Hemispherical	UG-32(f)	UG-33(c)
Conical (no transition to knuckle)	UG-32(g)	UG-33(f)
Toriconical	UG-32(h)	UG-33(f)
Flat (pressure on either side)	UG	-34

GENERAL NOTE: Paragraph numbers are from ASME BPVC, Section VIII, Division 1.

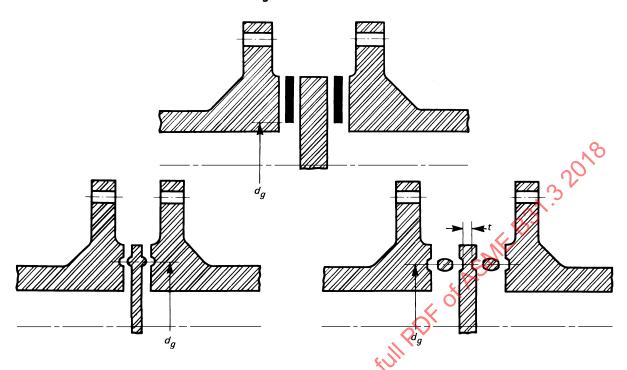
(e) The reinforcement area and reinforcement zone shall be calculated in accordance with para. 304.3.3 or 304.3.4, considering the subscript h and other references to the run or header pipe as applying to the closure. Where the closure is curved, the boundaries of the reinforcement zone shall follow the contour of the closure, and dimensions of the reinforcement zone shall be measured parallel to and perpendicular to the closure surface.

- (f) If two or more openings are to be located in a closure, the rules in paras. 304.3.3 and 304.3.4 for the reinforcement of multiple openings apply.
- (g) The additional design considerations for branch connections discussed in para. 304.3.5 apply equally to openings in closures.

304.5 Pressure Design of Flanges and Blanks 304.5.1 Flanges — General (18)

- (a) Flanges not in accordance with para. 303, or 304.5.1(b) or (d), shall be qualified as required by para. 304.7.2.
- (b) A flange may be designed in accordance with ASME BPVC, Section VIII, Division 1, Mandatory Appendix 2 (Rules for Bolted Flange Connections with Ring Type Gaskets) or ASME BPVC, Section VIII, Division 2, 4.16 (Design Rules for Flanged Joints), using the allowable stresses and temperature limits of this Code. Nomenclature shall be as defined in Appendix 2, except as follows:
 - P = design gage pressure
 - S_a = bolt design stress at atmospheric temperature
 - S_b = bolt design stress at design temperature
 - S_f = product SEW [of the stress value, S; the appropriate quality factor, E, from Table A-1A or Table A-1B; and weld joint strength reduction

Figure 304.5.3 Blanks



factor in accordance with para. 302.3.5(e)] for flange or pipe material. See para. 302.3.2(e).

- (c) The rules in (b) above are not applicable to a flanged joint having a gasket that extends outside the bolts (usually to the outside diameter of the flange)
- (d) For flanges that make solid contact outside the bolts, ASME BPVC, Section VIII, Division 1 Appendix Y should be used.
- (e) See Section VIII, Division 1, Appendix S, for considerations applicable to bolted joint assembly.

304.5.2 Blind Flanges

- (a) Blind flanges not in accordance with para. 303 or 304.5.2(b) shall be qualified as required by para. 304.7.2.
- (b) A blind flange may be designed in accordance with eq. (14). The minimum thickness, considering the manufacturer's minus tolerance, shall be not less than t_m

$$t_m = t + c \tag{14}$$

To calculate *t*, the rules of ASME BPVC, Section VIII, Division 1, UG-34 may be used with the following changes in nomenclature:

- c = sum of allowances defined in para. 304.1.1
- P = internal or external design gage pressure
- S_f = product SEW [of the stress value, S; the appropriate quality factor, E, from Table A-1A or Table A-1B; and weld joint strength reduction

- factor per para. 302.3.5(e)] for flange material. See para. 302.3.2(e).
- t = pressure design thickness, as calculated for the given styles of blind flange, using the appropriate equations for bolted flat cover plates in UG-34

304.5.3 Blanks

- (a) Blanks not in accordance with para. 303 or 304.5.3(b) shall be qualified as required by para. 304.7.2.
- (b) The minimum required thickness of a permanent blank (representative configurations shown in Figure 304.5.3) shall be calculated in accordance with eq. (15)

$$t_m = d_g \sqrt{\frac{3P}{16SEW}} + c \tag{15}$$

where

- c = sum of allowances defined in para. 304.1.1
- d_g = inside diameter of gasket for raised or flat face flanges, or the gasket pitch diameter for ring joint and fully retained gasketed flanges
- E = same as defined in para. 304.1.1
- P = design gage pressure
- S = same as defined in para. 304.1.1
- W = same as defined in para. 304.1.1

304.6 Reducers

304.6.1 Concentric Reducers

- (a) Concentric reducers not in accordance with para. 303 or 304.6.1(b) shall be qualified as required by para. 304.7.2.
- (b) Concentric reducers made in a conical or reversed curve section, or a combination of such sections, may be designed in accordance with the rules for conical and toriconical closures stated in para. 304.4.1.
- **304.6.2 Eccentric Reducers.** Eccentric reducers not in accordance with para. 303 shall be qualified as required by para. 304.7.2.

304.7 Pressure Design of Other Components

- **304.7.1 Listed Components.** Other pressure-containing components manufactured in accordance with standards in Table 326.1 may be utilized in accordance with para. 303.
- **304.7.2 Unlisted Components.** Pressure design of unlisted components to which the rules elsewhere in para. 304 do not apply shall be based on the pressure design criteria of this Code. The designer shall ensure that the pressure design has been substantiated through one or more of the means stated in (a) through (d). Note that designs are also required to be checked for adequacy of mechanical strength as described in para. 302.5. Documentation showing compliance with this paragraph shall be available for the owner's approval.
- (a) extensive, successful service experience under comparable conditions with similarly proportioned components of the same or like material.
- (b) experimental stress analysis, such as described in ASME BPVC, Section VIII, Division 2, Annex 5.F.
- (c) proof test in accordance with ASME B16.9, MSS SP-97, or ASME BPVC, Section VIII, Division 1, UG-101.
- (d) detailed stress analysis (e.g., finite element method) with results evaluated as described in ASME BPVC, Section VIII, Division 2, Part 5. The basic allowable stress from Table A-1 or Table A-1M shall be used in place of the allowable stress, *S*, in Division 2 where applicable. Load design factors used in a Division 2 evaluation shall be consistent with the design bases in para. 302.3.2. At design temperatures in the creep range, additional considerations beyond the scope of Division 2 may be necessary.
- (e) For any of the above, the designer may interpolate between sizes, wall thicknesses, and pressure classes, and may determine analogies among related materials.
- **304.7.3 Metallic Components With Nonmetallic Pressure Parts.** Components not covered by standards listed in Table 326.1, in which both metallic and nonmetallic parts contain the pressure, shall be evaluated by applicable requirements of para. A304.7.2 as well as those of para. 304.7.2.

304.7.4 Expansion Joints

- (a) Metallic Bellows Expansion Joints. The design of bellows type expansion joints shall be in accordance with Appendix X. See also Appendix F, para. F304.7.4 for further design considerations.
 - (b) Slip Type Expansion Joints
- (1) Pressure-containing elements shall be in accordance with para. 318 and other applicable requirements of this Code.
- (2) External piping loads shall not impose excessive bending on the joint.
- (3) The effective pressure thrust area shall be computed using the outside diameter of the pipe.
- (c) Other Types of Expansion Joint. The design of other types of expansion joint shall be qualified as required by para. 304.7.2.

FLUID SERVICE REQUIREMENTS FOR PIPING COMPONENTS

305 PIPE

Pipe includes components designated as "tube" or "tubing" in the material specification, when intended for pressure service.

305.1 General

Listed pipe may be used in Normal Fluid Service except as stated in paras. 305.2.1 and 305.2.2. Unlisted pipe may be used only as provided in para. 302.2.3.

305.2 Specific Requirements

305.2.1 Pipe for Category D Fluid Service. The following carbon steel pipe may be used only for Category D Fluid Service:

API 5L continuous welded (furnace butt-welded) ASTM A53, Type F

ASTM A134 made from other than ASTM A285 plate

305.2.2 Pipe Requiring Safeguarding. When used for other than Category D Fluid Service, the following carbon steel pipe shall be safeguarded:

ASTM A134 made from ASTM A285 plate ASTM A139

305.2.3 Pipe for Severe Cyclic Conditions

- (a) Except as limited in (b) through (d), only the following pipe may be used under severe cyclic conditions:
 - (1) pipe listed in Table A-1A, where $E_c \ge 0.90$, or
 - (2) pipe listed in Table A-1B, where $E_i \ge 0.90^7$
- (b) For API 5L pipe, only the following materials may be used:

⁷ See para. 302.3.3.

Grade A or B, seamless

Grade A or B, SAW, str. seam, $E_i \ge 0.95$

Grade X42, seamless

Grade X46, seamless

Grade X52, seamless

Grade X56, seamless

Grade X60, seamless

- (c) For copper pipe, only ASTM B42 may be used.
- (d) For copper alloy pipe, only ASTM B466 may be used.
- (e) For aluminum alloy pipe, only ASTM B210 and B241, both in tempers 0 and H112, may be used.

305.2.4 Elevated Temperature Fluid Service. In Elevated Temperature Fluid Service, all longitudinal or spiral (helical seam) welds in P-No. 4 or P-No. 5 materials shall be examined by 100% radiography or 100% ultrasonic examination. Acceptance criteria are as stated in para. 341.3.2 and in Table 341.3.2, for Normal Fluid Service, unless otherwise specified.

306 FITTINGS, BENDS, MITERS, LAPS, AND BRANCH CONNECTIONS

Fittings, bends, miters, laps, and branch connections may be used in accordance with paras. 306.1 through 306.5. Pipe and other materials used in such components shall be suitable for the manufacturing or fabrication process and the fluid service.

306.1 Pipe Fittings

306.1.1 Listed Fittings. Listed fittings may be used in Normal Fluid Service in accordance with para. 303

306.1.2 Unlisted Fittings. Unlisted fittings may be used only in accordance with para. 302.2.3.

306.1.3 Specific Fittings

- (a) Proprietary welding branch outlet fittings that have been design proof tested successfully as prescribed in ASME B16.9, MSS SP-97, or ASME BPVC, Section VIII, Division 1, UG-101 may be used within their established ratings.
- (b) The lap thickness of a proprietary "Type C" lap-joint stub-end buttwelding fitting shall conform to the requirements of para. 306.4.2 for flared laps.

306.1.4 Fittings for Severe Cyclic Conditions

- (a) Only the following fittings may be used under severe cyclic conditions:
 - (1) forged.
- (2) wrought, seamless or welded. If welded, requires 100% radiograph of welds in accordance with para. 344.5.1 and Table 341.3.2.
 - (3) cast, with factor $E_c \ge 0.90.7$
- (b) Fittings conforming to MSS SP-43, MSS SP-119, and proprietary "Type C" lap-joint stub-end welding fittings shall not be used under severe cyclic conditions.

306.2 Pipe Bends

306.2.1 General

- (a) A pipe bend made in accordance with paras. 332.2.1 and 332.2.2, and verified for pressure design in accordance with para. 304.2.1, is suitable for the same service as the pipe from which it is made.
- (b) A pipe bend made in accordance with para. 332.2.2, but not meeting the flattening limits of para. 332.2.1, may be qualified for pressure design by para. 304.7.2 and shall not exceed the rating of the straight pipe from which it is made
- **306.2.2 Corrugated and Other Bends.** Bends of other designs (such as creased or corrugated) shall be qualified for pressure design as required by para. 304.7.2.
- **306.2.3 Bends for Severe Cyclic Conditions.** A pipe bend designed as creased or corrugated shall not be used under severe cyclic conditions.

306.3 Miter Bends

306.3.1 General. Except as stated in para. 306.3.2, a miter bend made in accordance with para. 304.2.3 and welded in accordance with para. 311.1 is suitable for use in Normal Fluid Service.

306.3.2 Miter Bends for Category D Fluid Service. A (18) miter bend that makes a change in direction at a single foint (angle α in Figure 304.2.3) greater than 45 deg, or is welded in accordance with para. 311.1, may be used only for Category D Fluid Service.

306.3.3 Miter Bends for Severe Cyclic Conditions. A (18) miter bend to be used under severe cyclic conditions shall be made in accordance with para. 304.2.3 and welded in accordance with para. 311.1, and shall have an angle α (see Figure 304.2.3) \leq 22.5 deg.

306.4 Laps

The following requirements do not apply to fittings conforming to para. 306.1, specifically lap-joint stub ends conforming to ASME B16.9, nor to laps integrally hot-forged on pipe ends, except as noted in paras. 306.4.3 and 306.4.4(a).

- **306.4.1 Fabricated Laps.** A fabricated lap is suitable for use in Normal Fluid Service, provided that all of the following requirements are met:
- (a) The outside diameter of the lap shall be within the dimensional tolerances of the corresponding ASME B16.9 lap-joint stub end.
- (b) The lap thickness shall be at least equal to the nominal wall thickness of the pipe to which it is attached.
- (c) The lap material shall have an allowable stress at least as great as that of the pipe.
- (d) Welding shall be in accordance with para. 311.1 and fabrication shall be in accordance with para. 328.5.5.

- **306.4.2 Flared Laps.** See para. 308.2.5 for requirements of lapped flanges for use with flared laps. A flared lap is suitable for use in Normal Fluid Service, provided that all of the following requirements are met:
- (a) The pipe used shall be of a specification and grade suitable for forming without cracks, surface buckling, or other defects.
- (b) The outside diameter of the lap shall be within the dimensional tolerances of the corresponding ASME B16.9 lap-joint stub end.
 - (c) The radius of fillet shall not exceed 3 mm ($\frac{1}{8}$ in.).
- (d) The lap thickness at any point shall be at least 95% of the minimum pipe wall thickness, T, multiplied by the ratio of the pipe outside diameter to the diameter at which the lap thickness is measured.
- (e) Pressure design shall be qualified as required by para. 304.7.2.
- **306.4.3 Forged Laps.** A lap integrally hot-forged on a pipe end is suitable for Normal Fluid Service only when the requirements of para. 332 are met. Its dimensions shall conform to those for lap-joint stub ends given in ASME B16.9.

(18) 306.4.4 Laps for Severe Cyclic Conditions

- (a) A forged lap-joint stub end in accordance with para. 306.1 or a lap integrally hot-forged on a pipe end in accordance with para. 306.4.3 may be used under severe cyclic conditions.
- (b) A fabricated lap to be used under severe cyclic conditions shall conform to the requirements of para. 306.4.1, except that welding shall be in accordance with para. 311.1. A fabricated lap shall conform to a detail shown in Figure 328.5.5, illustration (d) or (e).
- (c) A flared lap is not permitted under severe cyclic conditions.

306.5 Fabricated Branch Connections

The following requirements do not apply to fittings conforming to para. 3061.

- **306.5.1 General.** Afabricated branch connection made and verified for pressure design in accordance with para. 304 37 and welded in accordance with para. 311 17 is suitable for use in Normal Fluid Service.
- (18) **306.5.2 Fabricated Branch Connections for Severe Cyclic Conditions.** A fabricated branch connection to be used under severe cyclic conditions shall conform to the requirements of para. 306.5.1, except that welding shall be in accordance with para. 311.1, with fabrication limited to a detail equivalent to Figure 328.5.4D, illustration (2) or (4), or to Figure 328.5.4E.

306.6 Thermowells

Thermowells shall comply with ASME PTC 19.3 TW where applicable.

307 VALVES AND SPECIALTY COMPONENTS

The following requirements for valves shall also be met as applicable by other pressure-containing piping components, such as traps, strainers, and separators. See also Appendix F, paras. F301.4 and F307.

307.1 General

307.1.1 Listed Valves. A listed valve is suitable for use in Normal Fluid Service, except as stated in para. 307.2.

307.1.2 Unlisted Valves. Unlisted valves may be used only in accordance with para. 302.2.3. Unless pressure-temperature ratings are established by the method set forth in ASME B16.34, pressure design shall be qualified as required by para. 304.7.2.

307.2 Specific Requirements

307.2.1 Bonnet Bolting. A bolted bonnet valve whose bonnet is secured to the body by less than four bolts, or by a U-bolt, may be used only for Category D Fluid Service.

307.2.2 Stem Retention. Valves shall be designed so that the stem seal retaining fasteners (e.g., packing, gland fasteners) alone do not retain the stem. Specifically, the design shall be such that the stem shall not be capable of removal from the valve, while the valve is under pressure, by the removal of the stem seal retainer (e.g., gland) alone.

308 FLANGES, BLANKS, FLANGE FACINGS, AND GASKETS

308.1 General

308.1.1 Listed Components. A listed flange, blank, or gasket is suitable for use in Normal Fluid Service, except as stated elsewhere in para. 308.

308.1.2 Unlisted Components. Unlisted flanges, blanks, and gaskets may be used only in accordance with para. 302.2.3.

308.2 Specific Requirements for Flanges

See Appendix F, paras. F308.2 and F312.

Table 308.2.1 Permissible Sizes/Rating Classes for (18) Slip-On Flanges Used as Lapped Flanges

_	Maximum	Flange Size
Rating Class	DN	NPS
150	300	12
300	200	8

GENERAL NOTE: Actual thickness of the slip-on flange at the bolt circle shall be at least equal to the minimum required flange thickness for lapped flanges in ASME B16.5.

308.2.1 Slip-On Flanges

- (a) A slip-on flange shall be double-welded as shown in Figure 328.5.2B when the service is
- (1) subject to severe erosion, crevice corrosion, or cyclic loading
 - (2) flammable, toxic, or damaging to human tissue
 - (3) under severe cyclic conditions
 - (4) at temperatures below -101°C (-150°F)
- (b) The use of slip-on flanges should be avoided where many large temperature cycles are expected, particularly if the flanges are not insulated.
- (c) Slip-on Flanges as Lapped Flanges. A slip-on flange may be used as a lapped flange only as shown in Table 308.2.1 unless pressure design is qualified in accordance with para. 304.5.1. A corner radius or bevel shall conform to one of the following as applicable:
- (1) For an ASME B16.9 lap joint stub end or a forged lap (see para. 306.4.3), the corner radius shall be as specified in ASME B16.5, Tables 9 and 12, dimension r.
- (2) For a fabricated lap, the corner bevel shall be at least half the nominal thickness of the pipe to which the lap is attached (see Figure 328.5.5).
 - (3) For a flared lap see para. 308.2.5.
- **308.2.2 Expanded-Joint Flanges.** A flange having an expanded-joint insert is subject to the requirements for expanded joints in para. 313.
- **308.2.3 Socket Welding and Threaded Flanges.** A socket welding flange is subject to the requirements for socket welds in para. 311.2.2. A threaded flange is subject to the requirements for threaded joints in para. 314.
- **308.2.4 Flanges for Severe Cyclic Conditions.** Unless it is safeguarded, a flange to be used under severe cyclic conditions shall be welding neck conforming to ASME B16.5 or ASME B16.47, or a similarly proportioned flange designed in accordance with para. 304.5.1.
- **308.2.5 Flanges for Flared Metallic Laps.** For a flange used with a flared metallic lap (para. 306.4.2), the intersection of face and bore shall be beveled or rounded approximately 3 mm $\frac{1}{16}$ in.). See also para. 308.2.1(c).

(18) 308.3 Flange Facings

The flange facing shall be compatible with the gasket and bolting employed.

(18) **308.4 Gaskets**

Gaskets shall be selected so that the required seating load is compatible with the flange rating and facing, the strength of the flange, and its bolting. See Appendix F, para. F308.4.

309 BOLTING

Bolting includes bolts, bolt studs, studs, cap screws, nuts, and washers. See also Appendix F, para. F309.

309.1 General

- **309.1.1 Listed Bolting.** Listed bolting is suitable for use in Normal Fluid Service, except as stated elsewhere in para. 309.
- **309.1.2 Unlisted Bolting.** Unlisted bolting may be used only in accordance with para. 302.2.3.
- **309.1.3 Bolting for Components.** Bolting for components conforming to a listed standard shall be in accordance with that standard if specified therein.
- **309.1.4 Selection Criteria.** Bolting selected shall be adequate to seat the gasket and maintain joint tightness under all design conditions:

309.2 Specific Bolting

- **309.2.1 Low Yield Strength Bolting.** Bolting having not more than 207 MPa (30 ksi) specified minimum yield strength shall not be used for flanged joints rated ASME B16.5 Class 400 and higher, nor for flanged joints using metallic gaskets, unless calculations have been made showing adequate strength to maintain joint tightness.
- other provisions of this Code, carbon steel bolting may be used with nonmetallic gaskets in flanged joints rated ASME B16.5 Class 300 and lower for bolt metal temperatures at -29°C to 204°C (-20°F to 400°F), inclusive. If these bolts are galvanized, heavy hexagon nuts, threaded to suit, shall be used.
- 309.2.3 Bolting for Metallic Flange Combinations. (18) Any bolting that meets the requirements of para. 309 may be used with any combination of flange material and facing. If either flange is to the ASME B16.1, ASME B16.24 manufactured from an ASTM B61 or an ASTM B62 casting, MSS SP-42, or MSS SP-51 specification, the bolting material shall be no stronger than low yield strength bolting unless
- (a) both flanges have flat faces and a full-face gasket is used, or
- (b) sequence and torque limits for bolt-up are specified, with consideration of sustained loads, displacement strains, occasional loads (see paras. 302.3.5 and 302.3.6), and strength of the flanges
- **309.2.4 Bolting for Severe Cyclic Conditions.** Low yield strength bolting (see para. 309.2.1) shall not be used for flanged joints under severe cyclic conditions.

309.3 Tapped Holes

Tapped holes for pressure-retaining bolting in metallic piping components shall be of sufficient depth that the thread engagement will be at least seven-eighths times the nominal thread diameter.

PART 4 FLUID SERVICE REQUIREMENTS FOR PIPING JOINTS

(18) 310 GENERAL

Piping joints shall be selected considering joint tightness and mechanical strength under expected service and test conditions of pressure, temperature, and external loading. See para. 302.5.

311 WELDED JOINTS

Joints may be made by welding in any material for which it is possible to qualify welding procedures, welders, and welding operators in conformance with the rules in Chapter V.

(18) 311.1 General

Welds shall conform to the following:

- (a) Welding shall be in accordance with para. 328.
- (b) Preheating and heat treatment shall be in accordance with paras. 330 and 331, respectively.
- (c) Examination shall be in accordance with para. 341.4.
- (d) Acceptance criteria shall be in accordance with para. 341.3.2.

(18) 311.2 Specific Requirements

311.2.1 Backing Rings and Consumable Inserts

- (a) If a backing ring is used where the resulting crevice is detrimental (e.g., subject to corrosion, vibration, or severe cyclic conditions), it should be removed and the internal joint face ground smooth. When it is impractical to remove the backing ring in such a case, consideration shall be given to welding without backing rings or to the use of consumable inserts or removable nonmetallic backing rings.
- (b) Split backing rings shall not be used under severe cyclic conditions.

311.2.2 Socket Welds

- (a) Socket welded joints (para. 328.5.2) should be avoided in any service where crevice corrosion or severe erosion may occur.
 - (b) Socket welded joints shall conform to the following:

- (1) Socket dimensions shall conform to ASME B16.5 for flanges and ASME B16.11 or MSS SP-119 for other socket-welding components.
- (2) Weld dimensions shall not be less than those shown in Figures 328.5.2B and 328.5.2C.
- (c) Socket welds larger than DN 50 (NPS 2) shall not be used under severe cyclic conditions.
- (d) A drain or bypass in a component may be attached by socket welding, provided the socket dimensions conform to Figure 4 in ASME B16.5.

311.2.3 Fillet Welds

- (a) Fillet welds in accordance with para. 328.5.2 may be used as primary welds to attach socket welding components and slip-on flanges.
- (b) Fillet welds may also be used to attach reinforcement and structural attachments, to supplement the strength or reduce stress concentration of primary welds, and to prevent disassembly of joints.
- **311.2.4 Seal Welds.** Seal welds (para. 328.5.3) may be used only to prevent leakage of threaded joints and shall not be considered as contributing any strength to the joints.

312 FLANGED JOINTS

(18)

See Appendix F, para. F312.1.

312.1 Joints Using Flanges of Different Ratings

Where flanges of different ratings are bolted together, the rating of the joint shall not exceed that of the lower rated flange. Bolting torque shall be limited so that excessive loads will not be imposed on the lower rated flange in obtaining a tight joint.

312.2 Metal to Nonmetal Flanged Joints

Where a metallic flange is bolted to a nonmetallic flange, both should be flat-faced. A full-faced gasket is preferred. If a gasket extending only to the inner edge of the bolts is used, bolting torque shall be limited so that the nonmetallic flange is not overloaded.

312.3 Flanged Joint Assembly

See para. 335.2.5.

313 EXPANDED JOINTS

(a) Expanded joints shall not be used under severe cyclic conditions. For other services, adequate means shall be provided to prevent separation of the joint. If the fluid is toxic or damaging to human tissue, safeguarding is required.

(18)	Table 314.2.1 Minimum Schedule of Components W	Vith
	External Threads	

	Notch- Sensitive	Size Range [Note (2)]		Minimum
Fluid Service	Material [Note (1)]	DN	NPS	Schedule [Note (3)]
Normal	Yes	≤40	≤1 ¹ / ₂	80
		50-150	2-6	40
		>150	>6	None
	No	≤150	≤6	40
		>150	>6	None
Category D	Either	All	All	None

NOTES:

- Carbon steel is generally considered to be notch sensitive, whereas stainless steel is generally considered to be not notch sensitive.
- (2) For sizes over DN 50 (NPS 2), the joint shall be safeguarded (see Appendix G) for a fluid service that is flammable, toxic, or damaging to human tissue.
- (3) Minimum schedules 40 and 80 are listed in ASME B36.10M, which are identical to schedules 40S and 80S listed in ASME B36.19M for DN 150 (NPS 6) and smaller.
- (b) Consideration shall be given to the tightness of expanded joints when subjected to vibration, differential expansion or contraction due to temperature cycling, or external mechanical loads.

314 THREADED JOINTS

314.1 General

Threaded joints are suitable for Normal Fluid Service except as stated elsewhere in para. 314. They may be used under severe cyclic conditions only as provided in paras. 314.2.1(c) and 314.2.2.

- (a) Threaded joints should be avoided in any service where crevice corrosion, severe erosion, or cyclic loading may occur.
- (b) When threaded joints are intended to be seal welded, thread sealing compound shall not be used.
- (c) Layout of piping employing threaded joints should, insofar as possible, minimize stress on joints, giving special consideration to stresses due to thermal expansion and operation of valves (particularly a valve at a free end). Provision should be made to counteract forces that would tend to unscrew the joints.
- (d) Except for specially designed joints employing lens rings or similar gaskets, threaded flanges in which the pipe ends project through to serve as the gasket surface may be used only for Category D Fluid Service.

314.2 Specific Requirements

- **314.2.1 Taper-Threaded Joints.** For joints in which the (18) threads of both mating components conform to ASME B1.20.1,
- (a) the minimum thickness of components with external threads shall be the greater of t_m in accordance with para. 304.1.1 and the schedule shown in Table 314.2.1
- (b) threaded components shall be checked for adequacy of mechanical strength as described in para. 302.5
- (c) threaded components of a specialty nature that are not subject to external moment loading, such as thermometer wells, may be used under severe cyclic conditions

A coupling having straight threads may be used only for Category D Fluid Service, and only with taper-threaded mating components.

314.2.2 Straight-Threaded Joints. Threaded joints in which the tightness of the joint is provided by a seating surface other than the threads (e.g., a union comprising male and female ends joined with a threaded union nut, or other constructions shown typically in Figure 335.3.3) may be used. If such joints are used under severe cyclic conditions and are subject to external moment loadings, safeguarding is required.

315 TUBING JOINTS

315.1 General

In selecting and applying flared, flareless, and compression type tubing fittings, the designer shall consider the possible adverse effects on the joints of such factors as assembly and disassembly, cyclic loading, vibration, shock, and thermal expansion and contraction.

315.2 Joints Conforming to Listed Standards (18)

Joints using flared, flareless, or compression type tubing fittings covered by listed standards may be used in Normal Fluid Service provided that

- (a) the fittings and joints are compatible with the tubing with which they are to be used (considering maximum and minimum wall thickness) and are used within the pressure-temperature limitations of the fitting and the joint
- (b) the joints are safeguarded when used under severe cyclic conditions

315.3 Joints Not Conforming to Listed Standards (18)

Joints using flared, flareless, or compression type tubing fittings not listed in Table 326.1 may be used in accordance with para. 315.2 provided that the design is qualified in accordance with para. 304.7.2.

316 CAULKED JOINTS

Caulked joints such as bell type joints shall be limited to Category D Fluid Service and to a temperature not over 93°C (200°F). They shall be used within the pressure-temperature limitations of the joint and pipe. Provisions shall be made to prevent disengagement of joints, to prevent buckling of the piping, and to sustain lateral reactions produced by branch connections or other causes.

317 SOLDERED AND BRAZED JOINTS

317.1 Soldered Joints

Soldered joints shall be made in accordance with the provisions of para. 333 and may be used only in Category D fluid service. Fillet joints made with solder metal are not permitted. The low melting point of solder shall be considered where possible exposure to fire or elevated temperature is involved.

317.2 Brazed and Braze Welded Joints

- (a) Brazed and braze welded joints made in accordance with the provisions in para. 333 are suitable for Normal Fluid Service. They shall be safeguarded in fluid services that are flammable, toxic, or damaging to human tissue. They shall not be used under severe cyclic conditions. The melting point of brazing alloys shall be considered where possible exposure to fire is involved.
- (b) Fillet joints made with brazing filler metal are not permitted.

318 SPECIAL JOINTS

Special joints are those not covered elsewhere in Chapter II, Part 4, such as bell type and packed gland type joints.

318.1 General

- **318.1.1 Listed Joints.** Joints using listed components are suitable for Normal Whid Service.
- **318.1.2 Unlisted Joints.** For joints that utilize unlisted components, pressure design shall be qualified as required by para. 304.7.2.

318.2 Specific Requirements

- **318.2.1 Joint Integrity.** Separation of the joint shall be prevented by a means that has sufficient strength to withstand anticipated conditions of service.
- **318.2.2 Joint Interlocks.** Either mechanical or welded interlocks shall be provided to prevent separation of any joint used for a fluid service that is flammable, toxic, or damaging to human tissues, of any joint to be used under severe cyclic conditions, and of any joint exposed to temperatures in the creep range.

318.2.3 Bell and Gland Type Joints. Bell-type and (18) gland-type joints used under severe cyclic conditions shall be safeguarded.

PART 5 FLEXIBILITY AND SUPPORT

319 PIPING FLEXIBILITY

319.1 Requirements

- **319.1.1 Basic Requirements.** Piping systems shall have sufficient flexibility to prevent thermal expansion or contraction or movements of piping supports and terminals from causing
- (a) failure of piping or supports from overstress or fatigue
 - (b) leakage at joints
- (c) detrimental stresses or distortion in piping and valves or in connected equipment (e.g., pumps and turbines), resulting from excessive thrusts and moments in the piping
- **319.1.2 Specific Requirements.** In para. 319, concepts, data, and methods are given for determining the requirements for flexibility in a piping system and for assuring that the system meets all of these requirements. In brief, these requirements are that
- (a) the computed stress range at any point due to displacements in the system shall not exceed the allowable stress range established in para. 302.3.5
- (b) reaction forces computed in para. 319.5 shall not be detrimental to supports or connected equipment
- (c) computed movement of the piping shall be within any prescribed limits, and properly accounted for in the flexibility calculations
- If it is determined that a piping system does not have adequate inherent flexibility, means for increasing flexibility shall be provided in accordance with para. 319.7.

319.2 Concepts

Concepts characteristic of piping flexibility analysis are covered in the following paragraphs. Special consideration is given to displacements (strains) in the piping system, and to resultant axial, bending, and torsional displacement stress ranges.

319.2.1 Displacement Strains

(a) Thermal Displacements. A piping system will undergo dimensional changes with any change in temperature. If it is constrained from free expansion or contraction by connected equipment and restraints such as guides and anchors, it will be displaced from its unrestrained position.

- (b) Restraint Flexibility. If restraints are not considered rigid, their flexibility may be considered in determining displacement stress range and reactions.
- (c) Externally Imposed Displacements. Externally caused movement of restraints will impose displacements on the piping in addition to those related to thermal effects. Movements may result from tidal changes (dock piping), wind sway (e.g., piping supported from a tall slender tower), or temperature changes in connected equipment.

Movement due to earth settlement, since it is a single cycle effect, will not significantly influence fatigue life. A displacement stress range greater than that permitted by para. 302.3.5(d) may be allowable if due consideration is given to avoidance of excessive localized strain and end reactions.

(d) Total Displacement Strains. Thermal displacements, reaction displacements, and externally imposed displacements all have equivalent effects on the piping system, and shall be considered together in determining the total displacement strains (proportional deformation) in various parts of the piping system.

319.2.2 Displacement Stresses

- (a) Elastic Behavior. Stresses may be considered proportional to the total displacement strains in a piping system in which the strains are well-distributed and not excessive at any point (a balanced system). Layout of systems should aim for such a condition, which is assumed in flexibility analysis methods provided in this Code.
- (b) Overstrained Behavior. Stresses cannot be considered proportional to displacement strains throughout a piping system in which an excessive amount of strain may occur in localized portions of the system (an unbalanced system). Operation of an unbalanced system in the creep range may aggravate the deleterious effects due to creep strain accumulation in the most susceptible regions of the system. Unbalance may result from one or more of the following:
- (1) highly stressed small size pipe runs in series with large or relatively stiff pipe runs.
- (2) a local reduction in size or wall thickness, or local use of material having reduced yield strength (for example, girth welds of substantially lower strength than the base metal).
- (3) a line configuration in a system of uniform size in which the expansion or contraction must be absorbed largely in a short offset from the major portion of the run.
- (4) variation of piping material or temperature in a line. When differences in the elastic modulus within a piping system will significantly affect the stress distribution, the resulting displacement stresses shall be computed based on the actual elastic moduli at the respective operating temperatures for each segment in the system and then multiplied by the ratio of the elastic

modulus at ambient temperature to the modulus used in the analysis for each segment.

Unbalance should be avoided or minimized by design and layout of piping systems, particularly those using materials of low ductility. Many of the effects of unbalance can be mitigated by selective use of cold spring. If unbalance cannot be avoided, the designer shall use appropriate analytical methods in accordance with para. 319.4 to assure adequate flexibility as defined in para. 319.1.

319.2.3 Displacement Stress Range

- (a) In contrast with stresses from sustained loads, such as internal pressure or weight, displacement stresses may be permitted to attain sufficient magnitude to cause local yielding in various portions of a piping system. When the system is initially operated at the condition of greatest displacement (highest or lowest temperature, or greatest imposed movement) from its installed condition, any yielding or creep brings about a reduction or relaxation of stress. When the system is later returned to its original condition (or a condition of opposite displacement), a reversal and redistribution of stresses occurs that is referred to as self-springing. It is similar to cold springing in its effects.
- (b) While stresses resulting from displacement strains diminish with time due to yielding or creep, the algebraic difference between strains in the extreme displacement condition and the original (as-installed) condition (or any anticipated condition with a greater differential effect) remains substantially constant during any one cycle of operation. This difference in strains produces a corresponding stress differential, the displacement stress range, that is used as the criterion in the design of piping for flexibility. In evaluating systems where supports may be active in some conditions and not others (e.g., pipes lifting off supports), this difference in strains may be influenced by the changing distribution of sustained load. In such cases, the displacement strain range is based on the algebraic difference between the calculated positions of the pipe that define the range. In addition to the displacement strain, each calculated position shall include the sustained loads present in the condition under evaluation. See para. 302.3.5(d) for the allowable stress range, S_A , and para. 319.4.4(a) for the computed displacement stress range, S_E .
- **319.2.4 Cold Spring.** Cold spring is the intentional deformation of piping during assembly to produce a desired initial displacement and reaction. Cold spring is beneficial in that it serves to balance the magnitude of the reaction under initial and extreme displacement conditions. When cold spring is properly applied there is less likelihood of overstrain during initial operation; hence, it is recommended especially for piping materials of limited ductility. There is also less deviation from asinstalled dimensions during initial operation, so that

hangers will not be displaced as far from their original settings.

Inasmuch as the service life of a piping system is affected more by the range of stress variation than by the magnitude of stress at a given time, no credit for cold spring is permitted in stress range calculations. However, in calculating the thrusts and moments where actual reactions as well as their range of variations are significant, credit is given for cold spring.

319.3 Properties for Flexibility Analysis

The following paragraphs deal with properties of piping materials and their application in piping flexibility stress analysis.

319.3.1 Thermal Expansion Data

- (a) Values for Stress Range. Values of thermal displacements to be used in determining total displacement strains for computing the stress range shall be determined from Appendix C as the algebraic difference between the value at maximum metal temperature and that at the minimum metal temperature for the thermal cycle under analysis.
- (b) Values for Reactions. Values of thermal displacements to be used in determining total displacement strains for computation of reactions on supports and connected equipment shall be determined as the algebraic difference between the value at maximum (or minimum) temperature for the thermal cycle under analysis and the value at the temperature expected during installation.
- 319.3.2 Modulus of Elasticity. The reference modulus of elasticity at 21°C (70°F), E_a , and the modulus of elasticity at maximum or minimum temperature, E_m , shall be taken as the values shown in Appendix of or the temperatures determined in para. 319.3.1(a) or (b). For materials not included in Appendix C, reference shall be made to authoritative source data, such as publications of the National Institute of Standards and Technology.
- **319.3.3 Poisson's Ratio.** Poisson's ratio may be taken as 0.3 at all temperatures for all metals. More accurate and authoritative data may be used if available.

319.3.4 Allowable Stresses

- (a) The allowable displacement stress range, S_A , and permissible additive stresses shall be as specified in para. 302.3.5(d) for systems primarily stressed in bending and/or torsion.
- (b) The stress intensification factors in Appendix D have been developed from fatigue tests of representative piping components and assemblies manufactured from ductile ferrous materials. The allowable displacement stress range is based on tests of carbon and austenitic stainless steels. Caution should be exercised when using eqs. (1a) and (1b) (para. 302.3.5) for allowable displacement stress range for some nonferrous materials

(e.g., certain copper and aluminum alloys) for other than low cycle applications.

319.3.5 Dimensions. Nominal thicknesses and outside diameters of pipe and fittings shall be used in flexibility calculations.

319.3.6 Flexibility and Stress Intensification Factors. (18)

The flexibility factors, k, and stress intensification factors, i, shall not be less than unity. In the absence of more directly applicable data, the flexibility factor, k, and stress intensification factor, i, shown in Appendix D shall be used for flexibility calculations described in para. 319.4.

Flexibility factors and stress intensification factors may be developed in accordance with ASME B31J, Nonmandatory Appendices B and A, respectively.

For piping components or attachments (such as valves, strainers, anchor rings, or bands) not covered in Table D300, suitable stress intensification factors may be assumed by comparison of their significant geometry with that of the components shown. The validity of any assumptions is the responsibility of the designer. If two or more of the geometries shown in Appendix D are combined, their combined k and i might be significantly different from the values shown. Examples include trunnions on elbows and branch connection fittings welded to anything other than straight pipe.

319.4 Flexibility Analysis

- 319.4.1 Formal Analysis Not Required. No formal analysis of adequate flexibility is required for a piping system that
- (a) duplicates, or replaces without significant change, a system operating with a successful service record
- (b) can readily be judged adequate by comparison with previously analyzed systems
- (c) is of uniform size, has no more than two points of fixation, no intermediate restraints, and falls within the limitations of empirical eq. (16)⁸

$$\frac{Dy}{(L-U)^2} \le K_{\rm I} \tag{16}$$

where

D =outside diameter of pipe, mm (in.)

 E_a = reference modulus of elasticity at 21°C (70°F),

 $K_1 = 208\ 000\ S_A/E_a,\ (\text{mm/m})^2$ = 30 $S_A/E_a,\ (\text{in./ft})^2$

⁸ WARNING: No general proof can be offered that this equation will yield accurate or consistently conservative results. It is not applicable to systems used under severe cyclic conditions. It should be used with caution in configurations such as unequal leg U-bends or near-straight "sawtooth" runs, or for large thin-wall pipe ($i \ge 5$), or where extraneous displacements (not in the direction connecting anchor points) constitute a large part of the total displacement. There is no assurance that terminal reactions will be acceptably low, even if a piping system falls within the limitations of eq. (16).

L = developed length of piping between anchors, m

 S_A = allowable displacement stress range in accordance with eq. (1a), MPa (ksi)

U =anchor distance, straight line between anchors, m

y = resultant of total displacement strains, mm (in.),to be absorbed by the piping system

319.4.2 Formal Analysis Requirements

- (a) Any piping system that does not meet the criteria in para. 319.4.1 shall be analyzed by a simplified, approximate, or comprehensive method of analysis, as appropriate.
- (b) A simplified or approximate method may be applied only if used within the range of configurations for which its adequacy has been demonstrated.
- (c) Acceptable comprehensive methods of analysis include analytical and chart methods that provide an evaluation of the forces, moments, and stresses caused by displacement strains (see para. 319.2.1).
- (d) Comprehensive analysis shall take into account stress intensification factors for any component other than straight pipe. Credit may be taken for the extra flexibility of such a component.

319.4.3 Basic Assumptions and Requirements. Standard assumptions specified in para. 319.3 shall be followed in all cases. In calculating the flexibility of a piping system between anchor points, the system shallbe treated as a whole. The significance of all parts of the line and of all restraints introduced for the purpose of reducing moments and forces on equipment or small branch lines, and also the restraint introduced by support friction, shall be recognized. Consider all displacements, as outlined in para. 319.2.1, over the temperature range defined by para. 319.3.1.

319.4.4 Flexibility Stresses (18)

(a) The axial, bending, and torsional displacement stress ranges shall be computed using the reference modulus of elasticity at 21°C (70°F), E_a , except as provided in para. 319.2.2(b)(4), and then combined in accordance with eq. (17) to determine the computed displacement stress range, Se which shall not exceed the allowable displacement stress range, S_A , in para. 302.3.5(d). See also eq. (1d) and Appendix S, Example 3 for the greatest computed displacement stress range.

$$S_E = \sqrt{(|S_a| + S_b)^2 + (2S_t)^2}$$
 (17)

where

 A_p = cross-sectional area of pipe; see para. 319.3.5 \vec{F}_a = axial force range between any two conditions being evaluated

 i_q = axial stress intensification factor. In the absence of more-applicable data, $i_a = 1.0$ for elbows, pipe bends, and miter bends (single, closely spaced, and widely spaced), and $i_a = i_o$ (or i when listed) in Appendix D for other components; see also para. 319.3.6.

 i_t = torsional stress intensification factor. In the absence of more-applicable data, $i_t = 1.0$; also see para. 319.3.6.

 M_t = torsional moment range between any two conditions being evaluated

 S_a = axial stress range due to displacement strains $= i_a F_a / A_p$

 S_b = bending stress range due to displacement strains

 S_t = torsional stress range due to displacement strains

 $= i_t M_t / 2Z$

= $i_t M_t / 2Z$ Z = section modulus of pipe; see para. 319.3.5

(b) The bending stress range, S_b , to be used in eq. (17) for elbows, miter bends, and full size outlet branch connections (Legs 1, 2, and 3) shall be calculated in accordance with eq. (18), with moments as shown in Figures 319.4.4A and 319.4.4B

$$S_b = \frac{\sqrt{(i_i M_i)^2 + (i_o M_o)^2}}{7} \tag{18}$$

 i_i = in-plane stress intensification factor; see para. 319.3.6

 i_0 = out-plane stress intensification factor; see para. 319.3.6

 M_i = in-plane bending moment range between any two conditions being evaluated

 M_o = out-plane bending moment range between any two conditions being evaluated

(c) The bending stress range, S_b , to be used in eq. (17) for reducing outlet branch connections shall be calculated in accordance with eqs. (19) and (20), with moments as shown in Figure 319.4.4B.

For header (Legs 1 and 2)

$$S_b = \frac{\sqrt{(i_i M_i)^2 + (i_o M_o)^2}}{Z}$$
 (19)

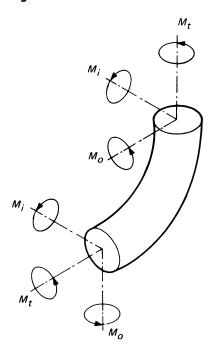
For branch (Leg 3), use eq. (20) when i_i or i_0 is taken from Appendix D; when both i_i and i_o are taken from ASME B31J or determined by experimental or analytical means, e.g., ASME B31J, Nonmandatory Appendix A, use eq. (19)

$$S_b = \frac{\sqrt{(i_i M_i)^2 + (i_o M_o)^2}}{Z_o}$$
 (20)

 r_2 = mean branch cross-sectional radius

 $\overline{T_h}$ = thickness of pipe matching branch

Figure 319.4.4A Moments in Bends



 $\overline{T_h}$ = thickness of pipe matching run of tee or header exclusive of reinforcing elements

 T_S = effective branch wall thickness, lesser of $\overline{T_h}$ and $\overline{\overline{T_h}}$

 Z_e = effective section modulus of branch = $\pi r_2^2 T_S$; see para. 319.3.5

319.5 Reactions

Reaction forces and moments used to design restraints and supports for a piping system, and to evaluate the effects of piping displacement on connected equipment, shall be based on the maximum load from operating conditions, including weight, pressure, and other sustained loads; thermal displacement; and, where applicable, occasional loads. The reactions shall be calculated using the modulus of elasticity at the temperature of the condition, E_m (E_a may be used instead of E_m when it provides a more conservative result). The temperature of the condition may differ in different locations within the piping system.

Where cold spring is used in the piping system, experience has shown that it cannot be fully assured. Therefore, the reactions shall be computed both with the assumption that only two-thirds of the design cold spring is present, and with four-thirds of the design cold spring present.

If it is necessary to determine the reactions at ambient temperature, the designer shall consider loads at that condition, including the design cold spring and self springing of piping. Self springing may occur if the operating stress in the piping system exceeds the yield strength of the material or if the piping operates at temperatures in the creep range of the material.

319.5.1 Maximum Reactions for Simple Systems. For a two-anchor piping system without intermediate restraints, the maximum instantaneous values of reaction forces and moments may be estimated from eqs. (21) and (22).

(a) For Extreme Displacement Conditions, R_m . The temperature for this computation is the maximum or minimum metal temperature defined in para. 319.3.1(b), whichever produces the larger reaction.

$$R_m = R\left(1 - \frac{2C}{3}\right) \frac{E_m}{E_a} \tag{21}$$

where

C = cold-spring factor varying from zero for no cold spring to 1.0 for 100% cold spring. (The factor two-thirds is based on experience showing that specified cold spring cannot be fully assured, even with elaborate precautions.)

 E_a = reference modulus of elasticity at 21°C (70°F)

 E_m = modulus of elasticity at maximum or minimum metal temperature

R range of reaction forces or moments (derived from flexibility analysis) corresponding to the full displacement stress range and based on E_a

 R_m = estimated instantaneous maximum reaction force or moment at maximum or minimum metal temperature

(b) For Original Condition, R_{α} . The temperature for this computation is the expected temperature at which the piping is to be assembled.

 $R_a = CR$ or C_1R , whichever is greater, where nomenclature is as in para. 319.5.1(a) and

$$C_{\rm l} = 1 - \frac{S_h E_a}{S_E E_m} \tag{22}$$

= estimated self-spring or relaxation factor; use zero if value of C_1 is negative

 R_a = estimated instantaneous reaction force or moment at installation temperature

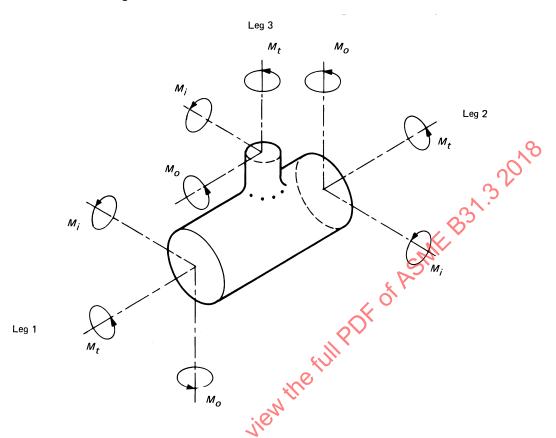
 S_E = computed displacement stress range (see para. 319.4.4)

 S_h = see definition in para. 302.3.5(d)

319.5.2 Maximum Reactions for Complex Systems.

For multianchor piping systems and for two-anchor systems with intermediate restraints, eqs. (21) and (22) are not applicable. Each case must be studied to estimate location, nature, and extent of local overstrain, and its effect on stress distribution and reactions.

Figure 319.4.4B Moments in Branch Connections



319.6 Calculation of Movements

Calculations of displacements and rotations at specific locations may be required where clearance problems are involved. In cases where small-size branch pipes attached to stiffer run pipes are to be calculated separately, the linear and angular movements of the junction point must be calculated or estimated for proper analysis of the branch.

319.7 Means of Increasing Flexibility

The layout of piping often provides inherent flexibility through changes in direction, so that displacements produce chiefly bending and torsional strains within prescribed limits. The amount of axial tension or compression strain (which produces large reactions) usually is small.

Where the piping lacks built-in changes of direction, or where it is unbalanced [see para. 319.2.2(b)], large reactions or detrimental overstrain may be encountered. The designer should consider adding flexibility by one or more of the following means: bends, loops, or offsets; swivel joints; corrugated pipe; expansion joints of the bellows or slip-joint type; or other devices permitting angular, rotational, or axial movement. Suitable anchors, ties, or

other devices shall be provided as necessary to resist end forces produced by fluid pressure, frictional resistance to movement, and other causes. When expansion joints or other similar devices are provided, the stiffness of the joint or device should be considered in any flexibility analysis of the piping.

320 ANALYSIS OF SUSTAINED LOADS

320.1 Basic Assumptions and Requirements

Sustained conditions may be evaluated by detailed analysis, approximate methods, or simplified means such as span tables. When detailed analysis is performed, the stress due to sustained loads, S_L , shall be computed and combined as described in this paragraph and shall not exceed the allowable described in para. 302.3.5(c). See Appendix S, Example 2 for guidance on loading conditions and support scenarios that result in the greatest S_L for each operating condition being considered. The loads due to weight should be based on the nominal thickness of all system components unless otherwise justified in a more rigorous analysis. Section moduli used to compute the stresses in this paragraph shall be based on nominal pipe dimensions less allowances, i.e., the sum of mechanical (thread or groove depth), internal

and external corrosion, and erosion allowances. Areas used to compute the stresses in this paragraph assume nominal pipe dimensions less allowances affecting the inside diameter of the pipe, i.e., the sum of mechanical and internal corrosion and erosion allowances. It is the responsibility of the designer to determine sustained stress indices, I_a , I_b , I_o , and I_b when a piping component is not explicitly addressed in Appendix D, e.g., base-ells, reducing elbows, crosses, close proximity findings, etc., as well as elbows, pipe bends, or miters other than 90 deg or supported by a trunnion. Sustained stress indices shall not be lower than 1.00.

(18) 320.2 Stress Due to Sustained Loads

The equation for the stress due to sustained loads, such as pressure and weight, S_L , is provided in eq. (23a). Equations for the stress due to sustained bending moments, S_b , are presented in eqs. (23b1) and (23b2).

$$S_L = \sqrt{(|S_a| + S_b)^2 + (2S_t)^2}$$
 (23a)

$$S_b = \frac{\sqrt{(I_i M_i)^2 + (I_o M_o)^2}}{Z}$$
 (23b1)

For branch (Leg 3 in Figure 319.4.4B), use eq. (23b2) only when I_i or I_o is based upon i, i_i , or i_o taken from Appendix D; when both I_i and I_o are taken from ASME B31J or determined by experimental or analytical means, e.g., ASME B31J, Nonmandatory Appendix D, use eq. (23b1).

$$S_b = \frac{\sqrt{(I_i M_i)^2 + (I_o M_o)^2}}{Z_e}$$
 (23b2)

where

 I_i = sustained in-plane moment index. In the absence of more-applicable data, I_i is taken as the greater of $0.75i_i$ or 1.00.

of $0.75i_i$ or 1.00. I_o = sustained out-plane moment index. In the absence of more-applicable data, I_o is taken as the greater of $0.75i_o$ or 1.00.

 M_i = in-plane moment due to sustained loads, e.g., pressure and weight

 M_o = out-plane moment due to sustained loads, e.g., pressure and weight

Z = sustained section modulus. Z in eqs. (23b1) and (23c) is described in para. 319.4.4 but is computed in this paragraph using nominal pipe dimensions less allowances; see para. 320.1.

 Z_e = sustained effective section modulus. Z_e in eq. (23b2) is described in para. 319.4.4, using i_i from Appendix D in T_s calculation, but Z_e is computed in this paragraph using nominal pipe dimensions less allowances; see para. 320.1.

The equation for the stress due to sustained torsional moment, S_b is

$$S_t = \frac{I_t M_t}{2Z} \tag{23c}$$

where

 I_t = sustained torsional moment index. In the absence of more-applicable data, I_t is taken as 1.00.

 M_t = torsional moment due to sustained loads, e.g., pressure and weight

The equation for the stress due to sustained longitudinal force, S_{av} is

$$S_a = \frac{I_a F_a}{A_p} \tag{23d}$$

where

 A_p = cross-sectional area of the pipe, considering nominal pipe dimensions less allowances; see para. 320.1

 F_a = longitudinal force due to sustained loads, e.g., pressure and weight

 I_a = sustained longitudinal force index. In the absence of more-applicable data, I_a is taken as 1.00.

The sustained longitudinal force, F_a , includes the sustained force due to pressure, which is P_jA_f unless the piping system includes an expansion joint that is not designed to carry this force itself, where P_j is the internal operating pressure for the condition being considered, $A_f = \pi d^2/4$, and d is the pipe inside diameter considering pipe wall thickness less applicable allowances; see para. 320.1. For piping systems that contain expansion joints, it is the responsibility of the designer to determine the sustained longitudinal force due to pressure in the piping system.

321 PIPING SUPPORT

321.1 General

The design of support structures (not covered by this Code) and of supporting elements (see definitions of piping and pipe supporting elements in para. 300.2) shall be based on all concurrently acting loads transmitted into such supports. These loads, defined in para. 301, include weight effects, loads introduced by service pressures and temperatures, vibration, wind, earthquake, shock, and displacement strain (see para. 319.2.2).

For piping containing gas or vapor, weight calculations need not include the weight of liquid if the designer has taken specific precautions against entrance of liquid into the piping, and if the piping is not to be subjected to hydrostatic testing at initial construction or subsequent inspections

321.1.1 Objectives. The layout and design of piping and its supporting elements shall be directed toward preventing the following:

- (a) piping stresses in excess of those permitted in this Code
 - (b) leakage at joints
- (c) excessive thrusts and moments on connected equipment (such as pumps and turbines)
- (d) excessive stresses in the supporting (or restraining) elements
- (e) resonance with imposed or fluid-induced vibrations
- (f) excessive interference with thermal expansion and contraction in piping which is otherwise adequately flexible
- (g) unintentional disengagement of piping from its supports
- (h) excessive piping sag in piping requiring drainage slope
- (i) excessive distortion or sag of piping (e.g., thermoplastics) subject to creep under conditions of repeated thermal cycling
- (j) excessive heat flow, exposing supporting elements to temperature extremes outside their design limits
- **321.1.2 Analysis.** In general, the location and design of pipe supporting elements may be based on simple calculations and engineering judgment. However, when a more refined analysis is required and a piping analysis, which may include support stiffness, is made, the stresses, moments, and reactions determined thereby shall be used in the design of supporting elements.
- **321.1.3 Stresses for Pipe Supporting Elements.** Allow able stresses for materials used for pipe supporting elements, except springs, shall be in accordance with para. 302.3.1. Longitudinal weld joint factors, E_j , however, need not be applied to the allowable stresses for welded piping components that are to be used for pipe supporting elements.

321.1.4 Materials

- (a) Permanent supports and restraints shall be of material suitable for the service conditions. If steel is cold-formed to a centerline radius less than twice its thickness, it shall be annealed or normalized after forming.
- (b) Gray, ductile, and malleable iron may be used for rollers, roller bases, anchor bases, and other supporting elements subject chiefly to compressive loading. Gray iron is not recommended if the piping may be subject to impact-type loading resulting from pulsation or vibration. Ductile and malleable iron may be used for pipe and beam clamps, hanger flanges, clips, brackets, and swivel rings.
- (c) Steel of an unknown specification may be used for pipe supporting elements that are not welded directly to pressure-containing piping components. (Compatible intermediate materials of known specification may be welded directly to such components.) Basic allowable stress in tension or compression shall not exceed 82 MPa (12 ksi) and the support temperature shall be

- within the range of -29°C to 343°C (-20°F to 650°F). For stress values in shear and bearing, see para. 302.3.1(b).
- (d) Wood or other materials may be used for pipe supporting elements, provided the supporting element is properly designed, considering temperature, strength, and durability.
- (e) Attachments welded or bonded to the piping shall be of a material compatible with the piping and service. For other requirements, see para. 321.3.2.
- **321.1.5 Threads.** Screw threads shall conform to ASME B1.1 unless other threads are required for adjustment under heavy loads. Turnbuckles and adjusting nuts shall have the full length of internal threads engaged. Any threaded adjustment shall be provided with a locknut, unless locked by other means.

321.2 Fixtures

321.2.1 Anchors and Guides

- (a) A supporting element used as an anchor shall be designed to maintain an essentially fixed position.
- (b) To protect terminal equipment or other (weaker) portions of the system, restraints (such as anchors and guides) shall be provided where necessary to control movement or to direct expansion into those portions of the system that are designed to absorb them. The design, arrangement, and location of restraints shall ensure that expansion joint movements occur in the directions for which the joint is designed. In addition to the other thermal forces and moments, the effects of friction in other supports of the system shall be considered in the design of such anchors and guides.
- (c) Piping layout, anchors, restraints, guides, and supports for all types of expansion joints shall be designed in accordance with para. X301.2 of Appendix X.

321.2.2 Inextensible Supports Other Than Anchors and Guides⁹

- (a) Supporting elements shall be designed to permit the free movement of piping caused by thermal expansion and contraction.
- (b) Hangers include pipe and beam clamps, clips, brackets, rods, straps, chains, and other devices. They shall be proportioned for all required loads. Safe loads for threaded parts shall be based on the root area of the threads.
- (c) Sliding Supports. Sliding supports (or shoes) and brackets shall be designed to resist the forces due to friction in addition to the loads imposed by bearing. The dimensions of the support shall provide for the expected movement of the supported piping.

⁹ Various types of inextensible (solid) and resilient supports are illustrated in MSS SP-58.

321.2.3 Resilient Supports⁹

- (a) Spring supports shall be designed to exert a supporting force, at the point of attachment to the pipe, equal to the load as determined by weight balance calculations. They shall be provided with means to prevent misalignment, buckling, or eccentric loading of the springs, and to prevent unintentional disengagement of the load.
- (b) Constant-support spring hangers provide a substantially uniform supporting force throughout the range of travel. The use of this type of spring hanger is advantageous at locations subject to appreciable movement with thermal changes. Hangers of this type should be selected so that their travel range exceeds expected movements.
- (c) Means shall be provided to prevent overstressing spring hangers due to excessive deflections. It is recommended that all spring hangers be provided with position indicators.
- **321.2.4 Counterweight Supports.** Counterweights shall be provided with stops to limit travel. Weights shall be positively secured. Chains, cables, hangers, rocker arms, or other devices used to attach the counterweight load to the piping shall be subject to the requirements of para. 321.2.2.
- **321.2.5 Hydraulic Supports.** An arrangement utilizing a hydraulic cylinder may be used to give a constant supporting force. Safety devices and stops shall be provided to support the load in case of hydraulic failure.

321.3 Structural Attachments

External and internal attachments to piping shall be designed so that they will not cause undue flattening of the pipe, excessive localized bending stresses, or harmful thermal gradients in the pipe wall. It is important that attachments be designed to minimize stress concentration, particularly in cyclic services.

- **321.3.1 Nonintegral Attachments.** Nonintegral attachments, in which the reaction between the piping and the attachment is by contact, include clamps, slings, cradles, Ubolts, saddles, straps, and clevises. If the weight of a vertical pipe is supported by a clamp, it is recommended to prevent slippage that the clamp be located below a flange, fitting, or support lugs welded to the pipe.
- (18) **321.3.2 Integral Attachments.** Integral attachments include plugs, ears, shoes, plates, trunnions, stanchions, structural shapes, and angle clips, cast on or welded to the piping. The material for integral attachments attached by welding shall be of good weldable quality. [See para. 321.1.4(e) for material requirements.] Preheating, welding, and heat treatment requirements shall be in accordance with Chapter V. Consideration shall be given to the localized stresses induced in the piping

component by welding the integral attachment, as well as differential thermal displacement strains between the attachment and the component to which it is attached. Welds shall be proportioned so that the shear stresses meet the requirements of para. 302.3.1(b). If the allowed stress values differ between the piping component and the attachment material, the lower of the two values shall be used. Where postweld heat treatment of the piping is required by para. 331, welds for structural attachments made directly to pressure-containing materials shall be postweld heat treated. Welds for structural attachments not made directly to pressure-containing materials do not require postweld heat treatment.

- (a) Integral reinforcement, complete encirclement reinforcement, or intermediate pads of suitable alloy and design may be used to reduce contamination or undesirable heat effects in alloy piping.
- (b) Intermediate pads, integral reinforcement, complete encirclement reinforcement, or other means of reinforcement may be used to distribute stresses.

The design of pipe-supporting elements and the local effects on the piping component are the responsibility of the designer. Nonmandatory guidance on the design of supports and attachments may be found as referenced in ASME BPVC, Section VIII, Division 1, Nonmandatory Appendix G, G-9. The designer is cautioned that not all the listed standards and bulletins in G-9 are well suited for use on branch-diameter-to-run-diameter and run-diameter-to-run-thickness ratios typical for pipe support component analyses (e.g., Appendix A of WRC Bulletin 537¹⁰ lists the limitations to WRC Bulletin 537).

321.4 Structural Connections

The load from piping and pipe supporting elements (including restraints and braces) shall be suitably transmitted to a pressure vessel, building, platform, support structure, foundation, or to other piping capable of bearing the load without deleterious effects. See Appendix F, para. F321.4.

PART 6 SYSTEMS

322 SPECIFIC PIPING SYSTEMS

322.3 Instrument Piping

322.3.1 Definition. Instrument piping within the scope of this Code includes all piping and piping components used to connect instruments to other piping or equipment, and control piping used to connect air or hydraulically operated control apparatus. It does not include

¹⁰ WRC (Welding Research Council) 537-2010, "Precision Equations and Enhanced Diagrams for Local Stresses in Spherical and Cylindrical Shells Due to External Loadings for Implementation of WRC Bulletin 107."

instruments, or permanently sealed fluid-filled tubing systems furnished with instruments as temperature or pressure responsive devices.

- **322.3.2 Requirements.** Instrument piping shall meet the applicable requirements of the Code and the following:
- (a) The design pressure and temperature for instrument piping shall be determined in accordance with para. 301. If more severe conditions are experienced during blowdown of the piping, they may be treated as occasional variations in accordance with para. 302.2.4.
- (b) Consideration shall be given to the mechanical strength (including fatigue) of small instrument connections to piping or apparatus (see para. 304.3.5).
- (c) Instrument piping containing fluids that are normally static and subject to freezing shall be protected by heat tracing or other heating methods, and insulation.
- (d) If it will be necessary to blow down (or bleed) instrument piping containing toxic or flammable fluids, consideration shall be given to safe disposal.

322.6 Pressure-Relieving Systems

Pressure-relieving systems within the scope of this Code shall conform to the following requirements. See also Appendix F, para. F322.6.

- **322.6.1 Stop Valves in Pressure Relief Piping.** If one or more stop valves are installed between the piping being protected and its protective device or devices, or between the protective device or devices and the point of discharge, they shall meet the requirements of (a) and either (b) of (c), below.
- (a) A full-area stop valve may be installed on the inlet side of a pressure-relieving device. A full area stop valve may be placed on the discharge side of a pressure-relieving device when its discharge is connected to a common header with other discharge lines from other pressure-relieving devices. Stop valves of less than full area may be used on both the inlet side and discharge side of pressure-relieving devices as outlined herein if the stop valves are of such type and size that the increase in pressure drop will not reduce the relieving capacity below that required, nor adversely affect the proper operation of the pressure-relieving device.
- (b) Stop valves to be used in pressure relief piping shall be so constructed or positively controlled that the closing of the maximum number of block valves possible at one

time will not reduce the pressure-relieving capacity provided by the unaffected relieving devices below the required relieving capacity.

(c) As an alternative to (b) above, stop valves shall be so constructed and arranged that they can be locked or sealed in either the open or closed position. See Appendix F, para. F322.6.

322.6.2 Pressure Relief Discharge Piping. Discharge lines from pressure-relieving safety devices shall be designed to facilitate drainage. When discharging directly to the atmosphere, discharge shall not impinge on other piping or equipment and shall be directed away from platforms and other areas used by personnel. Reactions on the piping system due to actuation of safety relief devices shall be considered, and adequate strength shall be provided to withstand these reactions.

322.6.3 Pressure-Relieving Devices

- (a) Pressure-relieving devices required by para. 301.2.2(a) shall be in accordance with ASME BPVC, Section VIII, Division 1, UG-125(c), UG-126, UG-127, and UG-132 through UG-136, excluding UG-135(e) and UG-136(c). The terms design pressure and piping system shall be substituted for maximum allowable working pressure and vessel, respectively, in these paragraphs. The required relieving capacity of any pressure-relieving device shall include consideration of all piping systems that it protects.
- (b) Relief set pressure¹² shall be in accordance with Section VIII, Division 1, with the exceptions stated in alternatives (1) and (2), below.
- (1) With the owner's approval, the set pressure may exceed the limits in Section VIII, Division 1, provided that the limit on maximum relieving pressure stated in (c) below will not be exceeded.
- (2) For a liquid thermal expansion relief device that protects only a blocked-in portion of a piping system, the set pressure shall not exceed the lesser of the system test pressure or 120% of design pressure.
- (c) The maximum relieving pressure¹³ shall be in accordance with Section VIII, Division 1, with the exception that the allowances in para. 302.2.4(f) are permitted, provided that all other requirements of para. 302.2.4 are also met.

¹¹The *design pressure* for pressure relief is the maximum design pressure permitted, considering all components in the piping system.

¹² Set pressure is the pressure at which the device begins to relieve, e.g., lift pressure of a spring-actuated relief valve, bursting pressure of a rupture disk, or breaking pressure of a breaking pin device.

¹³ Maximum relieving pressure is the maximum system pressure during a pressure-relieving event.

Chapter III Materials

323 GENERAL REQUIREMENTS

Chapter III states limitations and required qualifications for materials based on their inherent properties. Their use in piping is also subject to requirements and limitations in other parts of this Code [see para. 300(d)]. See also para. 321.1.4 for support materials, and Appendix F, para. F323, for precautionary considerations.

323.1 Materials and Specifications

- **323.1.1 Listed Materials.** Any material used in pressure-containing piping components shall conform to a listed specification except as provided in para. 323.1.2.
- **323.1.2 Unlisted Materials.** Unlisted materials may be used provided they conform to a published specification covering chemistry, physical and mechanical properties, method and process of manufacture, heat treatment, and quality control, and otherwise meet the requirements of this Code. See also ASME BPVC, Section II, Part D, Appendix 5. Allowable stresses shall be determined in accordance with the applicable allowable stress basis of this Code or more conservative basis.
- **323.1.3 Unknown Materials.** Materials of unknown specification shall not be used for pressure containing piping components.
- **323.1.4 Reclaimed Materials.** Reclaimed pipe and other piping components may be used, provided they are properly identified as conforming to a listed or published specification (para 323.1.1 or 323.1.2) and otherwise meet the requirements of this Code. Sufficient cleaning and inspection shall be made to determine minimum wall thickness and freedom from imperfections that would be unacceptable in the intended service.

323.2 Temperature Limitations

The designer shall verify that materials that meet other requirements of the Code are suitable for service throughout the operating temperature range.

323.2.1 Upper Temperature Limits, Listed Materials. A listed material may be used at a temperature above the maximum for which a stress value or rating is shown, only

- (a) there is no prohibition in Appendix A or elsewhere in the Code
- (b) the designer verifies the serviceability of the material in accordance with para. 323.2.4

323.2.2 Lower Temperature Limits, Listed Materials. (18) Listed materials shall be tested as described in Table 323.2.2 except as exempted by (d) through (j). See Appendix F, para. F323.2.2.

- (a) The allowable stress or component rating at any temperature colder than the minimum shown in Table A-1, Table A-1M, or Figure 323.2.2A shall not exceed the stress value or rating at the minimum temperature in Table A-1, Table A-1M, or the component standard.
- (b) The stress ratio is used in Figure 323.2.2B to determine the allowable reduction in the impact test exemption temperature. The stress ratio is defined as the maximum of the following:
- (1) circumferential pressure stress for the condition under consideration (based on minimum pipe wall thickness less allowances) divided by the basic allowable stress at the condition under consideration.
- (2) for piping components with pressure ratings, the pressure for the condition under consideration divided by the pressure rating at the condition under consideration.
- (3) combined stress due to pressure, dead loads, live loads, and displacement strain for the condition under consideration divided by the basic allowable stress at the condition under consideration. In calculating this combined stress, the forces and moments in the piping system for these combined sustained loads and displacement strains shall be calculated using nominal dimensions, and the stresses shall be calculated using eqs. (23a) through (23d) with all of the stress indices taken as 1.0 ($I_a = I_i I_o = I_t = 1.0$) and using section properties based on the nominal dimensions less corrosion, erosion, and mechanical allowances. Also see Appendix F, para. F323.2.2.
- (c) Minimum impact test exemption temperature reduction may be used only when all of the following apply:
- (1) The piping is not in Elevated Temperature Fluid Service.
- (2) Local stresses caused by shock loading, thermal bowing, and differential expansion between dissimilar metals (e.g., austenitic welded to ferritic) are less than 10% of the basic allowable stresses at the condition under consideration.
- (3) The piping is safeguarded from maintenance loads, e.g., using a valve wheel wrench on a small bore valve.
- (d) Impact testing of the base metal is not required if the design minimum temperature is warmer than or equal to the temperature listed in the Min. Temp. column of

Table 323.2.2 Requirements for Low Temperature Toughness Tests for Metals

These Toughness Test Requirements Are in Addition to Tests Required by the Material Specification

	-		•	-
Listed Materials	Type of Material 1 Gray iron 2 Malleable and ductile iron; carbon steel in accordance with	Design Minimum Tempera Tem Table A-1, Table A-1M, or Para A-1 No additional requirem A-2 No additional requirem	Column B Design Minimum Temperature Colder Than Minimum Temperature in Table A-1, Table A-1M, or Figure 323.2.2A or as Described in Para. 323.2.2(h) B-1 No additional requirements B-2 Materials designated in Box 2 shall not be used.	
	Note (1)	(a) Base Metal	(b) Weld Metal and Heat Affected Zone (HAZ) [Note (2)]	3
	3 Other carbon steels; low and intermediate alloy steels; and ferritic, martensitic, and duplex stainless steels	A-3 (a) No additional requirements	A-3 (b) Weld metal deposits shall be impact tested in accordance with para. 323.3 if design minimum temperature <-29°C (-20°F), except as provided in Notes (3) and (4), and except as follows: for materials listed for Curves C and D of Figure 323.2.2A, where corresponding welding consumables are qualified by impact testing at the design minimum temperature or lower in accordance with the applicable AWS specification, additional testing is not required.	B-3 Except as provided in Notes (3) and (4), heat treat base metal in accordance with applicable ASTM specification listed in para. 323.3.2; then impact test base metal, weld deposits, and HAZ in accordance with para. 323.3 [see Note (2)]. When materials are used at temperature below the assigned curve as permitted by Notes (2) and (3) of Figure 323.2.2A, weld deposits and HAZ shall be impact tested [see Note (2)].
	4 Austenitic stainless steels	A-4 (a) If (1) carbon content by analysis >0.1% or (2) material is not in solution heat treated condition, then impact test in accordance with para. 323.3 for design minimum temperature <-29°C (-20°F) except as provided in Notes (5) and (6)	A-4 (b) Weld metal deposits shall be impact tested in accordance with para. 323.3 if design minimum temperature <-29°C (-20°F) except as provided in para. 323.2.2 and in Notes (5) and (6)	B-4 Base metal and weld metal deposits shall be impact tested in accordance with para. 323.3. See Notes (2), (5), and (6).
	5 Austenitic ductile iron, ASTM A571	A-5 (a) No additional requirements	A-5 (b) Welding is not permitted	B-5 Base metal shall be impact tested in accordance with para. 323.3. Do not use <-196°C (-320°F). Welding is not permitted.
	6 Aluminum, copper, nickel, and their alloys; unalloyed titanium	A-6 (a) No additional requirements	A-6 (b) No additional requirements unless filler metal composition is outside the range for base metal composition; then test in accordance with item B-6	B-6 Designer shall be assured by suitable tests [see Note (7)] that base metal, weld deposits, and HAZ are suitable at the design minimum temperature
Unlisted Materials	comparable to those of a		cification. Where composition, heat ts for the corresponding listed mate able section of column B.	

NOTES:

(18)

- (1) Carbon steels conforming to the following are subject to the limitations in Box B-2: plates in accordance with ASTM A36, A283, and A1011; pipe in accordance with ASTM A134 when made from these plates; structural shapes in accordance with ASTM A992; and pipe in accordance with ASTM A53 Type F and API 5L Gr. A25 butt weld.
- (2) Impact tests that meet the requirements of Table 323.3.1, which are performed as part of the weld procedure qualification, will satisfy all requirements of para. 323.2.2, and need not be repeated for production welds.
- (3) See paras. 323.2.2(g) through (i).
- (4) Impact tests are not required when the maximum obtainable Charpy specimen has a width along the notch of less than 2.5 mm (0.098 in.). Under these conditions, and where the stress ratio defined in para. 323.2.2(b) is greater than 0.3, the design minimum temperature shall not be colder than the lower of -48°C (-55°F) or the minimum temperature for the material in Table A-1 or Table A-1M. See also para. 323.2.2(g).
- (5) Impact tests are not required when the maximum obtainable Charpy specimen has a width along the notch of less than 2.5 mm (0.098 in.).

Table 323.2.2 Requirements for Low Temperature Toughness Tests for Metals (Cont'd)

NOTES: (Cont'd)

- (6) For austenitic stainless steels, impact testing is not required if the design minimum temperature is warmer than or equal to −104°C (−155°F), and the stress ratio as defined in para. 323.2.2(b) is 0.3 or less. See also para. 323.2.2(g).
- (7) Tests may include tensile elongation, sharp-notch tensile strength (to be compared with unnotched tensile strength), or other tests, conducted at or colder than design minimum temperature. See also para. 323.3.4.

Table A-1, or Table A-1M, except as provided in Table 323.2.2, Box A-4(a) for austenitic stainless steel base material. In some cases, welds will require either impact testing or testing as described in Table 323.2.2, Box B-6 even when the base metal is not required to be tested. See (f) for steels or Table 323.2.2, Box A-6 (b) for other materials.

- (e) For carbon steels with a letter designation in the Min. Temp. column of Table A-1 or Table A-1M, the minimum temperature is defined by the applicable curve and Notes in Figure 323.2.2A. If a design minimum temperature–thickness combination is on or above the curve, impact testing exemption requirements described in (d) apply.
- (f) For steel materials, impact testing of welds, including those made in manufacturing (e.g., for seam welded pipe and welded tees), is required if either base material is required to be impact tested or if the design minimum temperature is colder than -29°C (-20°F), except for manufacturing welds in austenitic stainless steel base materials having a carbon content not exceeding 0.10% and supplied in the solution heat treated condition or as provided in Table 323.2.2, Boxes A-3(b) and A-4(b). For impact testing of production welds, see Table 323.2.2, Note (2).
- (g) For steels, impact testing is not required for material (including welds) if the stress ratio as defined in (b) is 0.3 or less, the design minimum temperature is warmer than or equal to -104°C (-155°F), and when (c) applies.
- (h) For carbon, low alloy, and intermediate alloy steel materials (including welds) that have not been qualified by impact testing, the minimum temperature from Table A-1, Table A-1M, or Figure 323.2.2A may be reduced to a temperature no colder than -48°C (-55°F) by the temperature reduction provided in Figure 323.2.2B when (c) applies. For carbon, low alloy, and intermediate alloy steel welds that require impact testing in accordance with Table 323.2.2, Box A-3(b), the temperature reduction from Figure 323.2.2B shall be applied to -29°C (-20°F).
- (i) For carbon, low alloy, and intermediate alloy steel materials (including welds) that have been qualified by impact testing, the permitted design minimum temperature may be reduced to a temperature no colder than -104°C (-155°F) by the temperature reduction from Figure 323.2.2B when (c) applies.

- (j) Impact testing is not required for the following combinations of weld metals and design minimum temperatures:
- (1) for austenitic stainless steel base materials having a carbon content not exceeding 0.10%, welded without filler metal, at design minimum temperatures of -104°C (-155°F) and warmer
 - (2) for austenitic weld metal
- (-a) having a carbon content not exceeding 0.10%, and produced with filler metals conforming to AWS A5.4, A5.9, A5.11, A5.14, or A5.22¹ at design minimum temperatures of -104°C (-155°F) and warmer, or
- (-b) having a carbon content exceeding 0.10%, and produced with filler metals conforming to AWS A5.4, A5.9, A5.11, A5.14, or A5.22¹ at design minimum temperatures of -48°C (-55°F) and warmer
- 323.2.3 Temperature Limits, Unlisted Materials. An unlisted material, acceptable under para. 323.1.2, shall be qualified for service at all temperatures within a stated range, from design minimum temperature to design maximum temperature, in accordance with para. 323.2.4.

323.2.4 Verification of Serviceability

- (a) When an unlisted material is to be used, or when a listed material is to be used above the highest temperature for which stress values appear in Appendix A, the designer is responsible for demonstrating the validity of the allowable stresses and other limits used in design and of the approach taken in using the material, including the derivation of stress data and the establishment of temperature limits.
- (b) Data for the development of design limits shall be obtained from a sound scientific program carried out in accordance with recognized technology for both the

 $^{^{1}\,\}mbox{Titles}$ of referenced AWS standards are as follows:

 $AWS\ A5.4/A5.4M, Specification\ for\ Stainless\ Steel\ Electrodes\ for\ Shielded\ Metal\ Arc\ Welding$

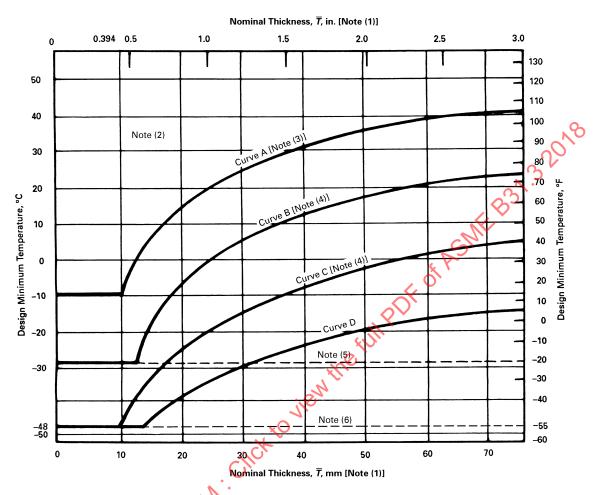
 $AWS\,A5.9/A5.9M, Welding\,Consumables-Wire\,Electrodes, Strip\,Electrodes,\,Wires,\,and\,Rods\,for\,Arc\,Welding\,of\,Stainless\,and\,Heat\,Resisting\,Steels-Classification$

 $A5.11/A5.11M, Specification for Nickel and Nickel-Alloy Welding \\ Electrodes for Shielded Metal Arc Welding$

A5.14/A5.14M, Specification for Nickel and Nickel-Alloy Bare Welding Electrodes and Rods

A5.22/A5.22M, Specification for Stainless Steel Flux Cored and Metal Cored Welding Electrodes and Rods

Figure 323.2.2A Minimum Temperatures Without Impact Testing for Carbon Steel Materials (See Table A-1 or Table A-1M for Designated Curve for a Listed Material; see Table 323.2.2A for Tabular Values)



(18)

- (1) For blind flanges and blanks made from materials with a letter designation in the Min. Temp. column of Table A-1 or Table A-1M, T shall be \frac{1}{4} of the total thickness, where the total thickness is the thickness of the blind flange or blank including the thickness of the facing(s), if applicable.
- (2) Any carbon steel material may be used to a minimum temperature of -29°C (-20°F) for Category D Fluid Service.
- (3) X Grades of API 5L, and ASTM A381 materials, may be used in accordance with Curve B if normalized or quenched and tempered.
- (4) The following materials may be used in accordance with Curve D if normalized:
 - (a) ASTM A516 plate, all grades
 - (b) ASTM A671 pipe made from A516 plate, all grades
 - (c) ASTM A672 pipe made from A516 plate, all grades
- (5) A welding procedure for the manufacture of pipe or components shall include impact testing of welds and HAZ for any design minimum temperature below -29°C (-20°F), except as provided in Table 323.2.2, A-3(b).
- (6) Impact testing in accordance with para. 323.3 is required for any design minimum temperature below –48°C (–55°F), except as permitted by Note (3) in Table 323.2.2.

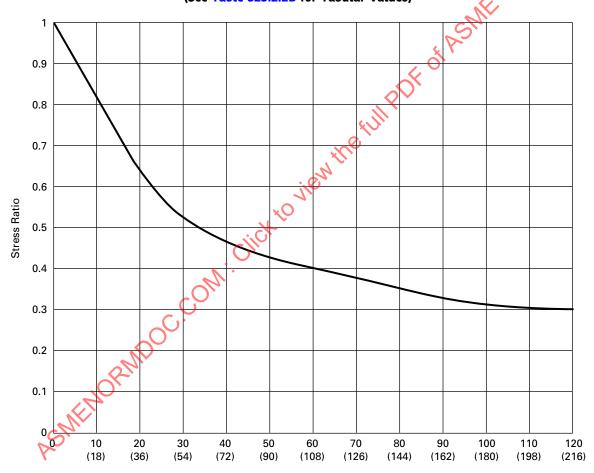
(18) Table 323.2.2A Tabular Values for Minimum Temperatures Without Impact Testing for Carbon Steel Materials (See Figure 323.2.2A for Curves)

Nominal Thickness,				Low	vest Exempti	ion Temperatı	ıre		
T [Note (1)]		Curv		Curv		Curv			
		[Note (2)]		[Note (3)]		[Note (3)]		Curve D	
mm	in.	°C	°F	°C	°F	°C	°F	°C	°F
6.4	0.25	-9.4	15	-28.9	-20	-48.3	-55	-48.3	-55
7.9	0.3125	-9.4	15	-28.9	-20	-48.3	-55	-48.3	-55
9.5	0.375	-9.4	15	-28.9	-20	-48.3	-55	-48.3	-55
10.0	0.394	-9.4	15	-28.9	-20	-48.3	-55	-48.3 C	-55
11.1	0.4375	-6.7	20	-28.9	-20	-41.7	-43	-48.3	-55
12.7	0.5	-1.1	30	-28.9	-20	-37.8	-36	-48.3	-55
14.3	0.5625	2.8	37	-21.7	-7	-35.0	-31	-4 5.6	-50
15.9	0.625	6.1	43	-16.7	2	-32.2	-26	-43.9	-47
17.5	0.6875	8.9	48	-12.8	9	-29.4	-21	-41.7	-43
19.1	0.75	11.7	53	-9.4	15	-27.2	-17	-40.0	-40
20.6	0.8125	14.4	58	-6.7	20	-25.0	-13	-38.3	-37
22.2	0.875	16.7	62	-3.9	25	-23.3	6 -10	-36.7	-34
23.8	0.9375	18.3	65	-1.7	29	-21.7	-7	-35.6	-32
25.4	1.0	20.0	68	0.6	33	-19.4	-3	-34.4	-30
27.0	1.0625	22.2	72	2.2	36	18.3	-1	-33.3	-28
28.6	1.125	23.9	75	3.9	39	16.7	2	-32.2	-26
30.2	1.1875	25.0	77	5.6	42	-15.6	4	-30.6	-23
31.8	1.25	26.7	80	6.7	44	-14.4	6	-29.4	-21
					Q _t				
33.3	1.3125	27.8	82	7.8	46	-13.3	8	-28.3	-19
34.9	1.375	28.9	84	8.9 9.4	48	-12.2	10	-27.8	-18
36.5 38.1	1.4375 1.5	30.0 31.1	86 88	10.6	49 51	-11.1 -10.0	12 14	-26.7 -25.6	-16 -14
				7					
39.7	1.5625	32.2	90	11.7	53	-8.9	16	-25.0	-13
41.3	1.625	33.3	92	12.8	55	-8.3	17	-23.9	-11
42.9	1.6875	33.9	93	13.9	57	-7.2	19	-23.3	-10
44.5	1.75	34.4	94	14.4	58	-6.7	20	-22.2	-8
46.0	1.8125	35.6	96	15.0	59	-5.6	22	-21.7	-7
47.6	1.875	36.1	97	16.1	61	-5.0	23	-21.1	-6
49.2	1.9375	36.7	98	16.7	62	-4.4	24	-20.6	-5
50.8	2.0	37.2	99	17.2	63	-3.3	26	-20.0	-4
52.4	2.0625	37,8	100	17.8	64	-2.8	27	-19.4	-3
54.0	2.125	38.3	101	18.3	65	-2.2	28	-18.9	-2
55.6	2.1875	38.9	102	18.9	66	-1.7	29	-18.3	-1
57.2	2.25	38.9	102	19.4	67	-1.1	30	-17.8	0
58.7	2.3125	39.4	103	20.0	68	-0.6	31	-17.2	1
60.3	2,375	40.0	104	20.6	69	0.0	32	-16.7	2
61.9	2.4375	40.6	105	21.1	70	0.6	33	-16.1	3
63.5	2.4373	40.6	105	21.7	70	1.1	34	-10.1 -15.6	4
65.1	2.5625	41.1	105	21.7	71	1.7	35	-15.0	5
66.7	2.625	41.7	107	22.8	73	2.2	36	-13.0 -14.4	6
68.3	2.6875	41.7	107	22.8	73 74	2.8	37	-13.9	7
69.9	2.75	42.2	108	23.3	74 75	3.3 3.9	38	-13.3	8
71.4	2.8125	42.2	108	23.9	75 76		39 40	-13.3 -12.8	9
73.0 74.6	2.875	42.8	109	24.4		4.4		-12.8 -12.2	
74.6 76.2	2.9375 3.0	42.8 43.3	109 110	25.0 25.0	77 77	4.4 5.0	40 41	-12.2 -11.7	10 11

Table 323.2.2A Tabular Values for Minimum Temperatures Without Impact Testing for Carbon Steel Materials (See Figure 323.2.2A for Curves) (Cont'd)

- (1) For blind flanges and blanks made from materials with a letter designation in the Min. Temp. column of Table A-1 or Table A-1M, \overline{T} shall be $\frac{1}{4}$ of the total thickness, where the total thickness is the thickness of the blind flange or blank including the thickness of the facing(s), if applicable.
- (2) X Grades of API 5L, and ASTM A381 materials, may be used in accordance with Curve B if normalized or quenched and tempered.
- (3) The following materials may be used in accordance with Curve D if normalized:
 - (a) ASTM A516 plate, all grades
 - (b) ASTM A671 pipe made from A516 plate, all grades
 - (c) ASTM A672 pipe made from A516 plate, all grades

(18) Figure 323.2.2B Reduction in Lowest Exemption Temperature for Steels Without Impact Testing (See Table 323.2.2B for Tabular Values)



Temperature Reduction, °C (°F)

GENERAL NOTE: See para. 323.2.2(b) to determine stress ratio.

Table 323.2.2B Tabular Values for Reduction in Lowest Exemption Temperature for Steels Without Impact Testing (See Figure 323.2.2B for Curve and Applicable Notes)

	Reduction in Exemption Temperature			Reduction in Exemption Temperature		
Stress Ratio	°C	°F	Stress Ratio	°C	°F	
1.00	0	0	0.64	20	36	
0.99	1	1	0.63	21	37	
0.98	1	2	0.62	21	38	
0.97	2	3	0.61	22	40	
0.96	2	4	0.60	23	41	
0.95	3	5	0.59	23	% 42	
0.94	3	6	0.58	24	30 44 46	
0.93	4	7	0.57	26	46	
0.92	4	8	0.56	26	47	
0.91	5	9	0.55	27	49	
0.90	6	10	0.54	28	51	
0.89	6	11	0.53	27 28 29	53	
0.88	7	12	0.52	31	56	
0.87	7	13	0.51	33	59	
0.86	8	14	0.50	34	61	
0.85	8	15	0.49	36	65	
0.84	9	16	0.48	38	68	
0.83	9	17	0.47	40	72	
			1			
0.82	10	18	0.46	42	76	
0.81	11	19	0.45	44	80	
0.80	11	20	0.44	47	85	
0.79	12	·· CAT	0.43	50	90	
0.78	12	22	0.42	53	96	
0.77	13	23	0.41	56	101	
0.76	13	24	0.40	60	108	
0.75	14	25	0.39	64	115	
0.74	140.	26	0.38	68	122	
0.73	15	27	0.37	72	130	
0.72	16	28	0.36	77	138	
0.71	16	29	0.35	82	147	
0.70	17	30	0.34	87	156	
	17	31	0.33	92	166	
0.69	18	32	0.32	98	177	
0.67	18	33	0.31	104	188	
0.66	18	33	0.30	111	200	
0.65	19	34	0.30	120	217	

material and the intended service conditions. Factors to be considered include

- (1) applicability and reliability of the data, especially for extremes of the temperature range
- (2) resistance of the material to deleterious effects of the fluid service and of the environment throughout the temperature range
- (3) determination of allowable stresses in accordance with para. 302.3

323.3 Impact Testing Methods and Acceptance Criteria

323.3.1 General. When impact testing is required by Table 323.2.2, provisions elsewhere in this Code, or the engineering design, it shall be done in accordance with Table 323.3.1 using the testing methods and acceptance criteria described in paras. 323.3.2 through 323.3.5.

323.3.2 Procedure. Impact testing of each product form of material for any specification (including welds in the components) shall be done using procedures and apparatus in accordance with ASTM A370. For material forms that are represented by the ASTM specifications listed below, impact tests shall be conducted in conformance with those requirements as well. When conflicts exist between the specific requirements of this Code and the requirements of those specifications, the requirements of this Code shall take precedence.

Product Form	ASTM Spec. No.
Pipe	A333
Tube	A334
Fittings	A420
Forgings	A350
Castings	A352
Bolting	A320
Plate	A20

GENERAL NOTE: Titles of referenced standards not listed in the Specifications Index for Appendix A are A20 General Requirements for Steel Plates for Pressure Vessels and A370 Test Methods and Definitions for Mechanical Testing of Steel Products.

323.3.3 Test Specimens. Each set of impact test specimens shall consist of three specimen bars. All impact tests shall be made using standard 10 mm (0.394 in.) square cross section Charpy V-notch specimen bars, except when the material shape or thickness does not permit. Charpy impact tests may be performed on specimens of full material thickness, which may be machined to remove surface irregularities. Alternatively, such material may be reduced in thickness to produce the largest possible Charpy subsize specimen. See Table 323.3.4.

- **323.3.4 Test Temperatures.** For all Charpy impact tests, the test temperature criteria in (a) or (b) shall be observed. The test specimens, as well as the handling tongs, shall be cooled for a sufficient length of time to reach the test temperature.
- (a) For Materials of Thickness Equal to or Greater Than 10 mm (0.394 in.). Where the largest attainable Charpy V-notch specimen has a width along the notch of at least 8 mm (0.315 in.), the Charpy test using such a specimen shall be conducted at a temperature not higher than the design minimum temperature. Where the largest possible test specimen has a width along the notch less than 8 mm, the test shall be conducted at a temperature lower than the design minimum temperature by the amount shown in Table 323.3.4 for that specimen width.
- (b) For Materials With Thickness Less Than 10 mm (0.394 in.). Where the largest attainable Charpy V-notch specimen has a width along the notch of at least 80% of the material thickness, the Charpy test of such a specimen shall be conducted at a temperature not higher than the design minimum temperature. Where the largest possible test specimen has a width along the notch of less than 80% of the material thickness, the test shall be conducted at a temperature lower than the design minimum temperature by an amount equal to the difference (referring to Table 323.3.4) between the temperature reduction corresponding to the actual material thickness and the temperature reduction corresponding to the Charpy specimen width actually tested

323.3.5 Acceptance Criteria

(18)

- (a) Minimum Energy Requirements. Except for bolting materials, the applicable minimum energy requirement for carbon and low alloy steels with specified minimum tensile strengths less than 656 MPa (95 ksi) shall be those shown in Table 323.3.5.
- (b) Lateral Expansion Requirements. Other carbon and low alloy steels having specified minimum tensile strengths equal to or greater than 656 MPa (95 ksi), all bolting materials, and all high alloy steels (P-Nos. 6, 7, 8, 10H, and 10I) shall have a lateral expansion opposite the notch of not less than 0.38 mm (0.015 in.) for all specimen sizes. The lateral expansion is the increase in width of the broken impact specimen over that of the unbroken specimen measured on the compression side, parallel to the line constituting the bottom of the V-notch (see ASTM A370).
- (c) Weld Impact Test Requirements. Where two base metals having different required impact test acceptance criteria are joined by welding, the impact test acceptance criteria shall conform to the requirements of the base material having a specified minimum tensile strength most closely matching the specified minimum tensile strength of the weld metal.

Table 323.3.1 Impact Testing Requirements for Metals

	Test acteristics	Column A Materials Tested by the Manufacturer [Note (1)] or Those in Table 323.2.2 Requiring Impact Tests Only on Welds	Column B Materials Not Tested by the Manufacturer or Those Tested But Heat Treated During or After Fabrication
Tests on Materials	Number of tests	A-1 The greater of the number required by (a) the material specification or (b) the applicable specification listed in para. 323.3.2 [Note (2)]	B-1 The number required by the applicable specification listed in para. 323.3.2 [Note (2)]
	Location and orientation of specimens	2 As required by the applicable specification listed i	in para. 323.3.2.
	Tests by	A-3 The manufacturer	B-3 The fabricator or erector
Tests on Welds in Fabrication	Test piece for preparation of impact specimens	4 One required for each welding procedure, for each classification), and for each flux to be used. Test pi heat treatment (including time at temperature or piping will have received.	eces shall be subjected to essentially the same
or Assembly	Number of test pieces [Note (3)]	 (a) One piece, thickness <i>T</i>, for each range of material thickness from <i>T</i>/2 to <i>T</i> + 6 mm (¹/₄ in.) (b) Unless required by the engineering design, pieces need not be made from each lot, nor from material for each job, provided that welds have been tested as required by Section 4 above, for the same type and grade of material (or for the same P-Number and Group Number in the ASME BPVC, Section IX), and of the same thickness range, and that records of the tests are made available 	B-5 (a) One piece from each lot of material in each specification and grade including heat treatment [Note (4)] unless (b) Materials are qualified by the fabricator or erector as specified in items B-1 and 2 above, in which case the requirements of item A-5 apply
	Location and orientation of specimens	 (a) Weld metal: across the weld, with notch in the we surface, with one face of specimen ≤1.5 mm (¹/2). (b) Heat affected zone (HAZ): across the weld and etching; notch axis shall be approximately normuch as possible of the HAZ in the fracture. 	χ_{16} in.) from the material surface. long enough to locate notch in the HAZ after
	Tests by	7 The fabricator or erector	

NOTFS.

- (1) A certified report of impact tests performed (after being appropriately heat treated as required by Table 323.2.2, item B-3) by the manufacturer shall be obtained as evidence that the material (including any welds used in its manufacture) meets the requirements of this Code and that
 - (a) the tests were conducted on specimens representative of the material delivered to and used by the fabricator or erector, or
- (b) the tests were conducted on specimens removed from test pieces of the material which received heat treatment separately in the same manner as the material (including heat treatment by the manufacturer) so as to be representative of the finished piping
- (2) If welding is used in manufacture, fabrication, or erection, tests of the HAZ will suffice for the tests of the base material.
- (3) The test piece shall be large enough to permit preparing three specimens from the weld metal and three from the HAZ (if required) in accordance with para. 323.3. If this is not possible, preparation of additional test pieces is required.
- (4) For purposes of this requirement, "lot" means the quantity of material described under the "Number of tests" provision of the specification applicable to the product term (i.e., plate, pipe, etc.) listed in para. 323.3.2.

Table 323.3.4 Charpy Impact Test Temperature Reduction

Actual Material Thickness [See Para. 323.3.4(b) or Charpy Impact Specimen Width Along the Notch [Note (1)]	Temperature Reduction Below Design Minimum Temperature		
mm	in.	°C	°F
10 (full size standard bar)	0.394	0	0
9	0.354	0	0
8	0.315	0	0
7.5 (³ / ₄ size bar)	0.295	2.8	5
7	0.276	4.4	8
6.67 (² / ₃ size bar)	0.262	5.6	10
6	0.236	8.3	15
•			
$5 (\frac{1}{2} \text{ size bar})$	0.197	11.1	20
4	0.157	16.7	30
3.33 ($\frac{1}{3}$ size bar)	0.131	19.4	35
3	0.118	22.2	40
2.5 ($\frac{1}{4}$ size bar)	0.098	27.8	50

GENERAL NOTE: These temperature reduction criteria do not apply when Table 323.3.5 specifies lateral expansion for minimum required values.

NOTE: (1) Straight-line interpolation for intermediate values is permitted.

(d) Retests

- (1) For Absorbed Energy Criteria. When the average value of the three specimens equals or exceeds the minimum value permitted for a single specimen and the value for more than one specimen is below the required average value or when the value for one specimen is below the minimum value permitted for a single specimen, a retest of three additional specimens shall be made. The value for each of these retest specimens shall equal or exceed the required average value.
- (2) For Lateral Expansion Criterion. If the value of lateral expansion for one specimen in a group of three is below 0.38 mm (0.015 in.) but not below 0.25 mm (0.01 in.), and if the average value for three specimens equals or exceeds 0.38 mm (0.015 in.), a retest of three additional specimens may be made, each of which must equal or exceed the specified minimum value of 0.38 mm (0.015 in.). In the case of heat treated materials, if the required values are not obtained in the retest or if the values in the initial test are below the minimum allowed for retest, the material may be reheat

treated and retested. After reheat treatment, a set of three specimens shall be made. For acceptance, the lateral expansion of each of the specimens must equal or exceed the specified minimum value of 0.38 mm (0.015 in.).

(3) For Erratic Test Results. When an erratic result is caused by a defective specimen or there is uncertainty in the test procedure, a retest will be allowed.

323.4 Fluid Service Requirements for Materials

323.4.1 General. Requirements in para. 323 4 apply to pressure-containing parts. They do not apply to materials used for supports, gaskets, packing, or bolting. See also Appendix F, para. F323.4.

323.4.2 Specific Requirements

(a) Ductile Iron. Ductile iron shall not be used for pressure containing parts at temperatures below -29°C (-20°F) (except austenitic ductile iron) or above 343°C (650°F). Austenitic ductile iron conforming to ASTM A571 may be used at temperatures below -29°C (-20°F) down to the temperature of the impact test conducted in accordance with that specification but not below -196°C (-320°F).

Valves having bodies and bonnets or covers made of materials conforming to ASTM A395 and meeting the requirements of ASME B16.42 and additional requirements of ASME B16.34 Standard Class, API 594, API 599, or API 609 may be used within the pressure–temperature ratings given in ASME B16.42.

Welding shall not be performed in the fabrication or repair of ductile iron components nor in assembly of such components in a piping system.

- (b) Other Cast Irons. The following shall not be used under severe cyclic conditions. If safeguarding is provided against excessive heat and thermal shock and mechanical shock and abuse, they may be used in other services subject to the following requirements:
- (1) Gray iron shall not be used above ground within process unit limits in hydrocarbon or other flammable fluid service at temperatures above 149°C (300°F) nor at gage pressures above 1 035 kPa (150 psi). In other locations the pressure limit shall be 2760 kPa (400 psi).
- (2) Malleable iron shall not be used in any fluid service at temperatures below -29°C (-20°F) or above 343°C (650°F) and shall not be used in flammable fluid service at temperatures above 149°C (300°F) nor at gage pressures above 2760 kPa (400 psi).
- (3) High silicon iron (14.5% Si) shall not be used in flammable fluid service. The manufacturer should be consulted for pressure–temperature ratings and for precautionary measures when using this material.

(c) Other Materials

(1) If welding or thermal cutting is performed on aluminum castings, the stress values in Appendix A and component ratings listed in Table 326.1 are not

Table 323.3.5 Minimum Required Charpy V-Notch Impact Values

		Energy [Note (2)]			
Number of Specimens	Fully Deoxidized Steels		Other Than Fully Deoxidized Steels		
[Note (1)]	Joules	ft-lbf	Joules	ft-lbf	
Average for 3 specimens	18	13	14	10	
Minimum for 1 specimen	14	10	10	7	
Average for 3 specimens	20	15	18	% 13	
Minimum for 1 specimen	16	12	14	10	
Average for 3 specimens	27	20	. Co V		
Minimum for 1 specimen	20	15	0	•••	
		Lateral 1	Expansion		
Minimum for 3 specimens		0.38 mm	(0.015 in.)		
Minimum for 3 specimens		0.38 mm	(0.015 in.)		
	Average for 3 specimens Minimum for 1 specimen Average for 3 specimens Minimum for 1 specimen Average for 3 specimens Minimum for 1 specimen Minimum for 3 specimens	Number of Specimens [Note (1)] Average for 3 specimens Minimum for 1 specimen Average for 3 specimens Minimum for 1 specimen Average for 3 specimens Minimum for 1 specimen 20 Average for 3 specimens Average for 3 specimens 27 Minimum for 1 specimen 20 Minimum for 3 specimens	Fully Deoxidized Steels Interest (Note (1)) Fully Deoxidized Steels Joules ft-lbf Average for 3 specimens 18 13 Minimum for 1 specimen 14 10 Average for 3 specimens 20 15 Minimum for 1 specimen 16 12 Average for 3 specimens 27 20 Minimum for 1 specimen 20 15 Lateral Lateral Minimum for 3 specimens 0.38 nm	Fully Deoxidized Other The Deoxidized Steels Deoxidized Deox	

- (1) See para. 323.3.5(d) for permissible retests.
- (2) Energy values in this Table are for standard size specimens. For subsize specimens, these values shall be multiplied by the ratio of the actual specimen width to that of a full-size specimen, 10 mm (0.394 in.).
- (3) For bolting of this strength level in nominal sizes M 52 (2 in.) and under, the impact requirements of ASTM A320 may be applied. For bolting over M 52, requirements of this Table shall apply.

applicable. It is the designer's responsibility to establish such stresses and ratings consistent with the requirements of this Code.

- (2) Lead and tin and their alloys shall not be used in flammable fluid services.
- **323.4.3 Cladding and Lining Materials.** Materials with metallic cladding or metallic lining may be used in accordance with the following provisions:
- (a) If piping components are made from integrally clad plate conforming to
- (1) ASTM A263, Corrosion-Resisting Chromium Steel Clad Plate, Sheet, and Strip
- (2) ASTM A264, Stainless Chromium-Nickel Steel Clad Plate, Sheet, and Strip
- (3) ASTM A265 Nickel and Nickel-Base Alloy Clad Plate, Sheet, and Strip

Then pressure design in accordance with rules in para. 304 may be based upon the total thickness of base metal and cladding after any allowance for corrosion has been deducted, provided that both the base metal and the cladding metal are acceptable for Code use under para. 323.1, and provided that the clad plate has been shear tested and meets all shear test requirements of the applicable ASTM specification. The allowable stress for each material (base and cladding) shall be taken from Appendix A, or determined in accordance with the rules in para. 302.3, provided, however, that the allowable stress used for the cladding portion of the design

thickness shall never be greater than the allowable stress used for the base portion.

- (b) For all other metallic clad or lined piping components, the base metal shall be an acceptable Code material as defined in para. 323.1 and the thickness used in pressure design in accordance with para. 304 shall not include the thickness of the cladding or lining. The allowable stress used shall be that for the base metal at the design temperature. For such components, the cladding or lining may be any material that, in the judgment of the user, is suitable for the intended service and for the method of manufacture and assembly of the piping component.
- (c) Except for components designed in accordance with provisions of para. 323.4.3(a), fluid service requirements for materials stated in this Code shall not restrict their use as cladding or lining in pipe or other components. Fluid service requirements for the outer material (including those for components and joints) shall govern, except that temperature limitations of both inner and outer materials, and of any bond between them, shall be considered.
- (d) Fabrication by welding of clad or lined piping components and the inspection and testing of such components shall be done in accordance with applicable provisions of ASME BPVC, Section VIII, Division 1, UCL-30 through UCL-52, or the provisions of Chapters V and VI of this Code, whichever are more stringent.

323.5 Deterioration of Materials in Service

Selection of material to resist deterioration in service is not within the scope of this Code. See para. 300(c)(6). Recommendations based on experience are presented for guidance in Appendix F, para. F323.

325 MATERIALS — MISCELLANEOUS

325.1 Joining and Auxiliary Materials

When selecting materials such as adhesives, cements, solvents, solders, brazing materials, packing, and O-rings for making or sealing joints, the designer shall consider their suitability for the fluid service. (Consideration should also be given to the possible effects of the

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Chapter IV Standards for Piping Components

326 DIMENSIONS AND RATINGS OF COMPONENTS

326.1 Dimensional Requirements

326.1.1 Listed Piping Components. Dimensional standards¹ for piping components are listed in Table 326.1. Dimensional requirements contained in specifications listed in Appendix A shall also be considered requirements of this Code.

326.1.2 Unlisted Piping Components. Piping components not listed in Table 326.1 or Appendix A shall meet the pressure design requirements described in para. 302.2.3 and the mechanical strength requirements described in para. 302.5.

326.1.3 Threads. The dimensions of piping connection threads not otherwise covered by a governing component standard or specification shall conform to the requirements of applicable standards listed in Table 326.1 or Appendix A.

326.2 Ratings of Components

326.2.1 Listed Components. The pressure-temperature ratings of components listed in Table 326.1 are accepted for pressure design in accordance with para. 303.

326.2.2 Unlisted Components. The pressure-temperature ratings of unlisted piping components shall conform to the applicable provisions of para. 304.

326.3 Reference Documents

The documents listed in Table 326.1 contain references to codes, standards, and specifications not listed in Table 326.1. Such unlisted codes, standards, and specifications shall be used only in the context of the listed documents in which they appear.

The design, materials, fabrication, assembly, examination, inspection, and testing requirements of this Code are not applicable to components manufactured in accordance with the documents listed in Table 326.1, unless specifically stated in this Code or the listed document.

¹ It is not practical to refer to a specific edition of each standard throughout the Code text. Instead, the approved edition references, along with the names and addresses of sponsoring organizations, are shown in Appendix E.

Table 326.1 Component Standards

Standard or Specification	Designation
Bolting	
Square and Hex Bolts and Screws (Inch Series)	ASME B18.2.1
Square and Hex Nuts (Inch Series)	ASME B18.2.2
Continuous Thread Stud, Double-End Stud, and Flange Bolting Stud (Stud Bolt) (Inch Series)	ASME B18.31.2
Metallic Fittings, Valves, and Flanges	
Gray Iron Pipe Flanges and Flanged Fittings	ASME B16.1
Malleable Iron Threaded Fittings	ASME B16.3
Gray Iron Threaded Fittings	ASME B16.4
Pipe Flanges and Flanged Fittings	ASME B16.5
Factory-Made Wrought Buttwelding Fittings	ASME B16.9
Face-to-Face and End-To-End Dimensions of Valves	ASME B16.10
Forged Fittings, Socket-Welding and Threaded	ASME B16.11
Ferrous Pipe Plugs, Bushings, and Locknuts With Pipe Threads	ASME B16.14
Cast Bronze Threaded Fittings, Class 125 and 250 [Note (1)]	ASME B16.15
Cast Copper Alloy Solder Joint Pressure Fittings	ASME B16.18
Wrought Copper and Copper Alloy Solder Joint Pressure Fittings	ASME B16.22
Cast Copper Alloy Pipe Flanges, Flanged Fittings, and Valves: Classes 150, 300, 600, 900, 1500, and 2500	ASME B16.24
Cast Copper Alloy Fittings for Flared Copper Tubes	ASME B16.26
Valves — Flanged, Threaded, and Welding End	ASME B16.34
Orifice Flanges, Class 300, 600, 900, 1500, and 2500	ASME B16.36
Malleable Iron Threaded Pipe Unions, Class 150, 250, and 300	ASME B16.39
Ductile Iron Pipe Flanges and Flanged Fittings, Class 150 and 300	ASME B16.42
Large Diameter Steel Flanges, NPS 26 Through NPS 60	ASME B16.47
Steel Line Blanks	ASME B16.48
Brazing Joints for Copper and Copper Alloy Pressure Fittings	ASME B16.50
Bioprocessing Equipment [Note (2)]	ASME BPE
Pipeline Valves [Note (3)]	API 6D
Flanged Steel Pressure-Relief Valves	API 526
Check Valves: Flanged, Lug, Wafer and Butt-welding	API 594
Metal Plug Valves — Flanged, Threaded, and Welding Ends	API 599
Bolted Bonnet Steel Gate Valves for Petroleum and Natural Gas Industries	API 600
Gate, Globe, and Check Valves for Sizes DN 100 and Smaller for the Petroleum and Natural Gas Industries	API 602
Corrosion-Resistant, Bolted Bonnet Gate Valves — Flanged and Butt-Welding Ends	API 603
Metal Ball Valves — Flanged, Threaded, and Welding End	API 608
Butterfly Valves: Double-tlanged, Lug- and Wafer-type	API 609
Ductile-Iron and Gray fron Fittings, 3 Inch Through 48 Inch (75 mm Through 1200 mm), for Water and Other Liquids	AWWA C110
Flanged Ductile From Pipe with Ductile-Iron or Gray-Iron Threaded Flanges	AWWA C115
Steel Pipe Flanges for Waterworks Service, Sizes 4 inch Through 144 inch (100 mm Through 3,600 mm)	AWWA C207
Dimensions for Fabricated Steel Water Pipe Fittings	AWWA C208
Metal-Seated Gate Valves for Water Supply Service	AWWA C500
Rubber-Seated Butterfly Valves	AWWA C504
Standard Finishes for Contact Faces of Pipe Flanges and Connecting-End Flanges of Valves and Fittings	MSS SP-6
Spot Facing for Bronze, Iron and Steel Flanges	MSS SP-9
Standard Marking Systems for Valves, Fittings, Flanges, and Unions	MSS SP-25
Class 150 (PN 20) Corrosion Resistant Gate, Globe, Angle and Check Valves With Flanged and Butt Weld Ends	MSS SP-42
Wrought Stainless Steel Butt-Welding Fittings Including Reference to Other Corrosion Resistant Materials [Note (4)]	MSS SP-43

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Table 326.1 Component Standards (Cont'd)

Standard or Specification	Designation
Metallic Fittings, Valves, and Flanges (Cont'd)	
Steel Pipeline Flanges	MSS SP-44
Bypass and Drain Connections	MSS SP-45
Class 150LW Corrosion Resistant Flanges and Cast Flanged Fittings	MSS SP-51
High Pressure Chemical Industry Flanges and Threaded Stubs for Use with Lens Gaskets	MSS SP-65
Gray Iron Gate Valves, Flanged and Threaded Ends	MSS SP-70
Gray Iron Swing Check Valves, Flanged and Threaded Ends	MSS SP-71
Ball Valves With Flanged or Buttwelding Ends for General Service	MSS SP-72
Specifications for High Test Wrought Buttwelding Fittings	MSS SP-75
Gray Iron Plug Valves, Flanged and Threaded Ends	MSS SP-78
Socket-Welding Reducer Inserts	MSS SP-79
Bronze Gate, Globe, Angle and Check Valves	MSS SP-80
Stainless Steel, Bonnetless, Flanged, Knife Gate Valves	MSS SP-81
Class 3000 Steel Pipe Unions, Socket-Welding and Threaded	MSS SP-83
Gray Iron Globe and Angle Valves, Flanged and Threaded Ends	MSS SP-85
Diaphragm Type Valves	MSS SP-88
Swage(d) Nipples and Bull Plugs	MSS SP-95
ntegrally Reinforced Forged Branch Outlet Fittings — Socket Welding, Threaded, and Buttwelding Ends	MSS SP-97
nstrument Valves for Code Applications	MSS SP-105
Cast Copper Alloy Flanges and Flanged Fittings Class 125, 150, and 300	MSS SP-106
Factory-Made Wrought Belled End Socket Welding Fittings [Note (5)]	MSS SP-119
Refrigeration Tube Fittings — General Specifications	SAE J513
Hydraulic Tube Fittings	SAE J514
Hydraulic Flanged Tube, Pipe, and Hose Connections, Four Bolt Split Flanged Type	SAE J518
Metallic Pipe and Tubes [Note (6)]	
Welded and Seamless Wrought Steel Pipe	ASME B36.10M
Stainless Steel Pipe	ASME B36.19N
Flanged Ductile-Iron Pipe with Ductile-Iron or Gray-Iron Threaded Flanges	
Thickness Design of Ductile-Iron Pipe	AWWA C150
Ductile-Iron Pipe, Centrifugally Cast for Water	AWWA C15
Steel Water Pipe 6 inches (150 mm) and Larger	AWWA C200
Miscellaneous	101/D D1
Jnified Inch Screw Threads (UN and UNR Thread Form)	ASME B1.
Pipe Threads, General Purpose (Inch)	ASME B1.20.3
Oryseal Pipe Threads (Inch)	ASME B1.20.3
Hose Coupling Screw Threads (Inch)	ASME B1.20.7
Metallic Gaskets for Pipe Flanges — Ring: Joint, Spiral Wound, and Jacketed	ASME B16.20
Nonmetallic Flat Gaskets for Pipe Flanges	ASME B16.23
Buttwelding Ends	ASME B16.25
Surface Texture (Surface Roughness, Waviness, and Lay)	ASME B46.3
Chermowells [Note (7)]	ASME PTC 19.3 TW
Specification for Threading, Gaging and Thread Inspection of Casing, Tubing, and Line Pipe Threads	API 51
Rubber Gasket Joints for Ductile-Iron Pressure Pipe and Fittings	AWWA C11
Grooved and Shouldered Joints [Note (8)]	AWWA C606
Flexible Metal Hose [Notes (9) and (10)]	BS 6501, Part 1
Pipe Hangers and Supports — Materials, Design, and Manufacture	MSS SP-58

Table 326.1 Component Standards (Cont'd)

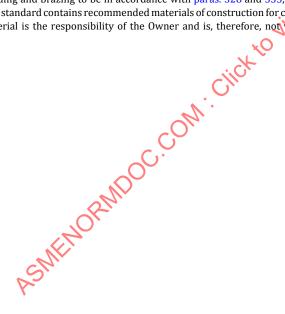
Standard or Specification	Designation
Metallic Fittings, Valves, and Flanges (Cont'd)	
Standard for Fire Hose Connections	NFPA 1963

GENERAL NOTES:

- (a) It is not practical to refer to a specific edition of each standard throughout the Code text. Instead, the approved edition references, along with the names and addresses of the sponsoring organizations, are shown in Appendix E.
- (b) Many of the listed standards allow the use of unlisted materials; see para. 323.1.2.

NOTES

- This standard allows straight pipe threads in sizes ≤ DN 15 (NPS ½); see last paragraph of para. 314.2.1.
- (2) Part DT of ASME BPE covers dimensions and tolerances for stainless steel automatic welding and hygienic clamp tube fittings and process components.
- (3) API 6D allows design and calculations for pressure-containing elements to be in accordance with various internationally recognized design codes or standards. Only API 6D valves with design and calculations for pressure-containing elements in accordance with ASME B16.34 are considered a "listed component" for the purpose of this Code.
- (4) Cautionary Note: See MSS SP-43 for special provisions concerning ratings. (In accordance with MSS SP-43, the pressure ratings for Class CR fittings are 30% of those calculated for straight seamless pipe of minimum wall thickness.)
- (5) MSS SP-119 includes three classes of fittings: MP, MARINE, and CR. Only the MP class fittings are considered a "Listed Component" for the purpose of this Code. Cautionary Note: See MSS SP-119 (Section 5) for special provisions concerning ratings. (In accordance with MSS SP-119, the pressure ratings for MP class fittings are 87.5% of those calculated for straight seattless pipe of minimum wall thickness.)
- (6) See also Appendix A.
- (7) ASME PTC 19.3 TW allows mechanical design of thermowells to be in accordance with various design codes. Only PTC 19.3 TW thermowells with design and calculations for pressure-containing elements in accordance with ASME B31.3 are considered a "listed component" for the purpose of this Code.
- (8) For use with this Code, the rated pressure of components covered by this standard shall be based on no greater than one-third the hydrostatic test failure pressure (the pressure at fracture or leakage), rather than one-half the hydrostatic test failure pressure specified in AWWA C606.
- (9) Welding and brazing to be in accordance with paras. 328 and 333, respectively, in lieu of the referenced specifications in this standard.
- (10) This standard contains recommended materials of construction for certain chemical services; the responsibility for the ultimate selection of material is the responsibility of the Owner and is, therefore, not within the scope of this Code.



Chapter V Fabrication, Assembly, and Erection

327 GENERAL

Metallic piping materials and components are prepared for assembly and erection by one or more of the fabrication processes covered in paras. 328, 330, 331, 332, and 333. When any of these processes is used in assembly or erection, requirements are the same as for fabrication.

328 WELDING AND BRAZING

Welding and brazing shall conform to the requirements of this Chapter and the applicable requirements of para. 311.2.

328.1 Responsibility

Each employer is responsible for

- (a) the welding and brazing performed by personnel of its organization
- (b) conducting the qualification tests required to qualify the welding or brazing procedure specifications used by personnel in its organization, except as provided in paras. 328.2.1 and 328.2.2
- (c) conducting the qualification tests required to qualify the welders, brazers, and operators, except as provided in para. 328.2.3

328.2 Welding and Brazing Qualification

Welding and brazing procedure specifications (WPSs and BPSs) to be followed in production welding shall be prepared and qualified, and welders, brazers, and operators shall be qualified as required by ASME BPVC, Section IX except as modified by para. 333 for brazing of Category D Fluid Service piping and by the following subparagraphs.

328.2.1 Standard Welding Procedure Specifications. Standard welding procedure specifications published by the American Welding Society and listed in ASME BPVC, Section IX, Appendix E are permitted for Code construction within the limitations established by ASME BPVC, Section IX, Article V.

328.2.2 Procedure Qualification by Others. In order to avoid duplication of effort and subject to the approval of the owner, WPSs and BPSs qualified by a technically competent group or agency may be used provided the following are met:

- (a) The procedures meet the requirements of ASME BPVC, Section IX and any additional qualification requirements of this Code.
- (b) The employer has qualified at least one welder, brazer, or operator following each WPS or BPS.
- (c) The employer's business name shall be shown on each WPS and BPS, and on each qualification record. In addition, qualification records shall be signed and dated by the employer, thereby accepting responsibility for the qualifications performed by others.

328.2.3 Performance Qualification by Others. In order to avoid duplication of effort and subject to the approval of the owner, an employer may accept the performance qualification of a welder, brazer, or operator made by a previous employer. This acceptance is limited to performance qualifications that were made on pipe or tube test coupons. The new employer shall have the WPS or BPS that was followed during qualification or an equivalent WPS or BPS that is within the limits of the essential variables set forth in ASME BPVC, Section IX. An employer accepting such qualification tests shall obtain a copy of the performance qualification test record from the previous employer. The record shall show the name of the employer by whom the welder, brazer, or operator was qualified and the date of that qualification. Evidence shall also be provided that the welder, brazer, or operator has maintained qualification in accordance with QW-322 and QB-322 of ASME BPVC, Section IX, except that this evidence may be provided by an employer responsible for the individual's welding or brazing performance even if not the original qualifying employer. The new employer's business name shall be shown on the qualification record, and it shall be signed and dated by the employer, thereby accepting responsibility for the qualifications performed by others.

328.2.4 Qualification Records. The employer shall maintain copies of the procedure and performance qualification records specified by ASME BPVC, Section IX that shall be available to the Inspector at the location where welding is being done.

328.3 Welding Materials

328.3.1 Electrodes and Filler Metal. Welding electrodes and filler metal, including consumable inserts, shall conform to the requirements of ASME BPVC,

Section II, Part C. An electrode or filler metal not conforming to the above may be used provided the WPS and the welders who will follow the WPS have been qualified as required by ASME BPVC, Section IX. Unless otherwise specified by the Designer, welding electrodes and filler metals used shall produce weld metal that complies with the following:

- (a) The nominal tensile strength of the weld metal shall equal or exceed the minimum specified tensile strength of the base metals being joined, or the weaker of the two if base metals of two different strengths are being joined.
- (b) The nominal chemical analysis of the weld metal shall be similar to the nominal chemical analysis of the major alloying elements of the base metal (e.g., $2\frac{1}{4}\%$ Cr, 1% Mo steels should be joined using $2\frac{1}{4}\%$ Cr, 1% Mo filler metals).
- (c) If base metals of different chemical analysis are being joined, the nominal chemical analysis of the weld metal shall be similar to either base metal or an intermediate composition, except as specified below for austenitic steels joined to ferritic steels.
- (d) When austenitic steels are joined to ferritic steels, the weld metal shall have a predominantly austenitic microstructure.
- (e) For nonferrous metals, the weld metal shall be that recommended by the manufacturer of the nonferrous base metal or by industry associations for that metal.

328.3.2 Weld Backing Material. When backing rings are used, they shall conform to the following:

- (a) Ferrous Metal Backing Rings. These shall be of weld able quality. Sulfur content shall not exceed 0.05%
- (b) If two abutting surfaces are to be welded to a third member used as a backing ring and one or two of the three members are ferritic and the other member or members are austenitic, the satisfactory use of such materials shall be demonstrated by welding procedure qualified as required by para. 328.2.

Backing rings may be of the continuous machined or split-band type. Some commonly used types are shown in Figure 328.3.2.

- (c) Nonferrous and Nonmetallic Backing Rings. Backing rings of nonferrous or nonmetallic material may be used, provided the designer approves their use and the welding procedure using them is qualified as required by para. 328.2
- **328.3.3 Consumable Inserts.** Consumable inserts may be used, provided they are of the same nominal composition as the filler metal, will not cause detrimental alloying of the weld metal, and the welding procedure using them is qualified as required by para. 328.2. Some commonly used types are shown in Figure 328.3.2.

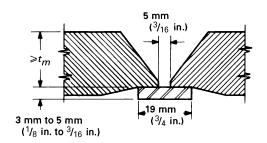
328.4 Preparation for Welding

328.4.1 Cleaning. Internal and external surfaces to be thermally cut or welded shall be clean and free from paint, oil, rust, scale, and other material that would be detrimental to either the weld or the base metal when heat is applied.

328.4.2 End Preparation

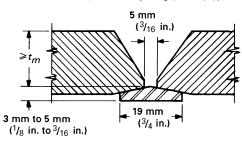
- (a) General
- (1) End preparation is acceptable only if the surface is reasonably smooth and true, and slag from oxygen or arc cutting is cleaned from thermally cut surfaces. Discoloration remaining on a thermally cut surface is not considered detrimental oxidation.
- (2) End preparation for groove welds specified in ASME B16.25, or any other that meets the WPS, is acceptable. [For convenience, the basic bevel angles of ASME B16.25 and some additional J-bevel angles are shown in Figure 328.4.2, illustrations (a) and (b).]
 - (b) Circumferential Welds
- (1) If component ends are trimmed as shown in Figure 328.3.2, illustration (a) or (b) to fit backing rings or consumable inserts, or as shown in Figure 328.4.3, illustration (a) or (b) to correct internal misalignment, such trimming shall not reduce the finished wall thickness below the required minimum wall thickness, t_m .
- (2) Component ends may be bored to allow for a completely recessed backing ring, provided the remaining net thickness of the finished ends is not less than t_m .
- (3) It is permissible to size pipe ends of the same nominal size to improve alignment if wall thickness requirements are maintained.
- (4) Where necessary, weld metal may be deposited inside or outside of the component to permit alignment or provide for machining to ensure satisfactory seating of rings or inserts.
- (5) When a girth or miter groove weld joins components of unequal wall thickness and one is more than $1\frac{1}{2}$ times the thickness of the other, end preparation and geometry shall be in accordance with acceptable designs for unequal wall thickness in ASME B16.25.
- (6) Butt-weld fittings manufactured in accordance with ASME B16.9 may be trimmed to produce an angular joint offset in their connections to pipe or to other butt-weld fittings without being subject to design qualifications in accordance with para. 304.7.2, provided the total angular offset produced between the two jointed parts does not exceed 3 deg.

Figure 328.3.2 Typical Backing Rings and Consumable Inserts



(c) Nonmetallic Removable Backing Ring (Refractory)

(a) Butt Joint With Bored Pipe Ends and Solid or Split Backing Ring [Note (1)]

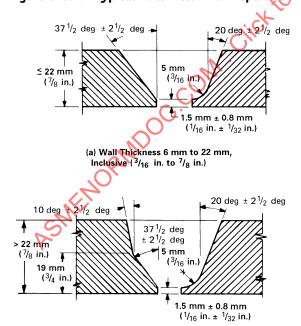


(d) Square Ring or Round Wire Type Flat Rectangular Ring Typical Consumable Inserts (f) Formed Ring Type (g) Y-Type

(b) Butt Joint With Taper-Bored Ends and Solid Backing Ring [Note (1)]

NOTE: (1) Refer to ASME B16.25 for detailed dimensional information or welding ends.

Figure 328.4.2 Typical Butt Weld End Preparation

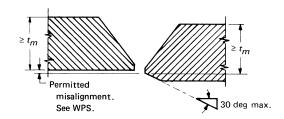


(b) Wall Thickness Over 22 mm (7/8 in.)

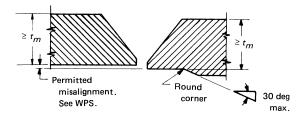
328.4.3 Alignment

- (a) Circumferential Welds
- (1) Inside surfaces of components at ends to be joined in girth or miter groove welds shall be aligned within the dimensional limits in the WPS and the engineering design.
- (2) If the external surfaces of the components are not aligned, the weld shall be tapered between them.
- (b) Longitudinal Welds. Alignment of longitudinal groove welds (not made in accordance with a standard listed in Table A-1, Table A-1M, or Table 326.1) shall conform to the requirements of para. 328.4.3(a).
 - (c) Branch Connection Welds
- (1) Branch connections that abut the outside surface of the run pipe shall be contoured for groove welds that meet the WPS requirements [see Figure 328.4.4, illustrations (a) and (b)].
- (2) Branch connections that are inserted through a run opening shall be inserted at least as far as the inside surface of the run pipe at all points [see Figure 328.4.4, illustration (c)] and shall otherwise conform to para. 328.4.3(c)(1).
- (3) Run openings for branch connections shall not deviate from the required contour more than the dimension *m* in Figure 328.4.4. In no case shall deviations of the shape of the opening cause the root spacing tolerance

Figure 328.4.3 Trimming and Permitted Misalignment



(a) Thicker Pipe Taper-Bored to Align



(b) Thicker Pipe Bored for Alignment

limits in the WPS to be exceeded. Weld metal may be added and refinished if necessary for compliance.

(d) Spacing. The root opening of the joint shall be within the tolerance limits in the WPS.

328.5 Welding Requirements

328.5.1 General

- (a) Welds, including addition of weld metal for alignment [paras. 328.4.2(b)(4) and 328.4.3(c)(3)], shall be made in accordance with a qualified procedure and by qualified welders or welding operators
- (b) Each qualified welder and welding operator shall be assigned an identification symbol. Unless otherwise specified in the engineering design, each pressure-containing weld or adjacent area shall be marked with the identification symbol of the welder or welding operator. In lieu of marking the weld, appropriate records shall be filed.
- (c) Tack welds at the root of the joint shall be made with filler metal equivalent to that used in the root pass. Tack welds shall be made by a qualified welder or welding operator. Tack welds shall be fused with the root pass weld, except that those that have cracked shall be removed. Bridge tacks (above the weld) shall be removed.
- (d) Peening is prohibited on the root pass and final pass of a weld.
- (e) No welding shall be done if there is impingement on the weld area of rain, snow, sleet, or excessive wind, or if the weld area is frosted or wet.
- (f) Welding End Valves. The welding sequence and procedure and any heat treatment for a welding end valve shall be such as to preserve the seat tightness of the valve.

- **328.5.2 Fillet and Socket Welds.** Fillet welds (including socket welds) may vary from convex to concave. The size of a fillet weld is determined as shown in Figure 328.5.2A.
- (a) Typical weld details for slip-on and socket welding flanges are shown in Figure 328.5.2B; minimum welding dimensions for other socket welding components are shown in Figure 328.5.2C or MSS SP-119.
- (b) If slip-on flanges are single welded, the weld shall be at the hub.
- **328.5.3 Seal Welds.** Seal welding shall be done by a qualified welder. Seal welds shall cover all exposed threads.

328.5.4 Welded Branch Connections

- (a) Figures 328.5.4A through 328.5.4F show acceptable details of branch connections with and without added reinforcement, in which the branch pipe is connected directly to the run pipe. The illustrations are typical and are not intended to exclude acceptable types of construction not shown.
- (b) Figure 328.3.4D shows basic types of weld attachments used in the fabrication of branch connections. The location and minimum size of attachment welds shall conform to the requirements herein. Welds shall be calculated in accordance with para. 304.3.3 but shall be not less than the sizes shown in Figure 328.5.4D. Figure 328.5.4F shows the basic types of attachment welds used with integrally reinforced branch connection fittings. The location and the minimum size of the attachment welds shall conform to the requirements of (i) below.
- (c) The nomenclature and symbols used herein, in Figure 328.5.4D, and in Figure 328.5.4F are

 \overline{T}_h = nominal thickness of branch

 \overline{T}_{L} = nominal thickness of header

 \overline{T}_m = nominal thickness of the branch weld for integrally reinforced branch connection fittings

- (1) as specified by the manufacturer of the branch connection fitting
- (2) the full depth of the resultant weld groove, after fit-up, if no manufacturer's weld thickness is specified
- (3) as documented and specified in the engineering design in accordance with para. 300(c)(3), or
- (4) calculated and documented in accordance with the requirements of para. 304.7.2

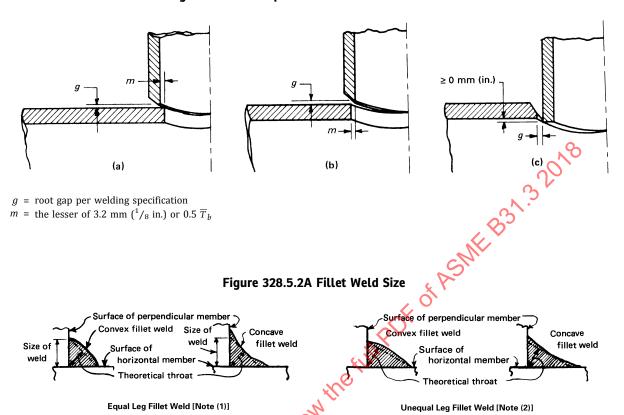
 \overline{T}_r = nominal thickness of reinforcing pad or saddle

 t_c = lesser of 0.7 \overline{T}_b or 6 mm ($\frac{1}{4}$ in.)

 $t_{\min} = \text{lesser of } \overline{T}_b \text{ or } \overline{T}_r$

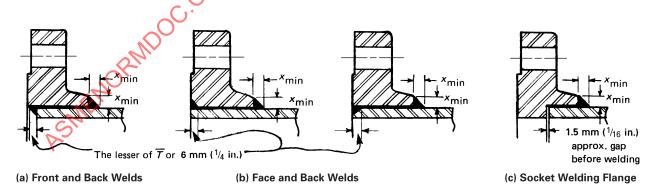
(d) Branch connections, including branch connection fittings (see paras. 300.2 and 304.3.2), that abut the outside of the run or that are inserted in an opening in

Figure 328.4.4 Preparation for Branch Connections



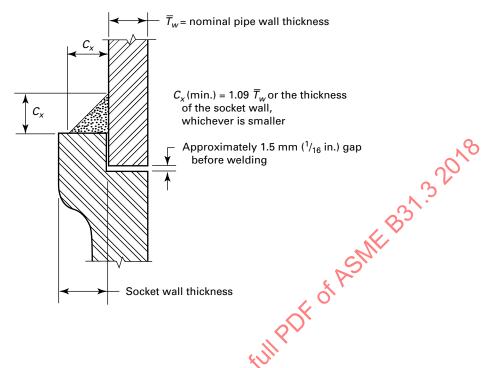
- (1) The size of an equal leg fillet weld is the leg length of the largest inscribed isosceles right triangle (theoretical throat = $0.707 \times \text{size}$).
- (2) The size of unequal leg fillet weld is the leg lengths of the largest right triangle that can be inscribed within the weld cross section [e.g., 13 mm × 19 mm ($\frac{1}{2}$ in. × $\frac{3}{4}$ in.)].

Figure 328.5.2B Typical Details for Double-Welded Slip-On and Socket Welding Flange Attachment Welds

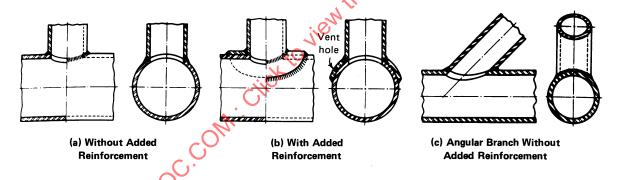


 x_{\min} = the lesser of 1.4 \overline{T} or the thickness of the hub

Figure 328.5.2C Minimum Welding Dimensions for Socket Welding Components Other Than Flanges



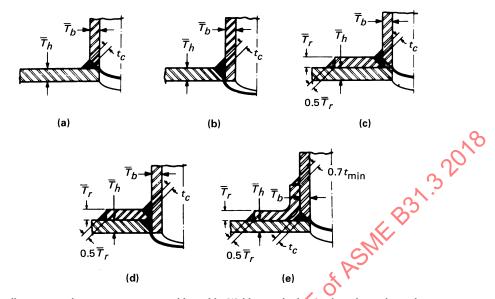
Figures 328.5.4A, B, C Typical Welded Branch Connections



the run shall be attached by fully penetrated groove welds. The welds shall be finished with cover fillet welds having a throat dimension not less than t_c . See Figure 328.5.4D, illustrations (1) and (2).

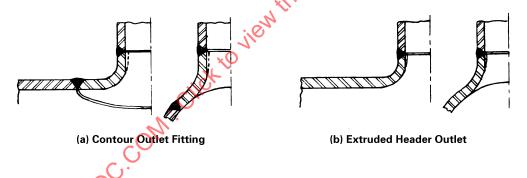
- (e) A reinforcing pad or saddle shall be attached to the branch pipe by either
- (1) a fully penetrated groove weld finished with a cover fillet weld having a throat dimension not less than t_c or
- (2) a fillet weld having a throat dimension not less than $0.7t_{\rm min}$. See Figure 328.5.4D, illustration (5).
- (f) The outer edge of a reinforcing pad or saddle shall be attached to the run pipe by a fillet weld having a throat dimension not less than $0.5 \overline{T}_r$. See Figure 328.5.4D, illustrations (3), (4), and (5).
- (g) Reinforcing pads and saddles shall have a good fit with the parts to which they are attached. A vent hole shall be provided at the side (not at the crotch) of any pad or saddle to reveal leakage in the weld between branch and run and to allow venting during welding and heat treatment. A pad or saddle may be made in more than one piece if joints between pieces have strength equivalent to pad or saddle parent metal, and if each piece has a vent hole.
- (h) Examination and any necessary repairs of the completed weld between branch and run shall be made before adding a pad or saddle.
- (i) Figure 328.5.4F shows additional integrally reinforced branch connections typical of MSS SP-97 fittings that abut the outside of the run attached by a full penetration groove weld. The welds shall be finished with cover fillets having a throat dimension not less than t_c . The cover

Figure 328.5.4D Acceptable Details for Branch Attachment Welds



GENERAL NOTE: These illustrations show minimum acceptable welds. Welds may be larger than those shown here.

Figure 328.5.4E Acceptable Details for Branch Attachment Suitable for 100% Radiography



fillet weld shall fill and smoothly transition to the attachment weld and run oipe or fitting.

328.5.5 Fabricated Laps. Figure 328.5.5 shows typical fabricated laps. Fabrication shall be in accordance with the applicable requirements of para. 328.5.4.

328.5.6 Welding for Severe Cyclic Conditions. A welding procedure shall be employed that provides a smooth, regular, fully penetrated inner surface.

328.6 Weld Repair

A weld defect to be repaired shall be removed to sound metal. Repair welds shall be made using a welding procedure qualified in accordance with para. 328.2.1, recognizing that the cavity to be repaired may differ in contour and dimensions from the original joint. Repair welds shall be made by welders or welding operators qual-

ified in accordance with para. 328.2.1. Preheating and heat treatment shall be as required for the original welding. See also para. 341.3.3.

328.7 Attachment Welds

Structural attachments may be made by complete penetration, partial penetration, or fillet welds.

Low energy capacitor discharge welding may be used for welding temporary attachments (e.g., thermocouples) and permanent nonstructural attachments without preheat above 10°C (50°F) or subsequent postweld heat treatment on P-No. 1 through P-No. 5B and P-No. 15E materials, provided

(a) a Welding Procedure Specification is prepared, describing the low energy capacitor discharge equipment, the combination of materials to be joined, and the

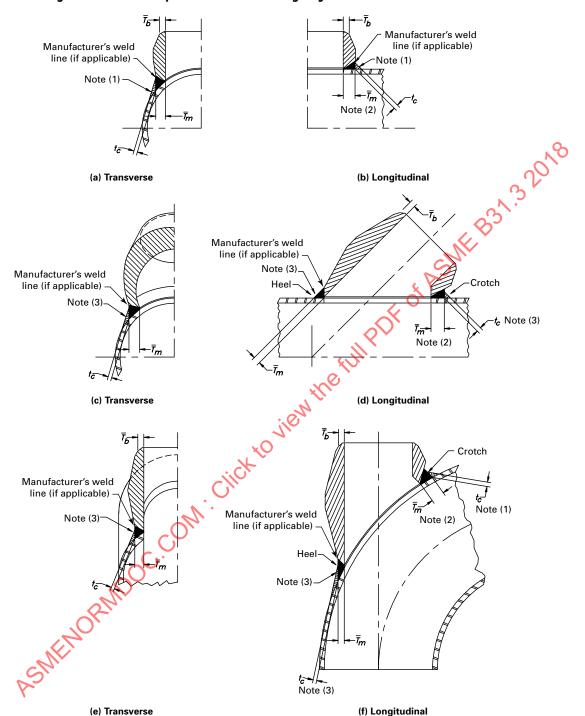


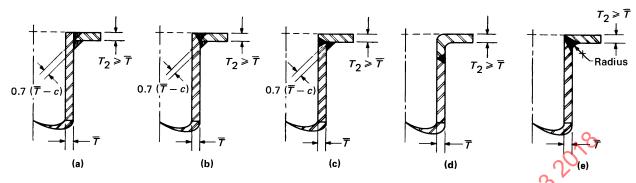
Figure 328.5.4F Acceptable Details for Integrally Reinforced Branch Connections

GENERAL NOTE: Welds shall be in accordance with para. 328.5.4(i).

NOTES:

- (1) Cover fillet weld shall provide a smooth transition to the run pipe with an equal leg fillet at the longitudinal section to an equal leg fillet, unequal (oblique) leg fillet, or groove butt joint at the transverse section (depending on branch connection size).
- (2) Heat treatment requirements shall be in accordance with para. 331.1.3(a).
- (3) Cover fillet weld shall provide a smooth transition to the run pipe with an equal leg fillet at the crotch in the longitudinal section to an equal leg fillet, unequal (oblique) leg fillet, or groove butt joint at the transverse section (depending on branch connection size) to nothing at the heel of the branch connection fitting in the longitudinal section.

Figure 328.5.5 Typical Fabricated Laps



GENERAL NOTE: Laps shall be machined (front and back) or trued after welding. Plate flanges in accordance with para 304.5 or lap joint flanges in accordance with ASME B16.5 may be used. Welds may be machined to radius, as in illustration (e), if necessary to match ASME B16.5 lap joint flanges.

technique of application; qualification of the welding procedure is not required

- (b) the energy output of the welding process is limited to 125 W-sec
- (c) for P-No. 5A, P-No. 5B, and P-No. 15E materials, the maximum carbon content of the material is 0.15%
- (d) after thermocouples are removed, the areas shall be visually examined for evidence of defects to be repaired

330 PREHEATING

330.1 General

The preheat requirements herein apply to all types of welding, including tack welds, repair welds, and seal welds on threaded joints.

330.1.1 Requirements. Unless specified otherwise in the engineering design, the minimum preheat temperatures for materials of various P-Numbers are given in Table 330.1.1. The thickness intended in Table 330.1.1 is that of the nominal thickness of the thicker component [as defined in para. 3311.3(c)]. Higher minimum preheat temperatures may be required by the WPS or by the engineering design.

330.1.2 Unlisted Materials. Preheat requirements for an unlisted material shall be specified in the WPS.

330.1.3 Preheat Temperature Verification

- (a) Preheat temperature shall be checked by use of temperature indicating crayons, thermocouple pyrometers, or other suitable means to ensure that the temperature specified in the WPS is obtained prior to and maintained during welding.
- (b) Thermocouples may be temporarily attached directly to pressure-containing parts using the low energy capacitor discharge method of welding in accordance with para. 328.7.

330.1.4 Preheat Zone. The preheat zone shall be at or above the specified minimum temperature in all directions from the point of welding for a distance of the larger of 75 mm (3 in.) or 1.5 times the greater nominal thickness.

The base metal temperature for tack welds shall be at or above the specified minimum temperature for a distance not less than 25 mm (1 in.) in all directions from the point of welding.

330.2 Specific Requirements

330.2.1 Different P-No. Materials. When welding two different P-No. materials, the preheat temperature shall be the higher temperature for the material being welded as shown in Table 330.1.1.

- **330.2.2 Interruption of Welding.** After welding commences, the minimum preheat temperature shall be maintained until any required PWHT is performed on P-Nos. 3, 4, 5A, 5B, 6, and 15E, except when all of the following conditions are satisfied:
- (a) A minimum of at least 10 mm ($\frac{3}{8}$ in.) thickness of weld is deposited or 25% of the welding groove is filled, whichever is less (the weld shall be sufficiently supported to prevent overstressing the weld if the weldment is to be moved or otherwise loaded). Caution is advised that the surface condition prior to cooling should be smooth and free of sharp discontinuities.
- (b) For P-Nos. 3, 4, and 5A materials, the weld is allowed to cool slowly to room temperature.
- (c) For P-Nos. 5B, 6, and 15E materials, the weld is subjected to an adequate intermediate heat treatment with a controlled rate of cooling. The preheat temperature may be reduced to 95°C (200°F) (minimum) for the purpose of root examination without performing an intermediate heat treatment. Intermediate heat treatment for P-No. 5B or P-No. 15E materials may be omitted when using low-hydrogen electrodes and filler metals classified

Table 330.1.1 Preheat Temperatures

Base Metal P-No.			Material kness	Additional Limits	Required Minim	um Temperature
[Note (1)]	Base Metal Group	mm	in.	[Note (2)]	°C	°F
1	Carbon steel	≤25	≤1	None	10	50
		>25	>1	$%C \le 0.30 \text{ [Note (3)]}$	10	50
		>25	>1	%C > 0.30 [Note (3)]	95	200
3	Alloy steel, $Cr \le \frac{1}{2}\%$	≤13	≤ ¹ / ₂	SMTS ≤ 450 MPa (65 ksi)	10	50
		>13	>1/2	SMTS ≤ 450 MPa (65 ksi)	95	200
		All	All	SMTS > 450 MPa (65 ksi)	95	200
4	Alloy steel, $\frac{1}{2}\%$ < Cr $\leq 2\%$	All	All	None	120	250
5A	Alloy steel	All	All	SMTS ≤ 414 MPa (60 ksi)	150	300
		All	All	SMTS > 414 MPa (60 ksi)	150	400
5B	Alloy steel	All	All	SMTS ≤ 414 MPa (60 ksi)	150	300
		All	All	SMTS > 414 MPa (60 ksi)	200	400
		>13	>1/2	%Cr > 6.0 [Note (3)]	200	400
6	Martensitic stainless steel	All	All	None	200 [Note (4)]	400 [Note (4)]
9A	Nickel alloy steel	All	All	None	120	250
9B	Nickel alloy steel	All	All	None	150	300
10I	27Cr steel	All	All	None	150 [Note (5)]	300 [Note (5)]
15E	9Cr-1Mo-V CSEF steel	All	All	None	200	400
	All other materials	<u>~()`</u>		None	10	50

- (1) P-Nos. and Group Nos. from ASME-BPVC, Section IX, QW/QB-422.
- (2) SMTS = Specified Minimum Tensile Strength.
- (3) Composition may be based on ladle or product analysis or in accordance with specification limits.
- (4) Maximum interpass temperature 315°C (600°F).
- (5) Maintain interpass temperature between 150°C and 230°C (300°F and 450°F).

by the filler metal specification with an optional supplemental diffusible-hydrogen designator of H4 or lower and suitably controlled by maintenance procedures to avoid contamination by hydrogen-producing sources. The surface of the base metal prepared for welding shall be free of contaminants.

- (d) After cooling and before welding is resumed, visual examination of the weld shall be performed to assure that no cracks have formed.
- (e) Required preheat shall be applied before welding is resumed.

331 HEAT TREATMENT

331.1 General

331.1.1 Postweld Heat Treatment Requirements

(18)

(a) PWHT shall be in accordance with the material groupings (P-Nos. and Group Nos.) and ranges in Table 331.1.1 except as provided in Table 331.1.2 and Table 331.1.3. See Appendix F, para. F331.1. The P-Numbers and Group Numbers are defined in ASME BPVC, Section IX, Table QW/QB-422. (Note that the P-Nos. are also listed in Appendix A.)

- (b) The PWHT to be used after production welding shall be specified in the WPS and shall be used in qualifying the welding procedure.
- (c) The engineering design shall specify the examination and/or other production quality control (not less than the requirements of this Code) to ensure that the final welds are of adequate quality.

331.1.2 Other Heat Treatments

- (a) Heat treatment for bending and forming shall be in accordance with para. 332.4.
- (b) See Table 302.3.5 for special heat treatment requirements for longitudinal or spiral (helical seam) welds in Elevated Temperature Fluid Service.

331.1.3 Definition of Thicknesses Governing PWHT

- (a) The term control thickness as used in Table 331.1.1 and Table 331.1.3 is the lesser of
 - (1) the thickness of the weld
- (2) the thickness of the materials being joined at the weld or the thickness of the pressure-containing material if the weld is attaching a nonpressure-containing material to a pressure-containing material.
- (b) Thickness of the weld, which is a factor in determining the control thickness, is defined as follows:
- (1) groove welds (girth and longitudinal) the thicker of the two abutting ends after weld preparation, including I.D. machining
 - (2) fillet welds the throat thickness of the weld
- (3) partial penetration welds the depth of the weld groove
- (4) material repair welds the depth of the cavity to be repaired
- (5) branch welds the dimension existing in the plane intersecting the longitudinal axes, calculated as indicated for each detail using the thickness through the weld for the details shown in Figure 328.5.4D and Figure 328.5.4F. This thickness shall be computed using the following formulas:

(-a) for Figure 328.5.4D use illustration (1) =
$$\overline{T}_b + t_c$$
 illustration (2) = $\overline{T}_h + t_c$ illustration (3) = greater of $\overline{T}_b + t_c$ or $\overline{T}_r + t_c$ illustration (4) = $\overline{T}_h + \overline{T}_r + t_c$ illustration (5) = $\overline{T}_b + t_c$

- (-b) for Figure 328.5.4F use $\overline{T}_m + t_c$ for all illustrations
- (c) The term nominal material thickness as used in Table 331.1.3 is the thicker of the materials being joined at the weld.

- **331.1.4 Heating and Cooling.** The heating method shall provide the required metal temperature, metal temperature uniformity, and temperature control, and may include an enclosed furnace, local flame heating, electric resistance, electric induction, or exothermic chemical reaction. Above 315°C (600°F), the rate of heating and cooling shall not exceed 335°C/h (600°F/hr) divided by one-half the maximum material thickness in inches at the weld, but in no case shall the rate exceed 335°C/h (600°F/hr). See Table 331.1.1 for cooling rate requirements for P-Nos. 7, 10I, 11A, and 62 materials.
- **331.1.6 Temperature Verification.** Heat treatment temperature shall be checked by thermocouple pyrometers or other suitable methods to ensure that the WPS requirements are met. See para. 328.7 for attachment of thermocouples by the low energy capacitor discharge method of welding.
- (a) If used, the heat treatment furnace shall be calibrated such that the PWHT can be controlled within the required temperature range.
- (b) Any required PWHT shall be as required by the qualified WPS
- (c) For welds that require PWHT in accordance with Table 331.1.1, the temperature of the material during PWHT shall be within the range specified. However, if specified by the designer, the range may be extended as permitted by Table 331.1.2, provided the lower critical temperature of the material is not exceeded.

331.2 Specific Requirements

Where warranted by experience or knowledge of service conditions, alternative methods of heat treatment or exceptions to the basic heat treatment provisions of para. 331.1 may be adopted as provided in paras. 331.2.1 and 331.2.2.

- **331.2.1 Alternative Heat Treatment.** Normalizing, or normalizing and tempering, or annealing may be applied in lieu of the required heat treatment after welding, bending, or forming, provided that the mechanical properties of any affected weld and base metal meet specification requirements after such treatment and that the substitution is approved by the designer.
- **331.2.2** Exceptions to Basic Requirements. As indicated in para. 331, the basic practices therein may require modification to suit service conditions in some cases. In such cases, the designer may specify more-stringent requirements in the engineering design, including heat treatment and hardness limitations for lesser thickness, or may specify less stringent heat treatment and hardness requirements, including none.

When provisions less stringent than those in para. 331 are specified, the designer must demonstrate to the owner's satisfaction the adequacy of those provisions by comparable service experience, considering service

Table 331.1.1 Postweld Heat Treatment

P-No. and Group No.	Holding Temperature Range,	Minimum Holding Time at Temperature for Control Thickness [Note (2)]			
(ASME BPVC, Section IX, QW/QB-420)	°C (°F) [Note (1)]	Up to 50 mm (2 in.)	Over 50 mm (2 in.)		
P-No. 1, Group Nos. 1-3	595 to 650 (1,100 to 1,200)	1 h/25 mm (1 hr/in.);	2 hr plus 15 min for each		
P-No. 3, Group Nos. 1 and 2	595 to 650 (1,100 to 1,200)	15 min min.	additional 25 mm (in.)		
P-No. 4, Group Nos. 1 and 2	650 to 705 (1,200 to 1,300)		over 50 mm (2 in.)		
P-No. 5A, Group No. 1	675 to 760 (1,250 to 1,400)				
P-No. 5B, Group No. 1	675 to 760 (1,250 to 1,400)				
P-No. 6, Group Nos. 1-3	760 to 800 (1,400 to 1,475)		\%		
P-No. 7, Group Nos. 1 and 2 [Note (3)]	730 to 775 (1,350 to 1,425)		-0/10		
P-No. 8, Group Nos. 1-4	PWHT not required unless required by WPS				
P-No. 9A, Group No. 1	595 to 650 (1,100 to 1,200)		ζ',5		
P-No. 9B, Group No. 1	595 to 650 (1,100 to 1,200)				
P-No. 10H, Group No. 1	PWHT not required unless required by WPS. If done, see Note (4).	«	B3132018		
P-No. 10I, Group No. 1 [Note (3)]	730 to 815 (1,350 to 1,500)	CN.			
P-No. 11A	550 to 585 (1,025 to 1,085) [Note (5)]	of AS			
P-No. 15E, Group No. 1	705 to 775 (1,300 to 1,425) [Notes (6) and (7)]	1 h/25 mm (1 hr/in.); 30 min min.	1 h/25 mm (1 hr/in.) up to 125 mm (5 in.) plus 15 min for each additional 25 mm (in.) over 125 mm (5 in.)		
P-No. 62	540 to 595 (1,000 to 1,100)		See Note (8)		
All other materials	PWHT as required by WPS	In accordance with WPS	In accordance with WPS		

GENERAL NOTE: The exemptions for mandatory PWHT are defined in Table 331.1.3.

NOTES:

(1) The holding temperature range is further defined in para. 331.1.6(c) and Table 331.1.2.

- (2) The control thickness is defined in para. 331.1.3.
- (3) Cooling rate shall not be greater than 55°C (100°F) per hour in the range above 650°C (1,200°F), after which the cooling rate shall be sufficiently rapid to prevent embrittlement.
 (4) If PWHT is performed after welding, it shall be within the following temperature ranges for the specific alloy, followed by rapid cooling:
- (4) If PWHT is performed after welding, it shall be within the following temperature ranges for the specific alloy, followed by rapid cooling Alloys S31803 and S32205 1020°C to 1100°C (1,870°F to 2,010°F)

Alloy S32550 — 1040°C to 1120°C (1,900°F to 2,050°F)

- Alloy S32750 1025°C to 1125°C (1,880°F to 2,060°F)
- All others 980°C to 1040°C (1800°F to 1,900°F)
- (5) Cooling rate shall be >165°C (300°F)/h to 315°C (600°F)/h.
- (6) The minimum PWHT holding temperature may be 675°C (1,250°F) for nominal material thicknesses [see para. 331.1.3(c)] ≤13 mm (½ in.).
- (7) The Ni + Mn content of the filler metal shall not exceed 1.2% unless specified by the designer, in which case the maximum temperature to be reached during PWHT shall be the A_1 (lower transformation or lower critical temperature) of the filler metal, as determined by analysis and calculation or by test, but not exceeding 800°C (1,470°F). If the 800°C (1,470°F) limit was not exceeded but the A_1 of the filler metal was exceeded or if the composition of the filler metal is unknown, the weld must be removed and replaced. It shall then be rewelded with compliant filler metal and subjected to a compliant PWHT. If the 800°C (1,470°F) limit was exceeded, the weld and the entire area affected by the PWHT will be removed and, if reused, shall be renormalized and tempered prior to reinstallation.
- (8) Heat treat within 14 days after welding. Hold time shall be increased by 1.2 h for each 25 mm (1 in.) over 25 mm (1 in.) thickness. Cool to 425°C (800°F) at a rate ≤280°C (500°F)/h.

Table 331.1.2 Alternate Postweld Heat Treatment Requirements for Carbon and Low Alloy Steels, P-Nos. 1 and 3

Decrease in Specified Minimum Temperature, °C (°F)	Minimum Holding Time at Decreased Temperature, h [Note (1)]
30 (50)	2
55 (100)	4
85 (150) [Note (2)]	10
110 (200) [Note (2)]	20

- (1) Times shown apply to thicknesses ≤25 mm (1 in.). Add 15 min/25 mm (15 min/in.) of thickness for control thicknesses >25 mm (1 in.) (see para. 331.1.3).
- (2) A decrease >55°C (100°F) below the minimum specified temperature is allowable only for P-No. 1, Group Nos. 1 and 2 materials.

temperature and its effects, frequency and intensity of thermal cycling, flexibility stress levels, probability of brittle failure, and other pertinent factors. In addition, appropriate tests shall be conducted, including WPS qualification tests.

331.2.3 Dissimilar Materials

- (a) Heat treatment of welded joints between dissimilar ferritic metals or between ferritic metals using dissimilar ferritic filler metal shall be at the higher of the temperature ranges in Table 331.1.1 for the materials in the joint. This may require the use of material transition joint designs.
- (b) Heat treatment of welded joints including both ferritic and austenitic components and filler metals shall be as required for the ferritic material or materials unless otherwise specified in the engineering design.
- **331.2.4 Delayed Heat Treatment.** If a weldment is allowed to cool prior to heat treatment, the rate of cooling shall be controlled or other means shall be used to prevent detrimental effects in the piping.
- **331.2.5 Partial Heat Treatment.** When an entire piping assembly to be heat treated cannot be fitted into the furnace, it is permissible to heat treat in more than one heat, provided there is at least 300 mm (1 ft) overlap between successive heats, and that parts of the assembly outside the furnace are protected from harmful temperature gradients. This method may not be used for austenitizing heat treatments for ferritic materials.
- **331.2.6 Local Heat Treatment.** Welds may be locally postweld heat treated by heating a circumferential band around the entire component with the weld located in the center of the band. The width of the band heated to the specified temperature range shall be at least three times the wall thickness at the weld of the thickest part being joined. For nozzle and attachment welds, the width of the

band heated to the specified temperature range shall extend beyond the nozzle weld or attachment weld on each side at least two times the run pipe thickness, and shall extend completely around the run pipe. Guidance for the placement of thermocouples on circumferential butt welds is provided in AWS D10.10, Sections 5, 6, and 8. Special consideration shall be given to the placement of thermocouples when heating welds adjacent to large heat sinks such as valves or fittings, or when joining parts of different thicknesses. No part of the materials subjected to the heat source shall exceed the lower critical temperature of the material except as permitted by para. 331.2.1. Particular care must be exercised when the applicable PWHT temperature is close to the material's lower critical temperature, such as for P-No. 15E materials or when materials of different PNos. are being joined. This method may not be used for austenitizing heat treatments.

332 BENDING AND FORMING

332.1 General **(**

Pipe may be bent and components may be formed by any hot or cold method that is suitable for the material, the fluid service, and the severity of the bending or forming process. The finished surface shall be free of cracks and substantially free from buckling. Thickness after bending or forming shall be not less than that required by the design.

332.2 Bending

332.2.1 Bend Flattening. Flattening of a bend, the difference between maximum and minimum diameters at any cross section, shall not exceed 8% of nominal outside diameter for internal pressure and 3% for external pressure. Removal of metal shall not be used to achieve these requirements.

332.2.2 Bending Temperature

- (a) Cold bending of ferritic materials shall be done at a temperature below the transformation range.
- (b) Hot bending shall be done at a temperature above the transformation range and in any case within a temperature range consistent with the material and the intended service.
- **332.2.3 Corrugated and Other Bends.** Dimensions and configuration shall conform to the design qualified in accordance with para. 306.2.2.

332.3 Forming

The temperature range for forming shall be consistent with material, intended service, and specified heat treatment.

¹ For pipe bending, PFI Standard ES-24, Pipe Bending Methods, Tolerances, Process and Material Requirements, may be used as a guide.

Table 331.1.3 Exemptions to Mandatory Postweld Heat Treatment

P-No. and Group No. (ASME BPVC, Section IX, QW/QB-420) [Note (1)]	Control Thickness, mm (in.) [Note (2)]	Type of Weld	Additional Limitations Required for Exemption From PWHT [Notes (3)-(5)]
P-No. 1, all Group Nos.	All	All	A preheat of 95°C (200°F) is applied prior to welding on any nominal material thickness >25 mm (1 in.) Multiple layer welds are used when the nominal material thickness >5 mm ($\frac{3}{16}$ in.) [Note (6)]
P-No. 3, Group Nos. 1 and 2	≤16 mm (⁵ / ₈ in.)	All	A preheat of 95°C (200°F) is applied prior to welding on any nominal material thickness >13 mm (½ in.) A specified carbon content of the base materials ≤0.25% Multiple layer welds are used when the nominal material thickness ×5 mm (¾ in.) [Note (6)]
P-No. 4, Group No. 1	≤16 mm (5% in.)	Groove	Mandatory preheat has been applied Specified carbon content of the base materials ≤0.15% Multiple layer welds are used when the nominal material thickness >5 mm (³₁6 in.) [Note (6)]
	≤16 mm (5% in.) except the thickness of a socket weld fitting or flange need not be considered	Socket and fillet welds	Mandatory preheat has been applied Throat thickness of the fillet weld or the socket weld ≤13 mm (½ in.) Specified carbon content of the pipe material ≤0.15% Nominal material thickness of the pipe ≤16 mm (⅙ in.) Multiple layer welds are used when the nominal material thickness >5 mm (⅙ in.) [Note (6)]
	≤16 mm (⁵ % in.)	Seal welds and non-load-carrying attachments [Note (7)]	Mandatory preheat has been applied Multiple layer welds are used when the nominal material thickness >5 mm ($\frac{3}{16}$ in.) [Note (6)]
P-No. 5A, Group No. 1	≤16 mm (⁵ / ₈ in.)	Groove	Mandatory preheat has been applied Specified carbon content of the base materials ≤0.15% Multiple layer welds are used when the nominal material thickness >5 mm (³ / ₁₆ in.) [Note (6)]
ASMENO	≤16 mm (5% in.) except the thickness of a socket weld fitting or flange need not be considered	Socket and fillet welds	Mandatory preheat has been applied Throat thickness of the fillet weld or the socket weld ≤13 mm (½ in.) Specified carbon content of the pipe material ≤0.15% Nominal thickness of the pipe ≤5 mm (¾ ₁₆ in.) Multiple layer welds are used when the nominal material thickness >5 mm (¾ ₁₆ in.) [Note (6)]
PS.	≤16 mm (5/8 in.)	Seal welds and non-load-carrying attachments [Note (7)]	Mandatory preheat has been applied Multiple layer welds are used when the nominal material thickness >5 mm (3/16 in.) [Note (6)]
P-No. 5B, Group No. 1			No exemptions from PWHT
P-No. 6, Group Nos. 1-3	All	All	Specified carbon content of the base materials ≤0.08% Nominal material thickness ≤10 mm (¾ in.) Weld filler metal is A-No. 8, A-No. 9, or F-No. 43 composition [Note (8)]

Table 331.1.3 Exemptions to Mandatory Postweld Heat Treatment (Cont'd)

P-No. and Group No. (ASME BPVC, Section IX, QW/QB-420) [Note (1)]	Control Thickness, mm (in.) [Note (2)]	Type of Weld	Additional Limitations Required for Exemption From PWHT [Notes (3)-(5)]
P-No. 7, Group No. 1	All	All	Specified carbon content of the base materials ≤0.08% Nominal material thickness ≤10 mm (³ / ₈ in.) Weld filler metal is A-No. 8, A-No. 9, or F-No. 43 composition [Note (8)]
P-No. 7, Group No. 2			No exemptions from PWHT
P-No. 8, all Group Nos.	All	All	PWHT neither required nor prohibited
P-No. 9A, Group No. 1	All	All	Specified carbon content of the pipe material ≤0.15% Nominal material thickness ≤13 mm (½ in.) Mandatory preheat has been applied
P-No. 9B, Group No. 1	All	All	Nominal material thickness <16 mm (54 in) and
P-No. 10H, Group No. 1	All	All the	PWHT neither required nor prohibited
P-No. 10I, Group No. 1	All	All the full po	PWHT neither required nor prohibited for nominal material thickness ≤13 mm (½ in.)
P-No. 11A	≤50 mm (2 in.)	All	
P-No. 15E			No exemptions from PWHT
P-No. 62	COM,		No exemptions from PWHT

- (1) If differences with the P-No. disted in Appendix A are found, the P-No. listed in ASME BPVC, Section IX, Table QW/QB-422 applies.
- (2) The control thickness is defined in para. 331.1.3.
- (3) The nominal material thickness is defined in para. 331.1.3(c).
- (4) No exemptions are permitted for PWHTs required by the designer or the WPS.
- (5) Additional exemptions for welds made in accordance with para. 328.7 may be taken for the materials addressed.
- (6) Single-layer or single-pass welds may be exempted from PWHT, provided the WPS has been qualified using single-pass welds with ±10% heat input and that all other conditions for exemption are met.
- (7) Non-load carrying attachments are defined as items where no pressure loads or significant mechanical loads are transmitted through the attachment to the pipe or pressure-containing material.
- (8) The A-Nos. and the F-Nos. are found in ASME BPVC, Section IX, Tables QW-442 and QW-432, respectively.

332.4 Required Heat Treatment

Heat treatment shall be performed in accordance with para. 331.1.1 when required by the following.

- **332.4.1 Hot Bending and Forming.** After hot bending and forming, heat treatment is required for P-Nos. 3, 4, 5, 6, and 10A materials in all thicknesses. Durations and temperatures shall be in accordance with para. 331.
- **332.4.2 Cold Bending and Forming.** After cold bending and forming, heat treatment is required (for all thicknesses, and with temperature and duration as given in Table 331.1.1) when any of the following conditions exist:
- (a) for P-Nos. 1 through 6 materials, where the maximum calculated fiber elongation after bending or forming exceeds 50% of specified basic minimum elongation (in the direction of severest forming) for the applicable specification, grade, and thickness. This requirement may be waived if it can be demonstrated that the selection of pipe and the choice of bending or forming process provide assurance that, in the finished condition, the most severely strained material retains at least 10% elongation.
- (b) for any material requiring impact testing, where the maximum calculated fiber elongation after bending or forming will exceed 5%.
 - (c) when specified in the engineering design.

333 BRAZING AND SOLDERING

333.1 Qualification

- **333.1.1 Brazing Qualification.** The qualification of brazing procedures, brazers, and brazing operators shall be in accordance with para. 328.2. For Category D Fluid Service at design temperature not over 93°C (200°F), such qualification is not required unless specified in the engineering design.
- **333.1.2 Soldering Qualification.** The qualification of solderers shall be in accordance with the requirements of ASTM B828, Standard Practice for Making Capillary Joints by Soldering of Copper and Copper Alloy Tube and Fittings.

333.2 Brazing and Soldering Materials

- **333.2.1 Brazing Filler Metal and Flux.** Brazing filler metal and flux shall comply with AWS A5.8, Specification for Filler Metals for Brazing and Braze Welding, and AWS A5.31, Specification for Fluxes for Brazing and Braze Welding, respectively, or other filler metals and fluxes that have been qualified in accordance with ASME BPVC, Section IX.
- **333.2.2 Soldering Filler Metal and Flux.** Soldering filler metal and flux shall comply with ASTM B32, Standard Specification for Solder Metal, and ASTM B813, Standard

Specification for Liquid and Paste Fluxes for Soldering of Copper and Copper Alloy Tube, respectively.

333.3 Preparation and Cleaning

- **333.3.1 Surface Preparation.** The surfaces to be brazed or soldered shall be clean and free from grease, oxides, paint, scale, and dirt of any kind. A suitable chemical or mechanical cleaning method shall be used if necessary to provide a clean wettable surface.
- **333.3.2 Joint Clearance.** The clearance between surfaces to be joined by soldering or brazing shall be no larger than necessary to allow complete capillary distribution of the filler metal.
 - **333.3.3 Flux Removal.** Residual flux shall be removed.

335 ASSEMBLY AND ERECTION

335.1 Alignment

- (a) Piping Distortions. Any distortion of piping to bring it into alignment for joint assembly that introduces a detrimental strain in equipment or piping components is prohibited.
- (b) Cold Spring. Before assembling any joints to be cold sprung guides, supports, and anchors shall be examined for errors that might interfere with desired movement or lead to undesired movement. The gap or overlap of piping prior to assembly shall be checked against the drawing and corrected if necessary. Heating shall not be used to help in closing the gap because it defeats the purpose of cold springing.
- (c) Flanged Joints. Unless otherwise specified in the engineering design, flanged joints shall be aligned as described in (1) or (2), and (3).
- (1) Before bolting, mating gasket contact surfaces shall be aligned to each other within 1 mm in 200 mm ($\frac{1}{16}$ in./ft), measured across any diameter.
- (2) The flanged joint shall be capable of being bolted such that the gasket contact surfaces bear uniformly on the gasket.
- (3) Flange bolt holes shall be aligned within 3 mm ($\frac{1}{8}$ in.) maximum offset.

335.2 Flanged Joints

335.2.1 Preparation for Assembly. Any damage to the gasket seating surface that would prevent gasket seating shall be repaired, or the flange shall be replaced.

335.2.2 Bolting Torque

- (a) In assembling flanged joints, the gasket shall be uniformly compressed to the proper design loading.
- (b) Special care shall be used in assembling flanged joints in which the flanges have widely differing mechanical properties. Tightening to a predetermined torque is recommended.

GENERAL NOTE: Threads are ASME B1.1 straight threads.

Figure 335.3.3 Typical Threaded Joints Using Straight Threads

335.2.3 Bolt Length. Bolts shall extend through their nuts such that there is complete thread engagement for

335.2.4 Gaskets. No more than one gasket shall be used between contact faces in assembling a flanged joint.

335.2.5 Flanged Joint Assembly. Assembly requirements for bolted flanged joints and flanged joint assembler qualifications shall be considered in the engineering design. For guidance, see ASME PCC-1, Guidelines for Pressure Boundary Bolted Flange Joint Assembly, and ASME BPVC, Section VIII, Division 1, Nonmandatory Appendix S.

335.3 Threaded Joints

the full depth of the nut.

(18) **335.3.1 Thread Compound or Lubricant.** Any compound or lubricant used on threads shall be suitable for the service temperatures and shall not react unfavorably with either the service fluid or the piping material.

335.3.2 Joints for Seal Welding. A threaded joint to be seal welded shall be made up without thread compound. A joint containing thread compound that leaks during leak testing may be seal welded in accordance with para. 328.5.3 provided all compound is removed from exposed threads.

335.3.3 Straight Threaded Joints. Typical joints using straight threads, with sealing at a surface other than the threads, are shown in Figure 335.3.3, illustrations (a), (b), and (c). Care shall be taken to avoid distorting the seat when incorporating such joints into piping assemblies by welding, brazing, or bonding.

335.4 Tubing Joints

335.4.1 Flared Tubing Joints. The sealing surface of the flare shall be examined for imperfections before assembly and any flare having imperfections shall be rejected.

335.4.2 Flareless and Compression Tubing Joints. Where the manufacturer's instructions call for a specified number of turns of the nut, these shall be counted from the point at which the nut becomes finger tight.

335.5 Caulked Joints

Caulked joints shall be installed and assembled in accordance with the manufacturer's instructions, as modified by the engineering design. Care shall be taken to ensure adequate engagement of joint members.

335.6 Expanded Joints and Special Joints

335.6.1 General. Expanded joints and special joints (as defined in para. 318) shall be installed and assembled in accordance with the manufacturer's instructions, as modified by the engineering design. Care shall be taken to ensure adequate engagement of joint members.

335.6.2 Packed Joints. Where a packed joint is used to absorb thermal expansion, proper clearance shall be provided at the bottom of the socket to permit this movement.

335.9 Cleaning of Piping

This Code does not prescribe mandatory procedures for flushing and cleaning. However, for potential hazards that may result from performing such procedures refer to Appendix F, para. F335.9 for precautionary considerations.

335.10 Identification of Piping

See Appendix F, para. F335.10.

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Chapter VI Inspection, Examination, and Testing

340 INSPECTION

340.1 General

This Code distinguishes between examination (see para. 341) and inspection. Inspection applies to functions performed for the owner by the owner's Inspector or the Inspector's delegates. References in this Code to the "Inspector" are to the owner's Inspector or the Inspector's delegates.

340.2 Responsibility for Inspection

It is the owner's responsibility, exercised through the owner's Inspector, to verify that all required examinations and testing have been completed and to inspect the piping to the extent necessary to be satisfied that it conforms to all applicable examination requirements of the Code and of the engineering design.

340.3 Rights of the Owner's Inspector

The owner's Inspector and the Inspector's delegates shall have access to any place where work concerned with the piping installation is being performed. This includes manufacture, fabrication, heat treatment, assembly, erection, examination, and testing of the piping. They shall have the right to audit any examination, to inspect the piping using any examination method specified by the engineering design, and to review all certifications and records necessary to satisfy the owner's responsibility stated in para. 340.2.

(18) 340.4 Qualifications of the Owner's Inspector

- (a) The owner's Inspector shall be designated by the owner and shall be the owner, an employee of the owner, an employee of an engineering or scientific organization, or the employee of a recognized insurance or inspection company acting as the owner's agent. The owner's Inspector shall not represent nor be an employee of the piping manufacturer, fabricator, or erector unless the owner is also the manufacturer, fabricator, or erector.
- (b) The owner's Inspector shall meet one of the following requirements:
- (1) have at least 10 years of experience in the design, fabrication, or examination of industrial pressure piping. Each 20% of satisfactorily completed work toward an

accredited engineering degree shall be considered equivalent to 1 year of experience, up to 5 years total.

- (2) have a professional engineering registration or nationally recognized equivalent with at least 5 years of experience in the design, fabrication, or examination of industrial pressure piping.
- (3) be a certified welding inspector or a senior certified welding inspector as defined in AWS QC1, Specification for AWS Certification of Welding Inspectors, or nationally recognized equivalent with at least 5 years of experience in the design, fabrication, or examination of industrial pressure piping.
- (4) be an authorized piping inspector as defined in API 570. Piping Inspection Code: In-service Inspection, Rating, Repair, and Alteration of Piping Systems, with at least 5 years of experience in the design, fabrication, or examination of industrial pressure piping.
- (c) In delegating performance of inspection, the owner's Inspector is responsible for determining that a person to whom an inspection function is delegated is qualified to perform that function.

341 EXAMINATION

341.1 General

Examination applies to quality control functions performed by the manufacturer (for components only), fabricator, or erector. Reference in this Code to an examiner is to a person who performs quality control examinations.

341.2 Responsibility for Examination

Inspection does not relieve the manufacturer, the fabricator, or the erector of the responsibility for

- (a) providing materials, components, and workmanship in accordance with the requirements of this Code and of the engineering design [see para. 300(b)(3)]
 - (b) performing all required examinations
- (c) preparing suitable records of examinations and tests for the Inspector's use

341.3 Examination Requirements

341.3.1 General. Prior to initial operation, each piping installation, including components and workmanship, shall be examined in accordance with the applicable

requirements of para. 341. The type and extent of any additional examination required by the engineering design, and the acceptance criteria to be applied, shall be specified. Joints not included in examinations required by para. 341.4 or by the engineering design are accepted if they pass the leak test required by para. 345.

- (a) For P-Nos. 3, 4, 5A, 5B, 5C, and 15E materials, examinations shall be performed after completion of heat treatment. However, examinations need not be repeated on welds or portions of welds that are subjected to additional heat treatments and have not been repaired by welding.
- (b) For a welded branch connection, the examination of, and any necessary repairs to, the pressure-containing weld shall be completed before any reinforcing pad or saddle is added.
- **341.3.2 Acceptance Criteria.** Acceptance criteria shall be as stated in the engineering design and shall at least meet the applicable requirements stated below.
- (a) Welds. See Figure 341.3.2 for typical weld imperfections.
 - (1) For radiography and visual, see Table 341.3.2.
 - (2) For magnetic particle, see para. 344.3.2.
 - (3) For liquid penetrant, see para. 344.4.2.
 - (4) For ultrasonic, see para. 344.6.2.
- (b) Castings. Acceptance criteria for castings are specified in para. 302.3.3.

341.3.3 Defective Components and Workmanship.

Defects (imperfections of a type or magnitude not acceptable by the criteria specified in para. 341.3.2) shall be repaired, or the defective item or work shall be replaced. Discontinuities detected outside the area required to be examined during weld joint examinations should be evaluated and resolved in a manner acceptable to the owner and designer.

Examination shall be as follows:

- (a) When the defective item or work is repaired, the repaired portion of the item or work shall be examined. The examination shall use the same methods and acceptance criteria employed for the original examination. See also para, 341.3.1(a).
- (b) When the defective item or work is replaced, the new item or work used to replace the defective item or work shall be examined. The examination shall use any method and applicable acceptance criteria that meet the requirements for the original examination. See also para. 341.3.1(a).
- **341.3.4 Progressive Sampling for Examination.** When required spot or random examination reveals a defect, then
- (a) two additional samples of the same kind (if welded or bonded joints, by the same welder, bonder, or operator) from the original designated lot shall be given the same type of examination

- (b) if the items examined as required by (a) above are acceptable, the defective item shall be repaired or replaced and reexamined as specified in para. 341.3.3, and all items represented by these two additional samples shall be accepted, but
- (c) if any of the items examined as required by (a) above reveals a defect, two further samples of the same kind shall be examined for each defective item found by that sampling
- (d) if all the items examined as required by (c) above are acceptable, the defective item(s) shall be repaired or replaced and reexamined as specified in para. 3.1.3.3, and all items represented by the additional sampling shall be accepted, but
- (e) if any of the items examined as required by (c) above reveals a defect, all items represented by the progressive sampling shall be either
- (1) repaired or replaced and reexamined as required, or
- (2) fully examined and repaired or replaced as necessary, and reexamined as necessary to meet the requirements of this Code
- (f) If any of the defective items are repaired or replaced, reexamined, and a defect is again detected in the repaired or replaced item, continued progressive sampling in accordance with (a), (c), and (e) is not required based on the new defects found. The defective item(s) shall be repaired or replaced and reexamined until acceptance as specified in para. 341.3.3. Spot or random examination (whichever is applicable) is then performed on the remaining unexamined joints.

341.4 Extent of Required Examination

- **341.4.1 Examination Normal Fluid Service.** Piping (18) in Normal Fluid Service shall be examined to the extent specified herein or to any greater extent specified in the engineering design. Acceptance criteria are as stated in para. **341.3.2** and in Table **341.3.2**, for Normal Fluid Service unless otherwise specified.
- (a) Visual Examination. At least the following shall be examined in accordance with para. 344.2:
- (1) sufficient materials and components, selected at random, to satisfy the examiner that they conform to specifications and are free from defects.
- (2) at least 5% of fabrication, as defined in para. 300.2.
- (3) 100% of all completed welds, except those in components made in accordance with a listed standard. See para. 341.5.1(a) for examination of longitudinal welds required to have a joint factor, E_j , of 0.90.
- (4) random examination of the assembly of threaded, bolted, and other joints to satisfy the examiner that they conform to the applicable requirements of para. 335. When pneumatic testing is to be performed, all threaded, bolted, and other mechanical joints shall be examined.

Figure 341.3.2 Typical Weld Imperfections

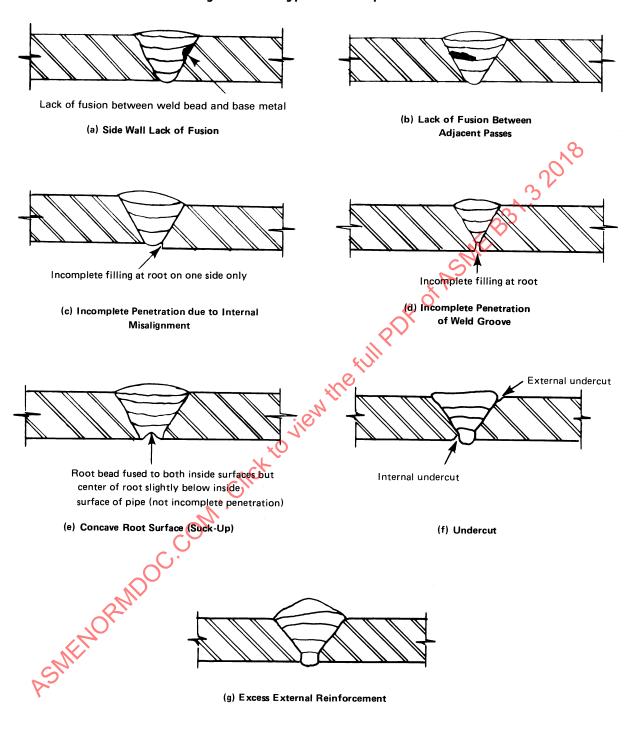


Table 341.3.2 Acceptance Criteria for Welds — Visual and Radiographic Examination

		Criteria (A t	to M) for Type:	Criteria (A to M) for Types of Welds and for Service Conditions [Note (1)]	for Service	Condition	IS [Note (1)]					
Normal	Normal and Category M Fluid	1 Fluid										
	Service	-	Sever	Severe Cyclic Conditions	ous		Category D	Category D Fluid Service	je.		Examin	Examination Methods
Girth, Miter		Sk	Girth, Miter									
Groove, and			Groove, and			Girth						
Branch	Longitudinal		Branch			and			Branch			
Connection Welds	Groove Weld	Fillet Weld	Connection Welds	Longitudinal Groove Weld	Fillet Weld	Miter Groove	Longitudinal Groove Weld	Fillet Weld	Connection Weld			
[Note (2)]	[Note (3)]	[Note (4)]	[Note (2)]	/ [Note (3)]	[Note (4)]	Welds	[Note (3)]	[Note (4)]	[Note (2)]	Weld Imperfection	Visual	Radiography
А	A	A	A	A	A	А	A	A	A	Crack	1	>
A	А	A	А	O A	А	C	A	N/A	A	Lack of fusion	>	`>
В	А	N/A	А	Q V	N/A	C	А	N/A	В	Incomplete penetration	>	`>
ш	丑	N/A	D	<u> </u>	N/A	N/A	N/A	N/A	N/A	Rounded Indications	:	`>
G	G	N/A	ĽL,	<u>.</u>	NA	N/A	N/A	N/A	N/A	Linear indications	:	`>
Н	А	Н	А	A	N	I	А	Н	Н	Undercutting	>	`>
A	А	А	А	А	A	Α .	А	А	А	Surface porosity or exposed slag inclusion [Note (5)]	`>	i
N/A	N/A	N/A	J	l l		NA	N/A	N/A	N/A	Surface finish	>	÷
Ж	K	N/A	Ж	K	N/A	×0	K	N/A	К	Concave surface, concave root, or burn-through	`>	>
Г	Г	LI.	T	ı	7	Σ	is of	×	Σ	Weld reinforcement or internal protrusion	`>	i

GENERAL NOTES:

- (a) Weld imperfections are evaluated by one or more of the types of examination methods given, as apecified in paras. 341.4.1, 341.4.2, 341.4.3, and M341.4, or by the engineering design. "N/A" indicates the Code does not establish acceptance criteria or does not require evaluation or this kind of imperfection for this type of weld.

 - (b) "N/A" indicates the Code does not establish acceptance criteria or does not require evaluation of this kind o
 (c) Check (✓) indicates examination method generally used for evaluating this kind of weld imperfection (d) Ellipsis (...) indicates examination method not generally used for evaluating this kind of weld imperfection.

- Longitudinal groove weld includes straight and spiral (helical) seam. Criteria are not intended to apply to welds made includes with a standard listed in Table A-1, Table A-1M, or i) Criteria given are for required examination. More συν τος 1.
 i) Criteria given are for required examination. More συν τος 1.
 i) Criteria given are for required examination woulds in branches συν τος 1.
 i) Longitudinal groove weld includes straight and spiral (helical) seam. Criteria are not intendeu τος 1.
 i) Longitudinal groove weld includes straight and spiral (helical) seam. Griteria are not intendeu. συν τος 1.
 i) These imperfections are evaluated only for welds ≤5 mm (³/₁₆ in.) in nominal thickness.
 i) These imperfections are evaluated only for welds ≤5 mm (³/₁₆ in.) in nominal thickness.

Criterion Value Notes for Table 341.3.2

(18)

	Criterion	
Symbol	Measure Measure	Acceptable Value Limits [Note (1)]
A	Extent of imperfection	Zero (no evident imperfection)
В	Cumulative length of Incomplete penetration	<38 mm (1.5 in.) in any 150 mm (6 in.) weld length or 25% of total weld length, whichever is less
C	Cumulative length of lack of fusion and incomplete penetration	<38 mm (1.5 in.) in any 150 mm (6 in.) weld length or 25% of total weld length, whichever is less
D	Size and distribution of rounded indications	See ASME BPVC, Section VIII, Division 1, Appendix 4 [Note (2)]
н	Size and distribution of rounded indigations	For $\overline{T}_{\nu} \le 6 \text{mm} \left(\frac{1}{4} \text{in.} \right)$, limit is same as D [Note (2)] For $\overline{T}_{\nu} > 6 \text{mm} \left(\frac{1}{4} \text{in.} \right)$, limit is 1.5 × D [Note (2)]
Ľ	Linear indications	
	Individual length	$\leq \overline{T}_{w}/3$
	Individual width	$\leq 2.5 \text{ mm } (^3/_{32} \text{ in.}) \text{ and } \leq \overline{T}_{w}/3$
	Cumulative length	$\leq \overline{T}_{w}$ in any 12 \overline{T}_{w} weld length [Note (2)]
Ð	Linear indications	
	Individual length	$\leq 2 \overline{T}_{w}$
	Individual width	$<$ 3 mm ($\frac{1}{8}$ in.) and $\leq \overline{T}_w/2$
	Cumulative length	$\mathcal{S}_{\text{A} \leq 4\overline{T}_{\text{w}}}$ in any 150 mm (6 in.) weld length [Note (2)]
Н	Depth of undercut	≤ 1 mm ($\frac{1}{32}$ in.) and $\leq \overline{T}_{W}/4$
	Cumulative length of internal and external undercut	<38 mm (1.5 in.) in any 150 mm (6 in.) weld length or 25% of total weld length, whichever is less
П	Depth of undercut	$\leq 1.5 \text{ mm} \left(\frac{7}{16} \text{ id.} \right) \text{ and } \leq \left[\overline{T}_w / 4 \text{ or } 1 \text{ mm} \left(\frac{1}{32} \text{ in.} \right) \right]$
	Cumulative length of internal and external undercut	<38 mm (1.5 in) m any 150 mm (6 in.) weld length or 25% of total weld length, whichever is less
ſ	Surface roughness	<12.5 μm (500 μin.) 🗞 jn accordance with ASME B46.1
Ж	Depth of surface concavity, root concavity, or burn-through	Total joint thickness, including weld reinforcement, $\geq \overline{T}_{\mu}$ [Notes (3) and (4)]
П		For $\overline{T}_{\mu\nu}$ mm (in.)
	any plane through the weld shall be within limits of the amplicable height value in the tabulation at right.	\$\(\lambde
	except as provided in Note (6). Weld metal shall merge	22
	smoothly into the component surfaces.), <25 (1)
		>25 (1)
Σ	Height of reinforcement or internal protrusion [Note (5)] as described in L. Note (6) does not apply.	Limit is twice the value applicable for L above
		Ď

NOTES:
(1) Where two limiting values are separated by "and," the lesser of the values determines acceptance. Where two sets of values are separated by "or," the larger value is acceptable. T_{iv} is the nominal wall thickness of the thinner of two components joined by a butt weld.

Criterion Value Notes for Table 341.3.2 (Cont'd)

NOTES: (Cont'd)

- (2) Porosity and inclusions such as slag or tungsten are defined as rounded indications where the maximum length is three times the width or less. These indications may be circular, elliptical, or irregular in shape; may have tails and may vary in density. Indications where the length is greater than three times the width are defined as linear indications and may also be slag, porosity, or
- For circumferential groove welded joints (hope, and headers made entirely without the addition of filler metal, external concavity shall not exceed the lesser of 1 mm (1/32 in.) or 10% of the oint nominal thickness. The contour of the concavity shall blend smoothly with the base metal. The total joint thickness, including any reinforcement, shall not be less than the minimum wall thickness, t_m. 3
 - For radiography, acceptability may be determined by comparing the density of the image through the affected area to the density through the adjacent base metal (\overline{T}_{μ}). If digital radiography is used, brightness comparison may be utilized. A density or brightness darker than the adjacent base metal is cause for rejection. 4
 - For groove welds, height is the lesser of the measurements, made from the surfaces of the adjacent components; both reinforcement and internal protrusion are permitted in a weld. For fillet welds, height is measured from the theoretical throat, Figure 328.5.2A; internal protrusion does not apply. (2)
 - (6) For welds in aluminum alloy only, internal protrusion shall hot exceed the following values:
 - (a) 1.5 mm ($\frac{1}{16}$ in.) for thickness ≤ 2 mm ($\frac{5}{64}$ in.)
- (b) 2.5 mm ($^{3}_{32}$ in.) for thickness >2 mm and <6 mm ($^{1}_{4}$ in.) For external reinforcement and for greater thicknesses, see the tabulation for symbol L.

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- (5) random examination during erection of piping, including checking of alignment, supports, and cold spring.
- (6) examination of erected piping for evidence of defects that would require repair or replacement, and for other evident deviations from the intent of the design.
 - (b) Other Examination
- (1) Not less than 5% of circumferential butt and miter groove welds shall be examined fully by random radiography in accordance with para. 344.5 or by random ultrasonic examination in accordance with para. 344.6. The welds to be examined in each designated lot shall include the work product of each welder or welding operator whose welds are part of the lot. The work of welders depositing only tack welds need not be represented as part of the lot. Welds shall also be selected to maximize coverage of intersections with longitudinal joints. When a circumferential weld with an intersecting longitudinal weld(s) is examined, at least the adjacent 38 mm ($1\frac{1}{2}$ in.) of each intersecting weld shall be examined. In-process examination in accordance with para. 344.7 may be substituted for all or part of the radiographic or ultrasonic examination on a weld-forweld basis if specified in the engineering design or specifically authorized by the Inspector.
- (2) Not less than 5% of all brazed joints shall be examined by in-process examination in accordance with para. 344.7, the joints to be examined being selected to ensure that the work of each brazer making the production joints is included.
- (c) Certifications and Records. The examiner shall be assured, by examination of certifications, records, and other evidence, that the materials and components are of the specified grades and that they have received required heat treatment, examination, and testing. The examiner shall provide the Inspector with a certification that all the quality control requirements of the Code and of the engineering design have been carried out.

341.4.2 Examination Category D Fluid Service. Piping and piping elements for Category D Fluid Service as designated in the engineering design shall be visually examined in accordance with para. 344.2 to the extent necessary to satisfy the examiner that components, materials, and workmanship conform to the requirements of this Code and the engineering design. Acceptance criteria are as stated in para. 341.3.2 and in Table 341.3.2, for Category D fluid service, unless otherwise specified.

341.4.3 Examination — **Severe Cyclic Conditions.** Piping to be used under severe cyclic conditions shall be examined to the extent specified herein or to any greater extent specified in the engineering design. Acceptance criteria are as stated in para. 341.3.2 and in Table 341.3.2, for severe cyclic conditions, unless otherwise specified.

- (a) Visual Examination. The requirements of para. 341.4.1(a) apply with the following exceptions:
 - (1) All fabrication shall be examined.
- (2) All threaded, bolted, and other joints shall be examined.
- (3) All piping erection shall be examined to verify dimensions and alignment. Supports, guides, and points of cold spring shall be checked to ensure that movement of the piping under all conditions of startup, operation, and shutdown will be accommodated without undue binding or unanticipated constraint.
- (b) Other Examination. All circumferential butt and miter groove welds and all fabricated branch connection welds comparable to those shown in Figure 328.5.4E shall be examined by 100% radiography in accordance with para. 344.5, or (if specified in the engineering design) by 100% ultrasonic examination in accordance with para. 344.6. Socket welds and branch connection welds that are not radiographed shall be examined by magnetic particle or liquid penetrant methods in accordance with para. 344.3 or 344.4.
- (c) In-process examination in accordance with para. 3447 supplemented by appropriate nondestructive examination, may be substituted for the examination required in (b) above on a weld-for-weld basis if specified in the engineering design or specifically authorized by the Inspector.
- (d) Certification and Records. The requirements of para. 341.4.1(c) apply.
- **341.4.4 Examination Elevated Temperature Fluid Service.** Piping in Elevated Temperature Fluid Service shall be examined to the extent specified herein or to any greater extent specified in the engineering design. Acceptance criteria are as stated in para. **341.3.2** and in Table **341.3.2**, for Normal Fluid Service, unless the requirements for severe cyclic conditions apply or otherwise specified.
- (a) Visual Examination. The requirements of para. 341.4.1(a) apply with the following exceptions:
 - (1) All fabrication shall be examined.
- (2) All threaded, bolted, and other joints shall be examined.
- (3) All piping erection shall be examined to verify dimensions and alignment. Supports, guides, and points of cold spring shall be checked to ensure that movement of the piping under all conditions of startup, operation, and shutdown will be accommodated without undue binding or unanticipated constraint.
- (b) Additional Examination. The examination requirements of para. 341.4.1(b) apply with the following exceptions:
- (1) Fabrication for longitudinal and spiral (helical seam) welds in P-No. 4 and P-No. 5 materials, except those in components made in accordance with a listed specification, shall be examined by 100% radiography

in accordance with para. 344.5, or by 100% ultrasonic examination in accordance with para. 344.6.

- (2) Socket welds and branch connection welds in P-No. 4 and P-No. 5 materials that are not radiographed or ultrasonically examined shall be examined by magnetic particle or liquid penetrant methods in accordance with para. 344.3 or 344.4.
- (c) Additional Examination Required for Autogenous Welds, Without Filler Metal, in Austenitic Stainless Steel and Austenitic High Nickel Alloys. Autogenously welded pipe shall receive nondestructive examination in accordance with the material specification. Autogenously welded expansion joint bellows shall be examined in accordance with para. X302.2.2(c).
- (d) Certification and Records. The requirements of para. 341.4.1(c) apply.

341.5 Supplementary Examination

Any of the methods of examination described in para. 344 may be specified by the engineering design to supplement the examination required by para. 341.4. The extent of supplementary examination to be performed and any acceptance criteria that differ from those in para. 341.3.2 shall be specified in the engineering design.

341.5.1 Spot Radiography

- (a) Longitudinal Welds. Spot radiography for longitudinal groove welds required to have a weld joint factor E_j of 0.90 requires examination by radiography in accordance with para. 344.5 of at least 300 mm (1 ft) in each 30 m (100 ft) of weld for each welder or welding operator. Acceptance criteria are those stated in Table 341.3.2 for radiography under Normal Fluid Service.
- (b) Circumferential Butt Welds and Other Welds. It is recommended that the extent of examination be not less than one shot on one in each 20 welds for each welder or welding operator. Unless otherwise specified, acceptance criteria are as stated in Table 341.3.2 for radiography under Normal Fluid Service for the type of joint examined.
- (c) Progressive Sampling for Examination. The provisions of para. 341/3.4 are applicable.
- (d) Welds to Be Examined. The locations of welds and the points at which they are to be examined by spot radiography shall be selected or approved by the Inspector.
- **341.5.2 Hardness Tests.** Hardness tests are not required to verify proper heat treatment except as otherwise specified in the engineering design.
- **341.5.3 Examinations to Resolve Uncertainty.** Any method may be used to resolve doubtful indications. Acceptance criteria shall be those for the required examination.

342 EXAMINATION PERSONNEL

342.1 Personnel Qualification and Certification

Personnel performing nondestructive examination to the requirements of this Code shall be qualified and certified for the method to be utilized following a procedure as described in ASME BPVC, Section V, Article 1, T-120(e) or (f).

342.2 Specific Requirement

For in-process examination, the examinations shall be performed by personnel other than those performing the production work.

343 EXAMINATION PROCEDURES

Any examination shall be performed in accordance with a written procedure that conforms to one of the methods specified in para. 344, including special methods (see para. 344.1.2). Procedures shall be written as required in ASME BPVC, Section V, Article 1, T-150. The employer shall make the examination procedures employed available to the Inspector.

344 TYPES OF EXAMINATION

344.1 General

- **344.1.1 Methods.** Except as provided in para. 344.1.2, any examination required by this Code, by the engineering design, or by the Inspector shall be performed in accordance with one of the methods specified herein.
- **344.1.2 Special Methods.** If a method not specified herein is to be used, it and its acceptance criteria shall be specified in the engineering design in enough detail to permit qualification of the necessary procedures and examiners.
- **344.1.3 Definitions.** The following terms apply to any type of examination:

100% examination: complete examination of all of a specified kind of item in a designated lot of piping¹

random examination²: complete examination of a percentage of a specified kind of item in a designated lot of piping¹

¹ A designated lot is that quantity of piping to be considered in applying the requirements for examination in this Code. The quantity or extent of a designated lot should be established by agreement between the contracting parties before the start of work. More than one kind of designated lot may be established for different kinds of piping work. See Pipe Fabrication Institute Standard ES-48, Random Examination, for examples of lot selection.

² Random or spot examination will not ensure a fabrication product of a prescribed quality level throughout. Items not examined in a lot of piping represented by such examination may contain defects that further examination could disclose. Specifically, if all radiographically disclosable weld defects must be eliminated from a lot of piping, 100% radiographic examination must be specified.

spot examination²: a specified partial examination of each of a specified kind of item in a designated lot of piping,¹ e.g., of part of the length of all shop-fabricated welds in a lot of jacketed piping

random spot examination²: a specified partial examination of a percentage of a specified kind of item in a designated lot of piping¹

344.2 Visual Examination

- observation of the external and internal portions of components, joints, and other piping elements that are readily accessible or can be exposed to view before, during, or after manufacture, fabrication, assembly, erection, examination, or testing. This examination includes verification of Code and engineering design requirements for materials, components, dimensions, joint preparation, alignment, welding, bonding, brazing, bolting, threading, or other joining method, supports, assembly, and erection.
- (18) **344.2.2 Method.** Visual examination shall be performed in accordance with ASME BPVC, Section V, Article 9. Examination shall be by the direct visual technique. The use of a remote visual technique and the acceptance criteria beyond the requirements of this Code shall be a matter of agreement between contracting parties prior to the start of fabrication.

Records of individual visual examinations are not required except for those of in-process examinations as specified in para. 344.7.

344.3 Magnetic Particle Examination

- **344.3.1 Method.** Examination of castings is covered in para. 302.3.3. Magnetic particle examination of welds and of components other than castings shall be performed in accordance with ASME BPVC, Section V, Article 7.
- **344.3.2 Acceptance Criteria.** Magnetic particle indications are caused by the attraction of the test media to surface or near-surface discontinuities in the area under test. However, all such indications are not necessarily imperfections, since excessive roughness, magnetic permeability variations, etc., may produce nonrelevant indications. Inadvertent accumulation of particles not related to magnetic attraction is classified as a false indication. Indications shall be verified as being relevant, nonrelevant, or false. Additional surface preparation and/or other test methods may be used as needed to verify the relevance of an indication.

An indication of an imperfection may be larger than the imperfection that causes it; however, the size of the indication is the basis for acceptance evaluation. Only indications that have any dimension greater than 1.5 mm ($^{1}/_{16}$ in.) shall be considered relevant.

(a) Indications

- (1) A linear indication is one having a length greater than three times its width.
- (2) A rounded indication is one of circular or elliptical shape with a length equal to or less than three times its width.
- (b) Examination. All surfaces to be examined shall be free of
 - (1) relevant linear indications
 - (2) relevant rounded indications >5.0 mm ($\frac{3}{16}$ in.)
- (3) four or more relevant rounded indications in a line separated by 1.5 mm ($\frac{1}{16}$ in.) or less, edge to edge

344.4 Liquid Penetrant Examination

- **344.4.1 Method.** Examination of castings is covered in para. 302.3.3. Liquid penetrant examination of welds and of components other than castings shall be performed in accordance with ASME BRVC, Section V, Article 6.
- **344.4.2 Acceptance Oriteria.** Liquid penetrant indications are caused by the bleed-out of a visible or fluorescent dye from a surface discontinuity in the area under test. However, all such indications are not necessarily imperfections, since excessive roughness, poor surface preparation, etc., may produce nonrelevant indications. Inadvertent evidence of penetrant not related to actual bleed-out is classified as a false indication. Indications shall be verified as being relevant, nonrelevant, or false. Additional surface preparation and/or other test methods may be used as needed to verify the relevance of an indication.

An indication of an imperfection may be larger than the imperfection that causes it; however, the size of the indication is the basis for acceptance evaluation. Only indications that have any dimension greater than 1.5 mm ($\frac{1}{16}$ in.) shall be considered relevant.

- (a) Indications
- (1) A linear indication is one having a length greater than three times its width.
- (2) A rounded indication is one of circular or elliptical shape with a length equal to or less than three times its width.
- (b) Examination. All surfaces to be examined shall be free of
 - (1) relevant linear indications
 - (2) relevant rounded indications >5.0 mm ($\frac{3}{16}$ in.)
- (3) four or more relevant rounded indications in a line separated by 1.5 mm ($\frac{1}{16}$ in.) or less, edge to edge

344.5 Radiographic Examination

344.5.1 Method. Radiography of castings is covered in (18) para. 302.3.3. Radiography of welds and of components other than castings shall be performed in accordance with ASME BPVC, Section V, Article 2. For the purpose of image quality indicator (IQI) selection, for welds with reinforcement, the thickness used shall be the nominal wall

thickness, \overline{T}_{w} plus the allowable external reinforcement and internal reinforcement (protrusion) combined.

344.5.2 Extent of Radiography

- (a) 100% Radiography. This applies only to girth and miter groove welds and to fabricated branch connection welds comparable to Figure 328.5.4E, unless otherwise specified in the engineering design.
- (b) Random Radiography. This applies only to girth and miter groove welds.
- (c) Spot Radiography. This requires a single exposure radiograph in accordance with para. 344.5.1 at a point within a specified extent of welding. For girth, miter, and branch groove welds, the minimum requirement is
- (1) for sizes \leq DN 65 (NPS $2^{1}/_{2}$), a single elliptical exposure encompassing the entire weld circumference
- (2) for sizes >DN 65, the lesser of 25% of the inside circumference or 152 mm (6 in.)

For longitudinal welds, the minimum requirement is 152 mm (6 in.) of weld length.

344.6 Ultrasonic Examination

- **344.6.1 Method.** Examination of castings is covered in para. 302.3.3; other product forms are not covered. Ultrasonic examination of welds shall be performed in accordance with ASME BPVC, Section V, Article 4, except that the alternative specified in (a) and (b) below is permitted for basic calibration blocks specified in T-434.2.1 and T-434.3.
- (a) When the basic calibration blocks have not received heat treatment in accordance with T-434.1.5, transfer methods shall be used to correlate the responses from the basic calibration block and the component. Transfer is accomplished by noting the difference between responses received from the same reference reflector in the basic calibration block and in the component and correcting for the difference.
- (b) The reference reflector may be a V-notch (which must subsequently be removed), an angle beam search unit acting as a reflector or any other reflector that will aid in accomplishing the transfer.
- (c) When the transfer method is chosen as an alternative, it shall be used, at the minimum
- (1) for sizes ≥DN 50 (NPS 2), once in each ten welded joints examined
- (2) for sizes >DN 50 and ≤DN 450 (NPS 18), once in each 1.5 m (5 ft) of welding examined
- (3) for sizes >DN 450, once for each welded joint examined
- (d) Each type of material and each size and wall thickness shall be considered separately in applying the transfer method. In addition, the transfer method shall be used at least twice on each type of weld joint.

- (e) The reference level for monitoring discontinuities shall be modified to reflect the transfer correction when the transfer method is used.
- **344.6.2 Acceptance Criteria.** Acceptance criteria shall (18) be as described in (a) or (b).
- (a) A linear-type discontinuity is unacceptable if the amplitude of the indication exceeds the reference level and its length exceeds
 - (1) 6 mm ($\frac{1}{4}$ in.) for $\overline{T}_w \le 19 \text{ mm} (\frac{3}{4} \text{ in.})$
 - (2) $\overline{T}_w/3$ for 19 mm ($^{3}/_{4}$ in.) $<\overline{T}_w \le 57$ mm ($^{2}/_{4}$ in.)
 - (3) 19 mm ($\frac{3}{4}$ in.) for $\overline{T}_w > 57$ mm ($2^{\frac{1}{4}}$ in.)
- (b) The fracture-mechanics-based ultrasonic examination acceptance criteria in Appendix R may be used if all requirements of Appendix R are met.

344.7 In-Process Examination

- **344.7.1 Definition.** In-process examination comprises examination of the following, as applicable:
 - (a) joint preparation and cleanliness
 - (b) preheating
- (c) fit-up, joint clearance, and internal alignment prior to joining
- (d) variables specified by the joining procedure, including filler material
 - (for welding) position and electrode
- (2) (for brazing) position, flux, brazing temperature, proper wetting, and capillary action
- (e) (for welding) condition of the root pass after cleaning external and, where accessible, internal aided by liquid penetrant or magnetic particle examination when specified in the engineering design
- (f) (for welding) slag removal and weld condition between passes
 - (g) appearance of the finished joint
- **344.7.2 Method.** The examination is visual, in accordance with para. 344.2, unless additional methods are specified in the engineering design.

345 TESTING

345.1 Required Leak Test

Prior to initial operation, and after completion of the applicable examinations required by para. 341, each piping system shall be tested to ensure tightness. The test shall be a hydrostatic leak test in accordance with para. 345.4 except as provided herein.

- (a) At the owner's option, a piping system in Category D fluid service may be subjected to an initial service leak test in accordance with para. 345.7, in lieu of the hydrostatic leak test.
- (b) Where the owner considers a hydrostatic leak test impracticable, either a pneumatic test in accordance with para. 345.5 or a combined hydrostatic-pneumatic test in

accordance with para. 345.6 may be substituted, recognizing the hazard of energy stored in compressed gas.

- (c) Where the owner considers both hydrostatic and pneumatic leak testing impracticable, the alternative specified in para. 345.9 may be used if both of the following conditions apply:
 - (1) a hydrostatic test would
 - (a) damage linings or internal insulation
- (b) contaminate a process that would be hazardous, corrosive, or inoperative in the presence of moisture
- (c) require significant support modifications for the hydrostatic test load or
- (d) present the danger of brittle fracture due to low metal temperature during the test
 - (2) a pneumatic test would
- (a) present an undue hazard of possible release of energy stored in the system or
- (b) present the danger of brittle fracture due to low metal temperature during the test
- (d) Unless specified in the engineering design, lines open to the atmosphere, such as vents or drains downstream of the last shutoff valve, need not be leak tested.

345.2 General Requirements for Leak Tests

Requirements in para. 345.2 apply to more than one type of leak test.

(18) **345.2.1 Limitations on Pressure**

- (a) Reduced Test Pressure. If the test pressure would produce a circumferential or longitudinal stress (based on minimum pipe wall thickness) in excess of yield strength at test temperature or is greater than 1.5 times the component rating at test temperature, the test pressure may be reduced to the maximum pressure that will not exceed the lesser of the yield strength or 1.5 times a component rating at test temperature. [See para. 302.3.2.] For metallic bellows expansion joints, see Appendix X, para. X302.2.3(a).
- (b) Test Fluid Expansion. If a pressure test is to be maintained for a period of time and the test fluid in the system is subject to thermal expansion, precautions shall be taken to avoid excessive pressure.
- (c) Preliminary Pneumatic Test. A preliminary test using air at no more than 170 kPa (25 psi) gage pressure may be made prior to hydrostatic testing to locate major leaks.

345.2.2 Other Test Requirements

- (a) Examination for Leaks. The leak test pressure shall be maintained for at least 10 min and then all joints and connections shall be examined for leaks. The test pressure may be reduced to not less than the design pressure while performing this examination.
- *(b) Heat Treatment.* Leak tests shall be conducted after any heat treatment has been completed.

(c) Low Test Temperature. The possibility of brittle fracture shall be considered when conducting leak tests at metal temperatures near the ductile-brittle transition temperature.

345.2.3 Special Provisions for Testing

- (a) Piping Components and Subassemblies. Piping components and subassemblies may be tested either separately or as assembled piping.
- (b) Flanged Joints. Flanged joints used to connect piping components and subassemblies that have previously been tested, and flanged joints at which a blank or blind is used to isolate equipment or other piping during a test, need not be leak tested in accordance with para. 345.1.
- (c) Closure Welds. The final weld connecting piping systems or components that have been successfully tested in accordance with para. 345 need not be leak tested provided the weld is examined in-process in accordance with para. 344.7 and passes with 100% radiographic examination in accordance with para. 344.5 or 100% ultrasonic examination in accordance with para. 344.6.
- (d) Instrument Connections. Threaded joints, tubing joints, or a combination of these joints used to connect instruments to previously leak tested piping need not be leak tested in accordance with para. 345.1.
 - (e) See also Appendix F, para. F345.2.3.

345.2.4 Externally Pressured Piping

- (a) Except as provided in (b) below, piping systems subject to external pressure shall be tested at an internal gage pressure 1.5 times the external differential pressure, but not less than 105 kPa (15 psi).
- (b) As an alternative to leak testing under internal pressure, piping systems designed for vacuum service only may be subjected to a vacuum leak test method, technique, and acceptance criteria specified by the owner. The vacuum leak test shall be performed following a written procedure complying with the applicable technical requirements of ASME BPVC, Section V, Article 10. Leak-testing personnel shall be qualified and certified as required by ASME BPVC, Section V, Article 1, T-120(e) or (f).

345.2.5 Jacketed Piping (18)

- (a) The internal line shall be leak tested on the basis of the internal or external design pressure, whichever results in a higher test pressure. This test must be performed before the jacket is completed if it is necessary to provide visual access to joints of the internal line as required by para. 345.3.1.
- (b) The jacket shall be leak tested in accordance with para. 345.1 based on the jacket design conditions. The test pressure is permitted to be lower when so specified in the engineering design.

345.2.6 Repairs or Additions After Leak Testing. If repairs or additions are made following the leak test, the affected piping shall be retested, except that for minor repairs or additions the owner may waive retest requirements when precautionary measures are taken to assure sound construction.

345.2.7 Test Records. Records shall be made of each piping system during the testing, including

- (a) date of test
- (b) identification of piping system tested
- (c) test fluid
- (d) test pressure
- (e) certification of results by examiner

These records need not be retained after completion of the test if a certification by the Inspector that the piping has satisfactorily passed pressure testing as required by this Code is retained.

345.3 Preparation for Leak Test

345.3.1 Joints Exposed

- (a) Except as provided in (b) and (c) below, all joints, welds (including structural attachment welds to pressurecontaining components), and bonds shall be left uninsulated and exposed for examination during leak testing.
- (b) Joints previously tested in accordance with this Code may be insulated or covered.
- (c) At the owner's option, joints in Category D Fluid Service that are subject to a hydrostatic leak test 3345.4 Hydrostatic Leak Test (para. 345.4) or an initial service leak test (para. 345.7) may be insulated and have protective weather sheathing installed prior to leak testing. Consideration shall be given to increasing the test period to allow time for possible leakage to pass through the insulation and weather sheathing.
- (d) All joints may be primed and painted prior to leak testing unless a sensitive leak test (para. 345.8) is required.

345.3.2 Temporary Supports. Piping designed for vapor or gas shall be provided with additional temporary supports, if necessary, to support the weight of test liquid.

345.3.3 Piping With Expansion Joints

(a) Unrestrained expansion joints depend on external main anchors to resist pressure thrust forces. Except as limited in para. 345.3.3(c), a piping system containing unrestrained expansion joints shall be leak tested without any temporary restraints in accordance with para. 345 up to 150% of the expansion joint design pressure. If the required test pressure exceeds 150% of the expansion joint design pressure and the main anchors are not designed to resist the pressure thrust forces at the required test pressure, for that portion of the test when the pressure exceeds 150% of the expansion joint design pressure, the expansion joint shall either

be temporarily removed or temporary restraints shall be added to resist the pressure thrust forces.

- (b) Self-restrained metallic bellows expansion joints (i.e., tied, hinged, pressure balanced, etc.) have restraint hardware designed to resist the pressure thrust forces. Except as limited in para. 345.3.3(c), a piping system containing self-restrained expansion joints shall be leak tested in accordance with para. 345. A self-restrained expansion joint previously shop tested by the manufacturer in accordance with Appendix X may be excluded from the system to be leak tested, except when a sensitive leak test in accordance with para. 345.8 is required. Restraint hardware for all types of expansion joints shall be designed for the pressure thrust forces at the test pressure.
- (c) When a metallic bellows expansion joint is installed in the piping system subject to a leak test and the leak test pressure determined in accordance with para. 345 exceeds the pressure of the test performed by the manufacturer in accordance with Appendix X, the required leak test pressure shall be reduced to the manufacturer's test pressure.

345.3.4 Limits of Tested Piping. Equipment that is not to be tested shall be either disconnected from the piping or isolated by blinds or other means during the test. A valve may be used provided the valve (including its closure mechanism) is suitable for the test pressure.

345.4.1 Test Fluid. The fluid shall be water unless there is the possibility of damage due to freezing or to adverse effects of water on the piping or the process (see para, F345.4.1). In that case another suitable nontoxic liquid may be used. If the liquid is flammable, its flash point shall be at least 49°C (120°F), and consideration shall be given to the test environment.

345.4.2 Test Pressure. Except as provided in para. 345.4.3, the hydrostatic test pressure at every point in a metallic piping system shall be as follows:

- (a) not less than 1.5 times the design pressure.
- (b) when the design temperature is greater than the test temperature, the minimum test pressure, at the point under consideration, shall be calculated using eq. (24).

$$P_T = 1.5 \, PS_T / S \tag{24}$$

where

P = internal design gage pressure

 P_T = minimum test gage pressure

- S = allowable stress at component design temperature for the prevalent pipe material; see Table A-1 or Table A-1M
- S_T = allowable stress at test temperature for the prevalent pipe material; see Table A-1 or Table A-1M

(c) in those cases where the piping system may not include pipe itself, any other component in the piping system, other than pipe-supporting elements and bolting, may be used to determine the S_T/S ratio based on the applicable allowable stresses obtained from Table A-1 or Table A-1M. In those cases where the piping system may be made up of equivalent lengths of more than one material, the S_T/S ratio shall be based on the minimum calculated ratio of the included materials.

345.4.3 Hydrostatic Test of Piping With Vessels as a System³

- (a) Where the test pressure of piping attached to a vessel is the same as or less than the test pressure for the vessel, the piping may be tested with the vessel at the piping test pressure.
- (b) Where the test pressure of the piping exceeds the vessel test pressure, and it is not considered practicable to isolate the piping from the vessel, the piping and the vessel may be tested together at the vessel test pressure, provided the owner approves and the vessel test pressure is not less than 77% of the piping test pressure calculated in accordance with para. 345.4.2(b).

345.5 Pneumatic Leak Test

- **345.5.1 Precautions.** Pneumatic testing involves the hazard of released energy stored in compressed gas. Particular care must therefore be taken to minimize the chance of brittle failure during a pneumatic leak test. Test temperature is important in this regard and must be considered when the designer chooses the material of construction. See para. 345.2.2(c) and Appendix F, paras. F323.4 and F345.5.1.
- **345.5.2 Pressure Relief Device.** A pressure relief device shall be provided, having a set pressure not higher than the test pressure plus the lesser of 345 kPa (50 psi) or 10% of the test pressure.
- **345.5.3 Test Fluid.** The gas used as test fluid, if not air, shall be nonflammable and nontoxic.
- **345.5.4 Test Pressure.** The test pressure shall be not less than 1.1 times the design pressure and shall not exceed the lesser of
 - (a) 133 times the design pressure
- (b) the pressure that would exceed 90% of the pressure described in para. 345.2.1(a)
- **345.5.5 Procedure.** The pressure shall be gradually increased until a gage pressure that is the lesser of one-half the test pressure or 170 kPa (25 psi) is attained, at which time a preliminary check shall be made, including examination of joints in accordance with para. 341.4.1(a).

Thereafter, the pressure shall be gradually increased in steps until the test pressure is reached, holding the pressure at each step long enough to equalize piping strains. The pressure shall then be reduced to the design pressure before examining for leakage in accordance with para. 345.2.2(a).

345.6 Hydrostatic-Pneumatic Leak Test

If a combination hydrostatic-pneumatic leak test is used, the requirements of para. 345.5 shall be met, and the pressure in the liquid filled part of the piping shall not exceed the limits stated in para. 345.1.2.

345.7 Initial Service Leak Test

This test is applicable only to piping in Category D Fluid Service, at the owner's option. See para. 345.1(a).

- **345.7.1 Test Fluid.** The test fluid is the service fluid.
- **345.7.2 Procedure.** During or prior to initial operation, the pressure shall be gradually increased in steps until the operating pressure is reached, holding the pressure at each step long enough to equalize piping strains. A preliminary check shall be made as described in para. 345.5.5 if the service fluid is a gas or vapor.
- **345.7.3 Examination for Leaks.** The examination for leaks required by para. 345.2.2(a) shall be conducted while the system is at operating pressure. It is permissible to omit examination for leaks of joints and connections previously tested in accordance with this Code.

345.8 Sensitive Leak Test

(18)

- **345.8.1 Precautions.** The precautions described in para. 345.5.1 shall be considered when applicable.
- **345.8.2 Method.** The test shall be the Bubble Test Direct Pressure Technique in accordance with ASME BPVC, Section V, Article 10, Mandatory Appendix I or another leak test method that has a demonstrated sensitivity not less than 10^{-3} std mL/s under test conditions.

When the Bubble Test — Direct Pressure Technique is used

- (a) the test pressure shall be at least the lesser of 105 kPa (15 psi) or 25% of the design pressure.
- (b) the pressure shall be gradually increased until a gage pressure equal to the lesser of one-half the test pressure or 170 kPa (25 psi) is attained, at which time a preliminary check shall be made. Then the pressure shall be gradually increased in steps until the test pressure is reached, the pressure being held long enough at each step to equalize piping strains.

345.9 Alternative Leak Test

The following procedures and leak test method may be used only under the conditions stated in para. 345.1(c).

³ The provisions of para. 345.4.3 do not affect the pressure test requirements of any applicable vessel code.

- 345.9.1 Examination of Welds. Welds, including those used in the manufacture of welded pipe and fittings, that have not been subjected to hydrostatic or pneumatic leak tests in accordance with this Code, shall be examined as follows:
- (a) Circumferential, longitudinal, and spiral (helical seam) groove welds shall be 100% radiographed in accordance with para. 344.5 or 100% ultrasonically examined in accordance with para. 344.6.
- (b) All welds, including structural attachment welds, not covered in (a) above, shall be examined using the liquid penetrant method (para. 344.4) or, for magnetic materials, the magnetic particle method (para. 344.3).
- 345.9.2 Flexibility Analysis. A flexibility analysis of the piping system shall have been made in accordance with the requirements of para. 319.4.2(b), if applicable, persion report of click to view the full hold of the persion of th or (c) and (d).

345.9.3 Test Method. The system shall be subjected to a sensitive leak test in accordance with para. 345.8.

346 RECORDS

346.2 Responsibility

It is the responsibility of the piping designer, the manufacturer, the fabricator, and the erector, as applicable, to prepare the records required by this Code and by the engineering design.

346.3 Retention of Records

Unless otherwise specified by the engineering design, the following records shall be retained for at least 5 years after the record is generated for the project:

- (a) examination procedures
- (b) examination personnel qualifications
- (c) examination reports

Chapter VII Nonmetallic Piping and Piping Lined With Nonmetals

A300 GENERAL STATEMENTS

- (a) Chapter VII pertains to nonmetallic piping and to piping lined with nonmetals.
- (b) The organization, content, and paragraph designations of this Chapter correspond to those of the first six Chapters (the base Code). The prefix A is used.
- (c) Provisions and requirements of the base Code apply only as stated in this Chapter.
- (d) Metallic piping that provides the pressure containment for a nonmetallic lining shall conform to the requirements of Chapters I through VI, and to those in Chapter VII not limited to nonmetals.
- (e) This Chapter makes no provision for piping to be used under severe cyclic conditions.
- (f) With the exceptions stated above, Chapter I applies in its entirety.

PART 1 CONDITIONS AND CRITERIA

A301 DESIGN CONDITIONS

Paragraph 301 applies in its entirety, with the exception of paras. 301.2 and 301.3. See below

A301.2 Design Pressure

Paragraph 301.2 applies in its entirety, except that references to paras. A302.2.4 and A304 replace references to paras. 302.2.4 and 304, respectively.

A301.3 Design Temperature

Paragraph 301.3 applies with the following exceptions.

A301.3.1 Design Minimum Temperature. Paragraph 301.3.1 applies; but see para. A323.2.2, rather than para. 323.2.2.

A301.3.2 Uninsulated Components. The component design temperature shall be the fluid temperature, unless a higher temperature will result from solar radiation or other external heat sources.

A302 DESIGN CRITERIA

Paragraph A302 states pressure-temperature ratings, stress criteria, design allowances, and minimum design values, together with permissible variations of these factors as applied to the design of piping.

A302.1 General

The designer shall be satisfied as to the adequacy of the nonmetallic material and its manufacture, considering at least the following:

- (a) tensile compressive, flexural, and shear strength, and modulus of elasticity, at design temperature (long term and short term)
 - (b) creep rate at design conditions
 - (6) design stress and its basis
- (d) ductility and plasticity
- (e) impact and thermal shock properties
- (f) temperature limits
- (g) transition temperature melting and vaporization
- (h) porosity and permeability
- (i) testing methods
- (j) methods of making joints and their efficiency
- (k) possibility of deterioration in service

A302.2 Pressure-Temperature Design Criteria

Ratings. Paragraph 302.2.1 applies, except that reference to Table A326.1 replaces reference to Table 326.1.

A302.2.2 Listed Components Not Having Specific Ratings. Nonmetallic piping components for which design stresses have been developed in accordance with para. A302.3, but which do not have specific pressure-temperature ratings, shall be rated by rules for pressure design in para. A304, within the range of temperatures for which stresses are shown in Appendix B, modified as applicable by other rules of this Code.

Piping components that do not have allowable stresses or pressure–temperature ratings shall be qualified for pressure design as required by para. A304.7.2.

A302.2.3 Unlisted Components. Paragraph 302.2.3 (18) applies, except that references to Table A326.1 and paras. A304 and A323 replace references to Table 326.1 and paras. 304 and 323, respectively.

A302.2.4 Allowances for Pressure and Temperature Variations

- (a) Nonmetallic Piping. Allowances for variations of pressure or temperature, or both, above design conditions are not permitted. The most severe conditions of coincident pressure and temperature shall be used to determine the design conditions for a piping system. See paras. 301.2 and 301.3.
- (b) Metallic Piping With Nonmetallic Lining. Allowances for pressure and temperature variations provided in para. 302.2.4 are permitted only if the suitability of the lining material for the increased conditions is established through prior successful service experience or tests under comparable conditions.

A302.2.5 Rating at Junction of Different Services.

When two services that operate at different pressuretemperature conditions are connected, the valve segregating the two services shall be rated for the more severe service condition.

A302.3 Allowable Stresses and Other Design Limits

A302.3.1 General

- (a) Table B-1 contains hydrostatic design stresses (HDS). Tables B-2 and B-3 provide listings of specifications that meet the criteria of paras. A302.3.2(b) and (c), respectively. Tables B-4 and B-5 contain allowable pressures. These HDS values, allowable stress criteria, and pressures shall be used in accordance with the Notes to Appendix B, and may be used in design calculations (where the allowable stress S means the appropriate design stress) except as modified by other provisions of this Code. Use of hydrostatic design stresses for calculations other than pressure design has not been verified. The bases for determining allowable stresses and pressures are outlined in para. A302.3.2.
- (b) The stresses and allowable pressures are grouped by materials and listed for stated temperatures. Straightline interpolation between temperatures is permissible.

A302.3.2 Bases for Allowable Stresses and Pres- (18) sures¹

- (a) Thermoplastics. The method of determining HDS is described in ASTM D2837. HDS values are given in Table B-1 for those materials and temperatures for which sufficient data have been compiled to substantiate the determination of stress.
- (b) Reinforced Thermosetting Resin (Laminated). The design stress (DS) values for materials listed in Table B-2 shall be one-tenth of the minimum tensile strengths specified in ASTM C582 and are valid only in the temperature range from -29°C (-20°F) through 82°C (180°F).
- (c) Reinforced Thermosetting Resin and Reinforced Plastic Mortar (Filament Wound and Centrifugally Cast). The hydrostatic design basis stress (HDBS) values for materials listed in Table B-3 shall be obtained by the procedures in ASTM D2992 and are valid only at 23°C (73°F). HDS shall be obtained by multiplying the HDBS by a service (design) factor² selected for the application, in accordance with procedures described in ASTM D2992, within the following limits:
- (1) When using the cyclic HDBS, the service (design) factor *F* shall not exceed 1.0.
- (2) When using the static HDBS, the service (design) factor R shall not exceed 0.5.
- (d) Other Materials. Allowable pressures in Tables B-4 and B-5 have been determined conservatively from physical properties of materials conforming to the listed specifications, and have been confirmed by extensive experience. Use of other materials shall be qualified as required by para. A304.7.2.

¹ Titles of ASTM Specifications and AWWA Standards referenced herein are as follows:

ASTM C14, Concrete Sewer, Storm Drain, and Culvert Pipe

ASTM C301, Method of Testing Vitrified Clay Pipe

ASTM C582, Contact-Molded Reinforced Thermosetting Plastic (RTP) Laminates for Corrosion Resistant Equipment

ASTM D2321, Practice for Underground Installation of Thermoplastic Pipe for Sewers and Other Gravity-Flow Applications

ASTM D2837, Test Method for Obtaining Hydrostatic Design Basis for Thermoplastic Pipe Materials or Pressure Design Basis for Thermoplastic Pipe Products

ASTM D2992, Practice for Obtaining Hydrostatic or Pressure Design Basis for "Fiberglass" (Glass-Fiber-RTR) Pipe and Fittings

ASTM D3839, Underground Installation of Fiberglass Pipe

AWWA C900, Polyvinyl Chloride (PVC) Pressure Pipe and Fabricated Fittings, 4 In. Through 60 In. (100 mm Through 1,500 mm)

AWWA C950, Glass-Fiber-Reinforced Thermosetting Resin Pressure Pipe

² The service (design) factor, *F*, should be selected by the designer after evaluating fully the service conditions and the engineering properties of the specific material under consideration. Aside from the limits in paras. A302.3.2(c)(1) and (2), it is not the intent of this Code to specify service (design) factors.

A302.3.3 Limits of Calculated Stresses Due to Sustained Loads¹

- (a) Internal Pressure Stresses. Limits of stress due to internal pressure are covered in para. A304.
- (b) External Pressure Stresses. Stresses due to uniform external pressure shall be considered safe when the wall thickness of the component and its means of stiffening have been qualified as required by para. A304.7.2.
- (c) External Loading Stresses. Design of piping under external loading shall be based on the following:
- (1) Thermoplastic Piping. ASTM D2321 or AWWA C900.
- (2) Reinforced Thermosetting Resin (RTR) and Reinforced Plastic Mortar (RPM) Piping. ASTM D3839 or Appendix A of AWWA C950.
- (3) Strain and possible buckling shall be considered when determining the maximum allowable deflection in (1) or (2) above, but in no case shall the allowable diametral deflection exceed 5% of the pipe inside diameter.
- (4) Nonmetallic piping not covered in (1) or (2) above shall be subjected to a crushing or three-edge bearing test in accordance with ASTM C14 or C301; the allowable load shall be 25% of the minimum value obtained

(18) A302.3.4 Limits of Calculated Stresses Due to Occasional Loads

- (a) Operation
- (1) For other than RTR and RPM piping, the sum of stresses in any component in a piping system due to sustained loads, such as pressure and weight, and of the stresses produced by occasional loads, such as wind or earthquake, shall not exceed the limits in the applicable part of para. A302.3.3.
- (2) For RTR and RPM piping, the sum of stresses due to operating loads plus stresses due to occasional loads may be as much as 1.33 times the limits in the applicable part of para. A302.3.3.
- (3) Wind and earthquake forces need not be considered as acting concurrently.
- (b) Test. Stresses due to test conditions are not subject to the limitations in para. A302.3.3. It is not necessary to consider other occasional loads, such as wind and earthquake, as occurring concurrently with test loads.

A302.4 Allowances

Paragraph 302.4 applies in its entirety.

PART 2 PRESSURE DESIGN OF PIPING COMPONENTS

A303 GENERAL

Paragraph 303 applies, except that references to Table A326.1 and para. A302.2.1 replace references to Table 326.1 and para. 302.2.1. For nonmetallic components, reference to para. A304 replaces reference to para. 304.

A304 PRESSURE DESIGN OF PIPING COMPONENTS

A304.1 Straight Pipe

A304.1.1 General

(a) The required thickness of straight sections of pipe shall be determined by eq. (25).

$$t_m = t + c \tag{25}$$

The minimum thickness T for the pipe selected, considering manufacturer's minus tolerance, shall be not less than t_m .

- (b) The following nomenclature is used in the equations for pressure design of straight pipe:
- = the sum of mechanical allowances (thread or groove depth) plus corrosion and erosion allowance. For threaded components, the nominal thread depth (dimension *h* of ASME B1.20.1 or equivalent) shall apply. For machined surfaces or grooves where the tolerance is not specified, the tolerance shall be assumed to be 0.5 mm (0.02 in.) in addition to the specified depth of the cut.

D =outside diameter of pipe

F = service (design) factor. See para. A302.3.2(c).

P = internal design gage pressure

S = design stress from applicable Table in Appendix B

- T = pipe wall thickness (measured or minimum in accordance with the purchase specification)
- t = pressure design thickness, as calculated in accordance with para. A304.1.2 for internal pressure or as determined in accordance with para. A304.1.3 for external pressure
- t_m = minimum required thickness, including mechanical, corrosion, and erosion allowances

A304.1.2 Straight Nonmetallic Pipe Under Internal

Pressure. The internal pressure design thickness, t, shall be not less than that calculated by one of the following equations, using stress values listed in or derived from the appropriate table in Appendix B:

(a) Thermoplastic Pipe [see para. A302.3.2(a)]

$$t = \frac{PD}{2S + P} \text{(Table B-1)} \tag{26a}$$

(b) RTR (Laminated) Pipe [see para. A302.3.2(b)]³

$$t = \frac{PD}{2S + P} \text{(Table B-2)} \tag{26b}$$

(c) RTR (Filament Wound) and RPM (Centrifugally Cast) Pipe [see para. A302.3.2(c)]³

$$t = \frac{PD}{2SF + P} \text{(Table B-3)} \tag{26c}$$

A304.1.3 Straight Pipe Under External Pressure

- (a) Nonmetallic Pipe. The external pressure design thickness, t, shall be qualified as required by para. A304.7.2.
 - (b) Metallic Pipe Lined With Nonmetals
- (1) The external pressure design thickness, *t*, for the base (outer) material shall be determined in accordance with para. 304.1.3.
- (2) The external pressure design thickness, *t*, for the lining material shall be qualified as required by para. A304.7.2.

A304.2 Curved and Mitered Segments of Pipe

A304.2.1 Pipe Bends. The minimum required thickness, t_m , of a bend, after bending, shall be determined as for straight pipe in accordance with para. A304.1.

A304.2.2 Elbows. Manufactured elbows not in accordance with para. A303 shall be qualified as required by para. A304.7.2.

A304.2.3 Miter Bends. Miter bends shall be qualified as required by para. A304.7.2.

A304.3 Branch Connections

A304.3.1 General. A pipe having a branch connection is weakened by the opening that must be made in it and, unless the wall thickness of the pipe is sufficiently in excess of that required to sustain the pressure, it is necessary to provide added reinforcement. The amount of reinforcement shall be qualified as required by para. A304.7.2 except as provided in para. A304.3.2.

A304.3.2 Branch Connections Using Fittings. It may be assumed without calculation that a branch connection has adequate strength to sustain the internal and external pressure that will be applied to it if it utilizes a fitting (a tee, lateral, or cross) in accordance with para. A303.

A304.3.3 Additional Design Considerations. The requirements of paras. A304.3.1 and A304.3.2 are intended to assure satisfactory performance of a branch connection

subjected only to internal or external pressure. The designer shall also consider paras. 304.3.5(a), (c), and (d).

A304.4 Closures

Closures not in accordance with para. A303 shall be qualified as required by para. A304.7.2.

A304.5 Pressure Design of Nonmetallic Flanges A304.5.1 General

- (a) Flanges not in accordance with para. A303, or A304.5.1(b) or (d) shall be qualified as required by para. A304.7.2.
- (b) Flanges for use with flat ring gaskets may be designed in accordance with ASME BPVC, Section VIII, Division 1, Appendix 2, except that the allowable stresses and temperature limits of this code shall govern. Nomenclature shall be as defined in ASME BPVC, except for the following:

P = design gage pressure

 S_a = bolt design stress at atmospheric temperature⁴

 S_b = bolt design stress at design temperature⁴

 S_f = allowable stress for flange material from Table B-1, B-2, or B-3

- (c) The rules in (b) above are not applicable to a flanged joint having a gasket that extends outside the bolts (usually to the outside diameter of the flange).
- (d) For flanges that make solid contact outside the bolts, ASME BPVC, Section VIII, Division 1, Appendix Y should be used.

A304.5.2 Blind Flanges. Blind flanges not in accordance with para. A303 may be designed in accordance with para. 304.5.2, except that allowable stress, *S*, shall be taken from Tables in Appendix B. Otherwise, they shall be qualified as required by para. A304.7.2.

A304.6 Reducers

Reducers not in accordance with para. A303 shall be qualified as required by para. A304.7.2.

A304.7 Pressure Design of Other Components

A304.7.1 Listed Components. Other pressure containing components, manufactured in accordance with standards in Table A326.1 but not covered elsewhere in para. A304, may be utilized in accordance with para. A303.

A304.7.2 Unlisted Components. Pressure design of unlisted components and joints, to which the rules elsewhere in para. A304 do not apply, shall be based on calculations consistent with the design criteria of this Code. Calculations shall be substantiated by one or both of the means stated in (a) and (b) below, considering

 $^{^3}$ The internal design pressure thickness, t, shall not include any thickness of the pipe wall reinforced with less than 20% by weight of reinforcing fibers.

⁴ Bolt design stresses shall not exceed those in Table A-2 or Table A-2M.

applicable ambient and dynamic effects in paras. 301.4 through 301.11.

- (a) extensive, successful service experience under comparable design conditions with similarly proportioned components made of the same or like material
- (b) performance test under design conditions including applicable dynamic and creep effects, continued for a time period sufficient to determine the acceptability of the component or joint for its design life
- For (a) or (b) above, the designer may interpolate between sizes, wall thicknesses, and pressure classes, and may determine analogies among related materials.

A304.7.3 Nonmetallic Components With Metallic Pressure Parts. Components not covered by standards in Table A326.1, in which both nonmetallic and metallic parts contain the pressure, shall be evaluated by applicable requirements of para. 304.7.2 as well as those of para. A304.7.2.

PART 3 FLUID SERVICE REQUIREMENTS FOR PIPING COMPONENTS

A305 PIPE

Listed pipe may be used in Normal Fluid Service, subject to the limitations of the pressure-containing material and para. A323.4. Unlisted pipe may be used only in accordance with para. A302.2.3.

A306 FITTINGS, BENDS, MITERS, LAPS, AND BRANCH CONNECTIONS

General. Fittings, bends, miters, laps, and branch connections may be used in accordance with paras. A306.1 through A306.5. Pipe and other materials used in such components shall be suitable for the manufacturing process and the fluid service.

A306.1 Pipe Fittings

A306.1.1 Listed Fittings. Listed fittings may be used in Normal Fluid Service subject to limitations on materials.

A306.1.2 Unlisted Fittings. Unlisted fittings may be used only in accordance with para. A302.2.3.

A306.2 Pipe Bends

A306.2.1 General. A bend made in accordance with para. A332 and verified for pressure design in accordance with para. A304.2.1 shall be suitable for the same service as the pipe from which it is made.

A306.2.2 Corrugated and Other Bends. Bends of other designs (such as creased or corrugated) shall be qualified for pressure design as required by para. A304.7.2.

A306.3 Miter Bends

Except as specified in para. 306.3.2, a miter bend that conforms to para. A304.2.3 may be used in Normal Fluid Service.

A306.4 Fabricated or Flared Laps

The following requirements do not apply to fittings conforming to para. A306.1.

A306.4.1 Fabricated Laps

- (a) The requirements in paras. 306.4.1(a) and (b) shall be met.
- (b) Lap material shall be suitable for the service conditions. Pressure design shall be qualified as required by para. A304.7.2.
- **A306.4.2 Flared Laps.** Flared laps shall not be used in nonmetallic piping.

A306.5 Fabricated Branch Connections

The following requirements do not apply to fittings conforming to para. A306.1.

A306.5.1 General. A fabricated branch connection made by bonding the branch pipe directly to the header pipe, with or without added reinforcement as stated in para. 328.5.4, and shown in Figure 328.5.4, may be used in Normal Fluid Service, provided that pressure design is qualified as required by para. A304.7.2.

A306.5.2 Specific Requirements. Fabricated branch connections shall be made as specified in para. A328.5.

A307 VALVES AND SPECIALTY COMPONENTS

Paragraph 307 applies in its entirety, except that in para. 307.1.2 references to paras. A302.2.3 and A304.7.2 replace references to paras. 302.2.3 and 304.7.2, respectively.

A308 FLANGES, BLANKS, FLANGE FACINGS, AND GASKETS

A308.1 General

Paragraph 308.1 applies, except that in para. 308.1.2 reference to para. A302.2.3 replaces reference to para. 302.2.3.

A308.2 Nonmetallic Flanges

A308.2.1 General

- (a) Flanges shall be adequate, with suitable facing, gasketing, and bolting, to develop the full rating of the joint and to withstand expected external loadings.
- (b) The designer should consult the manufacturer for ratings of flanges.

A308.2.2 Threaded Flanges. Threaded flanges are subject to the requirements for threaded joints in para. A314.

A308.3 Flange Facings

Paragraph 308.3 applies in its entirety.

A308.4 Limitations on Gaskets

See also Appendix F, para. F308.4.

A308.4.1 Lining Used as Facing or Gasket. Lining material extended over the flange face and used as a gasket shall conform to para. 308.4.

A309 BOLTING

Bolting includes bolts, bolt studs, studs, cap screws, nuts, and washers. See Appendix F, para. F309.

A309.1 General

Paragraph 309.1 applies in its entirety.

A309.2 Specific Bolting

Any bolting that meets the requirements of para. 309.1 may be used with any combination of flange materials and flange facings. Joint assembly shall conform to the requirements of para. A335.2.

A309.3 Tapped Holes in Nonmetallic Components

Tapped holes for pressure-retaining bolting in piping components may be used provided pressure design is qualified as required by para. A304.7.2.

PART 4 FLUID SERVICE REQUIREMENTS FOR PIPING JOINTS

A310 GENERAL

Paragraph 310 applies in its entirety.

A311 BONDED JOINTS IN PLASTICS

A311.1 General

Bonding shall be in accordance with para. A328 and examination shall be in accordance with para. A341.4.1 for use in Normal Fluid Service, subject to the limitations of the material.

A311.2 Specific Requirements

A311.2.1 Fillet Bonds. A fillet bond may be used only in conjunction with a qualified hot gas welding procedure for bonding (see para. A328.5.2).

A311.2.2 Seal Bonds. A seal bond may be used only to prevent leakage of a threaded joint and only if it has been demonstrated that there will be no deleterious effect on the materials bonded.

A311.2.3 Joints Limited to Category D Fluid Service. Joints that have been examined in accordance with para. 341.4.2 may be used only for Category D Fluid Service.

A312 FLANGED JOINTS

The designer should consult the manufacturer for ratings of flanged joints in nonmetallic piping and in piping lined with nonmetals.

A313 EXPANDED JOINTS

Paragraph 313 applies in its entirety.

A314 THREADED JOINTS

A314.1 General

A threaded joint is suitable for use in Normal Fluid Service, subject to the limitations of the material and requirements elsewhere in para. A314. A joint conforming to para. 324.1(d) shall not be used.

A314.2 Specific Requirements

A314.2.1 Thermoplastic Piping

- (a) Polyethylene (PE) pipe and tubing shall not be joined by threaded joints.
- (b) Threaded joints in other thermoplastic piping shall conform to all of the following:
- (1) The pipe wall shall be at least as thick as Schedule 80 as defined in ASTM D1785.
- (2) Threads shall be NPT, and shall conform to ASME B1.20.1 or ASTM F1498.
- (3) Threads shall conform to applicable standards in Table A326.1.
 - (4) A suitable thread sealant shall be used.

A314.2.2 Reinforced Thermosetting Resin Piping. Threaded joints in reinforced thermosetting resin (RTR) piping shall conform to the following:

- (a) External threads shall be factory cut or molded on special thick-walled pipe ends.
- (b) Matching internal threads shall be factory cut or molded in the fittings.
- (c) Threading of plain ends of RTR pipe is not permitted, except where such threads are limited to the function of a mechanical lock to matching internal threads factory cut or molded in the bottom portions of fittings with deep sockets.

(d) Factory cut or molded threaded nipples, couplings, or adapters, bonded to plain-end RTR pipe and fittings, may be used where it is necessary to provide connections to threaded metallic piping.

A314.2.3 Reinforced Plastic Mortar Piping. Threaded joints are not permitted in reinforced plastic mortar (RPM) piping.

A315 TUBING JOINTS

Paragraph 315 applies in its entirety, subject to material limitations, exclusion of 315.2(b) regarding severe cyclic conditions, and replacement of references to Table 326.1 and para. 304.7.2 with references to Table A326.1 and para. A304.7.2, respectively.

A316 CAULKED JOINTS

Paragraph 316 applies in its entirety.

A318 SPECIAL JOINTS

Special joints are those not covered elsewhere in Chapter VII, Part 4, such as bell type and packed gland type joints.

A318.1 General

Paragraph 318.1 applies in its entirety, except that, in para. 318.1.2, reference to para. A304.7.2 replaces reference to para. 304.7.2.

A318.2 Specific Requirements

Paragraph 318.2 applies with the exception of para. 318.2.3.

A318.3 Piping Lined With Nonmetals A318.3.1 Welding of Metallic Piping

- (a) General. Joints made in accordance with the rules in para. A329.1 may be used in Normal Fluid Service, subject to material limitations.
- (b) Specific Requirements. Welds shall be limited to those that do not affect the serviceability of the lining.

A318.3.2 Flared Linings

- (a) General. Flared ends of linings made in accordance with the rules in para. A329.2 may be used in Normal Fluid Service, subject to material limitations.
- (b) Specific Requirements. Flaring shall be limited to applications that do not affect the serviceability of the lining.

A318.4 Flexible Elastomeric Sealed Joints

Flexible elastomeric seals conforming to the following may be used in Normal Fluid Service, subject to material limitations:

- (a) Seals for joints in thermoplastic piping shall conform to ASTM D3139.
- (b) Seals for joints in RTR and RPM piping shall conform to ASTM D4161.

PART 5 FLEXIBILITY AND SUPPORT

A319 FLEXIBILITY OF NONMETALLIC PIPING

A319.1 Requirements

- **A319.1.1 Basic Requirements.** Piping systems shall be designed to prevent thermal expansion or contraction, pressure expansion, or movement of piping supports and terminals from causing
- (a) failure of piping or supports from overstrain or fatigue
 - (b) leakage at joints
- (c) detrimental stresses or distortion in piping or in connected equipment (e.g., pumps), resulting from excessive thrusts and moments in the piping

A319.1.2 Specific Requirements

- (a) In para. A319, guidance, concepts, and data are given to assist the designer in assuring adequate flexibility in piping systems. No specific stress-limiting criteria or methods of stress analysis are presented, since stress-strain behavior of most nonmetals differs considerably from that of metals covered by para. 319 and is less well defined for mathematical analysis.
- (b) Piping systems should be designed and laid out so that flexural stresses resulting from displacement due to expansion, contraction, and other movement are minimized. This concept requires special attention to supports, terminals, and other restraints, as well as to the techniques outlined in para. A319.7. See also para. A319.2.2(b).
- (c) Further information on design of thermoplastic piping can be found in PPI Technical Report TR-21.

A319.2 Concepts

- **A319.2.1 Displacement Strains.** The concepts of strain (18) imposed by restraint of thermal expansion or contraction, and by external movement, described in para. 319.2.1, apply in principle to nonmetals. Nevertheless, the assumption that stresses throughout the piping systems can be predicted from these strains because of fully elastic behavior of the piping materials is not always valid.
- (a) In thermoplastics piping, displacement strains are not likely to produce immediate failure but may result in detrimental distortion. Progressive deformation may occur upon repeated thermal cycling or on prolonged exposure to elevated temperature.

- (b) In brittle piping (e.g., porcelain and glass) and some RTR and RPM piping, the materials show rigid behavior and develop high displacement stresses up to the point of sudden breakage due to overstrain.
- (c) RTR and RPM piping are assumed to display linear elastic behavior, having displacement stresses proportional to displacement strains.

(18)A319.2.2 Displacement Stresses

- (a) Elastic Behavior. The assumption that displacement strains will produce proportional stress over a sufficiently wide range to justify an elastic stress analysis is not always valid for nonmetals. RTR and RPM piping shall be designed for linear elastic behavior, having displacement stresses proportional to displacement strains. In brittle piping, strains initially will produce relatively large elastic stresses. The total displacement strain must be kept small, however, since overstrain results in failure rather than plastic deformation. In thermoplastic piping, strains generally will produce stresses of the overstrained (plastic) type, even at relatively low values of total displacement strain. If a method of flexibility analysis that assumes elastic behavior is selected for thermoplastic piping, the designer shall demonstrate its validity for the piping system under consideration and shall establish safe limits for computed stresses.
- (b) Overstrained Behavior. Stresses cannot be considered proportional to displacement strains throughout a piping system in which an excessive amount of strain in which are excessive amount of the strain in t may occur in localized portions of the piping [an unbale] anced system; see para. 319.2.2(b)] or in which elastic behavior of the piping material cannot be assumed Overstrain shall be minimized by system layout and excessive displacements shall be minimized by special joints or expansion devices (see para. A319.7).
- **A319.2.3 Cold Spring.** Cold spring is the intentional deformation of piping during assembly to produce a desired initial displacement or reaction. Cold spring may be beneficial in serving to balance the magnitude of the reaction under initial and extreme displacement conditions. When cold spring is properly applied, there is less likelihood of overstrain during initial operation. There is also less deviation from as-installed dimensions during initial operation, so that hangers will not be displaced as far from their original settings. No credit for cold spring is permitted in stress range calculations, or in calculating thrusts and moments.

A319.3 Properties for Flexibility Analysis

A319.3.1 Thermal Expansion Data. Appendix C lists coefficients of thermal expansion for several nonmetals. More precise values in some instances may be obtainable from manufacturers of components. If these values are to be used in stress analysis, the thermal displacements shall be determined as stated in para. 319.3.1.

- A319.3.2 Modulus of Elasticity. Appendix C lists representative data on the tensile modulus of elasticity, E, for several nonmetals as obtained under typical laboratory rate of strain (loading) conditions. More precise values of the short-term and working estimates of effective moduli of elasticity for given conditions of loading and temperature may be obtainable from the manufacturer. For materials and temperatures not listed, refer to ASTM or PPI documents, or to manufacturer's data.
- (a) Because of their viscoelasticity, the effective moduli of thermoplastics under actual conditions of use will depend on both the specific course of the strain (or load) with time and the specific characteristics of the thermoplastic.
- (b) The modulus may also vary with the orientation of the specimen. Because the reinforcement plays a significant role in developing the physical properties for RTR and RPM piping, the modulus may vary with the type and orientation of the reinforcement.
- **A319.3.3 Poisson's Ratio.** Poisson's ratio varies widely depending upon material and temperature. For that reason, simplified formulas used in stress analysis for metals may not be valid for nonmetals. For RTR and RPM piping Poisson's ratio varies with the orientation of the reinforcement.
- A319.3.4 Dimensions. Nominal thicknesses and outside diameters of pipe and fittings shall be used in flex-

A319.4 Analysis

- A319.4.1 Formal Analysis Not Required. No formal analysis is required for a piping system that
- (a) duplicates, or replaces without significant change, a system operating with a successful service record
- (b) can readily be judged adequate by comparison with previously analyzed systems, or
- (c) is laid out with a conservative margin of inherent flexibility, or employs joining methods or expansion joint devices, or a combination of these methods, in accordance with manufacturers' instructions
- **A319.4.2 Formal Analysis Requirements.** For a piping system that does not meet the above criteria, the designer shall demonstrate adequate flexibility by simplified, approximate, or comprehensive stress analysis, using a method that can be shown to be valid for the specific case. If substantially elastic behavior can be demonstrated for the piping system [see para. A319.2.2(a)], methods outlined in para. 319.4 may be applicable.

A319.5 Reactions

Paragraph 319.5 may be applicable if a formal stress analysis can be shown to be valid for the specific case.

A319.6 Movements

Special attention shall be given to movement (displacement or rotation) of piping with respect to supports and points of close clearance. Movements of the run pipe at the junction of a small branch connection shall be considered in determining the need for flexibility in the branch pipe.

A319.7 Means of Increasing Flexibility

Piping layout often provides adequate inherent flexibility through changes in direction, wherein displacements produce chiefly bending and torsional strains of low magnitude. The amount of tension or compression strain (which can produce larger reactions) usually is small.

Where piping lacks inherent flexibility or is unbalanced, additional flexibility shall be provided by one or more of the following means: bends, loops, or offsets; swivel or flexible joints; corrugated, bellows, or slip-joint expansion joints; or other devices permitting angular, rotational, or axial movement. Suitable anchors, ties, or other devices shall be provided as necessary to resist end forces produced by fluid pressure, frictional resistance to movement, and other causes.

A321 PIPING SUPPORT

Paragraph 321 applies in its entirety.

A321.5 Supports for Nonmetallic Piping

A321.5.1 General. In addition to other applicable requirements of para. 321, supports, guides, and anchors shall be selected and applied to comply with the principles and requirements of para. A319 and the following:

- (a) Piping shall be supported, guided and anchored in such a manner as to prevent damage to the piping. Point loads and narrow areas of contact between piping and supports shall be avoided. Suitable padding shall be placed between piping and supports where damage to piping may occur.
- (b) Valves and equipment that would transmit excessive loads to the piping shall be independently supported to prevent such loads.
- (c) Consideration shall be given to mechanical guarding in traffic areas.
- (d) Manufacturers' recommendations for support shall be considered.

A321.5.2 Supports for Thermoplastic, RTR, and RPM Piping. Supports shall be spaced to avoid excessive sag or deformation at the design temperature and within the design life of the piping system. Decreases in the modulus of elasticity with increasing temperature and creep of material with time shall be considered when applicable. The coefficient of thermal expansion shall be considered in the design and location of supports.

A321.5.3 Supports for Brittle Piping. Brittle piping, such as glass, shall be well supported but free of hindrance to expansion or other movement. Not more than one anchor shall be provided in any straight run without an expansion joint.

PART 6 SYSTEMS

A322 SPECIFIC PIPING SYSTEMS

A322.3 Instrument Piping

Paragraph 322.3 applies in its entirety, except that references to paras. A301 and A302.2.4 replace references to paras. 301 and 302.2.4, respectively.

A322.6 Pressure-Relieving Systems

Paragraph 322,6 applies in its entirety, except for para. 322.6.3. See para. A322.6.3.

A322.6.3 Overpressure Protection. Paragraph 322.6.3 applies, except that maximum relieving pressure shall be in accordance with para. A302.2.4.

PART 7 MATERIALS

A323 GENERAL REQUIREMENTS

A323.1 Materials and Specifications

Paragraph 323.1 applies except for para. 323.1.4. See para. A323.1.4.

A323.1.4 Reclaimed Materials. Reclaimed piping components may be used, provided they are properly identified as conforming to a listed or published specification (see para. 323.1.1) and otherwise meet the requirements of this Code. The user shall verify that components are suitable for the intended service. Sufficient cleaning, examination, and testing shall be performed to determine the minimum available wall thickness and freedom from any of the following to an extent that would be unacceptable in the intended service:

- (a) imperfections
- (b) reduction of mechanical properties, or
- (c) absorption of deleterious substances

A323.2 Temperature Limitations

The designer shall verify that materials that meet other requirements of the Code are suitable for service throughout the operating temperature range. Also see the Notes for Tables B-1 through B-5 in Appendix B.

A323.2.1 Upper Temperature Limits, Listed Materials

- (a) Except as provided in (b) below, a listed material shall not be used at a design temperature higher than the maximum for which a stress value or rating is shown, or higher than the maximum recommended temperature in Table A323.4.2C for RTR materials and in Table A323.4.3 for thermoplastics used as linings.
- (b) A listed material may be used at a temperature higher than the maximum stated in (a) above if there is no prohibition in Appendix B or elsewhere in the Code, and if the designer verifies the serviceability of the material in accordance with para. 323.2.4.

A323.2.2 Lower Temperature Limits, Listed Materials

- (a) Materials for use at design minimum temperatures below certain limits must usually be tested to determine that they have suitable toughness for use in Code piping. Table A323.2.2 sets forth those requirements.
- (b) When materials are qualified for use at temperatures below the minimum temperature listed in Appendix B, the allowable stresses or pressures shall not exceed the values for the lowest temperatures shown.
- (c) See also the recommended limits in Table A323.4.2C for reinforced thermosetting resin pipe and in Table A323.4.3 for thermoplastics used as linings.

A323.2.3 Temperature Limits, Unlisted Materials. Paragraph 323.2.3 applies.

A323.2.4 Verification of Serviceability. When an unlisted material is to be used, or when a listed material is to be used above or below the limits in Appendix B, Table A323.4.2C, or Table A323.4.3, the designer shall comply with the requirements of para. 323.2.4.

A323.4 Fluid Service Requirements for Nonmetallic Materials

A323.4.1 General

- (a) Nonmetallic materials shall be safeguarded against excessive temperature, shock, vibration, pulsation, and mechanical abuse in all fluid services.
- (b) Requirements in para. A323.4 apply to pressure-containing parts. They do not apply to materials used for supports, gaskets, or packing. See also Appendix F, para. FA323.4.

A323.4.2 Specific Requirements

- (a) Thermoplastics
- (1) They shall not be used in flammable fluid service above ground, unless all of the following are met:
- (a) The size of the piping does not exceed DN 25 (NPS 1).
 - (b) Owner's approval is obtained.
- (c) Safeguarding in accordance with Appendix G is provided.

- (d) The precautions of Appendix F, paras. F323.1(a) through (c) are considered.
- (2) They shall be safeguarded when used in other than Category D Fluid Service.
- (3) PVC and CPVC shall not be used in compressed air or other compressed gas service.
- (b) Reinforced Plastic Mortars (RPM) Piping. This piping shall be safeguarded when used in other than Category D Fluid Service.
- (c) Reinforced Thermosetting Resins (RTR) Piping. This piping shall be safeguarded when used in toxic or flammable fluid services. Table A323.4.2C gives the recommended temperature limits for reinforced thermosetting resins.
 - (d) Borosilicate Glass and Porcelain
- (1) They shall be safeguarded when used in toxic or flammable fluid services.
- (2) They shall be safeguarded against large, rapid temperature changes in fluid services.

A323.4.3 Piping Lined With Nonmetals

- (a) Metallic Riping Lined With Nonmetals. Fluid service requirements for the base (outer) material in para. 323.4 govern except as stated in (d) below.
- (b) Nonmetallic Piping Lined With Nonmetals. Fluid service requirements for the base (outer) material in para. A323.4.2 govern, except as stated in (d) below.
- material that, in the judgment of the user, is suitable for the intended service and for the method of manufacture and assembly of the piping. Fluid service requirements in para. A323.4.2 do not apply to materials used as linings.
- (d) Properties of both the base and lining materials, and of any bond between them, shall be considered in establishing temperature limitations. Table A323.4.3 gives recommended temperature limits for thermoplastic materials used as linings.

A323.5 Deterioration of Materials in Service

Paragraph 323.5 applies in its entirety.

A325 MATERIALS — MISCELLANEOUS

Paragraph 325 applies in its entirety.

PART 8 STANDARDS FOR PIPING COMPONENTS

A326 DIMENSIONS AND RATINGS OF COMPONENTS

A326.1 Requirements

Paragraph 326 applies in its entirety except that references to Table A326.1 and Appendix B replace references to Table 326.1 and Appendix A, respectively.

Table A323.2.2 Requirements for Low Temperature Toughness Tests for Nonmetals

Type of Material	Column A At or Above Listed Minimum Temperature	Column B Below Listed Minimum Temperature
Listed nonmetallic materials	No added requirement	The designer shall have test results at or below the lowest expected service temperature which assure that the materials and bonds will have adequate toughness and are suitable at the design minimum temperature.
Unlisted materials	are comparable to the	ll conform to a published specification. Where composition, properties, and product form see of a listed material, requirements for the corresponding listed material shall be met. als shall be qualified as required in Column B.

GENERAL NOTE: These requirements are in addition to the requirements of the material specification.

Table A323.4.2C Recommended Temperature Limits for Reinforced Thermosetting Resin Pipe

		Recomm	ended Te	mperatu	re Limits
Mat	erials	Mini	mum	Maxi	mum
Resin	Reinforcing	°C	°F	°C	°F
Ероху	Glass fiber	-29	-20	149	300
Phenolic	Glass fiber	-29	-20	149	300
Furan	Carbon	-29	-20	93	200
Furan	Glass fiber	-29	-20	93	200
Polyester	Glass fiber	-29	-20	93	200
Vinyl ester	Glass fiber	-29	-20	93	200

GENERAL NOTE: These temperature limits apply only to materials listed and do not reflect evidence of successful use in specific fluid services at these temperatures. The designer should consult the manufacturer for specific applications, particularly as the temperature limits are approached.

A326.4 Abbreviations in Table A326.1 and Appendix B

The abbreviations tabulated below are used in this Chapter to replace lengthy phrases in the text, in the titles of standards in Table A326.1, and in the Specification Index for Appendix & Those marked with an asterisk (*) are in accordance with ASTM D1600, Standard Terminology for Abbreviated Terms Relating to Plastics. Those items marked with a dagger (†) are in accordance with ASTM F412, Standard Terminology Relating to Plastic Piping Systems.

Abbreviation	Term
ABS*†	Acrylonitrile-butadiene-styrene plastics
BPS	Bonding Procedure Specification
CPVC*†	Chlorinated poly(vinyl chloride) plastics
DR†	Dimension ratio
DS	Design stress
E-CTFE*	Ethylene-chlorotrifluoroethylene
ETFE*	Ethylene-tetrafluoroethylene copolymer
FEP*	Perfluoro (ethylene-propylene) copolymer

Table A323.4.3 Recommended Temperature Limits for Thermoplastics Used as Linings

Materials	Minir	num	Maxi	Maximum	
[Note (1)]	eC)	°F	°C	°F	
PFA	-198	-325	260	500	
PTFE	-198	-325	260	500	
FEP P	-198	-325	204	400	
ECTFE	-198	-325	171	340	
ETEE	-198	-325	149	300	
IL.					
PVDF	-18	0	135	275	
PP	-18	0	107	225	
PVDC	-18	0	79	175	

GENERAL NOTE: These temperature limits are based on material tests and do not necessarily reflect evidence of successful use as piping component linings in specific fluid services at these temperatures. The designer should consult the manufacturer for specific applications, particularly as temperature limits are approached.

NOTE: (1) See para. A326.4 for definitions of materials.

Table continued

Abbreviation	Term
HDBS	Hydrostatic Design Basis Stress
HDS†	Hydrostatic Design Stress
PB*†	Polybutylene-1
PE*†	Polyethylene
PEX	Cross-linked polyethylene
PFA*	Perfluoro (alkoxyalkane)
PP*†	Polypropylene
PQR	Procedure Qualification Record
PR†	Pressure rating
PTFE*	Polytetrafluoroethylene
PVC*†	Poly(vinyl chloride)
PVDC*	Poly(vinylidene chloride)
PVDF*	Poly(vinylidene fluoride)
RPM	Reinforced plastic mortar

Table continued

Abbreviation	Term
RTP	Reinforced thermosetting plastic
RTR	Reinforced thermosetting resin
SDR†	Standard dimension ratios
SIDR†	Standard inside diameter dimension ratio
WPS	Welding Procedure Specification

PART 9 FABRICATION, ASSEMBLY, AND ERECTION

A327 GENERAL

Piping materials and components are prepared for assembly and erection by one or more of the fabrication processes in paras. A328, A329, A332, and A334. When any of these processes is used in assembly and erection, requirements are the same as for fabrication.

A328 BONDING OF PLASTICS

Paragraph A328 applies only to joints in thermoplastic, RTR, and RPM piping. Bonding shall conform to paras. A328.1 through A328.7 and the applicable requirements of para. A311.

A328.1 Bonding Responsibility

Each employer is responsible for the bonding done by personnel of his/her organization and, except as provided in paras. A328.2.2 and A328.2.3, shall conduct the required performance qualification tests to qualify bonding procedure specifications (BPS) and bonders or bonding operators.

A328.2 Bonding Qualifications

A328.2.1 Qualification Requirements

- (a) Qualification of the BPS to be used, and of the performance of bonders and bonding operators, is required. To qualify a BPS, all tests and examinations specified therein and in para. A328.2.5 shall be completed successfully.
- (b) In addition to the procedure for making the bonds, the BPS shall specify at least the following:
- (1) all materials and supplies (including storage requirements)
- (2) tools and fixtures (including proper care and handling)
- (3) environmental requirements (e.g., temperature, humidity, and methods of measurement)
 - (4) joint preparation
 - (5) dimensional requirements and tolerances
 - (6) cure time
 - (7) protection of work

- (8) tests and examinations other than those required by para. A328.2.5
- (9) acceptance criteria for the completed test assembly

A328.2.2 Procedure Qualification by Others. Subject to the specific approval of the Inspector, a BPS qualified by others may be used provided that

- (a) the Inspector satisfies him/herself that the proposed qualified BPS has been prepared and executed by a responsible recognized organization with expertise in the field of bonding
- (b) by signature, the employer accepts both the BPS and procedure qualification record (PQR) as his/her own
- (c) the employer has at least one currently employed bonder who, while in his/her employ, has satisfactorily passed a performance qualification test using the proposed qualified BPS

A328.2.3 Performance Qualification by Others.

Without the Inspector's specific approval, an employer shall not accept a performance qualification test made by a bonder or bonding operator for another employer. If approval is given, it is limited to work on piping using the same or equivalent BPS. An employer accepting such performance qualification tests shall obtain a copy of the performance qualification test record from the previous employer, showing the name of the employer by whom the bonder or bonding operator was qualified, the date of such qualification, and the date the bonder or bonding operator last bonded pressure piping under such performance qualification.

A328.2.4 Qualification Records. The employer shall maintain a self-certified record, available to the owner or owner's agent and to the Inspector, of the BPS used and the bonders or bonding operators employed by him/her, and showing the dates and results of BPS qualifications and bonding performance qualifications.

A328.2.5 Qualification Tests. Tests, as specified in para. A328.2.1(a), shall be performed to qualify each BPS and the performance of each bonder and bonding operator. Test assemblies shall conform to (a) below and the test method shall be in accordance with either (b) or (c).

- (a) Test Assembly. The assembly shall be fabricated in one pipe size in accordance with the BPS and shall contain at least one of each different type of joint identified in the BPS. More than one test assembly may be prepared if necessary to accommodate all of the joint types or to assure that at least one of each joint type is loaded in both circumferential and longitudinal directions. The size of pipe and fittings in the assembly shall be as follows:
- (1) When the largest size to be qualified is DN 100 (NPS 4) or smaller, the test assembly shall be the largest size qualified.

(18)

Table A326.1 Component Standards

Standard or Specification	Designation
Nonmetallic Fittings, Valves, and Flanges	
Process Glass Pipe and Fittings	ASTM C599
Threaded PVC Plastic Pipe Fittings, Sch 80	ASTM D2464
PVC Plastic Pipe Fittings, Sch 40	ASTM D2466
PVC Plastic Pipe Fittings, Sch 80	ASTM D2467
Socket-Type ABS Plastic Pipe Fittings, Sch 40	ASTM D2468
Thermoplastic Gas Pressure Pipe, Tubing, and Fittings	ASTM D2513
Reinforced Epoxy Resin Gas Pressure Pipe and Fittings	ASTM D2517
Plastic Insert Fittings for PE Plastic Pipe	ASTM D2609
Socket-Type PE Fittings for Outside Diameter-Controlled PE Pipe and Tubing	ASTM D2683
CPVC Plastic Hot- and Cold-Water Distribution Systems	ASTM D2846/D2846M
Butt Heat Fusion PE Plastic Fittings for PE Plastic Pipe and Tubing	ASTM D3261
PB Plastic Hot- and Cold-Water Distribution Systems	ASTM D3201
Fiberglass RTR Pipe Fittings for Nonpressure Applications [Note (1)]	ASTM D3840
Machine Made "Fiberglass" (Glass-Fiber-Reinforced Thermosetting Resin) Flanges	ASTM D4024
Contact Molded Fiberglass RTR Flanges [Note (1)]	ASTM D5421
Fiberglass Pressure Pipe Fittings	ASTM D5685
Thoughton The Training The Trai	110111 20000
Threaded CPVC Plastic Pipe Fittings, Sch 80	ASTM F437
Socket-Type CPVC Plastic Pipe Fittings, Sch 40	ASTM F438
CPVC Plastic Pipe Fittings, Schedule 80	ASTM F439
Electrofusion Type PE Fittings for Outside Diameter Controlled PE Pipe and Tubing	ASTM F1055
Plastic-Lined Ferrous Metal Pipe, Fittings, and Flanges [Notes (2), (3), and (4)]	ASTM F1545
Pressure-Rated Polypropylene (PP) Piping Systems	ASTM F2389
Plastic Industrial Ball Valves [Notes (2) and (3)]	MSS SP-122
Nonmetallic Pipes and Tubes	
PE Line Pipe	API 15LE
Low Pressure Fiberglass Line Pipe	API 15LR
Reinforced Concrete Low-Head Pressure Pipe	ASTM C361
Process Glass Pipe and Fittings	ASTM C599
QN.	
ABS Plastic Pipe, Sch 40 and 80	ASTM D1527
PVC Plastic Pipe, Sch 40, 80 and 120	ASTM D1785
PE Plastic Pipe (SIDR-PR) Based on Controlled Inside Diameter	ASTM D2239
PVC Plastic Pressure-Rated Pipe (SDR Series)	ASTM D2241
ABS Plastic Pipe (SDR-PR)	ASTM D2282
Classification for Machine-Made RTR Pipe	ASTM D2310
PE Plastic Pipe, Sch 40 & 80, Based on Outside Diameter	ASTM D2447
Thermoplastic Gas Pressure Pipe, Tubing, and Fittings	ASTM D2513
Reinforced Epoxy Resin Gas Pressure Pipe and Fittings	ASTM D2517
PB Plastic Pipe (SDR-PR)	ASTM D2662
TB TRUSTIC TIPE (OBR TR)	
PB Plastic Tubing	ASTM D2666

Table A326.1 Component Standards (Cont'd)

Standard or Specification	Designation
Nonmetallic Pipes and Tubes (Cont'd)	
PE Plastic Tubing	ASTM D2737
CPVC Plastic Hot- and Cold-Water Distribution System	ASTM D2846/D2846M
Filament-Wound Fiberglass RTR Pipe [Note (1)]	ASTM D2996
Centrifugally Cast Fiberglass RTR Pipe	ASTM D2997
PB Plastic Pipe (SDR-PR) Based on Outside Diameter	ASTM D3000
PE Plastic Pipe (DR-PR) Based on Controlled Outside Diameter	ASTM D3035
PB Plastic Hot- and Cold-Water Distribution Systems	ASTM D3309
Fiberglass RTR Pressure Pipe [Note (1)]	ASTM D3517
Fiberglass RTR Sewer and Industrial Pressure Pipe [Note (1)]	ASTM D3754
CPVC Plastic Pipe, Sch 40 and 80	ASTM F441/F441M
CPVC Plastic Pipe (SDR-PR)	ASTM F442/F442M
Crosslinked Polyethylene/Aluminum/Crosslinked Polyethylene (PEX-AL-PEX) Pressure Pipe	ASTM F1281
Polyethylene/Aluminum/Polyethylene (PE-AL-PE) Composite Pressure Pipe	ASTM F1282
Polyolefin Pipe and Fittings for Corrosive Waste Drainage Systems [Notes (2) and (3)]	ASTM F1412
Plastic-Lined Ferrous Metal Pipe, Fittings, and Flanges [Notes (2), (3), and (4)]	ASTM F1545
PVDF Corrosive Waste Drainage Systems	ASTM F1673
Pressure-Rated Polypropylene (PP) Piping Systems	ASTM F2389
Metric and Inch-sized Crosslinked Polyethylene (PEX) Pipe	ASTM F2788/F2788M
Reinforced Concrete Pressure Pipe, Steel Cylinder Type, for Water and Other Liquids	AWWA C300
Prestressed Concrete Pressure Pipe, Steel Cylinder Type, for Water and Other Liquids	AWWA C301
Reinforced Concrete Pressure Pipe, Noncylinder Type	AWWA C302
Polyvinyl Chloride (PVC) Pressure Pipe and Fabricated Fittings, 4 In. Through 60 In. (100 mm Through 1,500 mm)	AWWA C900
Fiberglass Pressure Pipe	AWWA C950
Miscellaneous	
Contact-Molded RTP Laminates for Corrosion Resistant Equipment	ASTM C582
Threads for Fiberglass RTR Pipe (60 deg stub) [Note (1)]	ASTM D1694
Solvent Cements for ABS Plastic Pipe and Fittings	ASTM D2235
Solvent Cements for PVC Plastic Piping Systems	ASTM D2564
Joints for Plastic Pressure Pipes Using Flexible Elastomeric Seals	ASTM D3139
Fiberglass RTR Pipe Joints Using Flexible Elastomeric Seals [Note (1)]	ASTM D4161
Design and Construction of Nonmetallic Enveloped Gaskets for Corrosive Service	ASTM F336
Solvent Cements for CPVC Plastic Pipe and Fittings	ASTM F493
Taper Pipe Threads 60° for Thermoplastic Pipe and Fittings	ASTM F1498
Metal Insert Fittings for Polyethylene/Aluminum/Polyethylene and Crosslinked Polyethylene/Aluminum/ Crosslinked Polyethylene Composite Pressure Pipe	ASTM F1974

GENERAL NOTE: It is not practical to refer to a specific edition of each standard throughout the Code text. Instead, the approved edition references, along with the names and addresses of the sponsoring organizations, are shown in Appendix E.

NOTES:

- (1) The term "fiberglass RTR" takes the place of the ASTM designation "fiberglass (glass-fiber-reinforced thermosetting resin)."
- (2) This Standard allows the use of unlisted materials; see para. 323.1.2.
- (3) This Standard contains no pressure-temperature ratings.
- (4) Cautionary Note: A metallic piping component lined with nonmetal requires proper interaction between liner and host metallic piping component. This is demonstrated by qualification testing required in ASTM F1545. The designer should review this documentation for compliance.

- (2) When the largest size to be qualified is greater than DN 100 (NPS 4), the size of the test assembly shall be between 25% and 100% of the largest piping size qualified, but shall be a minimum of DN 100 (NPS 4).
- (b) Burst Test Method. The test assembly shall be subjected to a burst test in accordance with the applicable sections of ASTM D1599.⁵ The time to burst in this standard may be extended. The test is successful if failure initiates outside of any bonded joint.
- (c) Hydrostatic Test Method. The test assembly shall be subjected to hydrostatic pressure of at least P_T for not less than 1 hr with no leakage or separation of joints.
- (1) For thermoplastics, P_T shall be determined in accordance with eq. (27)

$$P_T = 0.80\overline{T} \left(\frac{S_S + S_H}{D - \overline{T}} \right) \tag{27}$$

where

D = outside diameter of pipe

 S_H = mean long-term hydrostatic strength (LTHS) in accordance with ASTM D2837. Use twice the 23°C (73°F) HDB design stress from Table B-1 if listed, or use manufacturer's data.

 S_S = mean short-term burst stress in accordance with ASTM D1599,⁵ from Table B-1 if listed, otherwise from manufacturer's data

 \overline{T} = nominal thickness of pipe

- (2) For RTR (laminated and filament-wound) and RPM P_T shall be 3 times the manufacturer's allowable pressure for the components being joined.
- (3) The test shall be conducted so that the joint is loaded in both the circumferential and longitudinal directions.

A328.2.6 Performance Requalification. Renewal of a bonding performance qualification is required when

- (a) a bonder or bonding operator has not used the specific bonding process for a period of 6 months or more, or
- (b) there is specific reason to question the individual's ability to make bonds that meet the BPS

A328.3 Bonding Materials and Equipment

A328.3.1 Materials. Bonding materials that have deteriorated by exposure to air or prolonged storage, or will not spread smoothly, shall not be used in making joints.

A328.3.2 Equipment. Fixtures and tools used in making joints shall be in such condition as to perform their functions satisfactorily.

A328.4 Preparation for Bonding

Preparation shall be defined in the BPS and shall specify such requirements as

- (a) cutting
- (b) cleaning
- (c) preheat
- (d) end preparation
- (e) fit-up

A328.5 Bonding Requirements

A328.5.1 General

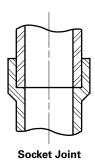
- (a) Production joints shall be made only in accordance with a written bonding procedure specification (BPS) that has been qualified in accordance with para. A328.2. Manufacturers of piping materials, bonding materials, and bonding equipment should be consulted in the preparation of the BPS.
- (b) Production joints shall be made only by qualified bonders or bonding operators who have appropriate training or experience in the use of the applicable BPS and have satisfactorily passed a performance qualification test that was performed in accordance with a qualified BPS
- (c) Each qualified bonder and bonding operator shall be assigned an identification symbol. Unless otherwise specified in the engineering design, each pressure-containing bond or adjacent area shall be stenciled or otherwise suitably marked with the identification symbol of the bonder or bonding operator. Identification stamping shall not be used and any marking paint or ink shall not be detrimental to the piping material. In lieu of marking the bond, appropriate records may be filed.
- (d) Qualification in one BPS does not qualify a bonder or bonding operator for any other bonding procedure.
 - (e) Longitudinal joints are not covered in para. A328.

A328.5.2 Hot Gas Welded Joints in Thermoplastic Piping⁵

- (a) Preparation. Surfaces to be hot gas welded together shall be cleaned of any foreign material. For butt welds, the joining edges should be beveled at 20 deg to 40 deg with 1 mm ($^{1}_{32}$ in.) root face and root gap.
- (b) Procedure. Joints shall be made in accordance with the qualified BPS.
- (c) Branch Connections. A fabricated branch connection shall be made by inserting the branch pipe in the hole in the run pipe. Dimensions of the joint shall conform to Figure 328.4.4, illustration (c). The hole in the run pipe shall be beveled at 45 deg. Alternatively, a fabricated branch connection shall be made using a manufactured full reinforcement saddle with integral socket.

⁵ Titles of referenced standards and specifications are listed in Table A326.1, except ASTM D1599, Test Method for Resistance to Short-Time Hydraulic Pressure of Plastic Pipe, Tubing, and Fittings; ASTM D2657, Practice for Heat Fusion Joining of Polyolefin Pipe and Fittings; ASTM D2855, Practice for Making Solvent-Cemented Joints with PVC Pipe and Fittings; and ASTM F1290, Practice for Electrofusion Joining Polyolefin Pipe and Fittings.

Figure A328.5.3 Thermoplastic Solvent Cemented Joint



A328.5.3 Solvent Cemented Joints in Thermoplastic Piping⁵

- (a) Preparation. Thermoplastic pipe and fitting surfaces shall be prepared in accordance with ASTM D2855 for PVC, ASTM F493 for CPVC, and ASTM D2235 for ABS. A dry fit test of each joint is required before solvent cementing. The pipe shall enter the fitting socket between one-third and two-thirds of the full socket depth when assembled by hand.
- (b) Procedure. Joints shall be made in accordance with the qualified BPS. ASTM D2855 provides a suitable basis for development of such a procedure. Solvent cements for PVC, CPVC, and ABS shall conform to ASTM D2564, D2846, and D2235, respectively. Application of cement to both surfaces to be joined and assembly of these surfaces shall produce a continuous bond between them with visual evidence of cement at least flush with the outer end of the fitting bore around the entire joint perimeter. See Figure A328.5.3.
- (c) Branch Connections. A fabricated branch connection shall be made using a manufactured full reinforcement saddle with integral branch socket. The reinforcement saddle shall be solvent cemented to the run pipe over its entire contact surface.

A328.5.4 Heat Fusion Joints in Thermoplastic Piping⁵

- (a) Preparation. Surfaces to be heat fused together shall be cleaned of all foreign material.
- (b) Procedure. Joints shall be made in accordance with the qualified BPS. The general procedures in ASTM D2657, Techniques I Socket Fusion, II Butt Fusion, and III Saddle Fusion, provide a suitable basis for development of such a procedure. Uniform heating of both surfaces to be joined and assembly of these surfaces shall produce a continuous homogeneous bond between them and shall produce a small fillet of fused material at the outer limits of the joint. See Figure A328.5.4 for typical heat fusion joints. Fixtures shall be used to align components when joints are made.
- (c) Branch Connections. A fabricated branch connection is permitted only where molded fittings are unavailable.

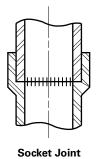
A328.5.5 Electrofusion Joints in Thermoplastic Piping⁵

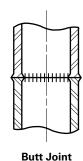
- (a) Preparation. Surfaces to be heat fused together shall be cleaned of all foreign material.
- (b) Procedure. Joints shall be made in accordance with the qualified BPS. The general procedures in ASTM F1290, Technique I Coupling Procedure and Technique II Saddle Procedure, provide a suitable basis for the development of such a procedure. See Figure A328.5.5.

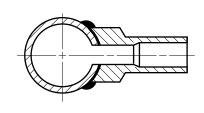
A328.5.6 Adhesive Joints in RTR and RPM Piping

- (a) Procedure. Joints shall be made in accordance with the qualified BPS. Application of adhesive to the surfaces to be joined and assembly of these surfaces shall produce a continuous bond between them and shall seal over all cuts to protect the reinforcement from the service fluid. See Figure A328.5.6.
- (b) Branch Connections. A fabricated branch connection shall be made using a manufactured full reinforcement saddle having a socket or integral length of branch pipe suitable for a nozzle or coupling. The hole in the run pipe shall be made with a hole saw; the cut

Figure A328.5.4 Thermoplastic Heat Fusion Joints







Saddle Joint

Figure A328.5.5 Thermoplastic Electrofusion Joints

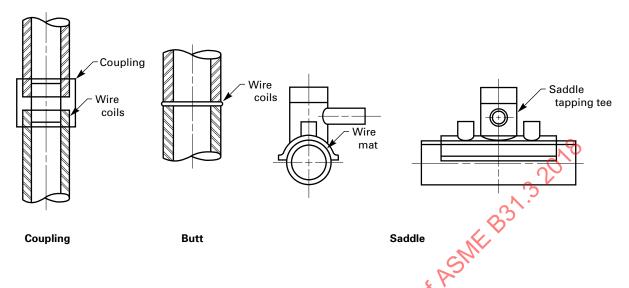


Figure A328.5.6 Fully Tapered Thermosetting Adhesive
Joint

Overwrapped Bell and Spigot Joint

Butt and Wrapped Joint

edges of the hole shall be sealed with adhesive at the time the saddle is bonded to the run pipe.

A328.5.7 Butt-and-Wrapped Joints in RTR and RPM Piping⁵

- (a) Procedure. Joints shall be made in accordance with the qualified BPS. Application of plies of reinforcement saturated with catalyzed resin to the surfaces to be joined shall produce a continuous structure with them. Cuts shall be sealed to protect the reinforcement from the service fluid. See Figure A328.5.7.
- (b) Branch Connections. For a fabricated branch connection made by inserting the branch pipe into a hole in the run pipe, the hole shall be made with a hole saw.

A328.6 Bonding Repair

Defective material, joints, and other workmanship that fails to meet the requirements of this Code and of the engineering design shall be repaired or replaced. See also para. 341.3.3.

Figure A328.5.7 Thermosetting Wrapped Joints

A328.7 Seal Bonds

If threaded joints are to be seal bonded in accordance with para. A311.2.2, the work shall be done by qualified bonders and all exposed threads shall be covered by the seal bond.

A329 FABRICATION OF PIPING LINED WITH NONMETALS

A329.1 Welding of Metallic Piping

A329.1.1 General

- (a) Paragraph A329.1 applies only to welding subassemblies of metallic piping that have previously been lined with nonmetals.
- (b) Welding that conforms to para. A329.1 may be used in accordance with para. A318.3.1.
- **A329.1.2 Specific Welding Requirements.** Welding shall conform to the requirements of para. 328 and the following additional requirements:
- (a) Modifications made in preparation for welding to suit manufacturer's recommendations shall be specified in the engineering design.
- (b) Welding shall be performed so as to maintain the continuity of the lining and its serviceability.
- (c) If a lining has been damaged, it shall be repaired or replaced.
- (d) Qualification to one WPS for a specific lining material does not qualify a welder or welding operator for any other welding procedure involving different lining materials.

A329.2 Flaring of Nonmetallic Linings A329.2.1 General

- (a) Paragraph A329.2 applies only to the flaring of linings in pipe that has previously been lined with nonmetals.
- (b) Flaring that conforms to para. A329.2 may be used in accordance with para. A318.3.2.
- (c) Flaring shall be performed only in accordance with a written flaring procedure specification, and only by qualified operators who have appropriate training or experience in the use of the applicable flaring procedure specification.

A332 BENDING AND FORMING

A332.1 General

Paragraph 3321 applies in its entirety.

A332.2 Bending

Paragraph 332.2 applies, except para. 332.2.2.

A332.3 Forming

Paragraph 332.3 applies, except for heat treatment.

A334 JOINING NONPLASTIC PIPING

A334.1 Borosilicate Glass Piping

Short unflanged pieces used to correct for differences between fabrication drawings and field dimensions may be cut to length and finished in the field.

A334.2 Repair of Defects

Defective material, joints, and other workmanship in nonplastic piping that fail to meet the requirements of para. A334 or of the engineering design shall be repaired or replaced.

Completed repairs and replacements shall be examined, subject to the same limitations on imperfections as the original work.

A335 ASSEMBLY AND ERECTION

A335.1 Alignment

Paragraph 335.1 applies in its entirety.

A335.2 Flanged and Mechanical Joints

Paragraph 335.2 applies in its entirety.

A335.2.5 Nonmetallic Bolted Joints

- (a) Bolted joints in nonmetallic piping may be assembled with any combination of flange material and flange facings, except that the following apply when other than flat face flanges and full face gaskets are used:
- (1) consideration shall be given to the strength of the flanges, and to sustained loads, displacement strains, and occasional loads described in paras. A302.3.3 and A302.3.4
- (2) an appropriate bolt-up sequence shall be specified
- (b) Appropriate limits shall be specified for bolt-up torque, and those limits shall not be exceeded.
- (c) Flat washers shall be used under bolt heads and nuts.

A335.2.6 Metallic Piping Lined With Nonmetals. In assembling mechanical joints in metallic piping lined with nonmetals, consideration shall be given to means for maintaining electrical continuity between pipe sections, where static sparking could cause ignition of flammable vapors. See Appendix F, para. FA323.4(a).

A335.3 Threaded Joints

Paragraph 335.3 applies except for para. 335.3.2. See para. A335.3.2.

A335.3.2 Joints for Seal Bonding. A threaded joint to be seal bonded shall be made up without thread compound. A joint containing thread compound that leaks during leak testing may be seal bonded in

accordance with para. A328.6, provided all compound is removed from exposed threads.

A335.3.4 Tools, Nonmetallic Piping. Either strap wrenches or other full circumference wrenches shall be used to tighten threaded pipe joints. Tools and other devices used to hold or apply forces to the pipe shall be such that the pipe surface is not scored or deeply scratched.

A335.3.5 RTR and RPM Piping. In assembling threaded joints in RTR and RPM piping, where threads may be exposed to fluids that can attack the reinforcing material, threads shall be coated with sufficient resin to cover the threads and completely fill the clearance between the pipe and the fitting.

A335.4 Tubing Joints

A335.4.1 Flared Joints in Thermoplastic Tubing. In addition to preparation in accordance with para. 335.4.1, the end of the tubing shall be cut perpendicular to the tube centerline, preferably with a tubing cutter specially made for thermoplastic tubing. No cuts, scratches, dirt, or surface damage to either inside or outside diameter are permitted on the pipe end to be flared.

A335.4.2 Flareless and Compression Tubing Joints. Paragraph 335.4.2 applies.

A335.5 Caulked Joints

Paragraph 335.5 applies.

A335.6 Special Joints

Paragraph 335.6 applies, except that expanded joints are not permitted.

A335.6.3 Flexible Elastomeric Sealed Joints. Assembly of flexible elastomeric sealed joints shall be in accordance with the manufacturer's recommendations and the following:

- (a) Seal and bearing surfaces shall be free from injurious imperfections.
- (b) Any lubricant used to facilitate joint assembly shall be compatible with the joint components and the intended service.
- (c) Proper joint clearances and piping restraints (if not integral in the joint design) shall be provided to prevent joint separation when expansion can occur due to thermal and/or pressure effects.

A335.8 Assembly of Brittle Piping

A335.8.1 General. Care shall be used to avoid scratching of brittle nonmetallic piping in handling and supporting. Any scratched or chipped components shall be replaced. Care shall be used in handling glasslined and cement-lined metal pipe because the lining

can be injured or broken by blows that do not dent or break the pipe.

A335.8.2 Borosilicate Glass Piping. In addition to the precaution in para. A335.8.1, borosilicate glass piping components shall be protected from weld spatter. Any component so damaged shall be replaced. Flanges and cushion inserts shall be carefully fitted and aligned to pipe, fittings, and valve ends. Gaskets shall be of the construction recommended for the joint. Installation and torquing of bolts shall be in accordance with the manufacturer's recommendations.

A335.9 Cleaning of Piping

See Appendix F, para. F335.9

PART 10 INSPECTION, EXAMINATION, AND TESTING

A340 INSPECTION

Paragraph 340 applies in its entirety.

A341 EXAMINATION

A341.1 General

Paragraph 341.1 applies.

A341.2 Responsibility for Examination

Paragraph 341.2 applies in its entirety.

A341.3 Examination Requirements

A341.3.1 Responsibility for Examination. Paragraph 341.3.1 applies, except for (a) and (b), which apply only for metals.

A341.3.2 Acceptance Criteria. Acceptance criteria shall be as stated in the engineering design, and shall at least meet the applicable requirements for bonds in Table A341.3.2 and requirements elsewhere in the Code.

A341.3.3 Defective Components and Workmanship. Paragraph 341.3.3 applies in its entirety.

A341.3.4 Progressive Sampling for Examination. Paragraph 341.3.4 applies in its entirety.

A341.4 Extent of Required Examination

- **A341.4.1 Examination Normally Required.** Piping in Normal Fluid Service shall be examined to the extent specified herein or to any greater extent specified in the engineering design. Acceptance criteria are as stated in para. A341.3.2 unless otherwise specified.
- (a) Visual Examination. At least the following shall be examined in accordance with para. 344.2:

Table A341.3.2 Acceptance Criteria for Bonds

	Thermoplastic Material		RTR and RPM Materials	
Type of Imperfection	Hot Gas Welded Joint	Solvent Cemented Joint	Heat Fusion Joint	[Note (1)] — Adhesive Cemented Joint
Cracks	None permitted	Not applicable	None permitted	None permitted
Unfilled areas in joint	None permitted	None permitted	None permitted	None permitted
Unbonded areas in joint	None permitted	None permitted	None permitted	None permitted
Inclusions of charred material	None permitted	Not applicable	None permitted	None permitted
Unfused filler material inclusions	None permitted	Not applicable	Not applicable	None permitted
Protrusion of material into pipe bore, % of pipe wall thickness	Not applicable	Cement, 50%	Fused material, 25%	Adhesive, 25%

NOTE: (1) RTR = reinforced thermosetting resin; RPM = reinforced plastic mortar.

- (1) materials and components in accordance with para. 341.4.1(a)(1).
- (2) at least 5% of fabrication. For bonds, each type of bond made by each bonder and bonding operator shall be represented.
- (3) 100% of fabrication for bonds other than circumferential, except those in components made in accordance with a listed specification.
- (4) assembly and erection of piping in accordance with paras. 341.4.1(a)(4), (5), and (6).
- (b) Other Examination. Not less than 5% of all bonded joints shall be examined by in-process examination in accordance with para. 344.7, the joints to be examined being selected to ensure that the work of each bonder and bonding operator making the production joints is examined.
- (c) Certifications and Records. Paragraph 341.4.(c) applies.

A341.4.2 Examination — **Category D Fluid Service.** Piping and piping elements for Category D Fluid Service as designated in the engineering design shall be visually examined to the extent necessary to satisfy the examiner that components, materials, and workmanship conform to the requirements of this Code and the engineering design.

A341.5 Supplementary Examination

A341.5.1 General. Any applicable method of examination described in para. 344 may be specified by the engineering design to supplement the examination required by para. A341.4. The extent of supplementary examination to be performed and any acceptance criteria that differ from those in para. A341.3.2 shall be specified in the engineering design.

A341.5.2 Examinations to Resolve Uncertainty. Paragraph 341.5.3 applies.

A342 EXAMINATION PERSONNEL

Paragraph 342 applies in its entirety.

A343 EXAMINATION PROCEDURES

Paragraph 343 applies in its entirety.

A344 TYPES OF EXAMINATION

A344.1 General

Paragraph 344.1 applies in its entirety.

A344.2 Visual Examination

Paragraph 344.2 applies in its entirety.

A344.5 Radiographic Examination

Radiographic examination may be used in accordance with para. 344.1.2.

A344.6 Ultrasonic Examination

Ultrasonic examination may be used in accordance with para. 344.1.2.

A344.7 In-Process Examination

Paragraph 344.7 applies in its entirety.

A345 TESTING

A345.1 Required Leak Test

- (a) Prior to initial operation, each piping system shall be tested to ensure tightness. The test shall be a hydrostatic leak test in accordance with para. A345.4, except as provided herein.
 - (b) Paragraphs 345.1(a) and (b) apply.

A345.2 General Requirements for Leak Test

Requirements in para. A345.2 apply to more than one type of leak test.

A345.2.1 Limitations on Pressure. Paragraphs 345.2.1(b) and (c) apply.

A345.2.2 Other Test Requirements

- (a) Paragraph 345.2.2(a) applies.
- (b) The possibility of brittle fracture shall be considered when conducting leak tests on brittle materials or at low temperature.
 - (c) Paragraphs 345.2.3 through 345.2.7 apply.

A345.3 Preparation for Leak Test

Paragraph 345.3 applies in its entirety, considering bonds in place of welds, and excluding expansion joints.

A345.4 Hydrostatic Leak Test

A345.4.1 Test Fluid. Paragraph 345.4.1 applies.

A345.4.2 Test Pressure

- (a) Nonmetallic Piping. Except as provided in para. A345.4.3, the hydrostatic test pressure at any point in a nonmetallic piping system shall be not less than 1.5 times the design pressure, but shall not exceed 1.5 times the maximum rated pressure of the lowest-rated component in the system.
- (b) Thermoplastic Piping. For piping systems in which the design temperature is above the test temperature, para. 345.4.2(b) applies, except that S and S_T shall be from Table B-1 instead of Table A-1 or Table A-1M.
- (c) Metallic Piping With Nonmetallic Lining. Paragraph 345.4.2 applies.

A345.4.3 Hydrostatic Test of Piping With Vessels as a System. Paragraph 345.4.3 applies.

A345.5 Pneumatic Leak Test

A345.5.1 Precautions. In addition to the requirements of para. 345.5.1, a pneumatic test of nonmetallic piping is permitted only with the owner's approval, and precautions in Appendix F, para. FA323.4 should be considered.

A345.5.2 Other Requirements

- (a) Paragraphs 345.5.2 through 345.5.5 apply.
- (b) PVC and CPVC piping shall not be pneumatically tested.

A345.6 Hydrostatic-Pneumatic Leak Test

If a combined hydrostatic-pneumatic leak test is used, the requirements of para. A345.5 shall be met, and the pressure in the liquid-filled part of the piping shall not exceed the values calculated in accordance with para. A345.4.2 or 345.4.2, as applicable.

A345.7 Initial Service Leak Test

Paragraph 345.7 applies in its entirety for Category D Fluid Service only.

A345.8 Sensitive Leak Test

Paragraph 345.8 applies.

🗘 A346 RECORDS

Paragraph 346 applies in its entirety.

Chapter VIII Piping for Category M Fluid Service

M300 GENERAL STATEMENTS

- (a) Chapter VIII pertains to piping designated by the owner as being in Category M Fluid Service. See para. 300(b)(1) and Appendix M.
- (b) The organization, content, and paragraph designations of this Chapter correspond to those of the base Code (Chapters I through VI) and Chapter VII. The prefix M is used.
- (c) Provisions and requirements of the base Code and Chapter VII apply only as stated in this Chapter.
- (d) Consideration shall be given to the possible need for engineered safeguards as described in Appendix G, para. G300.3, in addition to the inherent safeguards described in paras. G300.1 and G300.2.
- (e) This Chapter makes no provision for piping to be used under severe cyclic conditions. If it is not feasible to eliminate the severe cyclic conditions, the engineering design shall specify any necessary provisions in accordance with para. 300(c)(5).
 - (f) Chapter I applies in its entirety.

PART 1 CONDITIONS AND CRITERIA

M301 DESIGN CONDITIONS

Paragraph 301 applies in its entirety, with the exceptions of paras. 301.3 and 301.5. See paras. M301.3 and M301.5.

M301.3 Design Temperature, Metallic Piping

Use of any temperature other than the fluid temperature as the design temperature shall be substantiated by heat transfer calculations confirmed by tests or by experimental measurements.

M301.5 Dynamic Effects

Paragraph 301.5 applies with the exception of paras. 301.5.1 and 301.5.4. See paras. M301.5.1 and M301.5.4.

M301.5.1 Impact. Design, layout, and operation of piping shall be conducted so as to minimize impact and shock loads. In the event that such loadings are unavoidable, para. 301.5.1 applies.

M301.5.4 Vibration. Suitable dynamic analysis such as computer simulation, shall be made where recessary to avoid or minimize conditions that lead to detrimental vibration, pulsation, or resonance effects in the piping.

M302 DESIGN CRITERIA

M302.1 General

Paragraph M302 pertains to pressure-temperature ratings, stress criteria, design allowances, and minimum design values, together with permissible variations of these factors as applied to piping design. Paragraph 302 applies in its entirety, with the exception of para. 302.2.4. See para. M302.2.4.

M302.2.4 Allowance for Pressure and Temperature Variations, Metallic Piping. Use of allowances in para. 302.2.4 is not permitted.

PART 2 PRESSURE DESIGN OF METALLIC PIPING COMPONENTS

M303 GENERAL

Paragraph 303 applies in its entirety.

M304 PRESSURE DESIGN OF METALLIC COMPONENTS

Paragraph 304 applies in its entirety.

PART 3 FLUID SERVICE REQUIREMENTS FOR METALLIC PIPING COMPONENTS

M305 PIPE

M305.1 General

Listed pipe may be used in accordance with para. M305.2. Unlisted pipe may be used only as provided in para. 302.2.3.

M305.2 Specific Requirements for Metallic Pipe

Pipe listed in para. 305.2.2 shall not be used. The provision for severe cyclic conditions in para. 305.2.3 does not apply [see para. M300(e)].

M306 METALLIC FITTINGS, BENDS, MITERS, LAPS, AND BRANCH CONNECTIONS

General. Fittings, bends, miters, laps, and branch connections may be used in accordance with paras. M306.1 through M306.6. Pipe and other materials used in such components shall be suitable for the manufacturing process and the fluid service.

M306.1 Pipe Fittings

Paragraph 306.1 applies in its entirety, with the exception of paras. 306.1.3 and 306.1.4. See para. M306.1.3.

M306.1.3 Specific Fittings

- (a) Proprietary welding branch outlet fittings that have been design proof tested successfully as prescribed in ASME B16.9, MSS SP-97, or ASME BPVC, Section VIII, Division 1, UG-101 may be used within their established ratings.
- (b) Fittings conforming to MSS SP-43 and MSS SP-119 shall not be used.
- (c) Proprietary "Type C" lap-joint stub-end butt-welding fittings shall not be used.

M306.2 Pipe Bends

Paragraph 306.2 applies, except that bends designed as creased or corrugated shall not be used.

M306.3 Miter Bends

A miter bend shall conform to para 306.3.1 and shall not make a change in direction at a single joint (angle α in Figure 304.2.3) greater than 22.5 deg. Paragraph 306.3.3 does not apply [see para. M300(e)].

M306.4 Fabricated or Flared Laps

M306.4.1 General. The following requirements do not apply to fittings conforming to para. M306.1, nor to laps integrally forged on pipe ends. Paragraph 306.4.1 applies.

M306.4.2 Flared Laps. Flared laps shall not be used.

M306.5 Fabricated Branch Connections

The following requirements do not apply to fittings conforming to para. M306.1. Paragraph 306.5.1 applies, with the following exceptions:

(a) Of the methods listed in para. 304.3.1(a), the one in para. 304.3.1(a)(3) may be used only if those in paras. 304.3.1(a)(1) and (2) are unavailable.

(b) Of the branch connections described in paras. 304.3.2(b) and (c), those having threaded outlets are permitted only in accordance with para. M314 and those having socket welding outlets are permitted only in accordance with para. M311.2.

M306.6 Closures

The following requirements do not apply to blind flanges or to fittings conforming to para. M306.1. Of the closures described in para. 304.4, flat closures in accordance with ASME BPVC, Section VMI, Division 1, UG-34 and UW-13, and conical closures without transition knuckles [UG-32(g) and UG-33(f)], may be used only if others are not available. The requirements in M306.5 apply to openings in closures [see also para. 304.4.2(b)].

M307 METALLIC VALVES AND SPECIALTY COMPONENTS

The following requirements for valves shall also be met as applicable by other pressure-containing piping components, e.g., traps, strainers, and separators. See also Appendix P, paras. F301.4 and F307.

M307.1 General

Paragraph 307.1 applies, subject to the requirements in para. M307.2.

M307.2 Specific Requirements

- (a) Paragraph 307.2.2 applies.
- (b) Valves having threaded bonnet joints (other than union joints) shall not be used.
- (c) Only metallic valves conforming to the following requirements may be used:
- (1) Special consideration shall be given to valve design to prevent stem leakage to the environment.
- (2) Bonnet or cover plate closures and body joints shall be flanged, secured by at least four bolts with gasketing conforming to para. 308.4; or proprietary, attached by bolts, lugs, or other substantial means, and having a gasket design that increases gasket compression as fluid pressure increases; or secured with a full penetration weld made in accordance with para. M311; or secured by a straight thread sufficient for mechanical strength, a metal-to-metal seat, and a seal weld made in accordance with para. M311, all acting in series.

M308 FLANGES, BLANKS, FLANGE FACINGS, AND GASKETS

Paragraph 308.1 applies in its entirety.

M308.2 Specific Requirements for Metallic Flanges

Paragraph 308.2.4 does not apply [see para. M300(e)]. The following shall not be used:

- (a) single-welded slip-on flanges
- (b) expanded-joint flanges
- (c) slip-on flanges used as lapped flanges unless the requirements in para. 308.2.1(c) are met
- (d) threaded metallic flanges, except those employing lens rings or similar gaskets and those used in lined pipe where the liner extends over the gasket face

M308.3 Flange Facings

Paragraph 308.3 applies in its entirety.

M308.4 Gaskets

Paragraph 308.4 applies in its entirety.

M308.5 Blanks

All blanks shall be marked with material, rating, and size.

M309 BOLTING

Paragraph 309 applies, except for para. 309.2.4 [see para. M300(e)].

PART 4 FLUID SERVICE REQUIREMENTS FOR METALLIC PIPING JOINTS

M310 METALLIC PIPING, GENERAL

Paragraph 310 applies in its entirety.

M311 WELDED JOINTS IN METALLIC PIPING

Welded joints may be made in any metal for which it is possible to qualify welding procedures welders, and welding operators in accordance with para. M328.

M311.1 General

Paragraph 311.1 applies with the following exceptions:

- (a) Split backing rings shall not be used.
- (b) Socket welded joints greater than DN 50 (NPS 2) are not permitted.
- (c) Examination shall be in accordance with para. M341.4

M311.2 Specific Requirements

Paragraphs 311.2.1(a); 311.2.2(a), (b), and (d); 311.2.3; and 311.2.4 apply.

M312 FLANGED JOINTS IN METALLIC PIPING

Paragraph 312 applies in its entirety.

M313 EXPANDED JOINTS IN METALLIC PIPING

Expanded joints shall not be used.

M314 THREADED JOINTS IN METALLIC PIPING M314.1 General

Paragraphs 314.1(a), (b), and (c) apply.

M314.2 Specific Requirements

M314.2.1 Taper-Threaded Joints. Paragraph 314.2.1 applies except that only components suitable for Normal Fluid Service in sizes $8 \le DN \le 25$ ($\frac{1}{4} \le NPS \le 1$) are permitted (see Table 314.2.1). Sizes smaller than DN 20 (NPS $\frac{3}{4}$) shall be safeguarded (see Appendix G).

M314.2.2 Straight-Threaded Joints. Paragraph 314.2.2 applies. In addition, components shall have adequate mechanical strength and the joint shall have a confined seating surface not subject to relative rotation as or after the joint is tightened. [See Figure 335.3.3, illustrations (b) and (c) for acceptable construction.]

M315 TUBING JOINTS IN METALLIC PIPING

Paragraph 315 applies, except for para. 315.2(b).

M316 CAULKED JOINTS

Caulked joints shall not be used.

M317 SOLDERED AND BRAZED JOINTS

Soldered, brazed, and braze welded joints shall not be used.

M318 SPECIAL JOINTS IN METALLIC PIPING

Paragraph 318 applies, with the exception that adhesive joints and bell type joints shall not be used.

PART 5 FLEXIBILITY AND SUPPORT OF METALLIC PIPING

M319 FLEXIBILITY OF METALLIC PIPING

Paragraph 319 applies, with the exception that the simplified rules in para. 319.4.1(c) do not apply.

M320 ANALYSIS OF SUSTAINED LOADS

Paragraph 320 applies.

M321 PIPING SUPPORT

Paragraph 321 applies, except that supporting elements welded to the piping shall be of listed material.

PART 6 SYSTEMS

M322 SPECIFIC PIPING SYSTEMS

M322.3 Instrument Piping

Paragraph 322.3 applies, with the exception that for signal tubing in contact with process fluids and process temperature–pressure conditions

- (a) tubing shall be not larger than 16 mm ($\frac{5}{8}$ in.) 0.D. and shall be suitable for the service
- (b) an accessible block valve shall be provided to isolate the tubing from the pipeline
- (c) joining methods shall conform to the requirements of para. M315

M322.6 Pressure-Relieving Systems

Paragraph 322.6 applies, except for para. 322.6.3. See para. M322.6.3.

M322.6.3 Overpressure Protection

- (a) Paragraph 322.6.3(a) applies.
- (b) Relief set pressure shall be in accordance with ASME BPVC, Section VIII, Division 1.
- (c) The maximum relieving pressure shall be in accordance with Section VIII, Division 1.

PART 7 METALLIC MATERIALS

M323 GENERAL REQUIREMENTS

M323.1 Materials and Specifications

Paragraph 323.1.1 applies. See paras. M323.1.2, M323.1.3, and M323.1.4.

M323.1.2 Unlisted Materials. Paragraph 323.1.2 applies, with the additional requirement that the designer shall fully document the determination of allowable stresses as part of the engineering design.

M323.1.3 Unknown Materials. Materials of unknown specification shall not be used.

M323.1.4 Reclaimed Metallic Materials. Reclaimed materials may be used when the material certification records are available for the specific materials employed, and the designer is assured that the material is sound and free from harmful defects.

(18) M323.2 Temperature Limitations

Paragraph 323.2 applies with the exception that, in regard to lower temperature limits, the relaxation of minimum temperature limits stated in Notes (3) and (6) of Table 323.2.2 and in paras. 323.2.2(h) and (i) is not permitted.

M323.3 Impact Testing Methods and Acceptance Criteria

Paragraph 323.3 applies in its entirety.

M323.4 Fluid Service Requirements for Metallic Materials

Paragraph 323.4.1 applies.

M323.4.2 Specific Requirements. Paragraph 323.4.2 applies, except that cast irons other than ductile iron shall not be used for pressure-containing parts, and lead and tin shall be used only as linings.

M323.4.3 Metallic Cladding and Lining Materials. In addition to the requirements of para. 323.4.3, where materials covered in paras. 323.4.2(c)(2) and 323.4.3 are used as cladding or lining in which the cladding or lining also serves as a gasket or as part of the flange facing, consideration shall be given to the design of the flanged joint to prevent leakage to the environment.

M323.5 Deterioration of Materials in Service

Paragraph 323.5 applies in its entirety.

M325 MATERIALS — MISCELLANEOUS

M325.1 Joining and Auxiliary Materials

In applying para. 325, materials such as solvents, brazes, and solders shall not be used. Nonmetallic materials used as gaskets and packing materials shall be suitable for the fluid service.

PART 8 STANDARDS FOR PIPING COMPONENTS

M326 DIMENSIONS AND RATINGS OF COMPONENTS

Paragraph 326.1.3 applies.

M326.1 Dimensional Requirements

M326.1.1 Listed Piping Components. Except for prohibitions and restrictions stated elsewhere in Chapter VIII, components made in accordance with standards and specifications listed in Table 326.1 may be used in Category M service.

M326.1.2 Unlisted Piping Components. Paragraph 326.1.2 applies, except that dimensions of unlisted components shall be governed by requirements in paras. 303 and 304.

M326.2 Ratings of Components

Paragraph 326.2 applies in its entirety.

M326.3 Reference Documents

Paragraph 326.3 applies in its entirety.

PART 9 FABRICATION, ASSEMBLY, AND ERECTION OF METALLIC PIPING

M327 GENERAL

Metallic piping materials and components are prepared for assembly and erection by one or more of the fabrication processes in paras. M328, M330, M331, and M332. When any of these processes is used in assembly and erection, requirements are the same as for fabrication.

M328 WELDING OF METALS

Welding shall be in accordance with paras. M311.1 and 328, except see para. M328.3.

M328.3 Welding Materials

Paragraph 328.3 applies in its entirety, except that split backing rings shall not be used, and removable backing rings and consumable inserts may be used only where their suitability has been demonstrated by procedure qualification.

M330 PREHEATING OF METALS

Paragraph 330 applies in its entirety.

M331 HEAT TREATMENT OF METALS

Paragraph 331 applies in its entirety, with the exception that no requirements less stringent than those of Table 331.1.1 shall be specified.

M332 BENDING AND FORMING OF METALS

Paragraph 332 applies in its entirety, except that bending that conforms to para. 332.2.3 is not permitted.

M335 ASSEMBLY AND ERECTION OF METALLIC PIPING

M335.1 General

(18) **M335.1.1 Alignment.** In addition to the requirements of para. 335.1, any bending or forming required for alignment and fit-up shall be heat treated if required by para. 332.4.

M335.2 Flanged Joints

Paragraph 335.2 applies in its entirety.

M335.3 Threaded Joints

Paragraphs 335.3.1 and 335.3.2 apply. See paras. M335.3.3 and M335.3.4.

M335.3.3 Straight-Threaded Joints. The requirements of para. 335.3.3 are subject to the limitations in para. M322.

M335.3.4 Condition of Threads. Taper-threaded components and threaded ends permitted under para. M314.2.1 shall be examined before assembly for cleanliness and continuity of threads and shall be rejected if not in conformance with ASME B1.20.1 or other applicable standards.

M335.4 Tubing Joints

M335.4.1 Flared Tubing Joints. The requirements of para. 335.4.1 apply; however, see para. M322 for limitations associated with specific piping systems.

M335.4.2 Flareless and Compression Tubing Joints. The requirements of para. 335.4.2 apply; however, see para. M322 for limitations associated with specific piping systems.

M335.6 Special Joints

Special joints shall be in accordance with paras. M318 and 335.6.1.

M335.9 Cleaning of Piping

See Appendix F, para. F335.9.

M335.10 Identification of Piping

See Appendix F, para. F335.10.

PART 10 INSPECTION, EXAMINATION, TESTING, AND RECORDS OF METALLIC PIPING

M340 INSPECTION

Paragraph 340 applies in its entirety.

M341 EXAMINATION

Paragraphs 341.1, 341.2, 341.3, and 341.5 apply in their entirety. See para. M341.4.

M341.4 Extent of Required Examination

Paragraph 341.4.1 applies with the following exceptions:

- (a) Visual Examination
 - (1) All fabrication shall be examined.
- (2) All threaded, bolted, and other mechanical joints shall be examined.

(b) Other Examination. The radiography/ultrasonic examination requirements of para. 341.4.1(b)(1) apply, except that 100% of circumferential butt and miter welds and of fabricated lap and branch connection welds comparable to those shown in Figure 328.5.4E; Figure 328.5.4F; and Figure 328.5.5, illustrations (d) and (e), shall be examined.

M342 EXAMINATION PERSONNEL

Paragraph 342 applies.

M343 EXAMINATION PROCEDURES

Paragraph 343 applies.

M344 TYPES OF EXAMINATION

Paragraph 344 applies in its entirety.

M345 TESTING

Paragraph 345 applies, except that

- (a) a sensitive leak test in accordance with para. 345.8 shall be included in the required leak test (para. 345.1)
- (b) the initial service leak test (para. 345.7) does not apply

M346 RECORDS

Paragraph 346 applies in its entirety.

PARTS 11 THROUGH 20, CORRESPONDING TO CHAPTER VII

See para. M300(b).

MA300 GENERAL STATEMENTS

Paragraphs MA300 through MA346 apply to nonmetallic piping and piping lined with nonmetals, based on Chapter VII. Paragraph A300(d) applies.

PART 11 CONDITIONS AND CRITERIA

MA301 DESIGN CONDITIONS

Paragraph A301 applies in its entirety.

MA302 DESIGN CRITERIA

Paragraphs A302.1 and A302.4 apply. See paras. MA302.2 and MA302.3.

MA302.2 Pressure-Temperature Design Criteria

Paragraph A302.2 applies, with the exception of para. A302.2.4. See para. MA302.2.4.

MA302.2.4 Allowances for Pressure and Temperature Variation. Paragraph A302.2.4(a) applies to both nonmetallic piping and to metallic piping with nonmetallic lining.

MA302.3 Allowable Stresses and Other Design Limits

Paragraph A302.3 applies.

MA302.4 Allowances

Paragraph 302.4 applies in its entirety.

PART 12 PRESSURE DESIGN OF NONMETALLIC PIPING COMPONENTS

MA303 GENERAL

Paragraph A303 applies in its entirety.

MA304 PRESSURE DESIGN OF NONMETALLIC COMPONENTS

Paragraph A304 applies in its entirety.

PART 13 FLUID SERVICE REQUIREMENTS FOR NONMETALLIC PIPING COMPONENTS

MA305 PIPE

Paragraph A305 applies in its entirety.

MA306 NONMETALLIC FITTINGS, BENDS, MITERS, LAPS, AND BRANCH CONNECTIONS

Paragraphs A306.1 and A306.2 apply. See para. MA306.3.

MA306.3 Miter Bends

Miter bends not designated as fittings conforming to para. A306.1 shall not be used.

MA306.4 Fabricated Laps

Fabricated laps shall not be used.

MA306.5 Fabricated Branch Connections

Nonmetallic fabricated branch connections shall not be used.

MA307 VALVES AND SPECIALTY COMPONENTS

Paragraph A307 applies, except that nonmetallic valves and specialty components shall not be used.

MA308 FLANGES, BLANKS, FLANGE FACINGS, AND GASKETS

Paragraphs A308.1, 308.3, and A308.4 apply in their entirety. See para. MA308.2.

MA308.2 Nonmetallic Flanges

Threaded nonmetallic flanges shall not be used.

MA309 BOLTING

Paragraph A309 applies in its entirety.

PART 14 FLUID SERVICE REQUIREMENTS FOR NONMETALLIC PIPING JOINTS

MA310 GENERAL

Paragraph 310 applies in its entirety.

MA311 BONDED JOINTS

MA311.1 General

Paragraph A311.1 applies in its entirety.

MA311.2 Specific Requirements

Hot gas welded, heat fusion, solvent cemented, and adhesive bonded joints are not permitted except in linings.

MA312 FLANGED JOINTS

Paragraph 312 applies in its entirety.

MA313 EXPANDED JOINTS

Expanded joints shall not be used.

MA314 THREADED JOINTS

MA314.1 General

Threaded joints shall not be used.

MA315 TUBING JOINTS IN NONMETALLIC PIPING

Paragraph A315 applies in its entirety.

MA316 CAULKED JOINTS

Caulked joints shall not be used.

MA318 SPECIAL JOINTS

Paragraph A318 applies in its entirety.

PART 15 FLEXIBILITY AND SUPPORT OF NONMETALLIC PIPING

MA319 PIPING FLEXIBILITY

Paragraph A319 applies in its entirety.

MA321 PIPING SUPPORT

Paragraph A321 applies in its entirety

PART 16 NONMETALLIC AND NONMETALLIC-LINED SYSTEMS

MA322 SPECIFIC PIPING SYSTEMS

Paragraph A322 applies in its entirety.

PART 17 NONMETALLIC MATERIALS

MA323 GENERAL REQUIREMENTS

Paragraph A323.1 applies with the additional requirement described in para. MA323.1.2. Paragraph A323.2 applies in its entirety. See para. MA323.4.

MA323.1.2 Unlisted Materials. Paragraph 323.1.2 applies with the additional requirement that the designer shall fully document the determination of allowable stresses as part of the engineering design.

MA323.4 Fluid Service Requirements for Nonmetallic Materials

Paragraph A323.4.1 applies. See paras. MA323.4.2 and MA323.4.3.

MA323.4.2 Specific Requirements. Paragraph A323.4.2 applies, except that materials listed under paras. A323.4.2(a), (b), and (d) may be used only as linings. Thermoplastics may be used as gaskets in accordance with paras. M325.1 and MA323.4.3.

MA323.4.3 Nonmetallic Lining Materials. Paragraph A323.4.3 applies with the additional requirement that where a material in para. A323.4.2 is used as a lining that also serves as a gasket or as part of the flange facing, consideration shall be given to design of the flanged joint to prevent leakage to the environment.

PART 18 STANDARDS FOR NONMETALLIC AND NONMETALLIC-LINED PIPING COMPONENTS

MA326 DIMENSIONS AND RATINGS OF COMPONENTS

Paragraph A326 applies in its entirety. Table A326.1 applies, except for components and systems prohibited or restricted elsewhere in this Chapter.

PART 19 FABRICATION, ASSEMBLY, AND ERECTION OF NONMETALLIC AND NONMETALLIC-LINED PIPING

MA327 GENERAL

Paragraph A327 applies in its entirety.

MA328 BONDING OF PLASTICS

Paragraph A328 applies in its entirety.

MA329 FABRICATION OF PIPING LINED WITH NONMETALS

Paragraph A329 applies in its entirety.

MA332 BENDING AND FORMING

Paragraph A332 applies in its entirety.

MA334 JOINING NONPLASTIC PIPING

Paragraph A334 applies in its entirety.

MA335 ASSEMBLY AND ERECTION

Paragraph A335 applies in its entirety.

PART 20 INSPECTION, EXAMINATION, TESTING, AND RECORDS OF NONMETALLIC AND NONMETALLIC-LINED PIPING

MA340 INSPECTION

Paragraph 340 applies in its entirety.

MA341 EXAMINATION

Paragraph A341 applies in its entirety

MA341.1 General

Paragraphs 341.1, 341.2, A341.3, and A341.5 apply in their entirety. See para. MA341.4.

MA341.4 Extent of Required Examination

Paragraph A341.41 applies, except as follows:

- (a) Visual Examination
 - (1) All fabrication shall be visually examined.
- (2) All bolted and other mechanical joints shall be examined

MA342 EXAMINATION PERSONNEL

Paragraph 342 applies in its entirety.

MA343 EXAMINATION PROCEDURES

Paragraph 343 applies in its entirety.

MA344 TYPES OF EXAMINATION

Paragraph A344 applies in its entirety.

MA345 TESTING

Paragraph A345 applies except that

- (a) a sensitive leak test in accordance with para. 345.8 shall be included in the required leak test (para. A345.1)
- (b) the initial service leak test (para. A345.7) does not apply

MA346 RECORDS

Paragraph 346 applies in its entirety.

Chapter IX High Pressure Piping

(18) K300 GENERAL STATEMENTS

- (a) Applicability. This Chapter pertains to piping designated by the owner as being in High Pressure Fluid Service. See (e).
- (b) Responsibilities. In addition to the responsibilities stated in para. 300(b),
- (1) for piping designated as being in High Pressure Fluid Service, the owner shall provide all system operations information necessary for the designer to perform the analyses and testing required by this Chapter
- (2) the designer shall make a written report to the owner summarizing the design calculations and certifying that the design has been performed in accordance with this Chapter
- (c) The identification, intent, and Code requirements in paras. 300(a), (c), (d), (e), and (f) apply.
- (d) The organization, content, and, wherever possible, paragraph designations of this Chapter correspond to those of the first six Chapters (the base Code). The prefix K is used.
- (e) High Pressure Piping. This Chapter provides alternative rules for design and construction of piping designated by the owner as being in High Pressure Fluid Service.
- (1) Provisions and requirements of the base Code apply only as stated in this Chapter.
- (2) Use of this Chapter is permitted only at the option of the owner, and when the owner chooses to designate piping as being in High Pressure Fluid Service, its requirements apply in their entirety.
- (3) There are no pressure limitations for the application of these rules. See Appendix F, para. FK300.

(18) K300.1 Scope

The text introducing para. 300.1 applies.

K300.1.1 Content and Coverage. Paragraph 300.1.1 applies.

K300.1.2 Packaged Equipment Piping. Interconnecting piping as described in para. 300.1.2 shall conform to the requirements of this Chapter.

K300.1.3 Exclusions. In addition to the exclusions stated in para. 300.1.3, this Chapter excludes nonmetallic and nonmetallic-lined piping.

K300.1.4 Rounding. Paragraph 300.1.4 applies.

K300.1.5 Category M Fluid Service. This Chapter makes no provision for piping in Category M Fluid Service. If such piping is required by the owner, the engineering design shall be developed as provided in para. 300(c)(5).

K300.2 Definitions

Paragraph 300.2 applies except for terms relating only to nonmetals and severe cyclic conditions.

The term "allowable stress" is used in lieu of basic allowable stress

The term "safeguarding" and other terms characterizing hazardous fluid services are not used in this Chapter but should be taken into account in design.

K300.32Nomenclature

Paragraph 300.3 applies.

K300.4 Status of Appendices

(18)

Paragraph 300.4 and Table 300.4 apply, except for Appendices A, B, H, L, R, S, V, and X.

PART 1 CONDITIONS AND CRITERIA

K301 DESIGN CONDITIONS

(18)

Paragraph 301 applies with the exceptions of paras. 301.2, 301.3, 301.4.2, 301.5, and 301.7.3.

K301.2 Design Pressure

K301.2.1 General. Paragraph 301.2.1 applies, except that references to para. 302.2.4 are not applicable and refer to para. K304 instead of para. 304.

K301.2.2 Required Pressure Containment or Relief. Paragraphs 301.2.2(a) and (b) apply, but refer to para. K322.6.3 instead of para. 322.6.3. Paragraph 301.2.2(c) is not applicable.

K301.3 Design Temperature

Paragraph 301.3 applies with the exceptions of paras. 301.3.1 and 301.3.2 and the following exceptions in the text:

(a) Refer to para. K301.2 instead of para. 301.2.

(b) Refer to para. K301.3.2 instead of para. 301.3.2.

K301.3.1 Design Minimum Temperature. Paragraph 301.3.1 applies, but refer to para. K323.2.2 instead of para. 323.2.2.

K301.3.2 Uninsulated Components. The fluid temperature shall be used as the component temperature.

K301.4 Ambient Effects

K301.4.2 Fluid Expansion Effects. Paragraph 301.4.2 applies, except that reference to para. 322.6.3(b)(2) is not applicable.

K301.5 Dynamic Effects

Paragraph 301.5 applies with the exception of para. 301.5.4.

K301.5.4 Vibration. Suitable dynamic analysis shall be made where necessary, to avoid or minimize conditions that lead to detrimental vibration, pulsation, or resonance effects in the piping.

K301.7 Thermal Expansion and Contraction Effects

K301.7.3 Loads Due to Differences in Expansion Characteristics. Paragraph 301.7.3 applies, except that reference to metallic–nonmetallic piping is not applicable.

K302 DESIGN CRITERIA

K302.1 General

In para. K302, pressure-temperature ratings, stress criteria, design allowances, and minimum design values are stated, and permissible variations of these factors as applied to design of high pressure piping systems are formulated.

The designer shall be satisfied as to the adequacy of the design, and of materials and their manufacture, considering at least the following:

- (a) tensile, compressive, flexural, and shear strength at design temperature
 - (b) fatigue strength
 - (c) design stress and its basis
 - (d) ductility and toughness
- (e) possible deterioration of mechanical properties in service
 - (f) thermal properties
 - (g) temperature limits
 - (h) resistance to corrosion and erosion
 - (i) fabrication methods
 - (j) examination and testing methods
 - (k) hydrostatic test conditions
 - (1) bore imperfections

K302.2 Pressure-Temperature Design Criteria

Ratings. Pressure–temperature ratings for certain piping components have been established and are contained in some of the standards in Table K326.1. Unless limited elsewhere in this Chapter, those ratings are acceptable for design pressures and temperatures under this Chapter. With the owner's approval, the rules and limits of this Chapter may be used to extend the pressure–temperature ratings of a component beyond the ratings of the listed standard, but not beyond the limits stated in para. K323.2.

K302.2.2 Listed Components Not Having Specific Ratings

- (a) Piping components for which design stresses have been developed in accordance with para. K302.3, but that do not have specific pressure–temperature ratings, shall be rated by rules for pressure design in para. K304, within the range of temperatures for which stresses are shown in Table K-1, modified as applicable by other rules of this Chapter.
- (b) Piping components that do not have allowable stresses or pressure–temperature ratings shall be qualified for pressure design as required by para. K304.7.2.

K302.2.3 Unlisted Components. Piping components (18) not listed in Table K326.1 may be used subject to all of the following requirements:

- (a) The material shall comply with para. K323.
- (b) The designer shall be satisfied that the design is suitable for the intended service.
- (c) Pressure-temperature ratings shall be established in accordance with the rules in para. K304.
- (d) Fatigue analysis shall be performed as required by para. K304.8.

K302.2.4 Allowance for Pressure and Temperature (18) **Variations.** Variations in pressure, temperature, or both above the design conditions, except during pressure-relieving events (see para. K322.6.3), are not permitted for any piping system. The design pressure and design temperature resulting in the most severe coincident pressure and temperature shall determine the design conditions. See paras. K301.2 and K301.3.

K302.2.5 Ratings at Junction of Different Services. Paragraph 302.2.5 applies.

K302.3 Allowable Stresses and Other Design Limits

K302.3.1 General. The allowable stresses defined below shall be used in design calculations unless modified by other provisions of this Chapter.

(a) Tension. Allowable stresses in tension for use in design in accordance with this Chapter are listed in Table K-1, except that maximum allowable stress values and design stress intensity values for bolting, respectively, are listed in ASME BPVC, Section II, Part D, Tables 3 and 4.

The tabulated stress values in Table K-1 are grouped by materials and product form and are for stated temperatures up to the limit provided for the materials in para. K323.2.1. Straight line interpolation between temperatures to determine the allowable stress for a specific design temperature is permissible. Extrapolation is not permitted.

- (b) Shear and Bearing. Allowable stress in shear shall be 0.80 times the allowable stress in tension tabulated in Table K-1. Allowable stress in bearing shall be 1.60 times the allowable stress in tension.
- (c) Compression. Allowable stress in compression shall be no greater than the allowable stress in tension tabulated in Table K-1. Consideration shall be given to structural stability.
- (d) Fatigue. Allowable values of stress amplitude, which are provided as a function of design life in ASME BPVC, Section VIII, Division 2, Part 3, para. 3.15, or Section VIII, Division 3, Article KD-3, as applicable, may be used in fatigue analysis in accordance with para. K304.8.
- **K302.3.2 Bases for Allowable Stresses.** The bases for establishing allowable stress values for materials in this Chapter are as follows:
- (a) Bolting Materials. The criteria of ASME BRVC, Section II, Part D, Appendix 2, para. 2-120 or 2-130, or Section VIII, Division 3, Article KD-6, para. KD-620, as applicable, apply.
- (b) Other Materials. For materials other than bolting materials, the following rules apply:
- (1) Except as provided in (b)(2) below, allowable stress values at design temperature for materials shall not exceed the lower of two thirds of S_Y and two-thirds of S_{Yt} . S_{yt} is determined in accordance with eq. (31)

 $S_{yt} = S_Y R_Y \tag{31}$

where

 R_Y = ratio of the average temperature dependent trend curve value of yield strength to the room temperature yield strength

 S_Y = specified minimum yield strength at room temperature

 S_{vt} = yield strength at temperature

(2) For solution heat treated austenitic stainless steels and certain nickel alloys with similar stress–strain behavior, allowable stress values shall not exceed the lower of two-thirds of S_Y and 90% of S_{Vt} .

Application of stress values so determined is not recommended for flanged joints and other components in which slight deformation can cause leakage or malfunction. [These values are shown in *italics* or **boldface** in Table K-1, as explained in Table K-1, Note (12).] Instead, either 75% of the stress value in Table K-1 or two-thirds of the yield strength at temperature listed in ASME BPVC, Section II, Part D, Table Y-1, as applicable, should be used.

- (c) Unlisted Materials. For a material that conforms to para. K323.1.2, allowable stress values at design temperature shall not exceed the lower of two-thirds of S_V and two-thirds of S_{Vt} .
- (1) Except as provided in (c)(2) below, S_{yt} shall be determined in accordance with eq. (31).
- (2) If the yield strength at temperature for an unlisted material is contained in ASME BPVC, Section II, Part D, Table Y-1, that yield strength at temperature value may be used directly in the determination of allowable stress.
- (d) Cyclic Stresses Allowable values of alternating stress or equipment alternating stress, as applicable, shall be in accordance with ASME BPVC, Section VIII, Division 2, Part 3, para. 3.15 and Part 5; or Division 3, Article KD-3; respectively.
- **K302.3.3 Castings.** Cast piping components shall (18) conform to all of the following requirements:
- (a) All surfaces shall have a roughness average, R_a , not greater than 6.3 μ m R_a (250 μ in. R_a); see ASME B46.1 for a definition of R_a .
- (b) All nonferromagnetic surfaces shall be examined using the liquid penetrant method in accordance with ASTM E165, with acceptability judged in accordance with MSS SP-93, Table 1. All ferromagnetic surfaces shall be examined using either the liquid penetrant method or the magnetic particle method, in accordance with ASTM E165 or ASTM E709, respectively. Acceptability of imperfections, including those in weld repairs, shall be judged in accordance with MSS SP-93, Table 1 or MSS SP-53, Table 1, respectively.
- (c) Each casting shall be fully examined either ultrasonically in accordance with ASTM E114 or radiographically in accordance with ASTM E94. Cracks and hot tears (Category D and E discontinuities in accordance with the standards listed in Table K302.3.3D) and imperfections whose depths exceed 3% of nominal wall thickness are not permitted. Acceptable severity levels for radiographic examination of castings shall be in accordance with Table K302.3.3D.

K302.3.4 Weld Joint Quality Factor. Piping components containing welds shall have a weld joint quality factor $E_j = 1.00$ (see Table 302.3.4), except that the acceptance criteria for these welds shall be in accordance with

¹See Notes to Tables 302.3.3C and 302.3.3D for titles of standards referenced herein.

Table K302.3.3D Acceptable Severity Levels for Steel Castings

Thickness Examined, mm (in.)	Applicable Standards	Acceptable Severity Level	Acceptable Discontinuity Categories
$\overline{T} \le 51(2)$	ASTM E446	1	A, B, C
$51 < \overline{T} \le 114 (4.5)$	ASTM E186	1	A, B, C
$114 < \overline{T} \le 305 (12)$	ASTM E280	1	A, B, C

para. K341.3.2. Spiral (helical seam) welds are not permitted.

(18) K302.3.5 Limits of Calculated Stresses Due to Sustained Loads and Displacement Strains

- (a) Internal Pressure Stresses. Stresses due to internal pressure shall be considered safe when the wall thickness of the piping component, and its means of stiffening, meet the requirements of para. K304.
- (b) External Pressure Stresses. Stresses due to external pressure shall be considered safe when the wall thickness of the piping component, and its means of stiffening, meet the requirements of para. K304.
- (c) Stresses Due to Sustained Loads, S_L . The stresses due to sustained loads, S_L , in any component in a piping system (see para. K320) shall not exceed S_h , where S_h is the allowable stress provided in Table K-1 at the metal temperature for the operating condition being considered. The thick ness of pipe used in calculating S_L shall be the nominal thickness minus the mechanical, corrosion, and erosion allowance, c.
- (d) Allowable Displacement Stress Range, S_A . The computed displacement stress range, S_E , in a piping system (see para. 319.4.4) shall not exceed the allowable displacement stress range, S_A (see para. 319.2.3), calculated by

$$S_A = 1.25S_c + 0.25S_h$$
 (32)

where

- S_c = allowable stress from Table K-1 at minimum metal temperature expected during the displacement cycle under analysis
- S_h = allowable stress from Table K-1 at maximum metal temperature expected during the displacement cycle under analysis

(18) K302.3.6 Limits of Calculated Stresses Due to Occasional Loads

(a) Operation. Stresses due to occasional loads may be calculated using the equations for stress due to sustained loads in para. K320.2. The sum of the stresses due to sustained loads, such as pressure and weight, S_L , and of the stresses produced by occasional loads, such as wind and earthquake, may be as much as 1.2 times the allowable stress provided in Table K-1 at the metal

temperature for the occasional condition being considered. Where the allowable stress value in Table K-1 exceeds two-thirds of S_{yt} , S_L shall not exceed 90% of S_{yt} listed in ASME BPVC, Section II, Part D, Table Y-1. Wind and earthquake forces need not be considered as acting concurrently.

(b) Test. Stresses due to test conditions are not subject to the limitations in para. K302.3. It is not necessary to consider other occasional loads, such as wind and earthquake, as occurring concurrently with test loads.

K302.4 Allowances

In determining the minimum required thickness of a piping component, allowances shall be included for corrosion, erosion, and thread or groove depth. See the definition of c in para. K304.1.1(b).

K302.5 Mechanical Strength

Paragraph 302.5 applies.

PART 2 PRESSURE DESIGN OF PIPING COMPONENTS

K303 GENERAL

Components manufactured in accordance with standards listed in Table K326.1 shall be considered suitable for use at pressure–temperature ratings in accordance with para. K302.2.

K304 PRESSURE DESIGN OF HIGH PRESSURE COMPONENTS

K304.1 Straight Pipe

K304.1.1 General

(a) The required wall thickness of straight sections of pipe shall be determined in accordance with eq. (33).

$$t_m = t + c \tag{33}$$

The minimum wall thickness, T, for the pipe selected, considering manufacturer's minus tolerance, shall be not less than t_m .

(b) The following nomenclature is used in the equation for pressure design of straight pipe:

$$c = c_i + c_o$$

= the sum of mechanical allowances² (thread or groove depth) plus corrosion and erosion allowances (where c_i = the sum of *internal* allowances and c_o = the sum of *external* allowances). For threaded components, the nominal thread depth (dimension h of ASME B1.20.1 or

 $^{^2}$ For machined surfaces or grooves where the tolerance is not specified, the tolerance shall be assumed to be 0.5 mm (0.02 in.) in addition to the specified depth of the cut.

equivalent) shall apply, except that for straight threaded connections, the external thread groove depth need not be considered provided

- (a) it does not exceed 20% of the wall thickness;
- (b) the ratio of outside to inside diameter, D/d, is greater than 1.1;
- (c) the internally threaded attachment provides adequate reinforcement; and
- (d) the thread plus the undercut area, if any, does not extend beyond the reinforcement for a distance more than the nominal wall thickness of the pipe.
- t = pressure design wall thickness, as calculated in para. K304.1.2 for internal pressure, or in accordance with the procedure listed in para. K304.1.3 for external pressure
- t_m = minimum required wall thickness, including mechanical, corrosion, and erosion allowances

Adequate reinforcement by the attachment is defined as that necessary to ensure that the static burst pressure of the connection will equal or exceed that of the unthreaded portion of the pipe. The adequacy of the reinforcement shall be substantiated as required by para. K304.7.2.

(18) K304.1.2 Straight Pipe Under Internal Pressure

(a) Except as provided in (b) below for solution heat treated austenitic stainless steels and certain nickel alloys with similar stress–strain behavior, the internal pressure design wall thickness, *t*, shall be not less than that calculated in accordance with eq. (34a) for pipe with a specified outside diameter and minimum wall thickness, or eq. (34b) for pipe with a specified inside diameter and minimum wall thickness^{3,4}

$$t = \frac{D - 2c_0}{2} \left(1 - e^{-P/S} \right)$$
 (34a)

or

$$t = \frac{d + 2c_i}{2} \left(e^{\mathbf{P} \cdot \mathbf{S}} - 1 \right) \tag{34b}$$

Alternatively, the internal design gage pressure, P, may be calculated by eq. (35a) or $(35b)^{3,4}$

$$P = S \times \ln \left[\frac{D - 2c_o}{D - 2(T - c_i)} \right]$$
 (35a)

or

$$P = S \times \ln \left[\frac{d + 2(T - c_0)}{d + 2c_i} \right]$$
 (35b)

where

D = outside diameter of pipe. For design calculations in accordance with this Chapter, the outside diameter of the pipe is the maximum value allowable under the specifications. d = inside diameter of pipe. For design calculations in accordance with this Chapter, the inside diameter of the pipe is the maximum value allowable under the specifications.

P = internal design gage pressure

S = allowable stress from Table K-1

T = pipe wall thickness (measured or minimum in accordance with the purchase specification)

(b) At design temperatures where allowable stress, S, values in Table K-1 are in **boldface** (solution heat treated austenitic stainless steels and certain nickel alloys with similar stress–strain behavior only), the internal pressure design wall thickness, t, shall be not less than that calculated in accordance with eq. (34c) for pipe with a specified outside diameter and minimum wall thickness, or eq. (34d) for pipe with a specified inside diameter and minimum wall thickness^{3,4}

$$t = \frac{D - 2c_0}{2} \left(1 - e^{-1.155P/S} \right)$$
 (34c)

or

$$t = \frac{d + 2c_i}{2} \left(e^{1.15SP/S} - 1 \right)$$
 (34d)

Alternatively, the internal design gage pressure, P, may be calculated by eq. (35c) or (35d)^{3,4}

$$P = \frac{S}{1.155} \ln \left[\frac{D - 2c_0}{D - 2(T - c_i)} \right]$$
 (35c)

or

$$P = \frac{S}{1.155} \ln \left[\frac{d + 2(T - c_0)}{d + 2c_i} \right]$$
 (35d)

K304.1.3 Straight Pipe Under External Pressure. The pressure design thickness for straight pipe under external pressure shall be determined in accordance with para. K304.1.2 for pipe where D/t < 3.33, if at least one end of the pipe is exposed to full external pressure, producing a compressive axial stress. For $D/t \ge 3.33$, and for D/t < 3.33 where external pressure is not applied to at least one end of the pipe, the pressure design wall thickness shall be determined in accordance with para. 304.1.3 except that the stress values shall be taken from Table K-1.

 $^{^3}$ The intent of these equations is to provide a factor of not less than 1.732 (or $\sqrt{3}$) on the pressure required, according to the von Mises theory, to initiate yielding on the outside surface of a cylinder made from an elastic-perfectly plastic material. For solution heat treated austenitic stainless steels and certain nickel alloys with similar stress–strain behavior, this factor is as low as approximately 1.5 at elevated temperatures.

⁴ Any mechanical, corrosion, or erosion allowance, c, not specified as internal, c_i , or external, c_o , shall be assumed to be internal, i.e., $c = c_i$ and $c_o = 0$

K304.2 Curved and Mitered Segments of Pipe

K304.2.1 Pipe Bends. The minimum required wall thickness, t_m , of a bend, after bending, may be determined as for straight pipe in accordance with para. K304.1, provided that the bend radius of the pipe centerline is equal to or greater than ten times the nominal pipe outside diameter and the tolerances and strain limits of para. K332 are met. Otherwise the design shall be qualified as required by para. K304.7.2.

K304.2.2 Elbows. Manufactured elbows not in accordance with para. K303 and pipe bends not in accordance with para. K304.2.1 shall be qualified as required by para. K304.7.2.

K304.2.3 Miter Bends. Miter bends are not permitted.

K304.2.4 Curved Segments of Pipe Under External Pressure. The wall thickness of curved segments of pipe subjected to external pressure may be determined as specified for straight pipe in para. K304.1.3, provided the design length, *L*, is the running centerline length between any two sections that are stiffened in accordance with para. 304.1.3.

K304.3 Branch Connections

K304.3.1 General. Acceptable branch connections include a fitting in accordance with para. K303, an extruded outlet in accordance with para. 304.3.4, or a branch connection fitting (see para. 300.2) similar to that shown in Figure K328.5.4.

K304.3.2 Strength of Branch Connections

- (a) The opening made for a branch connection reduces both static and fatigue strength of the run pipe. There shall be sufficient material in the branch connection to contain pressure and meet reinforcement requirements.
- (b) Static pressure design of a branch connection not in accordance with para. K303 shall conform to para. 304.3.4 for an extruded outlet or shall be qualified as required by para. K304.7.2.

K304.3.3 Reinforcement of Welded Branch Connections. Branch connections made as provided in para. 304.3.3 are not permitted.

K304.4 Closures

- (a) Closures not in accordance with para. K303 or (b) below shall be qualified as required by para. K304.7.2.
- (b) Closures may be designed in accordance with the methods, allowable stresses, and temperature limits of ASME BPVC, Section VIII, Division 2 or Division 3, and ASME BPVC, Section II, Part D.

K304.5 Pressure Design of Flanges and Blanks K304.5.1 Flanges — General

- (a) Flanges not in accordance with para. K303 or (b) below shall be qualified as required by para. K304.7.2.
- (b) A flange may be designed in accordance with the methods, allowable stresses, and temperature limits of ASME BPVC, Section VIII, Division 2, Part 4, para. 4.16, or Part 5, or Division 3, Article KD-6, and ASME BPVC, Section II, Part D.

K304.5.2 Blind Flanges

- (a) Blind flanges not in accordance with para. K303 or (b) or (c) below shall be qualified as required by para. K304.7.2.
- (b) A blind flange may be designed in accordance with eq. (36). The thickness of the flange selected shall be not less than t_m (see para. K304.1.1 for nomenclature), considering manufacturing tolerance

$$t_m = t + c \tag{36}$$

The methods, allowable stresses, and temperature limits of ASME BPVC, Section VIII, Division 2, Part 4, para. 4.6 may be used, with the following changes in nomenclature, to calculate t_m :

- sum of mechanical allowances, defined in para. K304.1.1
- t = pressure design thickness as calculated for the given style of blind flange using the appropriate equation of ASME BPVC, Section VIII, Division 2, Part 4, para. 4.6
- (c) A blind flange may be designed in accordance with the rules, allowable stresses, and temperature limits of ASME BPVC, Section VIII, Division 3, Article KD-6 and ASME BPVC, Section II, Part D.
- **K304.5.3 Blanks.** Design of blanks shall be in accordance with para. 304.5.3(b), except that E shall be 1.00 and the definitions of S and c shall be in accordance with para. K304.1.1.

K304.6 Reducers

Reducers not in accordance with para. K303 shall be qualified as required by para. K304.7.2.

K304.7 Pressure Design of Other Components

K304.7.1 Listed Components. Other pressure-containing components manufactured in accordance with standards in Table K326.1 may be utilized in accordance with para. K303.

K304.7.2 Unlisted Components. Pressure design of unlisted components to which the rules elsewhere in para. K304 do not apply shall be based on the pressure design criteria of this Chapter. The designer shall ensure

that the pressure design has been substantiated through one or more of the means stated in (a), (b), and (c) below. Note that designs are also required to be checked for adequacy of mechanical strength as described in para. K302.5.

- (a) extensive, successful service experience under comparable design conditions with similarly proportioned components made of the same or like material.
- (b) performance testing sufficient to substantiate both the static pressure design and fatigue life at the intended operating conditions. Static pressure design may be substantiated by demonstrating that failure or excessive plastic deformation does not occur at a pressure equivalent to two times the internal design pressure, P. The test pressure shall be two times the design pressure multiplied by the ratio of allowable stress at test temperature to the allowable stress at design temperature, and by the ratio of actual yield strength to the specified minimum yield strength at room temperature from Table K-1.
- (c) detailed stress analysis (e.g., finite element method) with results evaluated as described in ASME BPVC, Section VIII, Division 3, Article KD-2, except that for linear elastic analyses
- (1) $S_y/1.5$ in Division 3 shall be replaced by S from Table K-1, and
- (2) the Division 3 stress intensity limits due to sustained loads may be increased by the same factor applied in para. K302.3.6(a) when wind or earthquake loads are included. However, this limit shall not exceed 90% of S_{yt} listed in ASME BPVC, Section II, Part Dable Y-1.
- (d) for (a), (b), and (c) above, interpolations supported by analysis are permitted between sizes, wall thicknesses, and pressure classes, as well as analogies among related materials with supporting material property data. Extrapolation is not permitted.

K304.7.3 Components With Nonmetallic Parts. Except for gaskets and packing, nonmetallic parts are not permitted.

(18) **K304.7.4 Expansion Joints.** Expansion joints are not permitted.

K304.8 Fatigue Analysis

K304.8.1 General. A fatigue analysis shall be performed on each piping system, including all components⁵ and joints therein, and considering the stresses resulting from attachments, to determine its suitability for the cyclic operating conditions⁶ specified in the engineering design. Except as permitted in (a) and (b) below,

or in paras. K304.8.4 and K304.8.5, this analysis shall be in accordance with ASME BPVC, Section VIII, Division 2 or Division 3.⁷ The cyclic conditions shall include pressure variations as well as thermal variations or displacement stresses. The requirements of para. K304.8 are in addition to the requirements for a flexibility analysis stated in para. K319. No formal fatigue analysis is required in systems that

- (a) are duplicates of successfully operating installations or replacements without significant change of systems with a satisfactory service record or
- (b) can readily be judged adequate by comparison with previously analyzed systems

K304.8.2 Amplitude of Alternating Stress

- (a) Fatigue Analysis Based Upon ASME BPVC, Section VIII, Division 2. The value of the alternating stress amplitude for comparison with design fatigue curves shall be determined in accordance with Part 5. The allowable amplitude of alternating stress shall be determined from the applicable design fatigue curve in Part 3, para. 3.15.
- (b) Fatigue Analysis Based Upon ASME BPVC, Section VIII, Division 3
- (1) The values of the alternating stress intensity, the associated mean stress, and the equivalent alternating stress intensity shall be determined in accordance with Articles KD-2 and KD-3. The allowable amplitude of the equivalent alternating stress shall be determined from the applicable design fatigue curve in Article KD-3.
- (2) If it can be shown that the piping component will fail in a leak-before-burst mode, the number of design cycles (design fatigue life) may be calculated in accordance with either Article KD-3 or Article KD-4. If a leak-before-burst mode of failure cannot be shown, the fracture mechanics evaluation outlined in Article KD-4 shall be used to determine the number of design cycles of the component.
- (c) Additional Considerations. The designer is cautioned that the considerations listed in para. K302.1 may reduce the fatigue life of the component below the value predicted by para. (a) or (b) above.

K304.8.3 Pressure Stress Evaluation for Fatigue Analysis

(a) For fatigue analysis of straight pipe, eq. (37) may be used to calculate the stress intensity⁸ at the inside surface due only to internal pressure

$$S = \frac{PD^2}{2(T - c)[D - (T - c)]}$$
 (37)

⁵ Bore imperfections may reduce fatigue life.

 $^{^6}$ If the range of temperature change varies, equivalent full temperature cycles N may be computed using eq. (1d) in para. 302.3.5.

⁷ Fatigue analysis in accordance with ASME BPVC, Section VIII, Division 2 or Division 3, requires that stress concentration factors be used in computing the cyclic stresses.

⁸ The term "stress intensity" is defined in ASME BPVC, Section VIII, Division 3.

Table K305.1.2 Required Ultrasonic or Eddy Current Examination of Pipe and Tubing for Longitudinal Defects

Diameter, mm (in.)	Examination Required	Paragraph Reference
$d < 3.2 (\frac{1}{8}) \text{ or}$ $D < 6.4 (\frac{1}{4})$	None	
$3.2 \binom{1}{8} \le d \le 17.5 \binom{11}{16}$ and $6.4 \binom{1}{4} \le D \le 25.4 (1)$	Eddy current (ET) [Note (1)] or ultrasonic (UT)	K344.8 or K344.6
$d > 17.5 (^{11}/_{16}) \text{ or } D > 25.4$ (1)	Ultrasonic (UT)	K344.6

NOTE: (1) This examination is limited to cold drawn austenitic stainless steel pipe and tubing.

- (b) For fatigue analysis of curved pipe, eq. (37) may be used, with the dimensions of the straight pipe from which it was formed, to calculate the maximum stress intensity at the inside surface due only to internal pressure, provided that the centerline bend radius is not less than ten times the nominal outside diameter of the pipe, and that the tolerance and strain limits of para. K332 are met. Bends of smaller radius shall be qualified as required by para. K304.7.2.
- (c) If the value of S calculated by eq. (37) exceeds three times the allowable stress from Table K-1 at the average temperature during the loading cycle, an inelastic analysis is required.
- **K304.8.4 Fatigue Evaluation by Test.** With the owner's approval, the design fatigue life of a component may be established by destructive testing in accordance with para. K304.7.2 in lieu of the above analysis requirements.
- **K304.8.5 Extended Fatigue Life.** The design fatigue life of piping components may be extended beyond that determined by ASME BPVC, Section VIII, Division 2, Part 3, para. 3.15 and Part 5; or Division 3, Article KD-3; as applicable, by the use of one of the following methods, provided that the component is qualified in accordance with para. K304.7.2:
 - (a) surface treatments, such as improved surface finish
- (b) prestressing methods, such as autofrettage, shot peening, or shrink fit

The designer is cautioned that the benefits of prestress may be reduced due to thermal, strain softening, or other effects.

PART 3 FLUID SERVICE REQUIREMENTS FOR PIPING COMPONENTS

K305 PIPE

Pipe includes components designated as "tube" or "tubing" in the material specification, when intended for pressure service.

K305.1 Requirements

K305.1.1 General. Pipe and tubing shall be either seamless or longitudinally welded with straight seam and a joint quality factor $E_j = 1.00$, examined in accordance with Note (2) of Table K341.3.2 Spiral (helical seam) welds are not permitted.

K305.1.2 Additional Examination. Pipe and tubing shall have passed a 100% examination for longitudinal defects in accordance with Table K305.1.2. This examination is in addition to acceptance tests required by the material specification.

K305.1.3 Heat Treatment. Heat treatment, if required, shall be in accordance with para. K331.

K305.1.4 Unlisted Pipe and Tubing. Unlisted pipe and tubing may be used only in accordance with para. K302.2.3.

K306 FITTINGS, BENDS, AND BRANCH CONNECTIONS

Pipe and other materials used in fittings, bends, and branch connections shall be suitable for the manufacturing or fabrication process and otherwise suitable for the service.

K306.1 Pipe Fittings

K306.1.1 General. All castings shall have examination (18) and acceptance criteria in accordance with para. K302.3.3. All welds shall have a weld quality factor $E_j = 1.00$, with examination and acceptance criteria in accordance with paras. K341 through K344. Spiral (helical seam) welds are not permitted. Listed fittings may be used in accordance with para. K303. Unlisted fittings may be used only in accordance with para. K302.2.3.

K306.1.2 Specific Fittings

- (a) Socket welding fittings are not permitted.
- (b) Threaded fittings are permitted only in accordance with para. K314.
- (c) Branch connection fittings (see para. 300.2) whose design has been performance tested successfully as required by para. K304.7.2(b) may be used within their established ratings.

K306.2 Pipe Bends

K306.2.1 General. A bend made in accordance with para. K332.2 and verified for pressure design in accordance with para. K304.2.1 shall be suitable for the same service as the pipe from which it is made.

K306.2.2 Corrugated and Other Bends. Bends of other design (such as creased or corrugated) are not permitted.

K306.3 Miter Bends

Miter bends are not permitted.

K306.4 Fabricated or Flared Laps

Only forged laps are permitted.

K306.5 Fabricated Branch Connections

Fabricated branch connections constructed by welding shall be fabricated in accordance with para. K328.5.4 and examined in accordance with para. K341.4.

K307 VALVES AND SPECIALTY COMPONENTS

The following requirements for valves shall also be met, as applicable, by other pressure-containing piping components, e.g., traps, strainers, and separators.

K307.1 General

Pressure design of unlisted valves shall be qualified as required by para. K304.7.2.

K308 FLANGES, BLANKS, FLANGE FACINGS, AND

K308.1 General

Pressure design of unlisted flanges shall be verified in accordance with para. K304.5.1 or qualified as required by para. K304.7.2.

K308.2 Specific Flanges

K308.2.1 Threaded Flanges. Threaded flanges may be used only within the limitations on threaded joints in para. K314.

K308.2.2 Other Flange Types. Slip-on, socket welding, and expanded joint flanges, and flanges for flared laps, are not permitted.

K308.3 Flange Facings

The flange facing shall be suitable for the service and for the gasket and bolting employed.

K308.4 Gaskets

Gaskets shall be selected so that the required seating load is compatible with the flange rating and facing, the strength of the flange, and its bolting. Materials shall be suitable for the service conditions. Mode of gasket failure shall be considered in gasket selection and joint design.

K308.5 Blanks

Blanks shall have a marking, identifying material, pressure–temperature rating, and size, that is visible after installation.

K309 BOLTING

Bolting, including bolts, bolt studs, studs, cap screws, nuts, and washers, shall meet the requirements of ASME BPVC, Section VIII, Division 2, Part 3, para. 3.7; Part 4, para. 4.16; and Part 5, para. 5.7. See also Appendix F, para. F309, of this Code.

PART 4 FLUID SERVICE REQUIREMENTS FOR PIPING JOINTS

K310 GENERAL

Joints shall be suitable for the fluid handled, and for the pressure-temperature and other mechanical loadings expected in service.

Factors such as assembly and disassembly (if applicable), cyclic loading, vibration, shock, bending, and thermal expansion and contraction of joints shall be considered in the engineering design.

K311 WELDED JOINTS

K311.1 General

Welds shall conform to the following:

- (a) Welding shall be in accordance with para. K328.
- (b) Preheating and heat treatment shall be in accordance with paras. K330 and K331, respectively.
- (c) Examination shall be in accordance with para. K341.4, with acceptance criteria as shown in Table K341.3.2.

K311.2 Specific Requirements

K311.2.1 Backing Rings and Consumable Inserts.

Backing rings shall not be used. Consumable inserts shall not be used in butt welded joints except when specified by the engineering design.

K311.2.2 Fillet Welds. Fillet welds may be used only for structural attachments in accordance with the requirements of paras. K321 and K328.5.2.

K311.2.3 Other Weld Types. Socket welds and seal welds are not permitted.

K312 FLANGED JOINTS

Flanged joints shall be selected for leak tightness, considering the requirements of para. K308, flange facing finish, and method of attachment. See also para. F312.

K312.1 Joints Using Flanges of Different Ratings

Paragraph 312.1 applies.

K313 EXPANDED JOINTS

Expanded joints are not permitted.

(18) K314 THREADED PIPE JOINTS

For the purposes of this paragraph, "pipe" does not include "tube" or "tubing."

K314.1 General

Except as provided in paras. K314.2 and K314.3, threaded pipe joints are not permitted.

- (a) Layout of piping shall be such as to minimize strain on threaded joints that could adversely affect sealing.
- (b) Supports shall be designed to control or minimize strain and vibration on threaded joints and seals.

K314.2 Taper-Threaded Pipe Joints

- (a) Taper-threaded pipe joints shall be used only for instrumentation, vents, drains, and similar purposes, and shall be not larger than DN 15 (NPS. (NPS. 1/2)).
- (b) Externally threaded piping components shall be at least Schedule 160 in nominal wall thickness. The nominal thickness of Schedule 160 piping is listed in ASME B36.10M for DN 15 (NPS ½) and in ASME B16.11 for sizes smaller than DN 15 (NPS ½).

K314.3 Straight-Threaded Pipe Joints

K314.3.1 Joints With Seal Formed by Projecting Pipe.

Threaded joints where the threads are used to attach flanges or fittings, and in which the pipe end projects through the flange or fitting and is machined to form the sealing surface with a lens ring, cone ring, the mating pipe end, or other similar sealing device, may be used. Such joints shall be qualified in accordance with para. K304.7.2.

K314.3.2 Other Straight-Threaded Joints

(a) Other Joints Using Components Conforming to Listed Standards. Pipe joints may incorporate straight-threaded fittings conforming to listed standards in Table K326.1, provided the fittings

- (1) are compatible with the pipe with which they are used, considering tolerances and other characteristics
 - (2) comply with para. K302.2.1 or para. K302.2.2
- (b) Other Joints Using Components Not Conforming to Listed Standards. Other straight-threaded pipe joints (e.g., a union comprising external and internal ends joined with a threaded union nut, or other constructions shown typically in Figure 335.3.3) may be used. Such joints shall be qualified by performance testing in accordance with para. K304.7.2(b). Testing shall be conducted for each material type/grade and heat treatment condition, component configuration (e.g., elbow), size (e.g., NPS), and pressure rating. Performance testing of joints in which the process of making up the joint involves significant uncontrolled loads (e.g., hammer unions) shall include testing designed to simulate actual loads.

K315 TUBING JOINTS

(18)

K315.1 Flared End Tubing Joints

Flared end tubing joints, whether the flare provides the seal, carries the load, or both, may be used, provided the type of fitting selected is adequate for the design pressure, other loadings, and the design temperature. The design shall also be qualified in accordance with para. K304.7.2.

K315.2 Flareless Tubing Joints Using Components Conforming to Listed Standards

Tubing joints may incorporate flareless type fittings conforming to listed standards in Table K326.1, provided the fittings

- (a) are compatible with the tubing with which they are used, considering tolerances and other characteristics
 - (b) comply with para. K302.2.1 or para. K302.2.2

K315.3 Flareless Tubing Joints Using Components Not Conforming to Listed Standards

Tubing joints may incorporate flareless type fittings not conforming to listed standards in Table K326.1, provided the type of fitting selected is adequate for the design pressure, other loadings, and the design temperature, and meets the requirements of para. K302.2.3.

K316 CAULKED JOINTS

Caulked joints are not permitted.

K317 SOLDERED AND BRAZED JOINTS

K317.1 Soldered Joints

Soldered joints are not permitted.

K317.2 Brazed Joints

(a) Braze welded joints and fillet joints made with brazing filler metal are not permitted.

(b) Brazed joints shall be made in accordance with para. K333 and shall be qualified as required by para. K304.7.2. Such application is the owner's responsibility. The melting point of brazing alloys shall be considered when exposure to fire is possible.

(18) K318 SPECIAL JOINTS

Special joints are those not covered elsewhere in this Part

K318.1 General

Joints may be used in accordance with para. 318.2 and the requirements for materials and components in this Chapter.

K318.2 Specific Requirements

K318.2.1 Prototype Tests. A prototype joint shall have been subjected to performance tests in accordance with para. K304.7.2(b) to determine the safety of the joint under test conditions simulating all expected service conditions. Testing shall include cyclic simulation.

K318.2.2 Prohibited Joints. Bell type and adhesive joints are not permitted.

PART 5 FLEXIBILITY AND SUPPORT

(18) K319 FLEXIBILITY

Flexibility analysis shall be performed for each piping system. Paragraphs 319.1 through 319.6 apply, except for para. 319.4.1(c). The computed displacement stress range shall be within the allowable displacement stress range in para. K302.3.5 and shall also be included in the fatigue analysis in accordance with para. K304.8.

(18) K320 ANALYSIS OF SUSTAINED LOADS

K320.1 Basic Assumptions and Requirements

Paragraph 320.1 applies, but refer to para. K302.3.5(c) instead of para. 302.3.5(c).

K320.2 Stress Due to Sustained Loads

Paragraph 320.2 applies, except that references to expansion joints are not applicable.

K321 PIPING SUPPORT

Piping supports and methods of attachment shall be in accordance with para. 321 except as modified below, and shall be detailed in the engineering design.

K321.1 General

K321.1.1 Objectives. Paragraph 321.1.1 applies, but substitute "Chapter" for "Code" in (a).

K321.1.4 Materials. Paragraph 321.1.4 applies, but replace (e) with the following:

(e) Attachments welded to the piping shall be of a material compatible with the piping and the service. Other requirements are specified in paras. K321.3.2 and K323.4.2(b).

K321.3 Structural Attachments

K321.3.2 Integral Attachments. Paragraph 321.3.2 applies, but substitute "K321.1.4(e)" for "321.1.4(e)" and "Chapter IX" for "Chapter V."

PART 6 SYSTEMS

K322 SPECIFIC PIPING SYSTEMS

K322.3 Instrument Piping

K322.3.1 Definition. Instrument piping within the scope of this Chapter includes all piping and piping components used to connect instruments to high pressure piping or equipment. Instruments, permanently sealed fluidfilled tubing systems furnished with instruments as temperature- or pressure-responsive devices, and control piping for air or hydraulically operated control apparatus (not connected directly to the high pressure piping or equipment) are not within the scope of this Chapter.

K322.3.2 Requirements. Instrument piping within the scope of this Chapter shall be in accordance with para. 322.3.2 except that the design pressure and temperature shall be determined in accordance with para. K301, and the requirements of para. K310 shall apply. Instruments, and control piping not within the scope of this Chapter, shall be designed in accordance with para. 322.3.

K322.6 Pressure-Relieving Systems

Paragraph 322.6 applies, except for para. 322.6.3.

K322.6.3 Overpressure Protection. Overpressure protection for high pressure piping systems shall conform to the following:

(a) The cumulative capacity of the pressure-relieving devices shall be sufficient to prevent the pressure from rising more than 10% above the piping design pressure at the operating temperature during the relieving condition for a single relieving device or more than 16% above the design pressure when more than one device is provided, except as provided in (c) below.

- (b) System protection must include one relief device set at or below the design pressure at the operating temperature for the relieving condition, with no device set to operate at a pressure greater than 105% of the design pressure, except as provided in (c) below.
- (c) Supplementary pressure-relieving devices provided for protection against overpressure due to fire or other unexpected sources of external heat shall be set to operate at a pressure not greater than 110% of the design pressure of the piping system and shall be capable of limiting the maximum pressure during relief to no more than 121% of the design pressure.

PART 7 MATERIALS

K323 GENERAL REQUIREMENTS

- (a) Paragraph K323 states limitations and required qualifications for materials based on their inherent properties. Their use is also subject to requirements elsewhere in Chapter IX and in Table K-1.
- (b) Specific attention should be given to the manufacturing process to ensure uniformity of properties throughout each piping component.
 - (c) See para. K321.1.4 for support materials.

K323.1 Materials and Specifications

K323.1.1 Listed Materials

- (a) Any material used in a pressure-containing piping component shall conform to a listed specification, except as provided in (b) below or in para. K3231.2.
- (b) Materials manufactured to specification editions different from those listed in Appendix E may be used, provided
- (1) the requirements for chemical composition and heat-treatment condition in the edition of the specification to which the material was manufactured meet the requirements of the listed edition
- (2) the specified minimum tensile and yield strengths, and, if applicable, the specified maximum tensile and yield strengths, required by the two editions of the specification are the same, and
- (3) the material has been tested and examined in accordance with the requirements of the listed edition of the specification

A material that does not meet the requirements of paras. K323.1.1(b)(1), (2), and (3) may be evaluated as an unlisted material in accordance with para. K323.1.2.

K323.1.2 Unlisted Materials. An unlisted material may be used, provided it conforms to a published specification covering chemistry, physical and mechanical properties, method and process of manufacture, heat treatment, and quality control, and otherwise meets the requirements of this Chapter. Allowable stresses shall be determined in

accordance with the applicable allowable stress basis of this Chapter or a more conservative basis.

K323.1.3 Unknown Materials. Materials of unknown specification, type, or grade are not permitted.

- **K323.1.4 Reclaimed Materials.** Reclaimed pipe and other piping components may be used provided they are properly identified as conforming to a listed specification, have documented service history for the material and fatigue life evaluation, and otherwise meet the requirements of this Chapter. Sufficient cleaning and inspection shall be made to determine minimum wall thickness and freedom from defects that would be unacceptable in the intended service.
- **K323.1.5 Product Analysis.** Conformance of materials to the product analysis chemical requirements of the applicable specification shall be verified, and certification shall be supplied. Requirements for product analysis are defined in the applicable materials specification.
- **K323.1.6 Repair of Materials by Welding.** A material defect may be repaired by welding, provided that all of the following criteria are met:
 - (a) The material specification provides for weld repair.
- (b) The welding procedure and welders or welding operators are qualified as required by para. K328.2.
- (c) The repair and its examination are performed in accordance with the material specification and with the owner's approval.

K323.2 Temperature Limitations (18)

The designer shall verify that materials that meet other requirements of this Chapter are suitable for service throughout the operating temperature range.

K323.2.1 Upper Temperature Limits, Listed Mate- (18) **rials.** A listed material shall not be used at a temperature above the maximum for which a stress value is shown in Appendix K, Table K-1.

K323.2.2 Lower Temperature Limits, Listed Materials

- (a) The lowest permitted service temperature for a component or weld shall be the impact test temperature determined in accordance with para. K323.3.4(a), except as provided in (b) or (c) below.
- (b) For a component or weld subjected to a longitudinal or circumferential stress \leq 41 MPa (6 ksi), the lowest service temperature shall be the lower of -46° C (-50° F) or the impact test temperature determined in para. K323.3.4(a).
- (c) For materials exempted from Charpy testing by Note (2) of Table K323.3.1, the service temperature shall not be lower than -46° C (-50° F).
- **K323.2.3 Temperature Limits, Unlisted Materials.** An unlisted material acceptable under para. K323.1.2 shall be qualified for service at all temperatures within a stated

range from design minimum temperature to design (maximum) temperature, in accordance with para. K323.2.4. However, the upper temperature limit shall be less than the temperature for which an allowable stress, determined in accordance with para. 302.3.2, is governed by the creep or stress rupture provisions of that paragraph.

(18) K323.2.4 Verification of Serviceability

- (a) When an unlisted material is used, the designer is responsible for demonstrating the validity of the allowable stresses and other design limits, and of the approach taken in using the material, including the derivation of stress data and the establishment of temperature limits.
- (b) Paragraph 323.2.4(b) applies except that allowable stress values shall be determined in accordance with para. K302.3.

K323.3 Impact Testing Methods and Acceptance Criteria

K323.3.1 General. Except as provided in Table K323.3.1, Note (2), piping components used in High Pressure Fluid Service shall be subjected to Charpy V-notch impact testing. The testing shall be performed in accordance with Table K323.3.1 on representative samples using the testing methods described in paras. K323.3.2, K323.3.3, and K323.3.4. Acceptance criteria are described in para. K323.3.5.

K323.3.2 Procedure. Paragraph 323.3.2 applies.

K323.3.3 Test Specimens

- (a) Each set of impact test specimens shall consist of three specimen bars. Impact tests shall be made using standard 10 mm (0.394 in.) square cross section Charpy V-notch specimen bars oriented in the transverse direction.
- (b) Where component size and/or shape does not permit specimens as specified in (a) above, standard 10 mm square cross-section longitudinal Charpy specimens may be prepared.
- (c) Where component size and/or shape does not permit specimens as specified in (a) or (b) above, subsize longitudinal Charpy specimens may be prepared. Test temperature shall be reduced in accordance with Table 323.3.4. See also Table K323.3.1, Note (2).
- (d) If necessary in (a), (b), or (c) above, corners of specimens parallel to and on the side opposite the notch may be as shown in Figure K323.3.3.
- **K323.3.4 Test Temperatures.** For all Charpy impact tests, the test temperature criteria in (a) or (b) below shall be observed.
- (a) Charpy impact tests shall be conducted at a temperature no higher than the lower of the following:
 (1) 20°C (70°F)

- (2) the lowest metal temperature at which a piping component or weld will be subjected to a stress greater than 41 MPa (6 ksi). In specifying the lowest metal temperature, the following shall be considered:
 - (-a) range of operating conditions
 - (-b) upset conditions
 - (-c) ambient temperature extremes
 - (-d) required leak test temperature
- (b) Where the largest possible test specimen has a width along the notch less than the lesser of 80% of the material thickness or 8 mm (0.315 in.), the test shall be conducted at a reduced temperature in accordance with Table 323.3.4, considering the temperature as reduced below the test temperature required by (a) above.

K323.3.5 Acceptance Criteria

- (a) Minimum Energy Requirements for Materials Other Than Bolting. The applicable minimum impact energy requirements for materials shall be those shown in Table K323.3.5. Lateral expansion shall be measured in accordance with ASTM A370 (for title see para. 323.3.2). The results shall be included in the impact test report.
- (b) Minimum Energy Requirements for Bolting Materials. The applicable minimum energy requirements shall be those shown in Table K323.3.5 except as provided in Table K323.3.1.
- (c) Weld Impact Test Requirements. Where two base metals having different required impact energy values are joined by welding, the impact test energy requirements shall equal or exceed the requirements of the base material having the lower required impact energy.
 - (d) Retests
- (1) Retest for Absorbed Energy Criteria. When the average value of the three specimens equals or exceeds the minimum value permitted for a single specimen, and the value for more than one specimen is below the required average value, or when the value for one specimen is below the minimum value permitted for a single specimen, a retest of three additional specimens shall be made. The value for each of these retest specimens shall equal or exceed the required average value.
- (2) Retest for Erratic Test Results. When an erratic result is caused by a defective specimen or uncertainty in the test, a retest will be allowed. The report giving test results shall specifically state why the original specimen was considered defective or which step of the test procedure was carried out incorrectly.

K323.4 Requirements for Materials

K323.4.1 General. Requirements in para. K323.4 apply to pressure-containing parts, not to materials used as supports, gaskets, packing, or bolting. See also Appendix F, para. F323.4.

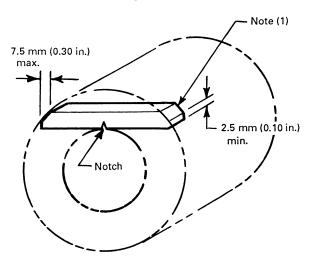
Table K323.3.1 Impact Testing Requirements

Test Characteristics Tests on Number of tests Materials		Column A Pipe, Tubes, and Components Made From Pipe or Tubes As required by the material specific permitted by Note (2).	Column B Other Components, Fittings, Etc. cation, or one test set per lot [see Note	Column C Bolts e (1)], whichever is greater, except as
	Location and orientation of specimens [see Note (3)]	(a) Transverse to the longitudinal axis, with notch parallel to axis. [See Note (4).] (b) Where component size and/ or shape does not permit specimens as specified in (a) above, paras. K323.3.3(b), (c), and (d) apply as needed.	(a) Transverse to the direction of maximum elongation during rolling or to direction of major working during forging. Notch shall be oriented parallel to direction of maximum elongation or major working. (b) If there is no single identifiable axis, e.g., for castings or triaxial forgings, specimens shall either meet the longitudinal values of Table K323.3.5, or three sets of orthogonal specimens shall be prepared, and the lowest impact values obtained from any set shall meet the transverse values of Table K323.3.5. (c) Where component size and/or shape does not permit specimens as specified in (a) or (b) above, paras. K323.3.3(c) and (d) apply as needed.	(a) Bolts ≤52 mm (2 in.) nominal size made in accordance with ASTM A320 shall meet the impact requirements of that specification. (b) For all other bolts longitudinal specimens shall be taken. The impact values obtained shall meet the transverse values of Table K323.3.5.
Tests on Welds in Fabrication or Assembly	Test pieces [see Note (5)]	or filler metal (i.e., AWS E-XXXX classification) and each flux to be used. All test pieces shall be subject heat treatment, including cooling rates and aggregate time at temperature or temperatures, essentially same as the heat treatment which the finished component will have received. (1) One test piece with a thickness <i>T</i> for each range of material thicknesses which can vary from ½ <i>T</i> to 6 mm (½ in.).		
	Number of test pieces [see Note (6)]			
	Location and orientation of specimens	(1) Weld metal impact specimens specimen shall be oriented so the specimen shall be within 1.5 m (2) Heat affected zone impact spec the notch in the heat affected z material surface in such a mannersulting fracture. (3) The impact values obtained from the specimen specimen such a manner sulting fracture.	shall be taken across the weld with at the notch axis is normal to the surfarm ($\frac{1}{16}$ in.) of the surface of the maximens shall be taken across the weld one, after etching. The notch shall beer as to include as much heat affection both the weld metal and heat a ues in Table K323.3.5 for the determinant of the shall be taken across the weld metal and heat a ues in Table K323.3.5 for the determinant of the shall be taken across the weld metal and heat a ues in Table K323.3.5 for the determinant of the shall be taken across the weld metal and heat a ues in Table K323.3.5 for the determinant of the shall be taken across the weld metal and heat a ues in Table K323.3.5 for the determinant of the shall be taken across the weld metal and heat a ues in Table K323.3.5 for the determinant of the shall be taken across the weld heat a shall be taken across the well be taken acros	n the notch in the weld metal. Each ace of the material and one face of the terial. I and have sufficient length to locate be cut approximately normal to the ted zone material as possible in the affected zone specimens shall be

NOTES:

- (1) A lot shall consist of pipe or components of the same nominal size, made from the same heat of material, and heat treated together. If a continuous type furnace is used, pipe or components may be considered to have been heat treated together if they are processed during a single continuous time period at the same furnace conditions.
- (2) Impact tests are not required when the maximum obtainable longitudinal Charpy specimen has a width along the notch less than 2.5 mm (0.098 in.). See para. K323.2.2(c).
- (3) Impact tests shall be performed on a representative sample of material after completion of all heat treatment and forming operations involving plastic deformation, except that cold bends made in accordance with para. K304.2.1 need not be tested after bending.
- (4) For longitudinally welded pipe, specimens shall be taken from the base metal, weld metal, and the heat affected zone.
- (5) For welds in the fabrication or assembly of piping or components, including repair welds.
- (6) The test piece shall be large enough to permit preparing the number of specimens required by para. K323.3. If this is not possible, additional test pieces shall be prepared.

Figure K323.3.3 Example of an Acceptable Impact Test Specimen



GENERAL NOTE: This Figure illustrates how an acceptable transverse Charpy specimen can be obtained from a tubing or component shape too small for a full length standard specimen in accordance with ASTM A370. The corners of a longitudinal specimen parallel to and on the side opposite the notch may be as shown.

NOTE: (1) Corners of the Charpy specimen [see para. K323.3.3(d)] may follow the contour of the component within the dimension limits shown.

K323.4.2 Specific Requirements

- (a) Ductile iron and other cast irons are not permitted.
- (b) Zinc-coated materials are not permitted for pressure containing components and may not be attached to pressure-containing components by welding.
- **K323.4.3 Metallic Clad and Lined Materials.** Materials with metallic cladding or lining may be used in accordance with the following provisions:
- (a) For metallic clad or lined piping components, the base metal shall be an acceptable material as defined in para. K323, and the thickness used in pressure design in accordance with para K304 shall not include the thickness of the cladding or hing. The allowable stress used shall be that for the base metal at the design temperature. For such components, the cladding or lining may be any material that, in the judgment of the user, is suitable for the intended service and for the method of manufacture and assembly of the piping component.
- (b) Fabrication by welding of clad or lined piping components and the inspection and testing of such components shall be done in accordance with applicable provisions of ASME BPVC, Section VIII, Division 1, UCL-30 through UCL-52, and the provisions of this Chapter.
- (c) If a metallic liner also serves as a gasket or as part of the flange facing, the requirements and limitations in para. K308.4 apply.

K323.5 Deterioration of Materials in Service

Paragraph 323.5 applies.

K325 MISCELLANEOUS MATERIALS

Paragraph 325 applies.

PART 8 STANDARDS FOR PIPING COMPONENTS

K326 REQUIREMENTS FOR COMPONENTS

K326.1 Dimensional Requirements

K326.1.1 Listed Piping Components. Dimensional standards for piping components are listed in Table K326.1. Dimensional requirements contained in specifications listed in Appendix K shall also be considered requirements of this Code.

K326.1.2 Unlisted Piping Components. Piping components not listed in Pable K326.1 or Appendix K shall meet the pressure design requirements described in para. K302.2 3 and the mechanical strength requirements described in para. K302.5.

K326.1.3 Threads. The dimensions of piping connection threads not otherwise covered by a governing component standard or specification shall conform to the requirements of applicable standards listed in Table K326.1 or Appendix K.

K326.2 Ratings of Components

K326.2.1 Listed Components. The pressure–temperature ratings of components listed in Table K326.1 are accepted for pressure design in accordance with para. K303.

K326.2.2 Unlisted Components. The pressure-temperature ratings of unlisted piping components shall conform to the applicable provisions of para. K304.

K326.3 Reference Documents

The documents listed in Table K326.1 contain references to codes, standards, and specifications not listed in Table K326.1. Such unlisted codes, standards, and specifications shall be used only in the context of the listed documents in which they appear.

The design, materials, fabrication, assembly, examination, inspection, and testing requirements of this Chapter are not applicable to components manufactured in accordance with the documents listed in Table K326.1, unless specifically stated in this Chapter or in the listed document.

Specimen	Pipe Wall or Component	Number of Specimens	Energy, J (ft-lbf) [Note (2)] fo Strength, M	•
Orientation	Thickness, mm (in.)	[Note (1)]	≤932 (≤135)	>932 (>135)
Transverse	≤25 (≤1)	Average for 3	27 (20)	34 (25)
		Minimum for 1	20 (15)	27 (20)
	>25 and ≤51 (>1 and ≤2)	Average for 3	34 (25)	41 (30)
		Minimum for 1	27 (20)	33 (24)
	>51 (>2)	Average for 3	41 (30)	47 (35)
		Minimum for 1	33 (24)	38 (28)
Longitudinal	≤25 (≤1)	Average for 3	54 (40)	68 (50)
		Minimum for 1	41 (30)	54 (40)
	>25 and ≤51 (>1 and ≤2)	Average for 3	68 (50)	81 (60)
		Minimum for 1	54 (40)	65 (48)
	>51 (>2)	Average for 3	81 (60)	95 (70)
		Minimum for 1	65 (48)	76 (56)

NOTES:

- (1) See para. K323.3.5(c) for permissible retests.
- (2) Energy values in this Table are for standard size specimens. For subsize specimens, these values shall be multiplied by the ratio of the actual specimen width to that of a full-size specimen, 10 mm (0.394 in.).

(18) K326.4 Repair of Piping Components by Welding

A defect in a piping component may be repaired by welding subject to all of the following requirements:

- (a) The piping component specification provides for weld repair or, if not covered by a specification, the manufacturer allows for weld repair.
- (b) The welding procedure and welders or welding operators are qualified as required by para. K328.2.
- (c) The repair and its examination are performed in accordance with the piping component specification or, if not covered by a specification, the manufacturer's requirements.
 - (d) The owner approves the weld repair.

PART 9 FABRICATION, ASSEMBLY, AND ERECTION

K327 GENERAL

Piping materials and components are prepared for assembly and erection by one or more of the fabrication processes covered in paras. K328, K330, K331, K332, and K333. When any of these processes is used in assembly or erection, requirements are the same as for fabrication.

K328 WELDING

Welding that conforms to the requirements of para. K328 may be used in accordance with para. K311.

K328.1 Welding Responsibility

Each employer is responsible for the welding done by the personnel of his/her organization and shall conduct the tests required to qualify welding procedures, and to qualify and as necessary requalify welders and welding operators.

K328.2 Welding Qualifications

K328.2.1 Qualification Requirements. Qualification of the welding procedures to be used and of the performance of welders and welding operators shall comply with the requirements of ASME BPVC, Section IX, except as modified herein.

- (a) Impact tests shall be performed for all procedure qualifications in accordance with para. K323.3.
- (b) Test weldments shall be made using the same specification and type or grade of base metal(s), and the same specification and classification of filler metal(s) as will be used in production welding.
- (c) Test weldments shall be subjected to essentially the same heat treatment, including cooling rate and cumulative time at temperature, as the production welds.

Table K326.1 Component Standards

Standard or Specification	Designation
Bolting	
Square and Hex Bolts and Screws, Inch Series; Including Hex Cap Screws and Lag Screws	ASME B18.2.1
Square and Hex Nuts (Inch Series)	ASME B18.2.2
Metallic Fittings, Valves, and Flanges	
Pipe Flanges and Flanged Fittings [Note (1)]	ASME B16.5
Factory-Made Wrought Buttwelding Fittings [Note (1)]	ASME B16.9
Forged Fittings, Socket Welding and Threaded [Note (1)]	ASME B16.11
Valves — Flanged, Threaded, and Welding End [Note (1)]	ASME B16.34
Line Blanks [Note (1)]	ASME B16.48
Standard Marking System for Valves, Fittings, Flanges, and Unions	MSS SP-25
High Pressure Chemical Industry Flanges and Threaded Stubs for Use with Lens Gaskets [Note (1)]	MSS SP-65
Metallic Pipe and Tubes	
Welded and Seamless Wrought Steel Pipe [Note (1)]	ASME B36.10M
Stainless Steel Pipe [Note (1)]	ASME B36.19M
Miscellaneous	
Threading, Gauging, and Thread Inspection of Casing, Tubing, and Line Pipe Threads	API 5B
Unified Inch Screw Threads (UN and UNR Thread Form)	ASME B1.1
Pipe Threads, General Purpose (Inch)	ASME B1.20.1
Metallic Gaskets for Pipe Flanges	ASME B16.20
Buttwelding Ends	ASME B16.25
Surface Texture (Surface Roughness, Waviness, and Lay)	ASME B46.1

GENERAL NOTE: The approved edition dates of these standards and specifications, along with the names and addresses of the sponsoring organizations, are shown in Appendix E.

NOTE: (1) The use of components made in accordance with these standards is permissible, provided they are

- (a) examined and leak tested in accordance with the requirements of paras. K341 and K345, respectively.
- (b) impact tested in accordance with the methods described in paras. K323.3.1 through K323.3.4, and meet the acceptance criteria specified in para. K323.3.5. Note that such impact testing may require the destruction of one component from the same lot as the component to be used in service [see Table K323.3.1, Note (1)].
- (d) When tensile specimens are required by ASME BPVC, Section IX, the yield strength shall also be determined, using the method required for the base metal. The yield strength of each test specimen shall be not less than the specified minimum yield strength at room temperature (S_Y) for the base metals joined. Where two base metals having different S_Y values are joined by welding, the yield strength of each test specimen shall be not less than the lower of the two S_Y values.
- (e) Mechanical testing is required for all performance qualification tests.
- (f) Qualification on pipe or tubing shall also qualify for plate, but qualification on plate does not qualify for pipe or tubing.
- (g) For thickness greater than 51 mm (2 in.), the procedure test coupon shall be at least 75% as thick as the thickest joint to be welded in production.

K328.2.2 Procedure Qualification by Others. Qualification of welding procedures by others is not permitted.

K328.2.3 Performance Qualification by Others. Welding performance qualification by others is not permitted.

K328.2.4 Qualification Records. Paragraph 328.2.4 applies.

K328.3 Materials

K328.3.1 Filler Metal. Filler metal shall be specified in the engineering design and shall conform to the requirements of ASME BPVC, Section IX. A filler metal not yet incorporated in ASME BPVC, Section IX may be used with the owner's approval if a procedure qualification test, including an all-weld-metal test, is first successfully made.

K328.3.2 Weld Backing Material. Backing rings shall not be used.

K328.3.3 Consumable Inserts. Paragraph 328.3.3 applies, except that procedures shall be qualified as required by para. K328.2.

K328.4 Preparation for Welding

K328.4.1 Cleaning. Paragraph 328.4.1 applies.

K328.4.2 End Preparation

- (a) General
- (1) Butt weld end preparation is acceptable only if the surface is machined or ground to bright metal.
- (2) Butt welding end preparation contained in ASME B16.25 or any other end preparation that meets the procedure qualification is acceptable. [For convenience, the basic bevel angles taken from ASME B16.25, with some additional J-bevel angles, are shown in Figure 328.4.2, illustrations (a) and (b).]
 - (b) Circumferential Welds
- (1) If components' ends are trimmed as shown in Figure 328.4.2, illustration (a) or (b) to accommodate consumable inserts, or as shown in Figure K328.4.3 to correct internal misalignment, such trimming shall not result in a finished wall thickness before welding less than the required minimum wall thickness, t_m .
- (2) It is permissible to size pipe ends of the same nominal size to improve alignment, if wall thickness requirements are maintained.
- (3) Where necessary, weld metal may be deposited on the inside or outside of the component to permit alignment or provide for machining to ensure satisfactory seating of inserts.
- (4) When a butt weld joins sections of unequal wall thickness and the thicker wall is more than $1\frac{1}{2}$ times the thickness of the other, end preparation and geometry shall be in accordance with acceptable designs for unequal wall thickness in ASME B16.5.

K328.4.3 Alignment

- (a) Girth Butt Welds
- (1) Inside diameters of components at the ends to be joined shall be aligned within the dimensional limits in the welding procedure and the engineering design, except that no more than 1.5 mm ($\frac{1}{16}$ in.) misalignment is permitted as shown in Figure K328.4.3.
- (2) If the external surfaces of the two components are not aligned, the weld shall be tapered between the two surfaces with a slope not steeper than 1:4.
- (b) Longitudinal Butt Joints. Preparation for longitudinal butt welds (not made in accordance with a standard listed in Table K-1 or Table K326.1) shall conform to the requirements of para. K328.4.3(a).
 - (c) Branch Connection Welds
- (1) The dimension m in Figure K328.5.4 shall not exceed ± 1.5 mm ($\frac{1}{16}$ in.).

(2) The dimension g in Figure K328.5.4 shall be specified in the engineering design and the welding procedure.

K328.5 Welding Requirements

- **K328.5.1 General.** The requirements of paras. 328.5.1(b), (d), (e), and (f) apply in addition to the requirements specified below.
- (a) All welds, including tack welds, repair welds, and the addition of weld metal for alignment [paras. K328.4.2(b)(3) and K328.4.3(c)(1)], shall be made by qualified welders or welding operators, in accordance with a qualified procedure.
- (b) Tack welds at the root of the joint shall be made with filler metal equivalent to that used for the root pass. Tack welds shall be fused with the root pass weld, except that those that have cracked shall be removed. Bridge tacks (above the root) shall be removed.
- **K328.5.2 Fillet Welds.** Fillet welds, where permitted (see para. K3112.2), shall be fused with and shall merge smoothly into the component surfaces.

K328,5:3 Seal Welds. Seal welds are not permitted.

K328.5.4 Welded Branch Connections. Branch connection fittings (see para. 300.2), attached by smoothly contoured full penetration groove welds of a design that permits 100% interpretable radiographic examination, are the only types acceptable.

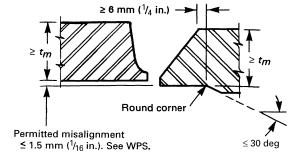
Figure K328.5.4 shows acceptable details of welded branch connections. The illustrations are typical and are not intended to exclude acceptable types of construction not shown.

K328.5.5 Fabricated Laps. Fabricated laps are not permitted.

K328.6 Weld Repair

Paragraph 328.6 applies, except that procedures and performance shall be qualified as required by para. K328.2.1. See also para. K341.3.3.

Figure K328.4.3 Pipe Bored for Alignment: Trimming and Permitted Misalignment



Branch - Bra

Figure K328.5.4 Some Acceptable Welded Branch Connections Suitable for 100% Radiography

K330 PREHEATING

K330.1 General

Paragraph 330.1 applies, except that seal welds are not permitted in this Chapter.

K330.1.1 Requirements. Paragraph 330.1.1 applies.

K330.1.2 Unlisted Materials. Paragraph 330.1.2 applies.

K330.1.3 Temperature Verification. Paragraph 330.1.3(a) applies. Temperature-indicating materials and techniques shall not be detrimental to the base metals.

K330.1.4 Preheat Zone. Paragraph 330.1.4 applies.

K330.2 Specific Requirements

Paragraph 330.2 applies in its entirety.

K331 HEAT TREATMENT

The text introducing para. 331 applies.

K331.1 General

K331.1.1 Heat Treatment Requirements. The provisions of para. 331 and Table 331.1.1 apply, except as specified below.

(a) Heat treatment is required for all thicknesses of P-Nos. 4 and 5 materials.

- (b) For welds other than longitudinal in quenched and tempered materials, when heat treatment is required by the engineering design, the temperature shall not be higher than 28°C (50°F) below the tempering temperature of the material.
- (c) Longitudinal welds in quenched and tempered material shall be heat treated in accordance with the applicable material specification.

K331.1.3 Governing Thickness. When components are joined by welding, the thickness to be used in applying the heat treatment provisions of Table 331.1.1 shall be that of the thicker component measured at the joint, except as follows:

In the case of fillet welds used for attachment of external nonpressure parts, such as lugs or other pipe-supporting elements, heat treatment is required when the thickness through the weld and base metal in any plane is more than twice the minimum material thickness requiring heat treatment (even though the thickness of the components at the joint is less than that minimum thickness) except as follows:

- (a) not required for P-No. 1 materials when weld throat thickness is $16 \text{ mm} (\frac{5}{8} \text{ in.})$ or less, regardless of base metal thickness.
- (b) not required for P-Nos. 3, 4, 5, 10A, and 10B materials when weld throat thickness is 6 mm ($\frac{1}{4}$ in.) or less, regardless of base metal thickness, provided that not less than the recommended minimum preheat is applied and

the specified minimum tensile strength of the base metal is less than 490 MPa (71 ksi).

(c) not required for ferritic materials when welds are made with filler metal that does not air harden. Austenitic welding materials may be used for welds to ferritic materials when the effects of service conditions, such as differential thermal expansion due to elevated temperature, or corrosion, will not adversely affect the weldment.

K331.1.4 Heating and Cooling. Paragraph 331.1.4 applies.

K331.1.6 Temperature Verification. Heat treatment temperature shall be checked by thermocouple pyrometers or other suitable methods to ensure that the WPS requirements are met. Temperature-indicating materials and techniques shall not be detrimental to the base metals.

K331.2 Specific Requirements

Paragraph 331.2 applies in its entirety.

K332 BENDING AND FORMING

K332.1 General

Pipe shall be hot or cold bent in accordance with a written procedure to any radius that will result in surfaces free of cracks and free of buckles. The procedure shall address at least the following, as applicable:

- (a) material specification and range of size and thickness
 - (b) range of bend radii and fiber elongation
- (c) minimum and maximum metal temperature during bending
 - (d) method of heating and maximum hold time
- (e) description of bending apparatus and procedure to be used
- (f) mandrels or material and procedure used to fill the bore
- (g) method for protection of thread and machined surfaces
 - (h) examination to be performed
 - (i) required heat treatment
- (j) postheat treatment dimensional adjustment technique

K332.2 Bending

K332.2.1 Bend Flattening. The difference between the maximum and the minimum diameters at any cross section of a bend shall not exceed 8% of nominal outside diameter for internal pressure and 3% for external pressure.

K332.2.2 Bending Temperature. Paragraph 332.2.2 applies, except that in cold bending of quenched and tempered ferritic materials, the temperature shall be at least 28°C (50°F) below the tempering temperature.

K332.3 Forming

Piping components shall be formed in accordance with a written procedure. The temperature range shall be consistent with material characteristics, end use, and specified heat treatment. The thickness after forming shall be not less than required by design. The procedure shall address at least the following, as applicable:

- (a) material specification and range of size and thickness
- (b) maximum fiber elongation expected during forming
- (c) minimum and maximum metal temperature during bending
 - (d) method of heating and maximum hold time
- (e) description of forming apparatus and procedure to be used
- (f) materials and procedures used to provide internal support during forming
 - (g) examination to be performed
 - (h) required heat treatment

K332.4 Required Heat Treatment

K332.4.1 Hot Bending and Forming. After hot bending and forming, heat treatment is required for all thicknesses of P.Nos. 3, 4, 5, 6, 10A, and 10B materials that are not quenched and tempered. Times and temperatures shall be in accordance with para. 331. Quenched and tempered materials shall be reheat treated to the original material specification.

K332.4.2 Cold Bending and Forming

- (a) After cold bending and forming, heat treatment in accordance with (b) below is required, regardless of thickness, when specified in the engineering design or when the maximum calculated fiber elongation exceeds 5% strain or 50% of the basic minimum specified longitudinal elongation for the applicable specification, grade, and thickness for P-Nos. 1 through 6 materials (unless it has been demonstrated that the selection of the pipe and the procedure for making the components provide assurance that the most severely formed portion of the material has retained an elongation of not less than 10%).
- (b) Heat treatment is required regardless of thickness and shall conform to the temperatures and durations given in Table 331.1.1, except that for quenched and tempered materials, the stress relieving temperature shall not exceed a temperature 28°C (50°F) below the tempering temperature of the material.

K333 BRAZING AND SOLDERING

Brazing shall be in accordance with para. 333. The owner shall specify examination requirements for brazed joints.

K335 ASSEMBLY AND ERECTION

K335.1 General

Paragraph 335.1 applies.

K335.2 Flanged Joints

Paragraph 335.2 applies, except that bolts shall extend completely through their nuts.

K335.3 Threaded Joints

Paragraph 335.3 applies, except that threaded joints shall not be seal welded.

K335.4 Special Joints

Special joints (as defined in para. K318) shall be installed and assembled in accordance with the manufacturer's instructions, as modified by the engineering design. Care shall be taken to ensure full engagement of joint members.

K335.5 Cleaning of Piping

See Appendix F, para. F335.9.

PART 10 INSPECTION, EXAMINATION, AND TESTING

K340 INSPECTION

Paragraphs 340.1 through 340.4 apply.

K341 EXAMINATION

Paragraphs 341.1 and 341.2 apply.

K341.3 Examination Requirements

K341.3.1 General. Prior to initial operation, each piping installation, including components and workmanship, shall be examined in accordance with para. K341.4 and the engineering design. If heat treatment is performed, examination shall be conducted after its completion.

K341.3.2 Acceptance Criteria. Acceptance criteria shall be as stated in the engineering design and shall at least meet the applicable requirements stated in (a) and (b) below, and elsewhere in this Chapter.

(a) Table K341.3.2 states acceptance criteria (limits on imperfections) for welds. See Figure 341.3.2 for typical weld imperfections.

Branch

Connection

Note (4)

Α

Fillet

Note (3)

Α

F

Table K341.3.2 Acceptance Criteria for Welds

Criteria (A-F) for Types of Welds, and for Required Examination Methods [Note (1)] Type of Weld Methods Ultrasonics Longitudinal Type of orGirth Groove Imperfection Visual Radiography Groove [Note (2)] Crack Α Α Lack of fusion Α Α

Α A Incomplete penetration Α Α Α A Internal porosity В В N/A В Linear indication C C N/A C Undercutting Α Α Α Α Surface porosity or exposed slag inclusion Α Α Α Α Concave root surface (suck-up) D D N/A D Surface finish Е Е Е Е

GENERAL NOTES:

Reinforcement or internal protrusion

(a) Weld imperfections are evaluated by one or more of the types of examination methods given, as specified in paras. K341.4.1 and K341.4.2.

F

- (b) "N/A" indicates this Chapter does not establish acceptance criteria or does not require evaluation of this kind of imperfection for this type of
- (c) Check (✓) indicates examination method generally used for evaluating this kind of weld imperfection.
- (d) Ellipsis (...) indicates examination method not generally used for evaluating this kind of weld imperfection.
- (e) Symbols A through F are explained in the table on the next page.

(18)

- (1) Criteria given are for required examination. More-stringent criteria may be specified in the engineering design.
- (2) Longitudinal welds include only those permitted in paras. K302.3.4 and K305. The criteria shall be met by all welds, including those made in accordance with a standard listed in Table K326.1 or in Appendix K.
- (3) Fillet welds include only those permitted in para. K311.2.2.
- (4) Branch connection welds include only those permitted in para. K328.5.4.

Criterion Value Notes for Table K341.3.2

	Criterion	
Symbol	Measure	Acceptable Value Limits [Note (1)]
Α	Extent of imperfection	Zero (no evident imperfection)
В	Size and distribution of internal porosity	See ASME BPVC, Section VIII, Division 1, Appendix 4
С	Internal slag inclusion, tungsten inclusion, or linear indication. Indications are unacceptable if the amplitude exceeds the reference level, or indications have lengths that exceed	
	Individual length [Note (2)]	6 mm ($\frac{1}{4}$ in.) for $\overline{T}_w \le 19$ mm ($\frac{3}{4}$ in.)
		$\overline{T}_{w}/3$ for 19 mm ($\frac{3}{4}$ in.) $< \overline{T}_{w} \le 57$ mm ($2\frac{1}{4}$ in.)
		$\overline{T}_w/3$ for 19 mm ($\frac{3}{4}$ in.) $<\overline{T}_w \le 57$ mm ($2\frac{1}{4}$ in.) 19 mm ($\frac{3}{4}$ in.) for $\overline{T}_w > 57$ mm ($2\frac{1}{4}$ in.)
	Cumulative length	$\leq \overline{T}_w$ in any 12 \overline{T}_w weld length
D	Depth of root surface concavity	Wall Thickness, $\overline{T}_{\!\scriptscriptstyle W^{\prime}}$ mm (in.) Depth of Surface Concavity, mm (in.)
		≤13 (½) ≤1.5 (以 ₁₆)
		>13 $\binom{1}{2}$ and ≤ 51 (2) $\leq 3 \binom{1}{8}$
		>51 (2) ≤4 (⁵ / ₃₂)
		and total joint thickness including weld reinforcement $\geq \overline{T}_{\!\scriptscriptstyle W}$
E	Surface roughness	\leq 12.5 μm (500 μin) R_a (see ASME B46.1 for definition of roughness average, R_a)
F	Height of reinforcement or internal protrusion [Note (3)] in any plane through the weld shall	Wall Thickness, External Weld Reinforcement $\overline{\mathcal{T}}_{w^n}$ mm (in.) or Internal Weld Protrusion, mm (in.)
	be within the limits of the applicable height value in the tabulation at the right. Weld metal	≤13 (½) ≤1.5 (½)
	shall be fused with and merge smoothly into	$(\frac{1}{2})$ and ≤51 (2) ≤3 ($\frac{1}{8}$)
	the component surfaces.	

NOTES:

- (1) Where two limiting values are given, the lesser measured value governs acceptance. \overline{T}_{w} is the nominal wall thickness of the thinner of two components joined by a butt weld.
- (2) For ultrasonic examination, refer to para. K344.63 for acceptable value limits.
- (3) For groove welds, height is the lesser of the measurements made from the surfaces of the adjacent components. For fillet welds, height is measured from the theoretical throat; internal protrusion does not apply. Required thickness t_m shall not include reinforcement or internal protrusion.
- (b) Acceptance criteria for castings are specified in para. K302.3.3.

K341.3.3 Defective Components and Workmanship.

Defects (imperfections of a type or magnitude not acceptable by the criteria specified in para. K341.3.2) shall be repaired, or the defective item or work shall be replaced. Examination shall be as follows:

- (a) When the defective item or work is repaired, the repaired portion of the item or work shall be examined. The examination shall use the same methods and acceptance criteria employed for the original examination. See also para. K341.3.1(a).
- (b) When the defective item or work is replaced, the new item or work used to replace the defective item or work shall be examined. The examination shall use any method and applicable acceptance criteria that meet the requirements for the original examination. See also para. K341.3.1(a).

K341.4 Extent of Required Examination

Piping shall be examined to the extent specified herein or to any greater extent specified in the engineering design.

K341.4.1 Visual Examination

- (a) The requirements of para. 341.4.1(a) apply with the following exceptions in regard to extent of examination:
 - (1) Materials and Components. 100%.
 - (2) Fabrication. 100%.
 - (3) Threaded, Bolted, and Other Joints. 100%.
- (4) Piping Erection. All piping erection shall be examined to verify dimensions and alignment. Supports, guides, and points of cold spring shall be checked to ensure that movement of the piping under all conditions of startup, operation, and shutdown will be accommodated without undue binding or unanticipated constraint.

- (b) Pressure-Containing Threads. 100% examination for finish and fit is required. Items with visible imperfections in thread finish and/or the following defects shall be rejected:
- (1) Tapered Threads. Failure to meet gaging requirements in API Spec 5B or ASME B1.20.1, as applicable.
- (2) Straight Threads. Excessively loose or tight fit when gaged for light interference fit.

K341.4.2 Radiographic and Ultrasonic Examination

- (a) All girth, longitudinal, and branch connection welds shall be 100% radiographically examined, except as permitted in (b) below.
- (b) When specified in the engineering design and with the owner's approval, ultrasonic examination of welds may be substituted for radiographic examination where $\overline{T}_w \geq 13 \, \text{mm} \left(\frac{1}{2} \, \text{in.} \right)$.
- (c) In-process examination (see para. 344.7) shall not be substituted for radiographic or ultrasonic examination of welds.

K341.4.3 Certifications and Records. Paragraph 341.4.1(c) applies.

K341.5 Supplementary Examination

Any of the examination methods described in para. K344 may be specified by the engineering design to supplement the examination required by para. K341.4. The extent of supplementary examination to be performed and any acceptance criteria that differ from those specified in para. K341.3.2 shall be specified in the engineering design.

K341.5.1 Hardness Tests. Paragraph 341.5.2 applies.

K341.5.2 Examinations to Resolve Uncertainty. Paragraph 341.5.3 applies.

K342 EXAMINATION PERSONNEL

Paragraph 342 applies in its entirety.

K343 EXAMINATION PROCEDURES

Paragraph 343 applies, except that the examination methods shall comply with para. K344.

K344 TYPES OF EXAMINATION

K344.1 General

Paragraphs 344.1.1 and 344.1.2 apply. In para. 344.1.3, terms other than "100% examination" apply only to supplementary examinations.

K344.2 Visual Examination

Paragraph 344.2 applies in its entirety.

K344.3 Magnetic Particle Examination

The method for magnetic particle examination shall be as specified in

- (a) paragraph K302.3.3(b) for castings
- (b) ASME BPVC, Section V, Article 7 for welds and other components

K344.4 Liquid Penetrant Examination

The method for liquid penetrant examination shall be as specified in

- (a) paragraph K302.3.3(b) for castings
- (b) ASME BPVC, Section V, Article 6 for welds and other components

K344.5 Radiographic Examination

The method for radiographic examination shall be as specified in

- (a) paragraph K302.33(c) for castings
- (b) ASME BPVC, Section V, Article 2 for welds and other components

K344.6 Ultrasonic Examination

K344.6.1 Castings. The method for ultrasonic examination of castings shall be as specified in para. K302.3.3(c).

K344.6.2 Pipe and Tubing

- (a) Method. Pipe and tubing, required or selected in accordance with Table K305.1.2 to undergo ultrasonic examination, shall pass a 100% examination for longitudinal defects in accordance with ASTM E213, Ultrasonic Testing of Metal Pipe and Tubing. Longitudinal (axial) reference notches shall be introduced on the outer and inner surfaces of the calibration (reference) standard in accordance with Fig. 3(c) of ASTM E213 to a depth not greater than the larger of 0.1 mm (0.004 in.) or 4% of specimen thickness and a length not more than 10 times the notch depth.
- (b) Acceptance Criteria. Any indication greater than that produced by the calibration notch represents a defect; defective pipe and tubing shall be rejected.
- (c) Records. For pipe and tubing that passes this examination, a report shall be prepared that contains at least the information specified in 15.2.1 through 15.2.6 of ASTM E213.

K344.6.3 Welds (18)

(a) Method. The method for ultrasonic examination of welds shall be as specified in ASME BPVC, Section V, Article 4 for nominal thickness, \overline{T}_{w} , greater than or equal to 13 mm ($\frac{1}{2}$ in.) but less than 25 mm (1 in.), and ASME BPVC, Section VIII, Division 3, KE-301 and KE-302 for nominal wall thickness, \overline{T}_{w} , greater than or equal to 25 mm (1 in.).

- (b) Acceptance Criteria. Cracks, lack of fusion, incomplete penetration, or undercutting are unacceptable regardless of size or length (see Table K341.3.2). In addition, for an internal slag inclusion, tungsten inclusion, or linear indication
- (1) for nominal wall thickness, \overline{T}_{w} , greater than or equal to 13 mm ($\frac{1}{2}$ in.) but less than 25 mm (1 in.), the acceptance criterion for the thickness to be examined specified in para. 344.6.2 applies.
- (2) for nominal wall thickness, \overline{T}_{w} , greater than or equal to 25 mm (1 in.), the acceptance criteria specified in ASME BPVC, Section VIII, Division 3, KE-333 for the thickness to be examined apply.

K344.7 In-Process Examination

Paragraph 344.7 applies in its entirety.

K344.8 Eddy Current Examination

- **K344.8.1 Method.** The method for eddy current examination of pipe and tubing shall follow the general guidelines of ASME BPVC, Section V, Article 8, subject to the following specific requirements:
- (a) Cold drawn austenitic stainless steel pipe and tubing, selected in accordance with Table K305.1.2 for eddy current examination, shall pass a 100% examination for longitudinal defects.
- (b) A calibration (reference) standard shall be prepared from a representative sample. A longitudinal (axial) reference notch shall be introduced on the inner surface of the standard to a depth not greater than the larger of 0.1 mm (0.004 in.) or 5% of specimen thickness and a length not more than 6.4 mm (0.25 in.).
- **K344.8.2 Acceptance Criteria.** Any indication greater than that produced by the calibration notch represents a defect; defective pipe or tubing shall be rejected.
- **K344.8.3 Records.** For pipe and tubing that passes this examination, a report shall be prepared that includes at least the following information:
 - (a) material identification by type, size, lot, heat, etc.
 - (b) listing of examination equipment and accessories
- (c) details of examination technique (including examination speed and frequency) and end effects, if any
- (d) description of the calibration standard, including dimensions of the notch, as measured
 - (e) examination results

K345 LEAK TESTING

K345.1 Required Leak Test

Prior to initial operation, each piping system shall be leak tested.

(a) Each weld and each piping component, except bolting and individual gaskets to be used during final system assembly and pressure-relieving devices to be

- used during operation, shall be hydrostatically or pneumatically leak tested in accordance with para. K345.4 or K345.5, respectively. The organization conducting the test shall ensure that during the required leak testing of components and welds, adequate protection is provided to prevent injury to people and damage to property from missile fragments, shock waves, or other consequences of any failure that might occur in the pressurized system.
- (b) In addition to the requirements of (a) above, a leak test of the installed piping system, excluding pressure-relieving devices to be used during operation, shall be conducted at a pressure not less than 110% of the design pressure to ensure tightness, except as provided in (c) or (d) below.
- (c) If the leak test required in (a) above is conducted on the installed piping system, the additional test in (b) above is not required.
- (d) With the owner's approval, pressure-relieving devices to be used during operation may be included in the leak test required in (b) above. The leak test pressure may be reduced to prevent the operation of, or damage to, the pressure-relieving devices, but shall not be less than 90% of the lowest set pressure of the pressure-relieving devices in the system.
- (e) For closure welds, examination in accordance with para K345.2.3(c) may be substituted for the leak test required in (a) above.
- (f) None of the following leak tests may be used in lieu of the leak tests required in para. K345.1:
 - (1) initial service leak test (para. 345.7)
 - (2) sensitive leak test (para. 345.8)
 - (3) alternative leak test (para. 345.9)

K345.2 General Requirements for Leak Tests

Paragraphs 345.2.4 through 345.2.7 apply. See below for paras. K345.2.1, K345.2.2, and K345.2.3.

K345.2.1 Limitations on Pressure

- (a) Through-Thickness Yielding. If the test pressure would produce stress (exclusive of stress intensification) in excess of S_{yt} at the outside surface of a component ¹⁰ at test temperature, as determined by calculation or by testing in accordance with para. K304.7.2(b), the test pressure may be reduced to the maximum pressure that will result in a stress (exclusive of stress intensification) at the outside surface that will not exceed S_{yt} .
 - (b) The provisions of paras. 345.2.1(b) and (c) apply.

K345.2.2 Other Test Requirements. Paragraph 345.2.2 applies. In addition, the minimum metal temperature during testing shall be not less than the impact test temperature (see para. K323.3.4).

¹⁰ See para. K304.1.2, footnote 4.

K345.2.3 Special Provisions for Leak Testing. Paragraphs K345.2.3(a), (b), and (c) below apply only to the leak test specified in para. K345.1(a). They are not applicable to the installed piping system leak test specified in para. K345.1(b).

- (a) Piping Components and Subassemblies. Piping components and subassemblies may be leak tested either separately or as assembled piping.
- (b) Flanged Joints. Flanged joints used to connect piping components that have previously been leak tested, and flanged joints at which a blank or blind flange is used to isolate equipment or other piping during the leak test, need not be leak tested.
- (c) Closure Welds. Leak testing of the final weld connecting piping systems or components that have been successfully leak tested is not required, provided the weld is examined in-process in accordance with para. 344.7 and passes the required 100% radiographic examination in accordance with para. K341.4.2.

K345.3 Preparation for Leak Test

Paragraph 345.3 applies in its entirety.

K345.4 Hydrostatic Leak Test

Paragraph 345.4.1 applies. See paras. K345.4.2 and K345.4.3 below.

K345.4.2 Test Pressure for Components and Welds.

Except as provided in para. K345.4.3, the hydrostatic regineering design. test pressure at every point in a metallic piping system shall be as follows:

- (a) not less than 1.25 times the design pressure.
- (b) when the design temperature is greater than the test temperature, the minimum test pressure, at the point under consideration, shall be calculated by eq. (38)

$$P_T = 1.25PS_T/S \tag{38}$$

where

P = internal design gage pressure

 P_T = minimum test gage pressure

- S = allowable stress at component design temperature for the prevalent pipe material; see Appendix K, Table K-1
- S_T = allowable stress at test temperature for the prevalent pipe material; see Table K-1
- (c) in those cases where the piping system may not include pipe itself, any other component in the piping system, other than pipe-supporting elements and bolting, may be used to determine the S_T/S ratio based on the applicable allowable stresses obtained from Table K-1. In those cases where the piping system may be made up of equivalent lengths of more than one mate-

rial, the S_T/S ratio shall be based on the minimum calculated ratio of the included materials.

K345.4.3 Hydrostatic Test of Piping With Vessels as a **System.** Paragraph 345.4.3(a) applies.

K345.5 Pneumatic Leak Test

Paragraph 345.5 applies, except for para. 345.5.4. See para. K345.5.4 below.

K345.5.4 Test Pressure. The pneumatic test pressure for components and welds shall be identical to that required for the hydrostatic test in accordance with para. K345.4.2.

K345.6 Hydrostatic-Pneumatic Leak Test for Components and Welds

If a combination hydrostatic-pneumatic leak test is used, the requirements of para. K345.5 shall be met, and the pressure in the liquid-filled part of the piping shall not exceed the limits stated in para. K345.4.2.

K346 RECORDS

K346.1 Responsibility

It is the responsibility of the piping designer, the manufacturer, the fabricator, and the erector, as applicable, to prepare the records required by this Chapter and by the

K346.2 Required Records

At least the following records, as applicable, shall be provided to the owner or the Inspector by the person responsible for their preparation:

(18)

- (a) the engineering design
- (b) material certifications
- (c) procedures used for fabrication, welding, heat treatment, examination, and testing
- (d) repair records of materials and piping components, including the welding procedure used for each, and location of repairs
- (e) performance qualifications for welders and welding operators
 - (f) qualifications of examination personnel
- (g) records of examination of pipe and tubing for longitudinal defects as specified in paras. K344.6.2(c) and K344.8.3, as applicable

K346.3 Retention of Records

The owner shall retain one set of the required records for at least 5 years after they are received.

Chapter X High Purity Piping

U300 GENERAL STATEMENTS

- (a) Chapter X pertains to piping designated by the owner as being in High Purity Fluid Service. See also Appendix M.
- (b) The organization, content, and paragraph designations of this Chapter correspond to those of the base Code (Chapters I through VI), Chapter VII, and Chapter VIII. The prefix U is used to designate Chapter X requirements.
- (c) Provisions and requirements of the base Code, Chapter VII, and Chapter VIII apply only as stated in this Chapter.
- (d) For piping not in High Purity Fluid Service, Code requirements are found in Chapters I through IX.
- (e) High Purity Piping. Chapter X provides alternative rules for design and construction of piping designated by the owner as being High Purity Fluid Service.
- (1) These rules apply only when specified by the owner, and only as a whole, not in part.
- (2) Chapter X rules do not provide for High Pressure Fluid Service.
- (3) Chapter VII applies to nonmetallic piping and piping lined with nonmetals in High Purity Fluid Service.

 (f) Chapter I applies.

PART 1 CONDITIONS AND CRITERIA

Chapter II, Part 1 applies. See para. U301.3.2(b)(5).

U301 DESIGN CONDITIONS

U301.3 Design Temperature

U301.3.2 Uninsulated Components

(b)

(5) compression, face seal, and hygienic clamped fittings and joints — 100% of the fluid temperature

PART 2 PRESSURE DESIGN OF PIPING COMPONENTS

Chapter II, Part 2 applies. See Figure U304.5.3 for representative configuration for metal face seal blanks.

PART 3 FLUID SERVICE REQUIREMENTS FOR PIPING COMPONENTS

Chapter II, Part 3 applies. See paras. U306.6, U307.3, and U308.

U306 FITTINGS, BENDS, MITERS, LAPS, AND BRANCH CONNECTIONS

U306.6 Tube Fittings

- (a) Tube fittings not listed in Table 326.1 or Appendix A shall meet the pressure design requirements described in para. 302.2.3 and the mechanical strength requirements described in para. 303.
- (b) Compression-type tube fittings may be used in accordance with para. U315.2 provided that the type of fitting selected complies with the following:
- (1) The gripping action of the fitting shall provide vibration resistance as demonstrated by exhibiting a stress intensity factor equal to or less than 1.5.
- (2) Intermixing of components from different manufacturers is permitted only when specified in the engineering design.
- (c) Face seal or hygienic clamp-type fittings in which the tightness of the joint is provided by a seating surface other than the threads (e.g., a metal face-seal fitting comprising internal and external threaded components, glands, and gasket or other constructions shown typically in Figure U335.7.1) may be used.

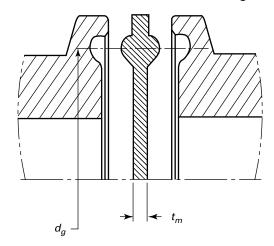
U307 VALVES AND SPECIALTY COMPONENTS U307.3 High Purity Fluid Service Valves

Valves such as ball, bellows, and diaphragm valves designed for High Purity Fluid Service that are not listed in Table 326.1 shall meet the pressure design requirements described in para. 302.2.2 and the mechanical strength requirements described in para. 303.

U308 FLANGES, BLANKS, FLANGE FACINGS, AND GASKETS

Flanges should be avoided whenever possible. When flanges are utilized, para. 308 applies, except expanded joint flanges described in para. 308.2.2 are not permitted.

Figure U304.5.3 Blanks



(a) Hygienic Clamp-Type Fitting



Chapter II, Part 4 applies, except expanded joints, flared tube fittings, and caulked joints, described in paras. 313, 315, and 316, respectively, are not permitted. See paras. U311, U311.1(c), U314, and U315.

U311 WELDED JOINTS

Paragraph 311 applies, except for para. 311.1(c). See para. U311.1(c).

U311.1 General

(c) Examination shall be in accordance with para. U341.4.1.

U314 THREADED JOINTS

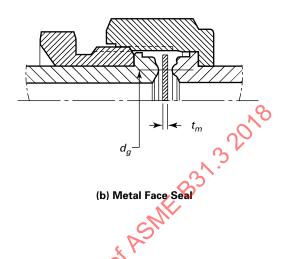
Threaded joints should be avoided whenever possible. When threaded joints are utilized, para. 314 applies.

U315 TUBING JOINTS

Paragraph 315 applies. See paras. U315.1, U315.2(c), and U315.3.

U315.1 General

In selecting and applying compression, face seal, and hygienic clamp-type tube fittings, the designer shall consider the possible adverse effects on the joints of such factors as assembly and disassembly, cyclic loading, vibration, shock, and thermal expansion and contraction. See para. FU315.



U315.2 Joints Conforming to Listed Standards

(c) Joints using compression, face seal, hygienic clamp, and automatic welding tube fittings covered by listed standards may be used.

#315.3 Joints Not Conforming to Listed Standards

- (a) Compression-type tube fitting joints shall be fully gageable on initial installation to ensure sufficient tightening.
- (b) Safeguarding is required for face seal or hygienic clamp-type joints used under severe cyclic conditions.

PART 5 FLEXIBILITY AND SUPPORT

Chapter II, Part 5 applies. See para. U319.3.6.

U319 PIPING FLEXIBILITY

U319.3 Properties for Flexibility Analysis

U319.3.6 Flexibility and Stress Intensification Factors. Paragraph 319.3.6 applies; however, piping components used in high-purity applications, e.g., multiport block valves, hygienic unions, crosses, and point-of-use and adaptor fittings, often do not have geometries similar to those in Table D300.

PART 6 SYSTEMS

Chapter II, Part 6 applies.

PART 7 METALLIC MATERIALS

The provisions and requirements in Chapter III for materials apply. Materials commonly used in high purity process piping systems include austenitic, ferritic, and duplex stainless steels, and nickel and nickel alloys.

PART 8 STANDARDS FOR PIPING COMPONENTS

Chapter IV applies.

PART 9 FABRICATION, ASSEMBLY, AND ERECTION

U327 GENERAL

Metallic piping materials and components are prepared for assembly and erection by one or more of the fabrication processes covered in paras. U328, U330, U331, and U332. When any of these processes is used in assembly or erection, requirements are the same as for fabrication.

U328 WELDING

Paragraph 328 applies, except for paras. 328.3.2, 328.5.4, and 328.5.5. See paras. U328.2.1(g) and (h) U328.4, U328.4.4, and U328.5.1(g) for additional requirements.

U328.2 Welding and Brazing Qualification U328.2.1 Qualification Requirements

- (g) A change in the type or nominal composition of the backing (purge) gas shall require requalification.
- (h) The welding process shall be orbital GTAW, except for tack welds. Tack welds made prior to orbital welding may be manual GTAW.

(18) U328.4 Preparation for Welding

Paragraph 328.4.1 applies. Additionally, when weld coupon examination is specified in the engineering design or in the referencing code or standard (e.g., ASME BPE or SEMI), primary weld coupons shall be made in accordance with para. U328.4.4(b)(1) and examined in accordance with para. U344.8 prior to the start of production welding. This will demonstrate that the orbital welding equipment is set up properly and the weld program is sufficient to make repeatable production welds in accordance with the qualified welding procedure specification (WPS).

U328.4.4 Preparation of Weld Coupons

- (a) Weld coupons shall be made by qualified welding operators using the same qualified WPS and the same variables used for production welds.
 - (b) Methods
- (1) Primary weld coupons shall be made from two short sections of tubing selected from the same diameter, wall thickness, and alloy as the material used for production. Sections shall be of sufficient length for fit up in the weld head allowing for attachment of inside diameter purge apparatus outside of the weld head. The sections shall be welded together in a square groove weld on a butt joint.
- (2) Production weld coupons may be made in accordance with para. U328.4.4(b)(1) or, at the owner's discretion, may be cut from actual production welds. The weld coupons shall be selected to ensure that the work product of each welding operator doing the production welding is represented.

U328.5 Welding Requirements

U328.5.1 General

(g) Tack welds shall be fully consumed after completion of the weld. Tack welds shall be made by a qualified welder or welding operator.

U330 PREHEATING

Paragraph 330 applies.

U331 HEAT TREATMENT

Paragraph 331 applies.

U332 BENDING AND FORMING

Paragraph 332 applies in its entirety.

U333 BRAZING AND SOLDERING

Brazing and soldering are not permitted.

U335 ASSEMBLY AND ERECTION

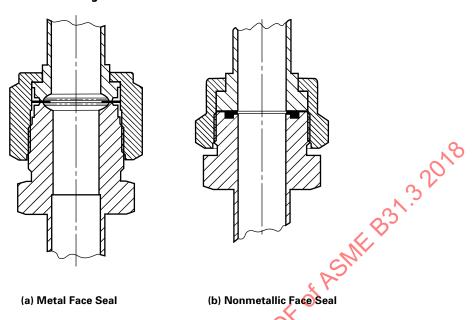
Paragraph 335 applies, except for paras. 335.4.1, 335.5, and 335.6. See paras. U335.7 and U335.8.

U335.7 Face Seal Joints

U335.7.1 Metal Face Seal. Metal face seal joints shall be installed and assembled in accordance with manufacturer's instructions. See Figure U335.7.1, illustration (a).

U335.7.2 Nonmetallic Face Seal. Nonmetallic face seal joints shall be installed and assembled in accordance with manufacturer's instructions. Care shall be taken to avoid distorting the seal when incorporating such joints into

Figure U335.7.1 Face Seal Joints



piping assemblies by welding. See Figure U335.7.1, illustration (b).

U335.8 Hygienic Clamp Joint Assembly

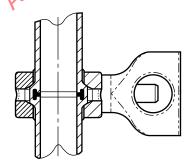
Hygienic clamp joint assembly components, e.g., those shown in Figures U335.8A, U335.8B, and U335.8C, shall be installed and assembled in accordance with the manufacturer's instructions. Care shall be taken to avoid distorting the seal when incorporating such joints into piping assemblies by welding.

PART 10 INSPECTION, EXAMINATION, AND TESTING

U340 INSPECTION

Paragraph 340 applies in its entirety.

Figure U335.8A Hygienic Clamp Joint Assembly



U341 EXAMINATION

Paragraph 341 applies. See paras. U341.3.2 and U341.4.1.

U341.3 Examination Requirements

U341.3.2 Acceptance Criteria. Acceptance criteria for (18) all coupon and production welds shall be as stated in the engineering design or in the referencing code or standard (e.g., ASME BPE or SEMI) and shall at least meet the applicable requirements in para. 341.3.2.

U341.4 Extent of Required Examination

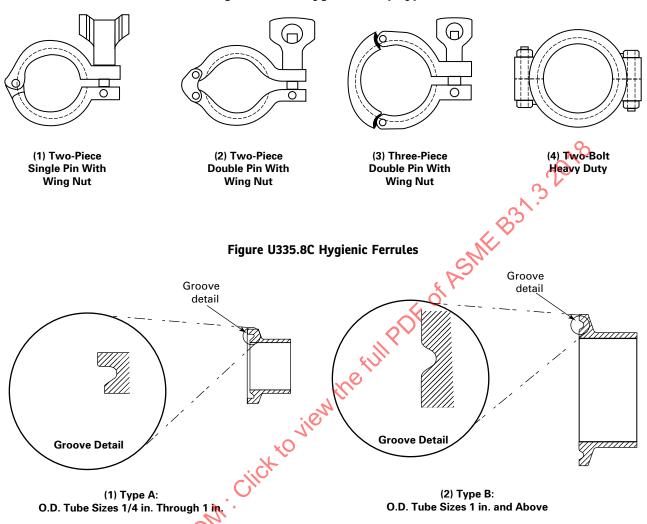
U341.4.1 Examination. A weld coupon examination in accordance with para. U344.8 may be used in lieu of the 5% random radiography/ultrasonic examination required in para. 341.4.1(b)(1) when the following are employed in fabrication:

- (a) autogenous automatic orbital welding
- (b) automatic orbital welding with the use of consumable insert rings

U341.4.5 Weld Coupon Examination. Weld coupons shall be made and examined in accordance with para. U344.8 when any of the following conditions exist:

- (a) beginning of shift
- (b) change of purge source
- (c) change of power supply
- (d) change of equipment, e.g., weld head, weld-head extensions, tungsten
 - (e) any time there is a weld defect

Figure U335.8B Hygienic Clamp Types



U342 EXAMINATION PERSONNEL

Paragraph 342 applies in its entirety. See para. U342.2(a).

U342.2 Specific Requirement

- (a) For weld coupon examination
- (1) the examinations shall be performed by personnel other than those performing the production work or
- (2) with the owner's approval, the personnel performing the production work shall be permitted to perform the examination, provided the personnel meet the personnel qualification and certification requirements in para. 342.1

U343 EXAMINATION PROCEDURES

Paragraph 343 applies.

U344 TYPES OF EXAMINATION

Paragraph 344 applies. See paras. U344.2 and U344.8.

U344.2 Visual Examination

Paragraph 344.2 applies, except that in addition to the method described in para. 344.2.2, borescopic examination shall be acceptable.

U344.8 Weld Coupon Examination

U344.8.1 Requirements. Weld coupon examination comprises examination of weld coupons for the following, as applicable:

- (a) prior to welding of coupons made in accordance with para. U328.4.4(b)(1)
 - (1) joint preparation and cleanliness
- (2) fit-up, collet or clamp grip, and alignment in the weld head

- (3) variables in the orbital welding machine specified in the WPS
- (b) after welding of coupons made in accordance with para. U328.4.4(b)(1), and for weld coupons made in accordance with para. U328.4.4(b)(2), for compliance with para. U341.3.2
 - (1) alignment
 - (2) weld penetration
 - (3) weld bead width variation
 - (4) weld bead meander
 - (5) discoloration
- (6) weld defects, e.g., cracks, porosity, or sulfur stringers

To allow direct visual examination of the inside surfaces, the weld coupon may be cut or a suitable indirect visual examination method (e.g., borescopic examination) may be used.

U344.8.2 Method. A weld coupon shall be made to allow visual examination in accordance with para. U344.2, unless otherwise specified in the engineering design.

U345 TESTING

Paragraph 345 applies except for paras. 345.1, 345.8, and 345.9. See paras. U345.1, U345.8, and U345.9.

U345.1 Required Leak Test

Paragraph 345.1 applies, except that, at the owner's option, a helium mass spectrometer test in accordance with para. U345.8.1 may be substituted for the hydrostatic leak test.

U345.8 Sensitive Leak Test

Paragraph 345.8 applies, except that the helium mass spectrometer test described in para. U345.8.1 is also an acceptable method.

- **U345.8.1 Helium Mass Spectrometer Test.** The test shall be one of the following methods and performed in accordance with the following:
- (a) For pressurized systems, the test shall be in accordance with ASME BPVC, Section V, Article 10, Appendix IV (Helium Mass Spectrometer Detector Probe Technique).
- (1) The test pressure shall be the lesser of 105 kPa (15 psig) gage or 25% of the design pressure.
- (2) Prior to testing, the test pressure shall be held a minimum of 30 min.
- (3) Unless otherwise specified in the engineering design, the system tested is acceptable when no leakage is detected that exceeds the allowable leakage rate of 1×10^{-4} std cc/s.

- (b) For evacuated systems, the test shall be in accordance with ASME BPVC, Section V, Article 10, Appendix V (Helium Mass Spectrometer Test Tracer Probe Technique).
- (1) The piping system shall be evacuated to an absolute pressure sufficient for connection of the helium mass spectrometer to the system.
- (2) Unless otherwise specified in the engineering design, the system tested is acceptable when no leakage is detected that exceeds the allowable leakage rate of 1×10^{-5} std cc/s.

U345.9 Alternative Leak Test

Paragraph 345.9 applies, except that welds may be examined by weld coupon examination method in accordance with para. U341.4.5 and the test method may be helium mass spectrometer test in accordance with para. U345.8.1.

U346 RECORDS

U346.2 Responsibility

It is the responsibility of the piping designer, the manufacturer, the fabricator, and the erector, as applicable, to prepare the records required by this Code, ASME BPE, SEMI, or other industry standard as specified in the engineering design.

U346.3 Retention of Records

Paragraph 346.3 applies.

PART 11 HIGH PURITY PIPING IN CATEGORY M FLUID SERVICE

UM300 GENERAL STATEMENTS

- (a) Chapter X, Part 11 pertains to piping designated by the owner as being high purity piping in Category M Fluid Service. See also Appendix M.
- (b) The organization, content, and paragraph designations of these Parts correspond to those of Chapter VIII. The prefix UM is used.
 - (c) Paragraphs M300(d), (e), and (f) apply.
- (d) Provisions and requirements of Chapter VIII apply with the additional requirements in paras. UM307, UM307.2, UM322, UM322.3, UM328, UM335, UM335.3.3, UM341, UM341.4(b)(1) and (2), and UM345(b).

UM307 METALLIC VALVES AND SPECIALTY COMPONENTS

Paragraph M307 applies in its entirety. See also para. UM307.2(a).

UM307.2 Specific Requirements

(a) For bellows or diaphragm sealed type valves, the bonnet or cover plate closure shall be secured by a straight thread sufficient for mechanical strength, have a metal-tometal seat, and include a secondary stem seal.

UM322 SPECIFIC PIPING SYSTEMS

Paragraph M322 applies, except for para. M322.3(c). See para. UM322.3(c).

UM322.3 Instrument Piping

(c) joining methods shall conform to the requirements of para. U315

UM328 WELDING OF MATERIALS

Welding shall be in accordance with paras. M311.1 and U328, except examination shall be in accordance with para. UM341.

UM335 ASSEMBLY AND ERECTION OF METALLIC

a. Us para. Paragraph M335 applies, except for para. M335.3.3. See para. UM335.3.3.

UM335.3.3 Straight-Threaded Joints. The requirements of para. M335.3.3 are subject to the limitations in para. UM322.

UM341 EXAMINATION

Paragraph M341 applies. See UM341.4(b)(1) and (2).

UM341.4 Extent of Required Examination

- (b) Other Examination
- (1) The 100% radiography/ultrasonic@xamination required in para. M341.4(b) applies.
- (2) The in-process examination alternative permitted in para. 341.4.1(b)(1) applies, except a weld coupon examination in accordance with para. U344.8 is also an acceptable substitute when specified in the engineering design or by the Inspector.

UM345 TESTING

Paragraph M345(a) applies. See para. UM345(b).

(b) A sensitive leak test in accordance with para. U345.8 shall be included in the required leak test (para. U345.1).

APPENDIX A ALLOWABLE STRESSES AND QUALITY FACTORS FOR METALLIC PIPING AND BOLTING MATERIALS

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(18)

Specification Index for Appendix A

Spec. No.	Title	Spec.	No. Title
ASTM		ASTM	(Cont'd)
A36	Carbon Structural Steel	A285	Pressure Vessel Plates, Carbon Steel, Low- and
A47	Ferritic Malleable Iron Castings		Intermediate-Tensile Strength
A48	Gray Iron Castings	A299	Pressure Vessel Plates, Carbon Steel, Manganese-
A53	Pipe, Steel, Black and Hot-Dipped, Zinc-Coated, Welded and Seamless		Silicon
A105	Carbon Steel Forgings for Piping Applications	A302	Pressure Vessel Plates, Alloy Steel, Manganese- Molybdenum and Manganese-Molybdenum- Nickel
A106	Seamless Carbon Steel Pipe for High-Temperature Service	A307	Carbon Steel Bolts and Studs, 60 000 PSI Tensile Strength
A126	Gray Iron Castings for Valves, Flanges, and Pipe Fittings	A312	Seamless, Welded, and Heavily Cold Worked Austenitic Stainless Steel Pipes
A134	Pipe, Steel, Electric-Fusion (Arc)-Welded (Sizes NPS 16 and Over)	A320	Alloy-Steel and Stainless Steel Bolting for Low- Temperature Service
A135	Electric-Resistance-Welded Steel Pipe	A333	Seamless and Welded Steel Pipe for Low-
A139	Electric-Fusion (Arc)-Welded Steel Pipe (NPS 4 and Over)	A333	Temperature Service and Other Applications with Required Notch Toughness
A179	Seamless Cold-Drawn Low-Carbon Steel Heat- Exchanger and Condenser Tubes	A334	Seamless and Welded Carbon and Alloy-Steel Tubes for Low-Temperature Service
A181 A182	Carbon Steel Forgings, for General-Purpose Piping Forged or Rolled Alloy and Stainless Steel Pipe	A335	Seamless Ferritic Alloy-Steel Pipe for High- Temperature Service
	Flanges, Forged Fittings, and Valves and Parts for High-Temperature Service	A350	Carbon and Low-Alloy Steel Forgings, Requiring Notch Toughness Testing for Piping Components
A193	Alloy-Steel and Stainless Steel Bolting for High Temperature or High Pressure Service and	A351	Castings, Austenitic, for Pressure-Containing Parts
A194	Other Special Purpose Applications Carbon Steel, Alloy Steel, and Stainless Steel Nuts for	A352	Steel Castings, Ferritic and Martensitic, for Pressure- Containing Parts, Suitable for Low-Temperature Service
	Bolts for High Pressure or High Temperature Service, or Both	A353	Pressure Vessel Plates, Alloy Steel, Double- Normalized and Tempered 9% Nickel
A197	Cupola Malleable Iron	A354	Quenched and Tempered Alloy Steel Bolts, Studs, and Other Externally Threaded Fasteners
A203	Pressure Vessel Plates, Alloy Steel, Nickel	A358	Electric-Fusion-Welded Austenitic Chromium-
A204 A213	Pressure Vessel Plates, Alloy Steel, Molybdenum Seamless Ferritic and Austenitic Alloy-Steel Boiler,		Nickel Stainless Steel Pipe for High-Temperature Service and General Applications
A216	Superheater, and Heat-Exchanger Tubes Steel Castings, Carbon, Suitable for Fusion Welding,	A369	Carbon and Ferritic Alloy Steel Forged and Bored Pipe for High-Temperature Service
A217	for High-Temperature Service Steel Castings, Martensitic Stainless and Alloy, for Pressure-Containing Parts, Suitable for High-	A376	Seamless Austenitic Steel Pipe for High- Temperature Service
A234	Temperature Service Piping Fittings of Wrought Carbon Steel and Alloy	A381	Metal-Arc-Welded Steel Pipe for Use With High- Pressure Transmission Systems
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A240	Plate, Sheet, and Strip for Pressure Vessels and for General Applications	A395	Ferritic Ductile Iron Pressure-Retaining Castings for Use at Elevated Temperatures
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A269	Seamless and Welded Austenitic Stainless Steel Tubing for General Service	A409	Welded Large Diameter Austenitic Steel Pipe for Corrosive or High-Temperature Service
A270	Seamless and Welded Austenitic and Ferritic/ Austenitic Stainless Steel Sanitary Tubing	A420	Piping Fittings of Wrought Carbon Steel and Alloy Steel for Low-Temperature Service
A276	Stainless Steel Bars and Shapes	A426	Centrifugally Cast Ferritic Alloy Steel Pipe for High-
A278	Gray Iron Castings for Pressure-Containing Parts for Temperatures Up to 650°F (350°C)	A437	Temperature Service Stainless and Alloy-Steel Turbine-Type Bolting
A283	Low and Intermediate Tensile Strength Carbon Steel Plates		Material Specially Heat Treated for High- Temperature Service

Specification Index for Appendix A (Cont'd)

Spec. 1	No. Title	Spec. N	o. Title
ASTM	(Cont'd)	ASTM	(Cont'd)
A451	Centrifugally Cast Austenitic Steel Pipe for High- Temperature Service	A815	Wrought Ferritic, Ferritic/Austenitic, and Martensitic Stainless Steel Piping Fittings
A453	High-Temperature Bolting, with Expansion Coefficients Comparable to Austenitic Stainless Steels	A860	Wrought High-Strength Ferritic Steel Butt-Welding Fittings
A479	Stainless Steel Bars and Shapes for Use in Boilers and Other Pressure Vessels	A928	Ferritic/Austenitic (Duplex) Stainless Steel Pipe Electric Fusion Welded with Addition of Filler
A487	Steel Castings Suitable for Pressure Service		Metal
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A516	Pressure Vessel Plates, Carbon Steel, for Moderate- and Lower-Temperature Service	A1010	Higher-Strength Martensitic Stainless Steel Plate, Sheet, and Strip
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A536	Ductile Iron Castings		Strength Low-Alloy with Improved Formability,
A537	Pressure Vessel Plates, Heat-Treated, Carbon- Manganese-Silicon Steel	A1053	and Ultra-High Strength Welded Ferritic-Martensitic Stainless Steel Pipe
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	Containing Parts Suitable for Low-Temperature Service	B43	Seamless Red Brass Pipe, Standard Sizes
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	for the Chemical Industry	B62	Composition Bronze or Ounce Metal Castings
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A645	Pressure Vessel Plates, 5 % and 5 ½ % Nickel Alloy	B75	Seamless Copper Tube
A 654	Steels, Specially Heat Treated	B88	Seamless Copper Water Tube
A671	Electric-Fusion-Welded Steel Pipe for Atmospheric and Lower Temperatures	B96	Copper-Silicon Alloy Plate, Sheet, Strip, and Rolled Bar for General Purposes and Pressure Vessels
A672	Electric-Fusion-Welded Steel Pipe for High- Pressure Service at Moderate Temperatures	B98	Copper-Silicon Alloy Rod, Bar and Shapes
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	for High-Pressure Service at High Temperatures	B148	Aluminum-Bronze Sand Castings
A694	Carbon and Altoy Steel Forgings for Pipe Flanges, Fittings, Valves, and Parts for High-Pressure	B150	Aluminum Bronze Rod, Bar and Shapes
	Transmission Service	B152	Copper Sheet, Strip, Plate and Rolled Bar
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	Special Quality, for Pressure Piping Components	B161	Nickel Seamless Pipe and Tube
	P	B162	Nickel Plate, Sheet and Strip
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A813	Single- or Double-Welded Austenitic Stainless Steel Pipe Cold Worked Welded Austenitic Stainless Steel Pipe		N06045, and N06696), Nickel-Chromium-Cobalt- Molybdenum Alloy (UNS N06617), and Nickel- Iron-Chromium-Tungsten Alloy (UNS N06674)
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Specification Index for Appendix A (Cont'd)

Spec.	No. Title	Spec. No. Title
ASTM	(Cont'd)	ASTM (Cont'd)
B167	Nickel-Chromium-Iron Alloys (UNS N06600, N06601, N06603, N06690, N06693, N06025, N06045, and N06696), Nickel-Chromium-Cobalt- Molybdenum Alloy (UNS N06617), and Nickel-	B409 Nickel-Iron-Chromium Alloy Plate, Sheet, and Str B423 Nickel-Iron-Chromium-Molybdenum-Copper Allo (UNS N08825, N08221, and N06845) Seamles Pipe and Tube
	Iron-Chromium-Tungsten Alloy (UNS N06674) Seamless Pipe and Tube	B424 Ni-Fe-Cr-Mo-Cu Alloy (UNS N08825, UNS N0822 and UNS N06845) Plate, Sheet, and Strip
B168	Nickel-Chromium-Iron Alloys (UNS N06600, N06601, N06603, N06690, N06693, N06025, N06045, and N06696), Nickel-Chromium-Cobalt-	B425 Ni-Fe-Cr-Mo-Cu Alloy (UNS N08825, UNS N0822 and UNS N06845) Rod and Bar
	Molybdenum Alloy (UNS N06617), and Nickel- Iron-Chromium-Tungsten Alloy (UNS N06674)	B435 UNS N06002, UNS N06230, UNS N12160, and U R30556 Plate, Sheet, and Strip
B169	Plate, Sheet and Strip Aluminum Bronze Sheet, Strip, and Rolled Bar	B443 Nickel-Chromium-Molybdenum-Columbium Allo (UNS N06625) and Nickel-Chromium-
B171	Copper-Alloy Plate and Sheet for Pressure Vessels, Condensers, and Heat Exchangers	Molybdenum-Silicon Alloy (UNS N06219) Plat Sheet, and Strip
B187	Copper, Bus Bar, Rod, and Shapes and General Purpose Rod, Bar, and Shapes	B444 Nickel-Chromium Molybdenum-Columbium Allo (UNS N06625 and UNS N06852) and Nickel- Chromium Molybdenum-Silicon Alloy (UNS N06219) Pipe and Tube
B209	Aluminum and Aluminum-Alloy Sheet and Plate	B446 Nickel-Chromium-Molybdenum-Columbium Allo
B210	Aluminum and Aluminum-Alloy Drawn Seamless Tubes	(UNS N06625), Nickel-Chromium-Molybdenun Silicon Alloy (UNS N06219), and Nickel- Chromium-Molybdenum-Tungsten Alloy (UNS
B211	Aluminum and Aluminum-Alloy Rolled or Cold Finished Bar, Rod, and Wire	N06650) Rod and Bar B462 Forged or Rolled UNS N06030, UNS N06022, UI
B221	Aluminum and Aluminum-Alloy Extruded Bars, Rods, Wire, Profiles, and Tubes	Chromium-Molybdenum-Tungsten Alloy (UNS N06650) Rod and Bar B462 Forged or Rolled UNS N06030, UNS N06022, UI N06035, UNS N06200, UNS N06059, UNS N1036 UNS N06686, UNS N08020, UNS N08024. UN
B241	Aluminum and Aluminum-Alloy Seamless Pipe and Seamless Extruded Tube	N08026, UNS N08367, UNS N10276, UNS N1066 UNS N10675, UNS N10629, UNS N08031, UN
B247 B265	Aluminum and Aluminum-Alloy Die Forgings, Hand Forgings, and Rolled Ring Forgings Titanium and Titanium Alloy Strip, Sheet, and Plate	N06045, UNS N06025, UNS R20033 Alloy Pip Flanges, Forged Fittings, and Valves and Parts t Corrosive High-Temperature Service
B280	Seamless Copper Tube for Air Conditioning and	B463 UNS N08020 Alloy Plate, Sheet, and Strip
DZOO	Refrigeration Field Service	B464 Welded UNS N08020 Alloy Pipe
B283	Copper and Copper-Alloy Die Forgings (Hot-	B466 Seamless Copper-Nickel Pipe and Tube
	Pressed)	B467 Welded Copper-Nickel Pipe
		B474 Electric Fusion Welded Nickel and Nickel Alloy Pi
B333 B335	Nickel-Molybdenum Alloy Plate, Sheet, and Strip Nickel-Molybdenum Alloy Rod	B491 Aluminum and Aluminum-Alloy Extruded Round Tubes for General-Purpose Applications
B345	Aluminum and Aluminum-Alloy Seamless Pipe and Seamless Extruded Tube for Gas and Oil	B493 Zirconium and Zirconium Alloy Forgings
	Transmission and Distribution Piping Systems	B514 Welded Nickel-Iron-Chromium Alloy Pipe
B348	Titanium and Titanium Alloy Bars and Billets	B515 Welded UNS N08120, UNS N08800, UNS N0881
B361	Rectory-Made Wrought Aluminum and Aluminum- Alloy Welding Fittings	and UNS N08811 Alloy Tubes B517 Welded Nickel-Chromium-Iron-Alloy (UNS N0660
B363	Seamless and Welded Unalloyed Titanium and Titanium Alloy Welding Fittings	UNS N06603, UNS N06025, and UNS N06045 Pipe
B366	Factory-Made Wrought Nickel and Nickel Alloy Fittings	B523 Seamless and Welded Zirconium and Zirconium Alloy Tubes
B367	Titanium and Titanium Alloy Castings	B547 Aluminum and Aluminum-Alloy Formed and Ar
B371	Copper-Zinc-Silicon Alloy Rod	Welded Round Tube
B381	Titanium and Titanium Alloy Forgings	B550 Zirconium and Zirconium Alloy Bar and Wire
B407	Nickel-Iron-Chromium Alloy Seamless Pipe and	B551 Zirconium and Zirconium Alloy Strip, Sheet, and Plate
א טדע	Tube	B564 Nickel Alloy Forgings
B408	Nickel-Iron-Chromium Alloy Rod and Bar	B572 UNS N06002, UNS N06230, UNS N12160, and U R30556 Rod

Specification Index for Appendix A (Cont'd)

Spec.	No. Title	Spec.	No.	Title
ASTM	(Cont'd)	ASTM	(Co	ont'd)
B574	Low-Carbon Nickel-Chromium-Molybdenum, Low-	B675		UNS N08367 Welded Pipe
	Carbon Nickel-Molybdenum-Chromium, Low- Carbon Nickel-Molybdenum-Chromium-	B688		Chromium-Nickel-Molybdenum-Iron (UNS N08366 and UNS N08367) Plate, Sheet, and Strip
	Tantalum, Low-Carbon Nickel-Chromium- Molybdenum-Copper, and Low-Carbon Nickel- Chromium-Molybdenum-Tungsten Alloy Rod	B690		Iron-Nickel-Chromium-Molybdenum Alloys (UNS N08366 and UNS N08367) Seamless Pipe and Tube
B575	Low-Carbon Nickel-Chromium-Molybdenum, Low-Carbon Nickel-Chromium-Molybdenum-Copper,	D704		C ₂
	Low-Carbon Nickel-Chromium-Molybdenum- Tantalum, Low-Carbon Nickel-Chromium-	B704		Welded UNS N06625, UNS N06219 and UNS N08825 Alloy Tubes
	Molybdenum-Tungsten, and Low-Carbon Nickel- Molybdenum-Chromium Alloy Plate, Sheet and Strip	B705		Nickel-Alloy (UNS N06625, N06219 and N08825) Welded Pipe
B581	Nickel-Chromium-Iron-Molybdenum-Copper Alloy	B709		Iron-Nickel-Chromium-Molybeenum Alloy (UNS N08028) Plate, Sheet, and Strip
B582	Rod Nickel-Chromium-Iron-Molybdenum-Copper Alloy	B725		Welded Nickel (UNS N02200/UNS N02201) and Nickel Copper Alloy (UNS N04400) Pipe
	Plate, Sheet, and Strip	B729		Seamless UNS N08020, UNS N08026, and UNS
B584	Copper Alloy Sand Castings for General Applications	3,2,		N08024 Nickel Alloy Pipe and Tube
B619	Welded Nickel and Nickel-Cobalt Alloy Pipe	B804		UNS N08367 and UNS N08926 Welded Pipe
B620	Nickel-Iron-Chromium-Molybdenum Alloy (UNS N08320) Plate, Sheet, and Strip	B861 B862		Titanium and Titanium Alloy Seamless Pipe Titanium and Titanium Alloy Welded Pipe
B621	Nickel-Iron-Chromium-Molybdenum Alloy (UNS N08320) Rod		Q.	Ø.
B622	Seamless Nickel and Nickel-Cobalt Alloy Pipe and Tube	E112		Standard Test Methods for Determining Average Grain Size
B625	UNS N08925, UNS N08031, UNS N08932, UNS N08926, UNS N08354, UNS N08830, and UNS R20033 Plate, Sheet, and Strip	F3125		High Strength Structural Bolts, Steel and Alloy Steel, Heat Treated, 120 ksi (830 MPa) and 150 ksi
B626	Welded Nickel and Nickel-Cobalt Alloy Tube			(1040 MPa) Minimum Tensile Strength
B649	Ni-Fe-Cr-Mo-Cu-N Low-Carbon Alloys (UNS N08925, UNS N08031, UNS N08354, and UNS	API		
	N08926), and Cr-Ni-Fe-N Low-Carbon Alloy (UNS R20033) Bar and Wire, and Ni-Gr-Fe-Mo-N Alloy (UNS N08936) Wire	5L		Line Pipe
B658	Seamless and Welded Zirconium and Zirconium Alloy Pipe	CSA Z245.	1	Steel Pipe
B668	UNS N08028 Seamless Pipe and Tube			

B668 UNS N08028 Seamless Pipe and Tube

GENERAL NOTE: It is not practical to refer to a specific edition of each standard throughout the Code text. Instead, the approved edition references, along with the names and addresses of the sponsoring organizations, are shown in Appendix E.

NOTES FOR TABLES A-1, A-1M, A-1A, A-1B, A-2, AND A-2M (18)

GENERAL NOTES:

- (a) The allowable stress values, P-Number assignments, weld joint and casting quality factors, and minimum temperatures in Tables A-1, A-1A, A-1B, A-2, and A-2M, together with the referenced Notes in the stress tables, are requirements of this Code.
- (b) Notes (1) through (7) are referenced in column headings and in body headings for material type and product form; Notes (8) and following are referenced in the Notes column for specific materials. Notes marked with an asterisk (*) restate requirements found in the text of the Code.
- (c) The stress values given in ksi as shown in Tables A-1 and A-2, and given in MPa as shown in Tables A-1M and A-2M, may be used. The values stated in ksi are not exact equivalents to the values stated in MPa. Therefore, for any given material, the user of the Code should use only the ksi or the MPa values.
- (d) For copper and copper alloys, the following symbols are used in the Temper column: H = drawn; H01 = quarter hard; H02 = half hard; H06 = extra hard; H55 = light drawn; H58 = drawn, general purpose; H80 = hard drawn; HR50 = drawn, stress relieved; M20 = hot rolled; O25 = hot rolled, annealed; O50 = light annealed; O60 = soft annealed; O61 = annealed; WO50 = welded, annealed; and WO61 = welded, fully finished, annealed.
- (e) For nickel and nickel alloys, the following abbreviations are used in the Class column: ann., annealed; C.D., cold worked; forg., forged; H.F., hot finished; H.R., hot rolled; H.W., hot worked; plt., plate; R., rolled; rel., relieved; sol., solution; str., stress; and tr., treated.
- (f) In Table A-1M, the following abbreviations are used in the Product Form column: forg., forgings; ftg., fittings; pl., plate; shps., shapes; sht., sheet; smls., seamless; and wld., welded.

NOTES:

- (1) *The stress values in Tables A-1 and A-1M, and the design stress values in Tables A-2 and A-2M, are basic allowable stresses in tension in accordance with para. 302.3.1(a). For pressure design, the stress values from Tables A-1 and A-1M are multiplied by the appropriate quality factor *E* (*E_c* from Table A-1A or *E_j* from Table A-1B). Stress values in shear and bearing are stated in para. 302.3.1(b); those in compression in para. 302.3.1(c).
- (2) *The quality factors for castings E_c in Table A-1A are basic factors in accordance with para. 302.3.3(b). The quality factors for longitudinal weld joints E_j in Table A-1B are basic factors in accordance with para. 302.3.4(a). See paras. 302.3.3(c) and 302.3.4(b) for enhancement of quality factors. See also para. 302.3.1(a), footnote 1.
- (3) The stress values for austenitic stainless steels in these Tables may not be applicable if the material has been given a final heat treatment other than that required by

- the material specification or by reference to Note (30) or (31).
- (4a) *In Table A-1, stress values printed in *italics* exceed two-thirds of the expected yield strength at temperature. Stress values in **boldface** are equal to 90% of expected yield strength at temperature. See paras. 302.3.2(d)(3) and (e).
- (4b) *In Table A-1M, stress values printed in italics are tensilecontrolled values. Yield-controlled stress values are in normal font and time-dependent stress values are in **bold-face**.
- (5) *See ASME BPVC, Section IX, QW-200.3 for a description of P-Number groupings. P-Numbers are indicated by number or by a number followed by a letter (e.g., 8, 5B, or 11A).
- (6) *The minimum temperature shown is that design minimum temperature for which the material is normally suitable without impact testing other than that required by the material specification. However, the use of a material at a design minimum temperature colder than -29°C (-20°F) is established by fules elsewhere in this Code, including para. 323.2.2 and other impact test requirements. For carbon steels with a letter designation in the Min. Temp. column, see para. 323.2.2(e) and the applicable curve and Notes in Figure 323.2.2A.
- The letter "a" indicates alloys that are not recommended for welding and that, if welded, must be individually qualified.

 The letter "b" indicates copper base alloys that must be individually qualified.
- (8) *There are restrictions on the use of this material in the text of the Code as follows:
- (a) See para. 305.2.1; temperature limits are -29°C to 186°C (-20°F to 366°F).
- (b) See para. 305.2.2; pipe shall be safeguarded when used outside the temperature limits in Note (8a).
 - (c) See Table 323.2.2, box B-2.
 - (d) See para. 323.4.2(a).
 - (e) See para. 323.4.2(b).
 - (f) See para. 309.2.1.
 - (g) See para. 309.2.2.
- (9) *For pressure-temperature ratings of components made in accordance with standards listed in Table 326.1, see para. 326.2.1. Stress values in Tables A-1 and A-1M may be used to calculate ratings for unlisted components, and special ratings for listed components, as permitted by para. 303.
- (9a) Component standards listed in Table 326.1 impose the following restrictions on this material when used as a forging: composition, properties, heat treatment, and grain size shall conform to this specification; manufacturing procedures, tolerances, tests, certification, and markings shall be in accordance with ASTM B564.

- (10) *This casting quality factor is applicable only when proper supplementary examination has been performed (see para. 302.3.3).
- (11) *For use under this Code, radiography shall be performed after heat treatment.
- (12) *Certain forms of this material, as stated in Table 323.2.2, must be impact tested to qualify for service below -29°C (-20°F). Alternatively, if provisions for impact testing are included in the material specification as supplementary requirements and are invoked, the material may be used down to the temperature at which the test was conducted in accordance with the specification.
- (13) Properties of this material vary with thickness or size. Stress values are based on minimum properties for the thickness listed.
- (14) For use in Code piping at the stated stress values, the required minimum tensile and yield properties must be verified by tensile test. If such tests are not required by the material specification, they shall be specified in the purchase order.
- (15) These stress values are established from a consideration of strength only and will be satisfactory for average service. For bolted joints where freedom from leakage over a long period of time without retightening is required, lower stress values may be necessary as determined from the flexibility of the flange and bolts and corresponding relaxation properties.
- (16) DELETED.
- (17) DELETED.
- (18) DELETED.
- (19) *This specification includes requirements for random radiographic inspection for mill quality control. If the 0.90 joint factor is to be used, the welds shall meet the requirements of Table 341.3.2 for longitudinal butt welds with spot radiography in accordance with Table 302.3.4. This shall be a matter of special agreement between purchaser and manufacturer.
- (20) For pipe sizes ≥DN 200 (NPS 8) with wall thicknesses ≥Sch 140, the specified minimum tensile strength is 483 MPa (70 ksi).
- (21) For material thickness >127 mm (5 in.), the specified minimum tensile strength is 483 MPa (70 ksi).
- (21a) For material thickness 127 mm (5 in.), the specified minimum tensile strength is 448 MPa (65 ksi).
- (22) The minimum tensile strength for weld (qualification) and stress values shown shall be multiplied by 0.90 for pipe having an outside diameter less than 51 mm (2 in.) and a *D/t* value less than 15. This requirement may be waived if it can be shown that the welding procedure to be used will consistently produce welds that meet the listed minimum tensile strength of 165 MPa (24 ksi).
- (23) DELETED.
- (24) Yield strength is not stated in the material specification.

 The value shown is based on yield strengths of materials with similar characteristics.
- (25) This steel may develop embrittlement after service at approximately 316°C (600°F) and higher temperature.
- (26) This unstabilized grade of stainless steel increasingly tends to precipitate intergranular carbides as the carbon content increases above 0.03%. See also para. F323.4(c)(2).

- (27) For temperatures above 427°C (800°F), these stress values apply only when the carbon content is 0.04% or higher.
- (28) For temperatures above 538°C (1,000°F), these stress values apply only when the carbon content is 0.04% or higher.
- (29) The stress values above 538°C (1,000°F) listed here shall be used only when the steel's austenitic micrograin size, as defined in ASTM E112, is No. 6 or less (coarser grain). Otherwise, the lower stress values listed for the same material, specification, and grade shall be used.
- (30) For temperatures above 538°C (1,000°F), these stress values may be used only if the material has been heat treated by heating to a minimum temperature of 1093°C (2,000°F) and quenching in water or rapidly cooling by other means.
- (31) For temperatures above 538°C (1,000°F), these stress values may be used only if the material has been heat treated by heating to a minimum temperature of 1038°C (1,900°F) and quenching in water or rapidly cooling by other means.
- (32) Stress values shown are for the lowest strength base material permitted by the specification to be used in the manufacture of this grade of fitting. If a higher strength base material is used, the higher stress values for that material may be used in design.
- (33) For welded construction with work hardened grades, use the stress values for annealed material; for welded construction with precipitation hardened grades, use the special stress values for welded construction given in the Tables.
- (34) If material is welded, brazed, or soldered, the allowable stress values for the annealed condition shall be used.
- (35) This steel is intended for use at high temperatures; it may have low ductility and/or low impact properties at room temperature after being used above the temperature indicated by para. F323.4(c)(4).
- (36) The specification permits this material to be furnished without solution heat treatment or with other than a solution heat treatment. When the material has not been solution heat treated, the minimum temperature shall be -29°C (-20°F) unless the material is impact tested in accordance with para. 323.3.
- (37) Impact requirements for seamless fittings shall be governed by those listed in this Table for the particular base material specification in the grades permitted (A312, A240, and A182). When A276 materials are used in the manufacture of these fittings, the Notes, minimum temperatures, and allowable stresses for comparable grades of A240 materials shall apply.
- (38) DELETED.
- (39) This material when used below −29°C (−20°F) shall be impact tested if the carbon content is above 0.10%.
- (40) *This casting quality factor can be enhanced by supplementary examination in accordance with para. 302.3.3(c) and Table 302.3.3C. The higher factor from Table 302.3.3C may be substituted for this factor in pressure design equations.
- (41) Design stresses for the cold drawn temper are based on hot rolled properties until required data on cold drawn are submitted.
- (42) This is a product specification. No design stresses are necessary. Limitations on metal temperature for materials covered by this specification are as follows:

Grade(s)	Metal Temperature, °C (°F)
1	-29 to 482 (-20 to 900)
2, 2H, and 2HM	-48 to 593 (-55 to 1,100)
3	-29 to 593 (-20 to 1,100)
4	-48 to 593 (-55 to 1,100)
4L	-101 to 593 (-150 to 1,100)
6	-29 to 427 (-20 to 800)
7	-48 to 593 (-55 to 1,100)
7L	-101 to 593 (-150 to 1,100)
7M	-48 to 593 (-55 to 1,100)
7ML	-73 to 593 (-100 to 1,100)
8FA [see Note (39)]	-29 to 427 (-20 to 800)
8MA and 8TA	-198 to 816 (-325 to 1,500)
8, 8A, and 8CA	-254 to 816 (-425 to 1,500)

- (42a) DELETED.
- (42b) This is a product specification. No design stresses are necessary. For limitations on usage, see paras. 309.2.1 and 309.2.2.
- (43) *The stress values given for this material are not applicable when either welding or thermal cutting is employed [see para. 323.4.2(c)].
- (44) This material shall not be welded.
- (45) Stress values shown are applicable for "die" forgings only.
- (46) Lines of allowable stresses in Tables A-1 and A-1M for all materials in A312 include heavily cold worked (HCW) material as defined in A312, para. 6.1.4.
- (47) If no welding is employed in fabrication of piping from these materials, the stress values may be increased to 230 MPa (33.3 ksi).
- (48) The stress value to be used for this gray iron material at its upper temperature limit of 232°C (450°F) is the same as that shown in the 204°C (400°F) column.
- (49) If the chemical composition of this Grade is such as to render it hardenable, qualification under P-No. 6 is required.
- (50) This material is grouped in P-No 7 because its hardenability is low.(51) This material may require special consideration for
- (51) This material may require special consideration for welding qualification. See ASME BPVC, Section IX, QW/QB-422. For use in this Code, a qualified WPS is required for each strength level of material.
- (52) Copper-silicon alloys are not always suitable when exposed to certain media and high temperature, particularly above 100°C (212°F). The user should satisfy himself/herself that the alloy selected is satisfactory for the service for which it is to be used.
- (53) Stress relief heat treatment is required for service above 232°C (450°F).
- (54) The maximum operating temperature is arbitrarily set at 260°C (500°F) because hard temper adversely affects design stress in the creep rupture temperature ranges.
- (55) Pipe produced to this specification is not intended for high temperature service. The stress values apply to either nonexpanded or cold expanded material in the asrolled, normalized, or normalized and tempered condition.
- (56) Because of thermal instability, this material is not recommended for service above 427°C (800° F).

- (57) Conversion of carbides to graphite may occur after prolonged exposure to temperatures over 427°C (800°F). See para. F323.4(b)(2).
- (58) Conversion of carbides to graphite may occur after prolonged exposure to temperatures over 468°C (875°F). See para. F323.4(b)(3).
- (59) For temperatures above 482°C (900°F), consider the advantages of killed steel. See para. F323.4(b)(4).
- (60) For all design temperatures, the maximum hardness shall be Rockwell C35 immediately under the thread roots. The hardness shall be taken on a flat area at least 3 mm ($\frac{1}{8}$ in.) across, prepared by removing threads. No more material than necessary shall be removed to prepare the area. Hardness determination shall be made at the same frequency as tensile tests.
- (61) Annealed at approximately 982°C (1,800°F).
- (62) Annealed at approximately 1121°C (2,050°F).
- (63) For stress relieved tempers (7351, T3510, T3511, T451, T4510, T4511, T651, T6510, T6511), stress values for material in the listed temper shall be used.
- (64) The minimum tensile strength of the reduced section tensile specimen in accordance with ASME BPVC, Section IX, QW-462.1, shall not be less than 758 MPa (110.0 ks).
- (65) The minimum temperature shown in Tables A-1 and A-1M is for the heaviest wall meeting the specified mechanical property requirements in the specification. The minimum temperature for lighter walls shall be as shown in the following tabulation:

Impact Test Temperature (°C) for Plate Thicknesses Shown

Spec. No. and Grade	Max. 51 mm	Over 51 mm to 76 mm
A203 A	-68	-59
A203 B	-68	-59
A203 D	-101	-87
A203 E	-101	-87

Impact Test Temperature (°F) for Plate Thicknesses Shown

Spec. No. and Grade	Max. 2 in.	Over 2 in. to 3 in.
A203 A	-90	-75
A203 B	-90	-75
A203 D	-150	-125
A203 E	-150	-125

- (66) Stress values shown are 90% of those for the corresponding core material.
- (67) For use under this Code, the heat treatment requirements for pipe manufactured to A671, A672, and A691 shall be as required by para. 331 for the particular material being used.
- (68) The tension test specimen from plate 12.7 mm ($\frac{1}{2}$ in.) and thicker is machined from the core and does not include the cladding alloy; therefore, the stress values listed are those for materials less than 12.7 mm.
- (69) This material may be used only in nonpressure applications.

- (70) Alloy 625 (UNS N06625) in the annealed condition is subject to severe loss of impact strength at room temperature after exposure in the range of 538° C to 760° C (1,000°F to 1,400°F).
- (71) These materials are normally microalloyed with Cb, V, and/or Ti. Supplemental specifications agreed to by manufacturer and purchaser commonly establish chemistry more restrictive than the base specification, as well as plate rolling specifications and requirements for weldability (i.e., C-equivalent) and toughness.
- (72) For service temperature >454°C (850°F), weld metal shall have a carbon content >0.05%.
- (73) Heat treatment is required after welding for all products of zirconium Grade R60705. See Table 331.1.1.
- (74) Mechanical properties of fittings made from forging stock shall meet the minimum tensile requirements of one of the bar, forging, or rod specifications listed in Table 2 of B366 for which tensile testing is required.
- (75) Stress values shown are for materials in the normalized and tempered condition, or when the heat treatment is unknown. If material is annealed, use the following values above 510°C (950°F):

Temp., °C	538	566	593	621	649
S, MPa	55.1	39.3	26.2	16.5	9.6

Temp., °F	1,000	1,050	1,100	1,150	1,200
S, ksi	8.0	5.7	3.8	2.4	1.4

- (76) DELETED.
- (77) The pipe grades listed below, produced in accordance with CSA (Canadian Standards Association) Z245.1, shall be considered as equivalents to API 5L and treated as listed materials.

Grade	Fauiva	lents

urauc	Lyurvaiciics
API 5L	CSA Z24 5.1
В	241
X42	290
X46	317
X52	359
X56	386
X60	414
X65	448
X70	483
X80	550
(

- (78) Not permitted for the P4 and P5 materials in Table 302.3.5 for Elevated Temperature Fluid Service.
- (79) For use under this Code, impact testing shall be performed in accordance with para. 323.3 at the design minimum temperature but not warmer than -29°C (-20°F).

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Table A-1 Basic Allowable Stresses in Tension for Metals

				-	-		Specifie Strengt			Allowa					
Material	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100		300	400	500	600	650
Iron — Cast	ings														
Gray	A48	20	F11401		(8e)(48)	-20	20		2.0	2.0	2.0	2.0			
Gray	A278	20	F11401		(8e)(48)	-20	20		2.0	2.0	2.0	2.0			
Gray	A126	A	F11501		(8e)(9)(48)	-20	21		2.0	2.0	2.0	2.0	%		
Gray	A48	25	F11701		(8e)(48)	-20	25		2.5	2.5	2.5	2.5			
Gray	A278	25	F11701		(8e)(48)	-20	25		2.5	2.5	2,5	2.5			
Gray	A48	30	F12101		(8e)(48)	-20	30		3.0	3.0	3.0	3.0			
Gray	A278	30	F12101		(8e)(48)	-20	30		3.0	3.0	3.0	3.0			
Gray	A126	В	F12102	•••	(8e)(9)(48)	-20	31	۵	3.0	3.0	3.0	3.0			
Gray	A48	35	F12401		(8e)(48)	-20	35	o' i	3.5	3.5	3.5	3.5			
Gray	A278	35	F12401		(8e)(48)	-20	35		3.5	3.5	3.5	3.5			
Gray	A48	40	F12801		(8e)(9)(48)	-20	40		4.0	4.0	4.0	4.0			
Gray	A126	С	F12802		(8e)(9)(48)	-20	41		4.0	4.0	4.0	4.0			
Gray	A278	40	F12803		(8e)(9)(53)	1 ©20	40		4.0	4.0	4.0	4.0	4.0	4.0	4.0
Gray	A48	45	F13101		(8e)(48)	-20	45		4.5	4.5	4.5	4.5			
Gray	A48	50	F13501		(8e)(48)	-20	50		5.0	5.0	5.0	5.0			
Gray	A278	50	F13502		(8e)(53)	-20	50		5.0	5.0	5.0	5.0	5.0	5.0	5.0
Gray	A48	55	F13801	*V.:	(8e)(48)	-20	55		5.5	5.5	5.5	5.5			
Gray	A48	60	F14101) _{[2}	(8e)(48)	-20	60		6.0	6.0	6.0	6.0			
Gray	A278	60	F14102		(8e)(53)	-20	60		6.0	6.0	6.0	6.0	6.0	6.0	6.0
Cupola malleable	A197	- NAC	F22000		(8e)(9)	-20	40	30	8.0	8.0	8.0	8.0	8.0	8.0	8.0
Malleable	A47	32510	F22200		(8e)(9)	-20	50	32.5	10.0	10.0	10.0	10.0	10.0	10.0	10.0
Ferritic ductile	A395	60-40-18	F32800		(8d)(9)	-20	60	40	20.0	19.0	17.9	16.9	15.9	14.9	14.1
Austenitic ductile	A571	D-2M	F43010	1	(8d)	-20	65	30	20.0						
Ductile	A536	65-45-12	F33100		(8d)(9)	-20	65	45	21.7	21.7	21.7	21.7	21.6		

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(18)

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Numbe	ers in Pa	arentheses	Refer to N	lotes for App	endix A Ta	bies; Sj	pecifications Ar	e asim (Speci Min Strengt	fied 1.	Basic Stres at Temp		ksi, l ıre,
				Class/				Min.			Min.		
Material	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Size, in.	P-No. (5)	Notes	Temp., °F (6)	Tensile	Vield	Temp.	200	300
Carbon Steel				remper	****	(0)	Notes	1 (0)	Tenone	Ticiu	10 100		500
A285 Gr. A	A134					1	(8b)(57)	В	45	24	15.0	14.7	14.2
A285 Gr. A		A45	 К01700			1	(57)(59)(67)	В	45	24	15.0	14.7	
						_	(0.)(0.)	_			3		
Butt weld	API 5L	A25				1	(8a)(77)	-20	45	25	15.0	15.0	14.7
Smls & ERW	API 5L	A25				1	(57)(59)(77)	В	45	25 ³	15.0	15.0	14.7
									~<	, `			
	A179		K01200			1	(57)(59)	-20	47	26	15.7	15.7	15.3
								. 5					
Type F	A53	A	K02504			1	(8a)	20	48	30	16.0	16.0	
	A139	A				1	(8b)	A	48	30	16.0	16.0	
	A587		K11500			1	(57)(59)	-20	48	30	16.0	16.0	16.0
	450		1702504			1	(57)(50)	D	40	20	160	160	160
	A53 A106	A A	K02504 K02501			1	(57)(59)	В	48 48	30	16.0 16.0	16.0 16.0	
	A106	A				1 1	(57)	B B	48	30 30	16.0	16.0	
	A369	FPA	 K02501			1.	(6X)(59) (57)	В	48	30	16.0	16.0	
	API 5L					. 61	(57)(59)	В	48	30	16.0	16.0	
	AII JL	А				110	(37)(39)	ь	40	30	10.0	10.0	10.0
A285 Gr. B	A134				×O	1	(8b)(57)	В	50	27	16.7	16.5	15.9
A285 Gr. B	A672	A50	K02200		- Ch	1	(57)(59)(67)	В	50	27	16.7	16.5	
				Ċ	110								
A285 Gr. C	A134					1	(8b)(57)	Α	55	30	18.3	18.3	17.7
	A524	II	K02104			1	(57)	-20	55	30	18.3	18.3	17.7
	A333	1	K03008	Ο'		1	(57)(59)	-50	55	30	18.3	18.3	17.7
	A334	1	K03008	<u></u>		1	(57)(59)	-50	55	30	18.3	18.3	17.7
A285 Gr. C	A671	CA55	K02801			1	(59)(67)	Α	55	30	18.3	18.3	17.7
A285 Gr. C	A672	A55	K02801			1	(57)(59)(67)	Α	55	30	18.3	18.3	17.7
A516 Gr. 55	A672	C55	K01800			1	(57)(67)	С	55	30	18.3	18.3	17.7
		.0%											
A516 Gr. 60	A671	CC60	K02100			1	(57)(67)	C	60	32	20.0	19.5	18.9
A515 Gr. 60	A671	CB60	K02401			1	(57)(67)	В	60	32	20.0	19.5	18.9
A515 Gr. 60	A672	B60	K02401			1	(57)(67)	В	60	32	20.0	19.5	18.9
A516 Gr. 60	A672	C60	K02100			1	(57)(67)	С	60	32	20.0	19.5	18.9
	•												
	A139	В	K03003			1	(8b)	A	60	35	20.0	20.0	20.0
		_	*****				(==) (==)	_		0.5	20.0	00 -	000
	A135		K03018			1	(57)(59)	В	60	35	20.0	20.0	
	A524	I	K02104			1	(57)	-20	60	35	20.0	20.0	20.0
	450	D	VO2CCE			4	(=7)(=0)		60	25	20.0	20.0	20.0
	A53	В	K03005			1	(57)(59)	В	60	35	20.0	20.0	
	A106	В	K03006			1	(57)	В	60	35	20.0	20.0	
•••	A333	6	K03006			1	(57)	-50	60	35	20.0	20.0	
•••	A334	6	K03006			1	(57)	-50	60	35	20.0	20.0	20.0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	Type/ Grade	Spec. No.
	300	000	030	700	730	000	030	700	750	1,000	-	•		and Tubes
13.7	13.0	12.3	11.9	11.5	10.7	9.2	7.9	5.9					1/0	A134
13.7	13.0	12.3	11.9	11.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	A45	A672
													b	
14.2												0	A25	API 5L
14.2	•••										<	$S_{\mathcal{D}}$	A25	API 5L
											~	•		
14.8	14.1	13.3	12.8	12.4	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0		A179
										D	9			
16.0										£ 1			A	A53
									<				Α	A139
16.0	16.0	15.3	14.6	12.5	10.7	9.2	7.9		~O					A587
									(4.					
16.0	16.0	15.3	14.6	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	A	A53
16.0	16.0	15.3	14.6	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	A	A106
16.0	16.0	15.3	14.6	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	Α	A135
16.0	16.0	15.3	14.6	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	FPA	A369
16.0	16.0	15.3	14.6	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	A	API 5L
						9.2)							
15.4	14.7	13.8	13.3	12.5	10.7		7.9	5.9						A134
15.4	14.7	13.8	13.3	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	A50	A672
454	460	450	440	440		100	0.7							
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9			•••			A134
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5			II	A524
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5	1.6	1.0	1	A333
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5	1.6	1.0	1	A334
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5	1.6	1.0	CA55	A671
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5	1.6	1.0	A55	A672
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5	1.6	1.0	C55	A672
102	17.4	_\Q'	15.8	15.2	13.9	11.4	8.7	5.9	4.0	2 5			CCGO	A 6 7 1
18.2 18.2	17.4	16.4 16.4	15.8	15.3 15.3	13.9	11.4	8.7	5.9	4.0	2.5 2.5	 1.6	1.0	CC60 CB60	A671 A671
18.2	17.4	16.4	15.8	15.3	13.9	11.4	8.7	5.9	4.0 4.0	2.5	1.6	1.0	В60	A671 A672
18.2	17.4		15.8	15.3	13.9		8.7	5.9		2.5				A672 A672
10.2	77.4	16.4	13.0	13.3	13.7	11.4	0.7	3.9	4.0	2.3	1.6	1.0	C60	A072
													В	A139
		•••	•••	•••		•••	•••	•••					Ь	HI37
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5			В	A135
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5			I	A524
17.7	17.0	11.7	17.5	10.7	10.7	11.7	0.7	5.7	1.0	2.3		•••	•	11021
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	В	A53
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	В	A106
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	6	A333
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	6	A334
17.7	17.0	11.7	17.0	10.7	10.7	11.1	0.7	5.7	1.0	2.0	1.0	1.0	5	11001

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Number		ar entireses	Neier to A	oces for hyp	ciuix ii Tu	bies, o _l	pecifications Ar	e norm e	Speci Mir Strengt	fied 1.	Basic Stres at Temp	Allow s, <i>S</i> , l Meta	ksi, l ure,
	_			Class/				Min.			Min.		
Material	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Size, in.	P-No. (5)	Notes	Temp., °F (6)	Tensile	Vield	Temp.	200	300
Carbon Steel				Temper	****	(0)	Hotes	1 (0)	Tenone	Ticia	10 100		
car bon seeci	A369	FPB	K03006			1	(57)	-20	60	35	20.0	20.0	20.0
	A381	Y35				1		A	60	35	20.0	20.0	
	API 5L					1	 (57)(59)(77)	В	60	35	20.0	20.0	
	02	2	•••			-	(0.)(0.)()	2	00	0	\ ·	20.0	_0.0
	A139	С	K03004			1	(8b)	Α	60	420	20.0	20.0	20.0
	A139	D	K03010			1	(8b)	Α	60	46	20.0	20.0	
	API 5L	X42				1	(55)(77)	Α	60	42	20.0	20.0	20.0
	A381	Y42				1		A	60	42	20.0	20.0	20.0
								~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~					
	A381	Y48				1		A	62	48	20.7	20.7	20.7
)`					
	API 5L	X46		•••		1	(55)(77)	A	63	46	21.0	21.0	21.0
	A381	Y46				1	KIII.	A	63	46	21.0	21.0	21.0
	A 201	VEO				1	ine	Λ.	6.1	E0	21.2	21.2	21.2
	A381	Y50				1	101	A	64	50	21.3	21.3	21.3
A516 Gr. 65	A671	CC65	K02403			(A)	(57)(67)	В	65	35	21.7	21.4	20.6
A515 Gr. 65	A671	CB65	K02800			1,1	(57)(67)	A	65	35	21.7	21.4	20.6
A515 Gr. 65	A672	B65	K02800		, XO	1	(57)(67)	A	65	35	21.7	21.4	20.6
A516 Gr. 65	A672	C65	K02403		"CX	1	(57)(67)	В	65	35	21.7	21.4	20.6
	A139	E	K03012) <u>,</u>	1	(8b)	Α	66	52	22.0	22.0	22.0
	API 5L	X52				1	(55)(77)	Α	66	52	22.0	22.0	22.0
	A381	Y52		~O/2		1		Α	66	52	22.0	22.0	22.0
A516 Gr. 70	A671	CC70	K02700	$\mathcal{O}_{\mathbf{c}}$		1	(57)(67)	В	70	38	23.3	23.2	22.4
A515 Gr. 70	A671	CB70	K03101		•••	1	(57)(67)	A	70	38	23.3	23.2	
A515 Gr. 70	A672	B70	K03101			1	(57)(67)	A	70	38	23.3	23.2	
A516 Gr. 70		•	K02700			1	(57)(67)	В	70	38	23.3	23.2	
							(-)(-)						
	A106		K03501	•••		1	(57)	В	70	40	23.3	23.3	
A537 Cl. 1	A671		K12437	•••	$\leq 2^{1}/_{2}$ thk.	1	(67)	D	70	50	23.3	23.3	
A537 Cl. 1	A672		K12437		$\leq 2^{1}/_{2}$ thk.	1	(67)	D	70	50	23.3	23.3	
A537 Cl. 1	A691	CMSH-70	K12437	•••	$\leq 2^{1}/_{2}$ thk.	1	(67)	D	70	50	23.3	23.3	22.8
	API 5L	X56				1	(51)(55)(71) (77)	A	71	56	23.7	23.7	23.7
	A381	Y56				1	(51)(55)(71)	A	71	56	23.7	23.7	23.7
A299 Gr. A	A671	CK75	K02803		>1 thk.	1	(57)(67)	A	75	40	25.0	24.4	23.6
A299 Gr. A	A672	N75	K02803		>1 thk.	1	(57)(67)	A	75	40	25.0	24.4	23.6
A299 Gr. A	A691	CMS-75	K02803		>1 thk.	1	(57)(67)	A	75	40	25.0	24.4	
A299 Gr. A	A671	CK75	K02803		≤1 thk.	1	(57)(67)	A	75	42	25.0	25.0	24.8

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	Type/ Grade	Spec. No.
							000	700	700		n Steel			es (Cont'd)
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	FPB	A369
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	Y35	A381
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	В	API 5L
												0		
											, <	S	С	A139
													D	A139
20.0											Al.		X42	API 5L
20.0										🔈	.		Y42	A381
										9,				
20.7	20.7	20.7	18.7						<				Y48	A381
21.0								🐧	X				X46	API 5L
21.0								ري					Y46	A381
21.3	21.3	21.3	18.7				, 9	(L)					Y50	A381
							N							
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0	6.3	4.0	2.5			CC65	A671
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0	6.3	4.0	2.5	1.6	1.0	CB65	A671
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0	6.3	4.0	2.5	1.6	1.0	B65	A672
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0	6.3	4.0	2.5	1.6	1.0	C65	A672
													E	A139
22.0					V								X52	API 5L
22.0				C	12.								Y52	A381
				\mathcal{C}										
21.6	20.6	19.4	18.8	18.1	14.8	12.0	9.3	6.7	4.0	2.5			CC70	A671
21.6	20.6	19.4	18.8	18.1	14.8	12.0	9.3	6.7	4.0	2.5	1.6	1.0	CB70	A671
21.6	20.6	19.4	18.8	18.1	14.8	12.0	9.3	6.7	4.0	2.5	1.6	1.0	B70	A672
21.6	20.6	19.4	18.8	18.1	14.8	12.0	9.3	6.7	4.0	2.5	1.6	1.0	C70	A672
22.8	21.7	20.4	19.8	18.3	14.8	12.0							С	A106
22.7	22.7	22.4	21.9	18.3									CD70	A671
22.7	22.7	22.4	21.9	18.3									D70	A672
22.7	22.7	22.4	21.9	18.3									CMSH-70	A691
22.7	Y 22.7	22.1	21.7	10.5	•••		•••			•••		•••	GMSH 70	71071
23.7													X56	API 5L
23.7													Y56	A381
22.8	21.7	20.4	19.8	19.1	15.7	12.6	9.3	6.7	4.0	2.5	1.6	1.0	CK75	A671
22.8	21.7	20.4	19.8	19.1	15.7	12.6	9.3	6.7	4.0	2.5	1.6	1.0	N75	A672
22.8	21.7	20.4	19.8	19.1	15.7	12.6	9.3	6.7	4.0	2.5	1.6	1.0	CMS-75	A691
23.9	22.8	21.5	20.8	19.6									CK75	A671

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

									-	Speci Mir Strengt	1.	at Temp	s, <i>S</i> , l Meta	ksi, l ure,
Material	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper		Size, in.	P-No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300
Carbon Steel	— Pipe	es and Tub	es										0	
A299 Gr. A	A672	N75	K02803		≤1	thk.	1	(57)(67)	A	75	42	25.0	25.0	24.8
A299 Gr. A	A691	CMS-75	K02803		≤1	thk.	1	(57)(67)	A	75	42	25.0	25.0	24.8
	API 5L	X60					1	(51)(55)(71) (77)	A	75	60%	25.0	25.0	25.0
	API 5L	X65					1	(51)(55)(71) (77)	A	77	65	25.7	25.7	25.7
	API 5L	X70					1	(51)(55)(71) (77)	Į.	82	70	27.3	27.3	27.3
	API 5L	X80					1	(51)(55)(71) (77)	≪ ^{OA}	90	80	30.0	30.0	30.0
	A381	Y60					1	(51)(71)	A	75	60	25.0	25.0	25.0
Carbon Steel	— Pipe	es (Structu	ral Grade)					60						
A283 Gr. A	A134						1	(8a)(8c)	-20	45	24	15.0	14.7	14.2
A1011 Gr. 30	A134						jien	(8a)(8c)	-20	49	30	16.3	16.3	16.3
A283 Gr. B	A134					:X-,C	1	(8a)(8c)	-20	50	27	16.7	16.5	15.9
A1011 Gr. 33	A134					.	1	(8a)(8c)	-20	52	33	17.3	17.3	17.3
A1011 Gr. 36	A134			ON.			1	(8a)(8c)	-20	53	36	17.7	17.7	17.7
A1011 Gr. 40	A134		··· رن				1	(8a)(8c)	-20	55	40	18.3	18.3	18.3
A36	A134		NDC				1	(8a)(8c)	-20	58	36	19.3	19.3	19.3
A283 Gr. D	A134						1	(8a)(8c)	-20	60	33	20.0	20.0	19.5
A1011 Gr. 45		CHO!					1	(8a)(8c)	-20	60	45	20.0	20.0	20.0
A1011 Gr. 50	A134						1	(8a)(8c)	-20	65	50	21.7	21.7	21.7
Carbon Steel	V Plat	es, Bars. S	hapes, and	Sheets										
	A285		K01700				1	(57)(59)	В	45	24	15.0	14.7	14.2
	A285	В	K02200				1	(57)(59)	В	50	27	16.7	16.5	15.9
	A516	55	K01800				1	(57)	С	55	30	18.3	18.3	17.7
	A285		K02801				1	(57)(59)	A	55	30	18.3	18.3	
	A516	60	K02100				1	(57)	С	60	32	20.0	19.5	18.9

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

													Type/	
400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100		Spec. No.
										Carb	on Steel	— Pipe	. 7	es (Cont'd)
23.9	22.8	21.5	20.8	19.6									N75	A672
23.9	22.8	21.5	20.8	19.6		***							CMS-75	A691
25.0												_ට ි `	X60	API 5L
25.7											NE		X65	API 5L
27.3										« P	9		X70	API 5L
30.0					•••	•••	•••		\ \	(O'		•••	X80	API 5L
25.0								10 (1)					Y60	A381
								61)	Car	bon Stee	l — Pip	es (Structi	ıral Grade)
13.7							Wo.	He						A134
16.3							lien							A134
						- 'Y-'								A134
17.3					C									A134
17.7				 C	<i>M</i>									A134
18.3														A134
19.3			MDC											A134
														A134
20.0		No												A134
21.7	SM													A134
	T								Car	rbon Ste	el — Pla	tes. Bai	rs. Shanes.	and Sheets
13.7	13.0	12.3	11.9	11.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0		A285
						<u>-</u>		~	***					
15.4	14.7	13.8	13.3	12.5	10.7	9.2	7.9	5.9	4.0	2.5	1.6	1.0	В	A285
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7						55	A516
17.1	16.3	15.3	14.8	14.3	13.0	10.8	8.7	5.9	4.0	2.5	1.6	1.0	С	A285
18.2	17.4	16.4	15.8	15.3	13.9	11.4	8.7						60	A516

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

									Speci Mir Strengt	n.	at Temj	Allow ss, S, I Meta perati lote (ksi, l ure,
Material	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300
Carbon Steel	— Plat	es, Bars, S	hapes, and	Sheets								0	
	A515	60	K02401			1	(57)	В	60	32	20.0	19.5	18.9
	A696	В	K03200			1	(57)	Α	60	35	20.0	20.0	20.0
											3°		
	A516	65	K02403			1	(57)	В	65	350	21.7	21.4	20.6
	A515	65	K02800			1	(57)	A	65	35)	21.7	21.4	20.6
									N				
	A516	70	K02700			1	(57)	В	C70	38	23.3	23.2	22.4
	A515	70	K03101			1	(57)	A	70	38	23.3	23.2	22.4
	A696	С	K03200			1	(57)	A	70	40	23.3	23.3	23.3
	A537		K12437	1	$\leq 2^{1}/_{2}$ thk.	1		D	70	50	23.3	23.3	22.8
)`					
	A299	A	K02803		>1 thk.	1	(57)	A	75	40	25.0	24.4	23.6
	A299	A	K02803		≤1 thk.	1	(57)	A	75	42	25.0	25.0	24.8
							e`						
Carbon Steel	— Plat	es, Bars, S	hapes, and	Sheets (Stru	ctural)		KL,						
	A283	Α	K01400			. N	(8c)(57)	Α	45	24	15.0	14.7	14.2
					•	ile							
	A1011	30	K02502		xO	1	(8c)(57)	Α	49	30	16.3	16.3	16.3
	A283	В	K01702			1	(8c)(57)	A	50	27	16.7	16.5	15.9
	A1011	33	K02502		ijo.	1	(8c)(57)	A	52	33	17.3	17.3	17.3
) `								
	A1011	36	K02502	V.		1	(8c)(57)	A	53	36	17.7	17.7	17.7
				~O/									
	A283	С	K02401	\bigcirc		1	(8c)(57)	A	55	30	18.3	18.3	
	A1011	40	K02502			1	(8c)(57)	A	55	40	18.3	18.3	18.3
			.00										
	A36		K02600			1	(8c)	A	58	36	19.3	19.3	19.3
		- 8	.										
	A283		K02702			1	(8c)(57)	A	60	33	20.0	20.0	
	A1011	45	K02507			1	(8c)(57)	A	60	45	20.0	20.0	20.0
			*******				(0.)(555)			=0	04.5	04.5	04.5
	A1011		K02507		•••	1	(8c)(57)	A	65	50	21.7	21.7	
	A992				•••	1	(8c)(57)	A	65	50	19.9	19.9	19.9
Combon Stool	For	aluan aud l	Cittings.										
Carbon Steel	— For	_	_			1	(0)(57)(50)	-20	60	30	20.0	102	177
			K03009			1	(9)(57)(59)					18.3	
	A181		K03502	60		1	(9)(57)(59)	A	60	30	20.0	18.3	1/./
	A420	WPL6	K03006			1	(57)	-50	60	35	20.0	20.0	20.0
	A420 A234	WPL6	K03006			1	(57) (57)(59)	-50 B	60	35	20.0	20.0	
***	A434	AAID	702000			1	(37)(39)	Д	00	33	20.0	20.0	20.0
	A694	F42	K03014			1	(9)	-20	60	42	20.0	20.0	20.0
	11071		.100011		•••	1	(-)	20			_0.0	20.0	_0.0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

-														
													Type/	
400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100		Spec. No.
											es, Bars,	Shapes	s, and Shee	ts (Cont'd)
18.2	17.4	16.4	15.8	15.3	13.9	11.4	8.7	5.9	4.0	2.5			60	A515
19.9	19.0	17.9	17.3	15.6									B	A696
												,	5	
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0					\sim	65	A516
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0	6.3	4.0	2.5		\$	65	A515
21.6	20.6	19.4	18.8	18.1	14.8	12.0	9.3			(26.		70	A516
21.6	20.6	19.4	18.8	18.1	14.8	12.0	9.3	6.7	4.0	2.5			70	A515
22.8	21.7	20.5	19.7	18.3						O i			С	A696
22.7	22.7	22.4	21.9	18.3									Cl. 1	A537
									00	•				
22.8	21.7	20.4	19.8	19.1	15.7	12.6	9.3	6.7	4.0	2.5	1.6	1.0	Α	A299
23.9	22.8	21.5	20.8	19.6	15.7	12.6	9.3	6,7	4.0	2.5	1.6	1.0	Α	A299
								`.~e``						
							,	Carbon	Steel -	- Plates,	Bars, Sh	apes, a	nd Sheets	(Structural)
13.7	13.0	12.3	11.9	11.5	10.7		N						Α	A283
							ile							
16.3	16.3	15.3	14.6	12.5	10.7	xO							30	A1011
15.4	14.7	13.8	13.3	12.5	10.7	1							В	A283
17.3	17.3	16.9	14.6	12.5	10.7	10.							33	A1011
17.7	17.7	17.7	14.6	12.5	10.7								36	A1011
				_(
17.1	16.3	15.3	14.8	14.3	13.0								С	A283
18.3	18.3	18.3	18.3	15.6	13.0								40	A1011
19.3	19.3	18.4	17.8	15.6										A36
		-0	Za											
18.8	17.9	16.9	16.3	15.8	13.9								D	A283
20.0	20.0	20.0	20.0	16.9	13.9								45	A1011
21.7	21)7	21.7	20.5	16.9	13.9								50	A1011
19.9	19.9	19.9	18.9	15.5	12.8	10.5								A992
											Carbon S	Steel —	Forgings a	and Fittings
17.1	16.3	15.3	14.8	14.3	13.8	11.4	8.7	5.9	4.0	2.5			LF1	A350
17.1	16.3	15.3	14.8	14.3	13.8	11.4	8.7	5.9	4.0	2.5	1.6	1.0	Cl. 60	A181
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5			WPL6	A420
19.9	19.0	17.9	17.3	16.7	13.9	11.4	8.7	5.9	4.0	2.5	1.6	1.0	WPB	A234
20.0	19.7												F42	A694

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

·		uremeses	Telef to A	iotes for App	<u>vitain it i</u>	ables, s ₁	, consequences		Speci Mir Strengt	fied n.	Basic Stres at Temp		ksi, l ure,
				Class/				Min.			Min.		
Material	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Size, in.	P-No. (5)	Notes	Temp., °F (6)	Tensile	Viold	Temp.	200	300
Carbon Steel				Temper	111.	(3)	Notes	r (0)	Telisite	Heiu	10 100	200	300
car bon steer		L1	K02302	1		1	(9)	-20	60	42	20.0	20.0	20.0
	A707	L2	K02302	1		1	(9)	-50	60	42	20.0	20.0	
	A707	L3	K12510	1		1	(9)	-50 -50	60	42	20.0	20.0	
	A860	WPHY 42						-50 -50	60		20.0	20.0	
	A000	WFIII 42		•••		1	•••	-30	00	420	20.0	20.0	20.0
	A694	F46	K03014			1	(9)	-20	63	46	21.0	21.0	21.0
	A860	WPHY 46				1		-50	C 63	46	21.0	21.0	21.0
	A694	F52	K03014			1	(9)	20	66	52	22.0	22.0	22.0
	A707	L1	K02302	2	•••	1	(9)	✓ −20	66	52	22.0	22.0	
	A707	L2	K03301	2		1	(9)	-50	66	52	22.0	22.0	
	A707	L3	K12510	2		1	(9)	-50	66	52	22.0	22.0	
	A860	WPHY 52		-		1		-50	66	52	22.0	22.0	
						_				-			
	A350	LF2	K03011	1		1	(9)(57)	-50	70	36	23.3	22.0	21.2
	A350	LF2	K03011	2		11	(9)(57)	0	70	36	23.3	22.0	21.2
	A105		K03504			JIS .	(9)(57)(59)	-20	70	36	23.3	22.0	21.2
	A181		K03502	70	xC	1	(9)(57)(59)	A	70	36	23.3	22.0	21.2
	A234	WPC	K03501		· 45	1	(57)(59)	В	70	40	23.3	23.3	22.2
	A694	F56	K03014	···		1	(9)	-20	71	56	23.7	23.7	
	ЛОЭЧ	130	K03014		/	1	(9)	-20	/1	30	23.7	23.7	23.7
	A694	F60	K03014	Ob.		1	(9)	-20	75	60	25.0	25.0	25.0
	A707	L2	K03301	(3)		1	(9)	-50	75	60	25.0	25.0	25.0
	A707	L3	K12510	3		1	(9)	-50	75	60	25.0	25.0	25.0
	A860	WPHY 60	200			1		-50	75	60	25.0	25.0	25.0
	4.604	DOE O	1000014			4	(0)	20		6 5	25.5	05.5	25.5
	A694	F65	K03014			1	(9)	-20	77	65	25.7	25.7	
		WPHY 65				1		-50	77	65	25.7	25.7	
	A694	V	K03014			1	(9)(79)		82	70	27.3	27.3	
	A860	WPHY 70				1		-50	82	70	27.3	27.3	27.3
Carbon Steel	Cas	tings											
	A216		J02502			1	(57)	-20	60	30	20.0	18.3	17.7
	A352	LCB	J03003			1	(9)(57)	-50	65	35	21.7	21.4	20.6
	A352	LCC	J02505			1	(9)	-50	70	40	23.3	23.3	
							-						
	A216	WCB	J03002			1	(9)(57)	-20	70	36	23.3	22.0	21.2
	A216	WCC	J02503			1	(9)(57)	-20	70	40	23.3	23.3	23.3

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

													Type/	
400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	Grade	Spec. No.
									Ca	arbon St	eel — Fe	orgings	and Fitting	s (Cont'd)
20.0	19.7												L1	A707
20.0	19.7												Ω	A707
20.0	19.7												L3	A707
20.0	19.7											رس-	WPHY 42	A860
											<	S		
21.0	21.0										N/		F46	A694
21.0	21.0									(S. Car		WPHY 46	A860
										. 0	S)			
22.0	22.0									8,			F52	A694
22.0	22.0								🗸	,			L1	A707
22.0	22.0												L2	A707
22.0	22.0								X				L3	A707
22.0	22.0												WPHY 52	A860
								0						
20.5	19.6	18.4	17.8	17.2	14.8	12.0	9.3	6.7	4.0	2.5			LF2 Cl. 1	A350
20.5	19.6	18.4	17.8	17.2	14.8	12.0	9.3	6.7	4.0	2.5			LF2 Cl. 2	A350
20.5	19.6	18.4	17.8	17.2	14.8	12.0	9.3	6.7	4.0	2.5	1.6	1.0		A105
20.5	19.6	18.4	17.8	17.2	14.8	12.0	9.3	6.7	4.0	2.5	1.6	1.0	Cl. 70	A181
						1/10								
22.8	21.7	20.4	19.8	18.3	14.8	12.0							WPC	A234
23.7	23.7				C)								F56	A694
					1.									
25.0	25.0				14.								F60	A694
25.0	25.0												L2	A707
25.0	25.0		(L3	A707
25.0	25.0		O	·									WPHY 60	A860
			NO											
25.7	25.7	0	<i>U.</i>										F65	A694
25.7	25.7	O_{χ}											WPHY 65	A860
27.3		7											F70	A694
27.3	11.	\											WPHY 70	
	SI													
	P											Car	bon Steel -	- Castings
17.1	16.3	15.3	14.8	14.3	13.8	11.4	8.7	5.9	4.0	2.5	1.6		WCA	A216
19.9	19.0	17.9	17.3	16.7	13.9	11.4	9.0	6.3	4.0	2.5	1.6	1.0	LCB	A352
22.8	21.7	20.4	19.8	19.2									LCC	A352
20.5	19.6	18.4	17.8	17.2	14.8	12.0	9.3	6.7	4.0	2.5	1.6	1.0	WCB	A216
22.8	21.7	20.4	19.8	18.3	14.8	12.0	9.3	6.7	4.0	2.5			WCC	A216
-		-			-	-		-	-	-				-

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic
Allowable
Stress, S,
ksi, at Metal
Specified Min. Temperature,
Strongth ksi °E [Note (1)]

									Strengt		°F [Note	
				Class/				Min.			Min.	
Nominal Composition	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Size, in.	P-No. (5)	Notes	Temp., °F (6)	Tensile	Vield	Temp. to 100	200
Low and Intermedia				remper	111.	(3)	Notes	I (0)	Tensite	Ticiu	10 100)
$\frac{1}{2}$ Cr- $\frac{1}{2}$ Mo	A335	P2	K11547			3		-20	55	30	18.3	18.3
¹ / ₂ Cr- ¹ / ₂ Mo	A691	¹⁄2CR	K12143			3	(11)(67)	-20	55	330		18.3
A387 Gr. 2 Cl. 1		2								0 ·		
$C-\frac{1}{2}Mo$	A335	P1	K11522			3	(58)	-20	55	30	18.3	18.3
$C-\frac{1}{2}Mo$	A369	FP1	K11522			3	(58)	-20	55	30	18.3	18.3
$^{1}/_{2}Cr-^{1}/_{2}Mo$	A369	FP2	K11547			3		-20	55	30	18.3	18.3
$1Cr-\frac{1}{2}Mo$	A691	1CR	K11757			4	(11)(67)	-20	55	33	18.3	18.3
A387 Gr. 12 Cl. 1							,	-20 -20				
½Cr-½Mo	A426	CP2	J11547			3	(10)	-20	60	30	20.0	18.8
$1\frac{1}{2}Si-\frac{1}{2}Mo$	A335	P15	K11578			3		-20	60	30	20.0	18.8
$C-\frac{1}{2}Mo-Si$	A426	CP15	J11522			3	(10)	-20	60	30	20.0	18.8
1Cr- ¹ / ₂ Mo	A426	CP12	J11562			4	(18)	-20	60	30	20.0	18.1
5Cr-1 ¹ / ₂ Si- ¹ / ₂ Mo	A426	CP5b	J51545	•••		5BN	(10)	-20	60	30	20.0	18.1
3Cr-Mo	A426	CP21	J31545			5A	(10)	-20	60	30	20.0	18.7
561 110	20	0.21	,01010		×O	4011	(10)	_0		00	20.0	10.7
³ / ₄ Cr- ³ / ₄ Ni-Cu-Al	A333	4	K11267		F	4		-150	60	35	20.0	19.1
$2Cr-\frac{1}{2}Mo$	A369	FP3b	K21509	-Jil		4		-20	60	30	20.0	18.7
$1Cr-\frac{1}{2}Mo$	A335	P12	K11562	J :		4		-20	60	32	20.0	19.3
1Cr-½Mo	A369	FP12	K11562			4		-20	60	32	20.0	19.3
$1\frac{1}{4}Cr-\frac{1}{2}Mo-Si$	A335	P11	K11597			4		-20	60	30	20.0	18.5
$1\frac{1}{4}Cr-\frac{1}{2}Mo-Si$	A369	FP11	K11597			4		-20	60	30	20.0	18.5
		M										
1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si A387 Gr. 11 Cl. 1	A691	1 ¹ ⁄₄CR	K11789			4	(11)(67)	-20	60	35	20.0	20.0
5Cr- ¹ / ₂ Mo	A691	5CR	K41545			5B	(11)(67)	-20	60	30	20.0	18.1
A387 Gr. 5 Cl. 1							()()					
5Cr-½Mo	A335	P5	K41545			5B		-20	60	30	20.0	18.1
5Cr-½Mo-Si	A335	P5b	K51545			5B		-20	60	30	20.0	18.1
5Cr- ¹ / ₂ Mo-Ti	A335	P5c	K41245			5B		-20	60	30	20.0	18.1
5Cr- ¹ / ₂ Mo	A369	FP5	K41545			5B		-20	60	30	20.0	18.1
06 414	4005	DO.	1100011			ED.		20		200	20.0	101
9Cr-1Mo	A335	P9	K90941			5B		-20 20	60	30	20.0	18.1
9Cr-1Mo	A369	FP9	K90941			5B		-20 20	60	30	20.0	18.1
9Cr-1Mo A387 Gr. 9 Cl. 1	A691	9CR	K90941			5B	(11)(67)	-20	60	30	20.0	18.1
3Cr-1Mo	A335	P21	K31545			5A		-20	60	30	20.0	18.7

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

300	400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	Type/ Grade	Spec.
												Low a	nd Inte	rmedia	te Alloy	Steel _	Pipes
18.0	17.4	16.9	16.4	16.1	15.7	15.4	14.9	14.5	13.9	9.2	5.9					P2	A335
18.3	18.3	18.3	18.0	17.7	17.3	16.9	16.4	15.9	14.3	9.2	5.9					½CR	A691
															0,	1.	
18.0	17.4	16.9	16.4	16.1	15.7	15.4	14.9	14.5	13.7	8.2	4.8	4.0	2.4		8	P1	A335
18.0	17.4	16.9	16.4	16.1	15.7	15.4	14.9	14.5	13.7	8.2	4.8	4.0	2.4		<u>ر "</u>	FP1	A369
18.0	17.4	16.9	16.4	16.1	15.7	15.4	14.9	14.5	13.9	9.2	5.9	4.1	2.5	CM		FP2	A369
17.6	17.6	17.2	16.8	16.5	16.3	16.0	15.7	15.4	15.0	11.3	7.2	4.5	2.8	1.8	1.1	1CR	A691
													o Š	•			
10.0	174	16.0	16.4	16.1	157	15 /	140	145	120	9.2	5.9	4.0	2.4			CP2	A426
18.0 18.2	17.4 17.7	16.9 17.3	16.4 16.8	16.1 16.6	15.7 16.3	15.4 15.9	14.9 15.4	14.5 13.8	13.9 12.5	10.0	6.3	4.0	2.4 2.4			P15	A335
18.2	17.7	17.3	16.8	16.6	16.3	15.9	15.4	13.8	12.5	10.0	6.3	4.0	2.4		•••	CP15	A426
10.2	17.7	17.5	10.0	10.0	10.5	13.7	13.4	13.0	12.5	10.0	60	7.0	2.7			CI IS	ATZU
17.0	16.2	15.7	15.2	15.0	14.8	14.6	14.3	14.0	13.6	11.3	7.2	4.5	2.8	1.8	1.1	CP12	A426
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	0.8	5.8	4.2	2.9	1.8	1.0	CP5b	A426
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	16.0	12.0	9.0	7.0	5.5	4.0	2.7	1.5	CP21	A426
								×	0								
18.2	17.3	16.4	15.5	15.0				*								4	A333
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.5	12.5	10.0	6.2	4.2	2.6	1.4	1.0	FP3b	A369
							\cdot										
18.1	17.3	16.7	16.3	16.0	15.8	15.5		14.9	14.5	11.3	7.2	4.5	2.8	1.8	1.1	P12	A335
18.1	17.3	16.7	16.3	16.0	15.8	15.5	15.3	14.9	14.5	11.3	7.2	4.5	2.8	1.8	1.1	FP12	A369
17.6	16.0	16.2	157	15 4	65 4	110	111	140	12.6	0.2	()	4.2	2.0	1.0	1.2	D11	422F
17.6 17.6	16.8 16.8	16.2 16.2	15.7 15.7	15.4 15.4	15.1 15.1	14.8 14.8	14.4 14.4	14.0 14.0	13.6 13.6	9.3 9.3	6.3 6.3	4.2 4.2	2.8 2.8	1.9 1.9	1.2 1.2	P11 FP11	A335 A369
17.0	10.0	10.2	13.7		1 3.1	14.0	14.4	14.0	13.0	9.3	0.3	4.2	2.0	1.9	1.2	LLII	A309
20.0	19.6	18.9	18.3	18.0	17.6	17.2	16.8	16.4	13.7	9.3	6.3	4.2	2.8	1.9	1.2	1 ¹ / ₄ CR	A691
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	5CR	A691
17.1	17.2		10.0	10.0	10.5	13.7	13.1	11.5	10.7	0.0	3.0	1.2	2.7	1.0	1.0	SGR	71071
	c	H.															
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	P5	A335
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	P5b	A335
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	P5c	A335
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	FP5	A369
	17.2	17.1	16.8		16.3	15.9		14.8	14.1	10.6	7.4	5.0	3.3	2.2	1.5	P9	A335
	17.2	17.1	16.8	16.6	16.3		15.4	14.8	14.1	10.6	7.4	5.0	3.3	2.2	1.5	FP9	A369
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.8	14.1	10.6	7.4	5.0	3.3	2.2	1.5	9CR	A691
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	16.0	12.0	9.0	7.0	5.5	4.0	2.7	1.5	P21	A335

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic Allowable

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Stress, S, ksi, at Metal Specified Min. Temperature, Strength, ksi °F [Note (1)] Min. Min. Class/ **Nominal** Spec. Type/ UNS Condition/ Size, P-No. Temp., Temp. Composition °F (6) Tensile Yield to 100 200 No. Grade No. **Temper** in. (5) **Notes** Low and Intermediate Alloy Steel -**Pipes** 20.0 3Cr-1Mo A369 FP21 -20 60 30 18.7 K31545 5A 30 3CR 60 3Cr-1Mo A691 K31545 5A (11)(67)-2020.0 18.5 A387 Gr. 21 Cl. 1 $2^{1}/_{4}Cr-1Mo$ A691 2¹/₄CR K21590 5A (11)(67)(72)(75)-2030 20.0 18.7 A387 Gr. 22 Cl. 1 FP22 K21590 30 $2^{1}/_{4}Cr-1Mo$ A369 5A (72)(75)-20 60 20.0 18.7 **~**20 $2^{1}/_{4}Cr-1Mo$ A335 P22 K21590 5A (72)(75)60 30 20.0 18.7 2Ni-1Cu 9 -100 A333 K22035 9A 63 46 21.0 ... 2Ni-1Cu A334 9 K22035 9A -100 63 46 21.0 ... 7 A333 K21903 9A -10065 35 21.7 21.4 A334 7 K21903 9A -10065 35 21.7 21.4 9B A333 3 K31918 -15065 35 21.7 21.4 9B 3 A334 K31918 -15065 35 21.7 21.4 $C-\frac{1}{2}Mo$ A426 CP1 J12521 (10)(58)-2065 21.7 21.7 35 $C_{-1/2}^{-1}$ Mo A204 Gr. A K11820 3 65 21.7 A672 L65 (11)(58)(67)-2037 21.7 $C_{-1/2}^{-1}$ Mo A204 Gr. A A691 CM-65 K11820 3 21.7 (11)(58)(67)-20 65 37 21.7 21/4Ni A203 Gr. B CFB70 K22103 9A -20 70 40 23.3 A671 (11)(65)(67)3½Ni A203 Gr. E CFE70 K32018 9B 23.3 A671 (11)(65)(67)-2070 40 ... C-1/2Mo A204 Gr. B K12020 3 70 23.3 A672 L70 (11)(58)(67)-2040 23.3 $C_{-1/2}^{-1}$ Mo A204 Gr. B CM-70 A691 K12020 3 -2070 40 23.3 23.3 ... (11)(58)(67) $1\frac{1}{4}Cr-\frac{1}{2}Mo$ CP11 A426 J12072 4 (10)-2070 40 23.3 23.3 ... $2^{1}/_{4}Cr-1Mo$ A426 CP22 J21890 70 23.3 23.3 5A (10)(72)-2040 C-1/2Mo A204 Gr. C A672 L75 3 75 25.0 25.0 K12320 (11)(58)(67)-2043 C-1/2Mo A204 Gr. C 3 75 25.0 A691 CM-75 K12320 (11)(58)(67)-2043 25.0 P91 85 A335 K90901 ≤3 thk. 15E -2060 28.3 28.3 9Cr-1Mo-V 9Cr-1Mo-V A691 91 K90901 ≤3 thk. 15E (11)(67) -20 85 60 28.3 28.3 $5Cr-\frac{1}{2}Mo$ 90 30.0 A426 CP5 J42045 5B (10)-2060 29.9

 $2^{1}/_{4}Ni$

21/4Ni

3½Ni

 $3\frac{1}{2}Ni$

9Cr-1Mo

9Ni

9Ni

CP9

A426

A333 8

A334 8 J82090

K81340

K81340

5B

11A

11A

(10)

(47)

90

100

100

-20

-320

-320

30.0

33.3

33.3

60

75

75

29.9

33.3

33.3

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

300	400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	Type/ Grade	Spec. No.
										L	ow and	Intern	nediate	Alloy S	teel —	Pipes (cont d)
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	16.0	12.0	9.0	7.0	5.5	4.0	2.7	1.5	FP21	A369
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	16.0	12.0	9.0	7.0	5.5	4.0	2.7	1.5	3CR	A691
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.1	13.6	10.8	8.0	5.7	3.8	2.4	1.4	2 ¹ / ₄ CR	A691
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.1	13.6	10.8	8.0	5.7	3.8	C2,4	1.4	FP22	A369
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.1	13.6	10.8	8.0	5.7	3.8	2.4	1.4	P22	A335
													0	•			
																9	A333
												6				9	A334
20.6	19.9	18.9	17.5	16.7	15.7	13.9	11.4	9.0	6.5	4.5	2.5	1.6	1.0			7	A333
20.6	19.9	18.9	17.5	16.7	15.7	13.9	11.4	9.0	6.5	4.5	2.5	1.6	1.0			7	A334
										N	•						
20.6	19.9	18.9	17.5	16.7	15.7	13.9	11.4	9.0	6,5	,	2.5	1.6	1.0			3	A333
20.6	19.9	18.9	17.5	16.7	15.7	13.9	11.4	9.0	6.5	4.5	2.5	1.6	1.0			3	A334
21.0	20.3	19.7	19.1	18.7	18.4	17.9	17.4	16.9	13.7	8.2	4.8	4.0	2.4			CP1	A426
21.7	21.5	20.8	20.2	19.8	19.4	19.0	18.4	17.9	13.7	8.2	4.8	4.0	2.4			L65	A672
21.7	21.5	20.8	20.2	19.8	19.4	19.0	18.4	17.9	13.7	8.2	4.8	4.0	2.4			CM-65	A691
						di											
						\mathcal{O}										CFB70	A671
•••		•••			ر ن,			•••	•••							CFE70	A671
23.3	23.2	22.5	21.8	21.4	2 1.0	20.5	19.9	19.3	13.7	8.2	4.8	4.0	2.4			L70	A672
23.3	23.2	22.5	21.8	21,4	21.0	20.5	19.9	19.3	13.7	8.2	4.8	4.0	2.4			CM-70	A691
23.3	22.5	21.7	20.9	20.5	20.1	19.7	19.2	18.7	13.7	9.3	6.3	4.2	2.8	1.9	1.2	CP11	A426
22.6	22.6	22.6	22.6	22.6	22.6	22.6	22.6	21.9	15.8	11.4	7.8	5.1	3.2	2.0	1.2	CP22	A426
25.0	25.0	24.2	23.4	23.0	22.6	22.0	21.4	20.7	13.7	8.2	4.8	4.0	2.4			L75	A672
25.0	25.0	24.2	23.4	23.0	22.6	22.0	21.4	20.7	13.7	8.2	4.8	4.0	2.4			CM-75	A691
28.3	28.2	28.1	27.7	27.3	26.7	25.9	24.9	23.7	22.3	20.7	18.0	14.0	10.3	7.0	4.3	P91	A335
28.3	28.2	28.1	27.7	27.3	26.7	25.9	24.9	23.7	22.3	20.7	18.0	14.0	10.3	7.0	4.3	91	A691
29.1	28.8	28.7	28.3	27.9	27.3	26.5	25.5	24.2	16.4	11.0	7.4	5.0	3.3	2.2	1.5	CP5	A426
29.1	28.8	28.7	28.3	27.9	27.3	26.5	25.5	24.2	16.4	11.0	7.4	5.0	3.8	2.2	1.5	CP9	A426
																8	A333
																8	A334

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic
Allowable
Stress, S,
ksi, at Metal
Specified Min. Temperature,
Strength, ksi °F [Note (1)]

									Strengt	h, ksi	°F [Note (1)]	
Nominal	Spec.	Trme/	UNS	Class/ Condition/	Size,	P-No.		Min.			Min. Temp.	
Composition	No.	Type/ Grade	No.	Temper	in.	(5)	Notes	Temp., °F (6)	Tensile	Yield	to 100	200
Low and Intermedia	ite Alloy	Steel —	Plates	_							76	
$^{1}/_{2}Cr-^{1}/_{2}Mo$	A387	2	K12143	1		3		-20	55	33	18.3	18.3
$1Cr-\frac{1}{2}Mo$	A387	12	K11757	1		4		-20	55	330	18.3	18.0
9Cr-1Mo	A387	9	K90941	1		5B		-20	60	30	20.0	18.1
$1\frac{1}{4}Cr-\frac{1}{2}Mo-Si$	A387	11	K11789	1		4		-20	60	35	20.0	20.0
5Cr- ¹ / ₂ Mo	A387	5	K41545	1		5B		-20	60	30	20.0	18.1
3Cr-1Mo	A387	21	K31545	1		5A		-20	60	30	20.0	18.3
2½Cr-1Mo	A387	22	K21590	1		5A	(72)	←20	60	30	20.0	18.7
2½Ni	A203	A	K21703			9A	(12)(65)	-20	65	37	21.7	21.7
3½Ni	A203	D	K31718			9B	(12)(65)	-20	65	37	21.7	21.7
$C-\frac{1}{2}Mo$	A204	A	K11820			3	(58)	-20	65	37	21.7	21.7
$1Cr-\frac{1}{2}Mo$	A387	12	K11757	2		4	me'	-20	65	40	21.7	21.3
2 ¹ / ₄ Ni	A203	В	K22103			9A 🔥	(12)(65)	-20	70	40	23.3	23.3
3½Ni	A203	Е	K32018			9B	(12)(65)	-20	70	40	23.3	23.3
½Cr-½Mo	A387	2	K12143	2	Qy.	3		-20	70	45	23.3	23.3
$C-\frac{1}{2}Mo$	A204	В	K12020	-110		3	(58)	-20	70	40	23.3	23.3
$Mn-\frac{1}{2}Mo$	A302	A	K12021	· C		3		-20	75	45	25.0	25.0
$C-\frac{1}{2}Mo$	A204	С	K12320	M ::		3	(58)	-20	75	43	25.0	25.0
$1\frac{1}{4}$ Cr $-\frac{1}{2}$ Mo-Si	A387	11	K11789	2		4		-20	75	45	25.0	25.0
$5Cr-\frac{1}{2}Mo$	A387	5	K41545	2		5B	***	-20	75	45	25.0	24.9
3Cr-1Mo	A387	21	K31545	2		5A		-20	75	45	25.0	25.0
2 ¹ / ₄ Cr-1Mo	A387	22	K21590	2		5A	(72)	-20	75	45	25.0	25.0
$Mn-\frac{1}{2}Mo$	A302	В	K12022			3		-20	80	50	26.7	26.7
$Mn^{-1}/_{2}Mo^{-1}/_{2}Ni$	A302	С	K12039			3		-20	80	50	26.7	26.7
$Mn^{-1}/_{2}Mo^{-3}/_{4}Ni$	A302	D	K12054			3		-20	80	50	26.7	26.7
9Cr-1Mo-V	A387	91	K90901	2	≤3 thk	. 15E		-20	85	60	28.3	28.3
8Ni	A553	II	K71340			11A	(47)	-275	100	85	33.3	
$5Ni-\frac{1}{4}Mo$	A645	A	K41583			11A	•••	-275	95	65	31.7	31.7
9Ni	A553	I	K81340	•••		11A	(47)	-320	100	85	33.3	33.3
9Ni	A353		K81340			11A	(47)	-320	100	75	33.3	33.3
Low and Intermedia	-			and Fittings								
$C-\frac{1}{2}Mo$	A234	WP1	K12821			3	(58)	-20	55	30	18.3	18.3

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

300	400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	Type/ Grade	Spec.
												Low ar	nd Inte	rmediat	e Alloy	Steel _	Plates
18.3	18.3	18.3	18.0	17.7	17.3	16.9	16.4	15.9	14.3	9.2	5.9					2 Cl 🔼	A387
17.6	17.6	17.2	16.8	16.5	16.3	16.0	15.7	15.4	15.0	11.3	7.2	4.5	2.8	1.8	1.1	12 Gl. 1	A387
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.8	14.1	10.6	7.4	5.0	3.3	2.2	1.5	9 Cl. 1	A387
20.0	19.6	18.9	18.3	18.0	17.6	17.2	16.8	16.4	13.7	9.3	6.3	4.2	2.8	1.9	1.2	11 Cl. 1	1207
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	5.8	4.2	2.9	1.9	1.0	5 Cl. 1	A387
17.5	17.0	16.6	16.2	16.0	15.8	15.5	15.2	14.9	12.0	9.0	7.0	5.5	4.0	C ₂₎₇	1.5	21 Cl. 1	
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.1	13.6	10.8	8.0	5.7	3.8	2.4	1.4	22 Cl. 1	
													0				
21.7	21.1	20.0	18.5	17.6	16.6	13.9	11.4	9.0	6.5	4.5	2.5					A	A203
21.7	21.1	20.0	18.5	17.6	16.6	13.9	11.4	9.0	6.5	4.5	2.5	QV				D	A203
21.7	21.5	20.8	20.2	19.8	19.4	19.0	18.4	17.9	13.7	8.2	4.8	4.0	2.4			A	A204
20.8	20.8	20.8	20.3	20.0	19.7	19.4	19.1	18.6	18.0	11.3	7.2	4.5	2.8	1.8	1.1	12 Cl. 2	
										13							
23.3	22.8	21.6	20.0	19.0	16.9	13.9	11.4	9.0	6.5	4.5	2.5					В	A203
23.3	22.8	21.6	20.0	19.0	18.0	14.8	12.0	9.3	6.5	4.5	2.5					E	A203
23.3	23.3	23.3	23.3	23.3	23.3	23.1	22.4	21 😿	20.9	9.2	5.9					2 Cl. 2	A387
23.3	23.2	22.5	21.8	21.4	21.0	20.5	19.9	19.3	13.7	8.2	4.8	4.0	2.4			В	A204
								0,									
25.0	25.0	25.0	25.0	24.9	24.4	23.9	23.2	20.0	13.7	8.2	4.8					A	A302
25.0	25.0	24.2	23.4	23.0	22.6	22.0	21.4	20.7	13.7	8.2	4.8	4.0	2.4			С	A204
25.0	25.0	24.4	23.5	23.1	22.6	22.2	21.6	20.2	13.7	9.3	6.3	4.2	2.8	1.9	1.2	11 Cl. 2	A387
24.2	24.0	24.0	23.6	23.2	22.7	16.5	16.0	15.1	10.9	8.0	5.8	4.2	2.9	1.8	1.0	5 Cl. 2	A387
24.2	24.2	24.2	24.2	24.2	24.2	24.2	24.2	18.1	13.1	9.5	6.8	4.9	3.2	2.4	1.3	21 Cl. 2	
24.3	24.1	24.0	23.8	23.6	23.4	23.0	22.5	21.9	15.8	11.4	7.8	5.1	3.2	2.0	1.2	22 Cl. 2	
			Ó	Hi.													
26.7	26.7	26.7	26.7	26.7	26.7	26.5	25.7	20.0	13.7	8.2	4.8					В	A302
26.7	26.7	26.7	26.7	26.7	26.7	26.5	25.7	20.0	13.7	8.2	4.8					С	A302
26.7	26.7	26.7	26.7	26.7	26.7	26.5	25.7	20.0	13.7	8.2	4.8					D	A302
	C																
28.3	28.2	28.1	27.7	27.3	26.7	25.9	24.9	23.7	22.3	20.7	18.0	14.0	10.3	7.0	4.3	91 Cl. 2	A387
																11	A553
																II A	A645
																п	A043
																I	A553
																	A353
									Lo	ow and	d Inter	mediate	Alloy	Steel —	Forgin	igs and F	ittings
18.0	17.4	16.9	16.4	16.1	15.7	15.4	14.9	14.5	13.7	8.2	4.8	4.0	2.4			WP1	A234

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Allowable Stress, S, ksi, at Metal Specified Min. Temperature, Strength, ksi °F [Note (1)] Class/ Min. Min. **Nominal** Spec. Type/ UNS Condition/ Size, P-No. Temp., Temp. Composition °F (6) Tensile Yield 200 No. Grade No. **Temper** (5) **Notes** to 100 Low and Intermediate Alloy Steel — Forgings and Fittings $1Cr-\frac{1}{2}Mo$ A182 F12 K11562 1 (9) -20 60 20.0 19.3 4 32 32 1Cr-1/2Mo A234 WP12 K12062 1 -2060 20.0 19.3 4 ... 11/4Cr-1/2Mo-Si -20 30 A182 F11 K11597 1 4 (9) 20.0 18.5 $1\frac{1}{4}Cr-\frac{1}{2}Mo-Si$ A234 WP11 1 4 30 20.0 18.5 K11597 $2^{1}/_{4}Cr-1Mo$ 5A -20 60 30 20.0 A182 F22 K21590 1 (9)(72)(75) 18.7 $2^{1}/_{4}Cr-1Mo$ A234 WP22 K21590 1 5A (72)-20 60 30 20.0 18.7 $5Cr-\frac{1}{2}Mo$ A234 WP5 K41545 5B -20 60 30 20.0 18.1 9Cr-1Mo A234 WP9 K90941 -2060 30 20.0 18.1 3½Ni WPL3 A420 K31918 -150 65 35 21.7 21.4 $3\frac{1}{2}$ Ni (9) 23.3 A350 LF3 K32025 -15070 37.5 22.9 $\frac{1}{2}Cr - \frac{1}{2}Mo$ A182 F2 K12122 3 (9) -20 70 40 23.3 23.3 $C - \frac{1}{2}Mo$ F1 K12822 3 70 23.3 A182 (9)(58)-2040 23.3 $1Cr-\frac{1}{2}Mo$ A182 F12 K11564 2 4 (9) -2070 40 23.3 22.9 K12062 $1Cr-\frac{1}{2}Mo$ A234 WP12 2 4 -20 70 40 23.3 22.9 ... 11/4Cr-1/2Mo-Si 2 K11572 4 (9) -2070 40 23.3 23.3 2 $1\frac{1}{4}Cr-\frac{1}{2}Mo-Si$ WP11 K11572 4 -2070 40 23.3 23.3 5Cr-¹/₂Mo A182 F5 70 23.3 23.3 K41545 5B (9) -2040 (9) 3Cr-1Mo A182 F21 K31545 5A -20 75 25.0 25.0 45 $2^{1}/_{4}Cr-1Mo$ A182 F22 K21590 3 5A (9)(72)-20 75 45 25.0 25.0 $2^{1}/_{4}Cr-1Mo$ (72) A234 WP22 K21590 3 5A -2075 45 25.0 25.0 9Cr-1Mo A182 F9 K90941 (9) -20 85 55 28.3 28.3 5B 9Cr-1Mo-V A182 F91 K90901 ≤3 thk. 15E -2085 60 28.3 28.3 85 9Cr-1Mo-V A234 WP91 K90901 ≤3 thk. 15E -2060 28.3 28.3

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Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

300	400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	Type/ Grade	Spec.
-								Low	and In	terme	diate A	lloy Ste	el — F	orgings	and Fi	ttings (C	ont d)
																00) `
18.1	17.3	16.7	16.3	16.0	15.8	15.5	15.3	14.9	14.5	11.3	7.2	4.5	2.8	1.8	1.1	F12 CI. 1	A182
18.1	17.3	16.7	16.3	16.0	15.8	15.5	15.3	14.9	14.5	11.3	7.2	4.5	2.8	1.8	1.5	WP12	A234
															8	Cl. 1	
17.6	16.8	16.2	15.7	15.4	15.1	14.8	14.4	14.0	13.6	9.3	6.3	4.2	2.8	1.9	1.2	F11 Cl. 1	A182
17.6	16.8	16.2	15.7	15.4	15.1	14.8	14.4	14.0	13.6	9.3	6.3	4.2	2.8	1.9	1.2	WP11	A234
												,	6	~		Cl. 1	
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.1	13.6	10.8	8.0	5.7	3.8	2.4	1.4	F22 Cl. 1	A182
18.2	18.0	17.9	17.9	17.9	17.9	17.9	17.7	17.1	13.6	10.8	8.0	5.7	3.8	2.4	1.4	WP22	A234
											الري					Cl. 1	
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.3	10.9	8.0	6 5.8	4.2	2.9	1.8	1.0	WP5	A234
17.4	17.2	17.1	16.8	16.6	16.3	15.9	15.4	14.8	14.1	11.0	7.4	5.0	3.3	2.2	1.5	WP9	A234
20.6	19.9	18.9	17.5	16.7				×(Ò							WPL3	A420
22.1	21.4	20.3	18.8	17.9				ick.								LF3	A350
23.3	23.2	22.5	21.8	21.4	21.0	20.5	19.9	19.3	18.6	9.2	5.9					F2	A182
23.3	23.2	22.5	21.8	21.4	21.0	20.5	19.9	19.3	13.7	8.2	4.8	4.0	2.4			F1	A182
22.4	04.7	20.0	20.2	20.0	60.7		10.1	10.6	100	44.0	7.0	4.5	2.0	4.0	4.4	E40 Cl 0	1100
22.4	21.7	20.9	20.3	20.0	19.7	19.4	19.1	18.6	18.0	11.3	7.2	4.5	2.8	1.8	1.1	F12 Cl. 2	
22.4	21.7	20.9	20.3	20.0	1 9.7	19.4	19.1	18.6	18.0	11.3	7.2	4.5	2.8	1.8	1.1	WP12 Cl. 2	A234
23.3	22.5	21.7	20.9	20.5	20.1	19.7	19.2	18.7	13.7	9.3	6.3	4.2	2.8	1.9	1.2	F11 Cl. 2	A182
23.3	22.5	21.7		20.5	20.1	19.7	19.2	18.7	13.7	9.3	6.3	4.2	2.8	1.9	1.2	WP11	A234
	ć	ME														Cl. 2	
22.6	22.4	22.4	22.0	21.7	21.2	20.6	19.8	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	F5	A182
24.3	24.1	24.0	23.8	23.6	23.4	23.0	22.5	18.1	13.1	9.5	6.8	4.9	3.2	2.4	1.3	F21	A182
24.2	24.2	24.2	24.2	24.2	24.2	24.2	24.2	21.9	15.8	11.4	7.8	5.1	3.2	2.0	1.2	F22 Cl. 3	A182
24.2	24.2	24.2	24.2	24.2	24.2	24.2	24.2	21.9	15.8	11.4	7.8	5.1	3.2	2.0	1.2	WP22	A234
																Cl. 3	
27.4	27.2	27.1	26.8	26.3	25.8	25.0			15.2	10.6	7.4	5.0	3.3	2.2	1.5	F9	A182
28.3	28.2	28.1	27.7	27.3	26.7		24.9	23.7	22.3	20.7	18.0	14.0	10.3	7.0	4.3	F91	A182
28.3	28.2	28.1	27.7	27.3	26.7	25.9	44.9	23.7	22.3	20.7	18.0	14.0	10.3	7.0	4.3	WP91	A234

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

	Dasic
	Allowable
	Stress, S,
	ksi, at Metal
Specified Min.	Temperature
Ctuonath Irai	OF INote (1)1

									Strengt	h, ksi	°F [Not	e (1)]
				Class/				Min.			Min.	
Nominal	Spec.	Type/	UNS	Condition/	Size,			Temp.,	II		Temp.	200
Composition	No.	Grade	No.	Temper	in.	(5)	Notes	°F (6)	Tensile	Yield	to 100	200
Low and Intermedia	ite Alloy	Steel —	 Forgings 	and Fittings							710	
5Cr- ¹ / ₂ Mo	A182	F5a	K42544			5B	(9)	-20	90	65	30.0	29.9
9Ni	A420	WPL8	K81340			11A	(47)	-320	100	750	33.3	33.3
										0. V.		
Low and Intermedia	te Alloy	Steel —	- Castings						Q	50		
$C-\frac{1}{2}Mo$	A352	LC1	J12522			3	(9)(58)	-75	65	35	21.7	21.7
$C-\frac{1}{2}Mo$	A217	WC1	J12524			3	(9)(58)	-20	65	35	21.7	21.7
								~	O `			
2½Ni	A352	LC2	J22500			9A	(9)	-100	70	40	23.3	23.3
$3\frac{1}{2}$ Ni	A352	LC3	J31550			9B	(9)	-150	70	40	23.3	23.3
- 12			,									
$1\text{Ni}-\frac{1}{2}\text{Cr}-\frac{1}{2}\text{Mo}$	A217	WC4	J12082			4	(9) (9) (9)	-20	70	40	23.3	23.3
³ / ₄ Ni-1Mo- ³ / ₄ Cr	A217	WC5	J22000			4	(9)	-20	70	40	23.3	23.3
$1\frac{1}{4}\text{Cr} - \frac{1}{2}\text{Mo}$	A217	WC6	J12072			4	(9)	-20	70	40	23.3	23.3
$2^{1}/_{4}Cr-1Mo$	A217	WC9	J21890			5A		-20	70	40	23.3	23.3
27401-1110	AZ17	WG	J21070			JA	(A)	20	70	40	23.3	23.3
5Cr- ¹ / ₂ Mo	Δ217	C5	142045	W. Clic		- GR	(9)	-20	90	60	30.0	29.9
9Cr-1Mo	A217	C12	182090			5B	(9)	-20	90	60	30.0	29.9
)GI-11410	AZ17	CIZ	J02070		NO.	JD	(2)	20	70	00	30.0	2).)
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Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

300	400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	Type/ Grade	Spec.
								Low	and In							ttings (ont d)
29.1	28.8	28.7	28.3	27.9	27.3	26.5	25.5	14.3	10.9	8.0	5.8	4.2	2.9	1.8	1.0	F5a	A182
																WPL8	A420
															\sim	1.	
											Le	ow and	Interm	ediate	Alloy S	teel — C	astings
21.0	20.3	19.7	19.1	18.7	18.4										<u>/</u>	LC1	A352
21.0	20.3	19.7	19.1	18.7	18.4	17.9	17.4	16.9	13.7	8.2	4.8	4.0	2.4	CH		WC1	A217
													1	>			
23.3	22.8	21.6	20.0	19.0									~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~			LC2	A352
23.3	22.8	21.6	20.0	19.0												LC3	A352
23.3	23.3	23.0	22.4	22.1	21.7	21.2	20.6	19.8	14.3	9.2	5.9	V				WC4	A217
23.3	23.3	23.0	22.4	22.1	21.7	21.2	20.6	19.8	14.3	9.2	5.9	4.0	2.4			WC5	A217
23.3	22.5	21.7	20.9	20.5	20.1	19.7	19.2	18.7	13.7	9.3	6.3	4.2	2.8	1.9	1.2	WC6	A217
22.6	22.6	22.6	22.6	22.6	22.6	22.6	22.6	21.9	15.8	11.4	7.8	5.1	3.2	2.0	1.2	WC9	A217
20.4	200		20.0	0	0.7.0	065		440	400	71	= 0			4.0	4.0	0=	1015
29.1	28.8	28.7	28.3	27.9	27.3	26.5	25.5	14.3	10.9		5.8	4.2	2.9	1.8	1.0	C5	A217
29.1	28.8	28.7	28.3	27.9	27.3	26.5	25.5	24.2	15.2	10.6	7.4	5.0	3.3	2.2	1.5	C12	A217
				27.9 27.9				45	•								
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Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	ic Allo ss, <i>S</i> , Temp [Note	ksi, a eratu	t
Nominal	Product	Spec.	Type/	UNS	Class/ Condition/	Size,	P-No.		Min. Temp.,	Strengt	.II, KSI	Min. Temp.	INOTE	(1)]	
Composition	Form	No.	Grade	No.	Temper	in.	(5)	Notes	°F (6)	Tensile	Yield	to 100	200	300	400
Stainless Steel — Pi	•		*			2									
18Cr-10Ni-Ti	Smls. pipe		TP321	S32100		>3/8 thk.		(28)	-425	70	25	16.7		16.7	
18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100		>3/ ₈ thk.	8	(28)(36)	-425	70	25	16.7	16.7	16.7	16.7
18Cr-8Ni	Tube	A213	TP304L	S30403			8	(14)(36)	-425	70	25	16.7	16.7	16.7	15.8
18Cr-8Ni	Tube	A269	TP304L	S30403			8	(14)(36)	-425	70	25	16.7	16.7	16.7	15.8
18Cr-8Ni	Tube	A270	TP304L	S30403			8	(14)	-425	70	25	16.7	16.7	16.7	15.8
18Cr-8Ni	Pipe	A312	TP304L	S30403			8	•••	-425	70	25)	16.7	16.7	16.7	15.8
18Cr-8Ni	Pipe	A358	304L	S30403			8	(36)	-425	70	25	16.7	16.7	16.7	15.8
16Cr-12Ni-2Mo	Tube	A213	TP316L	S31603			8	(14)(36)	-425	70	25	16.7	16.7	16.7	15.7
16Cr-12Ni-2Mo	Tube	A269	TP316L	S31603			8	(14)(36)	-425	70	25	16.7	16.7	16.7	15.7
16Cr-12Ni-2Mo	Tube	A270	TP316L	S31603			8	(14)	-425	70	25	16.7	16.7	16.7	15.7
16Cr-12Ni-2Mo	Pipe	A312	TP316L	S31603			8		-425	70	25	16.7	16.7	16.7	15.7
16Cr-12Ni-2Mo	Pipe	A358	316L	S31603			8	(36)	-425	70	25	16.7		16.7	
16Cr-12Ni-2Mo-Ti	Tube	A213	TP316Ti	S31635			8	(30)	-325	75	30	20.0		20.0	
18Cr-10Ni-Ti	Smls. pipe	A312	TP321	S32100		>3/ ₈ thk.		(28)(30)	-425	70	25	16.7		16.7	
18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100		>3/8 thk.	9,	(28)(30) (36)	-425	70	25	16.7	16.7	16.7	16.7
18Cr-10Ni-Ti	Smls. pipe	A312	TP321H	S32109		>3/8 thk.		(30)	-325	70	25	16.7	16.7	16.7	16.7
18Cr-10Ni-Ti	Smls. pipe	A376	TP321H	S32109		> ³ / ₈ thk.	8	(30)(36)	-325	70	25	16.7	16.7	16.7	16.7
25Cr-12Ni		A451	СРН8	J93400			8	(26)(28) (35)	-325	65	28	18.7	18.7	18.5	18.0
25Cr-20Ni		A451	CPK20	J94202	HICK		8	(12)(28) (35)(39)	-325	65	28	18.7	18.7	18.5	18.0
								(00)(01)							
11Cr-Ti	Tube	A268	TP409	\$40900			7	(35)	-20	60	30	20.0			
18Cr-Ti	Tube	A268	TP430Ti	\$43036			7	(35)(49)	-20	60	40	20.0			
16Cr-14Ni-2Mo		A451	CPF10MC	J92971			8	(28)	-325	70	30	20.0			
16Cr-8Ni-2Mo	Pipe	A376	16-8-2H	S16800			8	(26)(31) (35)	-325	75	30	20.0			
12Cr-Al	Tube	A268	TP405	S40500			7	(35)	-20	60	30	20.0	20.0	19.6	19.3
13Cr	Tube	A268	TP410	S41000			6	(35)	-20	60	30	20.0	20.0	19.6	19.3
17Cr	Tube	A268	TP430	S43000			7	(35)(49)	-20	60	35	20.0	20.0	19.6	19.3
18Cr-13Ni-3Mo	Pipe	A312	TP317L	S31703			8		-325	75	30	20.0	20.0	20.0	18.9
25Cr-20Ni	Pipe	A312	TP310	S31009			8	(35)(39)	-325	75	30	20.0	20.0	20.0	20.0
25Cr-20Ni		A358	310S	S31008			8	(28)(35) (36)	-325	75	30	20.0	20.0	20.0	20.0
25Cr-20Ni	Pipe	A409	TP310S	S31008			8	(28)(31) (35)(36)	-325	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Smls. pipe	A312	TP321	S32100		≤3/ ₈ thk.	8	(28)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe	A312	TP321	S32100			8	(28)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe	A358	321	S32100			8	(28)(36)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100	•••	$\leq \frac{3}{8}$ thk.	8	(28)(36)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe	A409	TP321	S32100			8	(28)(36)	-425	75	30	20.0	20.0	20.0	20.0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
																Stai	nless S	Steel —	Pipes	and Tubes	(3)(4a)
	15.2									9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	TP321	A312
16.1	15.2	14.9	14.6	14.3	14.1	13.9	13.8	13.6	13.5	9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	TP321	A376
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	TP304L	A213
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0		TP304L	A269
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	TP304L	A270
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	TP304L	A312
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	304L	A358
140	14.0	127	12 5	122	120	127	12.4	191	110	11.6	11.4	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	TP316L	A213
	14.0									11.6	11.4	o.o 8.8	6.4	4.7	3.5		1.8	1.3	1.0	TP316L	A269
	14.0									11.6	11.4	8.8	6.4	4.7	3.5	2.5 2.5	1.8	1.3	1.0	TP316L	A270
	14.0									11.6	11.4	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	TP316L	A312
	14.0									11.6	11.4	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	316L	A358
	16.8									15.1	12.3	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316Ti	A213
17.0	10.0	20.0	10.2	10.1	10.,	10.0	1017	10.0	10.0	10.1	12.0	,.0	,			0.1	2.0		1.0		
16.1	15.2	14.9	14.6	14.3	14.1	13.9	13.8	13.6	13.5	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321	A312
16.1	15.2	14.9	14.6	14.3	14.1	13.9	13.8	13.6	13.5	12.3	9.1	6.9	5.40	4.1	3.2	2.5	1.9	1.5	1.1	TP321	A376
16.1	15.2	14.9	14.6	14.3	14.1	13.9	13.8	13.6	13.5	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321H	A312
16.1	15.2	14.9	14.6	14.3	14.1	13.9	13.8	13.6	13.5	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321H	A376
17.7	17.1	16.7	16.3	15.9	15.4	14.9	14.4	13.9	11.1	8.5	Q_5	5.0	3.8	2.9	2.3	1.8	1.3	0.9	0.8	СРН8	A451
17.7	17.1	16.7	16.3	15.9	15.4	14.9	14.4	13.9	11.3	9.8	8.5	7.3	6.0	4.8	3.5	2.4	1.6	1.1	0.8	CPK20	A451
										<i>y</i> .											
									<i>\</i> · ·											mp 400	1000
						•••	•••	S	7		•••		•••					•••	•••	TP409	A268 A268
				•••		•••		\mathbf{y}												TP430Ti CPF10MC	A451
				•••		(- ;; -				•••		•••					•••	•••	16-8-2H	A376
						50	<u> </u>													10 0 211	11370
19.0	18.5	18.1	17.7	17.1	16.4	15.6	14.3	8.4	4.0											TP405	A268
19.0	18.5	18.1	17.7	17.1	16.4	15.6	12.3	8.8	6.4	4.4	2.9	1.8	1.0							TP410	A268
19.0	18.5	18.1	17.7	17.1	16.4	15.6	12.0	9.2	6.5	4.5	3.2	2.4	1.8							TP430	A268
17.7	16.9	16.5	16.2	15.8	15.5	15.2														TP317L	A312
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	15.9	9.9	7.1	5.0	3.6	2.5	1.5	0.8	0.5	0.4	0.3	0.2	TP310	A312
	18.5								9.9	7.1	5.0	3.6	2.5	1.5	0.8	0.5	0.4	0.3	0.2	310S	A358
40.0	40.5	40.0	45.0	45.5	45.4	47.0	160	150	0.0	7.1	5 0	2.6	2.5	1.5	0.0	0.5	0.4	0.0	0.2	TD2100	4.400
19.3	18.5	18.2	17.9	17.7	17.4	1/.2	16.9	15.9	9.9	7.1	5.0	3.6	2.5	1.5	0.8	0.5	0.4	0.3	0.2	TP310S	A409
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	TP321	A312
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	TP321	A312
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	321	A358
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	TP321	A376
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	TP321	A409

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Streng		Stre Metal	ic Allov ess, <i>S</i> , k Tempe [Note	ksi, a eratu	t
Nominal	Product	Spec.	Type/	UNS	Class/ Condition/	-	P-No.		Min. Temp.,			Min. Temp.			400
Composition	Form	No.	Grade	No.	Temper	in.	(5)	Notes	°F (6)	Tensile	Yieia	to 100	200	300	400
Stainless Steel —	-		-					(0.0) (0.0)							
23Cr-12Ni	Pipe	A312	TP309				8	(28)(35) (39)	-325	75	30	20.0	20.0	20.0	20.0
23Cr-12Ni		A358	309S	S30908			8	(28)(31) (35)(36)	-325	75	30	20.0	20.0	2 0.0	20.0
18Cr-8Ni		A 4 F 1	CDEO	102600			0	(2()(20)	425	70	20	20:0	20.0	20.0	10.6
		A451	CPF8	J92600	•••		8	(26)(28)	-425		30 30	_ ,			
18Cr-10Ni-Cb	Pipe	A312	TP347	S34700			8		-425	75 75		20.0	20.0		
18Cr-10Ni-Cb	Pipe	A358	347	S34700			8	(30)(36)	-425	75 75	30/30	20.0	20.0		
18Cr-10Ni-Cb	Pipe	A376	TP347	S34700			8	(30)(36)	-425	75		20.0	20.0		
18Cr-10Ni-Cb	Pipe	A409	TP347	S34700			8	(30)(36)	-425	75	30	20.0	20.0		
18Cr-10Ni-Cb	Pipe	A312	TP348	S34800			8		-325	75	30	20.0	20.0		
18Cr-10Ni-Cb	Pipe	A358	348	S34800			8	(30)(36)	-325	75	30	20.0	20.0		
18Cr-10Ni-Cb	Pipe	A376	TP348	S34800			8	(30)(36)	-325	75	30	20.0	20.0		
18Cr-10Ni-Cb	Pipe	A409	TP348	S34800			8	(30)(36)	-325	75	30	20.0	20.0	20.0	20.0
25Cr-12Ni		A451	CPH10	J93402			8	(12)(14) (28)(35) (39)	-325	70	30	20.0	20.0	19.9	19.4
25Cr-12Ni		A451	СРН20	J93402		we.	8	(12)(14) (28)(35) (39)	-325	70	30	20.0	20.0	19.9	19.4
						11/2									
25Cr-20Ni	Pipe	A312	TP310H	S31009	1×0		8	(29)(35) (39)	-325	75	30	20.0	20.0	20.0	20.0
25Cr-20Ni	Pipe	A358	310S	S31008	Jick-		8	(28)(29) (35)(36)	-325	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Cb		A451	CPF8C	J92710			8	(28)	-325	70	30	20.0	20.0	20.0	18.6
18Cr-10Ni-Ti	Smls. pipe	1212	TP321	S32100		≤ ³ / ₈ thk.	0	(28)(30)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe		TR321	S32100	•••	-			-425 -425	75 75	30	20.0	20.0		
			321		•••		8	(28)(30)							
18Cr-10Ni-Ti	Wld. pipe	IN.)	S32100			8	(28)(30) (36)	-425	75	30	20.0	20.0		
18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100	•••	≤3/ ₈ thk.	8	(28)(30) (36)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe	A409	TP321	S32100			8	(28)(30) (36)	-425	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Smls. pipe	A312	TP321H	S32109		$\leq \frac{3}{8}$ thk.	8	(30)	-325	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe	A312	TP321H	S32109			8	(30)	-325	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Wld. pipe	A358	321H	S32109			8	(30)(36)	-325	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Smls. pipe	A376	TP321H	S32109		$\leq \frac{3}{8}$ thk.	8	(30)(36)	-325	75	30	20.0	20.0	20.0	20.0
16Cr-12Ni-2Mo	Tube	A213	TP316	S31600			8	(14)(26) (28)(31) (36)	-425	75	30	20.0	20.0	20.0	19.3
16Cr-12Ni-2Mo	Tube	A269	TP316	S31600			8	(14)(26) (28)(31) (36)	-425	75	30	20.0	20.0	20.0	19.3
16Cr-12Ni-2Mo	Tube	A270	TP316	S31600			8	(14)(26) (28)	-425	75	30	20.0	20.0	20.0	19.3
16Cr-12Ni-2Mo	Pipe	A312	TP316	S31600			8	(26)(28)	-425	75	30	20.0	20.0	20.0	19.3

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
															Stainle	ess Ste	el — Pi	ipes and	d Tube	s (3)(4a)	(Cont'd)
19.4	18.8	18.5	18.2	18.0	17.7	17.5	17.2	16.9	13.8	10.3	7.6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	8.0	TP309	A312
19.4	18.8	18.5	18.2	18.0	17.7	17.5	17.2	16.9	13.8	10.3	7.6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	0.8	3095	A358
175	16.6	162	150	155	152	140	116	112	122	0.5	7 5	6.0	4.0	2.0	2.2	2.7	2.2	2.0	h 7 .	CDEO	A451
	16.6	19.0								9.5	7.5	6.0	4.8	3.9	3.3	2.7	2.3		<i></i>	CPF8	
20.0									16.0	12.1 12.1	9.1 9.1	6.1	4.4 4.4	3.3	2.2	1.5	1.2	0.9	0.8	TP347 347	A312 A358
20.0	19.3								16.0			6.1				1.5	1.2	0.9			
	19.3								16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	7	0.8	TP347	A376
	19.3								16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	12	0.9	0.8	TP347	A409
	19.3								16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5 1.5	1.2	0.9	0.8	TP348	A312
20.0		19.0							16.0	12.1	9.1	6.1	4.4	3.3	2.2	()	1.2	0.9	0.8	348	A358
	19.3								16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	TP348	A376
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	8.0	TP348	A409
18.9	18.3	17.9	17.5	17.0	16.5	16.0	15.4	14.9	11.1	8.5	6.5	5.0	3.8	439	2.3	1.8	1.3	0.9	0.8	CPH10	A451
18.9	18.3	17.9	17.5	17.0	16.5	16.0	15.4	14.9	11.1	8.5	6.5	5.0	3.8	2.9	2.3	1.8	1.3	0.9	0.8	CPH20	A451
											i	10									
	18.5									10.3	7 6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	0.8	TP310H	A312
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	16.7	13.8	10.3	7.6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	0.8	310S	A358
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	8.0	CPF8C	A451
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321	A312
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321	A312
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	321	A358
19.3	18.3	17.8	17.5	17,2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321	A376
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321	A409
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321H	A312
	18.3									12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	TP321H	A312
		~)								12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5		321H	A358
	X								16.2		9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5		TP321H	A376
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316	A213
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316	A269
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316	A270
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316	A312

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Numbers	ii i urentiie	Ses Rei	er to Note	S IOI TIP	penaix A 13	ubics, s	peem	actions m	<u> </u>	Specifie Strengt	d Min.	Bas Stre Metal	ic Allowab ess, S, ksi, Temperat [Note (1)]	at ure,
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No.	Notes	Min. Temp., °F (6)	Tensile	Viold	Min. Temp. to 100	200 300	400
Stainless Steel — Pi				NO.	remper	111.	(3)	Notes	r (0)	Telisile	Heiu	10 100	200 300	400
16Cr-12Ni-2Mo	Pipe	A358	316	S31600			8	(26)(28) (31)(36)	-425	75	30	20.0	20.0 20.0	19.3
16Cr-12Ni-2Mo	Pipe	A376	TP316	S31600			8	(26)(28) (31)(36)	-425	75	30	20.0	20.0 20.0	19.3
16Cr-12Ni-2Mo	Pipe	A409	TP316	S31600			8	(26)(28) (31)(36)	-425	75	30	20.0	20.0 20.0	19.3
18Cr-13Ni-3Mo	Pipe	A312	TP317	S31700			8	(26)(28)	-325	75	30	20.0	20.0 20.0	19.3
18Cr-13Ni-3Mo	Pipe	A409	TP317	S31700			8	(26)(28) (31)(36)	-325	75	30)	20.0	20.0 20.0	19.3
16Cr-12Ni-2Mo	Pipe	A376	ТР316Н	S31609			8	(26)(31) (36)	-325	75	30	20.0	20.0 20.0	19.3
16Cr-12Ni-2Mo	Pipe	A312	ТР316Н	S31609			8	(26)	-325	75	30	20.0	20.0 20.0	19.3
18Cr-10Ni-Cb	Pipe	A376	TP347H	S34709			8	(30)(36)	-325	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A312	TP347	S34700			8	(28)	-425	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A358	347	S34700			8	(28)(30) (36)	-425	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A376	TP347	S34700			1810	(28)(30) (36)	-425	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A409	TP347	S34700		"ien	8	(28)(30) (36)	-425	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A312	TP348	S34800		7.	8	(28)	-325	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A358	348	S34800			8	(28)(30) (36)	-325	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A376	TP348	S34800			8	(28)(30) (36)	-325	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A409	TP348	S34800			8	(28)(30) (36)	-325	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A312	TP347H	\$34709			8		-325	75	30	20.0	20.0 20.0	20.0
18Cr-10Ni-Cb	Pipe	A312	TP348H	S34809			8		-325	75	30	20.0	20.0 20.0	20.0
18Cr-8Ni	Tube	A213	TP304	S30400			8	(14)(26) (28)(31) (36)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Tube	A269	TP304	S30400			8	(14)(26) (28)(31) (36)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Tube	A270	TP304	S30400			8	(14)(26) (28)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Pipe	A312	TP304	S30400			8	(26)(28)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Pipe	A358	304	S30400			8	(26)(28) (31)(36)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Pipe	A376	TP304	S30400			8	(20)(26) (28)(31) (36)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Pipe	A376	TP304H	S30409			8	(26)(31) (36)	-325	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Pipe	A409	TP304	S30400			8	(26)(28) (31)(36)	-425	75	30	20.0	20.0 20.0	18.6
18Cr-8Ni	Pipe	A312	TP304H	S30409			8	(26)	-325	75	30	20.0	20.0 20.0	18.6
18Cr-12Ni-2Mo		A451	CPF8M	J92900			8	(26)(28)	-425	70	30	20.0	20.0 18.9	17.0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
															Stainle	ss Stee	l — Pi	pes and	d Tube	s (3)(4a)	(Cont'd)
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	316	A358
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316	A376
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316	A409
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7_	1.3	TP317	A312
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP317	A409
10.0	17.0	16.6	16 2	161	150	157	15 6	15 4	15 2	151	124	0.0	7.4		4.1	2.1	2.2	17	1.2	TD21611	1276
18.0	17.0	10.0	10.3	10.1	15.9	15./	15.0	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316H	A376
																9.5					
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	TP316H	A312
															N						
20.0	19.3									17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP347H	A376
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP347	A312
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	347	A358
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	N.S.	5.9	4.4	3.2	2.5	1.8	1.3	TP347	A376
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP347	A409
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP348	A312
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	348	A358
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP348	A376
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18,1	ر 17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP348	A409
200	400	400	40.	40 =	400	400	40.4		1	45.4		40.5	7 .0	.		0.0	0.5	4.0	4.0	mpo 4511	1010
20.0	19.3							\sim		17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP347H	A312
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	TP348H	A312
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304	A213
					N																
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304	A269
			_	\mathcal{O}																	
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304	A270
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304	A312
	16.6									12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	304	A358
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304	A376
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	ТР304Н	A376
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304	A409
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	TP304H	A312
	15.0									11.5	8.9	6.9	5.4	4.3	3.4	2.8	2.3	1.9		CPF8M	A451

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	c Allo ss, S, I Temp [Note	ksi, a eratu	t
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300	400
Stainless Steel — Pipe	s and Tube	es <mark>(3)(4</mark> a	a)												
44Fe-25Ni-21Cr-Mo	Tube	A249		N08904			45		-325	71	31	20.7	20.7	20.4	18.7
44Fe-25Ni-21Cr-Mo	Pipe	A312	•••	N08904			45		-325	71	31	20.7	20,7	20.4	18.7
20Cr-Cu	Tube	A268	TP443	S44300			a	(7)(35)	-20	70	40	23.3	23.3	23.3	23.3
27Cr	Tube	A268	TP446-1	S44600			10I	(35)	-20	70	40	23.3	23.3	22.5	21.9
12Cr	Wld. pipe	A1053	50	S41003			7		-20	70	50	23.3	23.3	23.3	22.8
25Cr-8Ni-N		A451	CPE20N	J92802			8	(35)(39)	-325	80	40	26.7	26.7	26.7	26.7
23Cr-4Ni-Mo-Cu-N		A789		S32304			10H	(25)	-60	87	58	29.0	27.9	26.1	24.7
23Cr-4Ni-Mo-Cu-N		A790		S32304 S32304			10H	(25)	-60	87	58	29.0	27.9		
23Cr-4Ni-Mo-Cu-N	 Wld. pipe		2304	S32304 S32304			10H	(25)	-6 0	87	58	29.0	27.9		
			2301						^{7′} O,	•					
20Cr-18Ni-6Mo	Pipe	A813		S31254			8	(8)	-325	94	44	29.3	29.3		
20Cr-18Ni-6Mo	Pipe	A814		S31254			8	(8)	-325	94	44	29.3	29.3	28.9	26.7
13Cr		A426	CPCA15	J91150			6	(10)(35)	-20	90	65	30.0			
20Cr-18Ni-6Mo	Wld. pipe	A358		S31254		>3/16	8 0		-325	95	45	30.0	30.0	30.0	27.4
20Cr-18Ni-6Mo	Wld pipe			S31254		≤ ³ / ₁₆	8		-325	100	45	30.0	30.0		
000 FW 0M W		4.500		004000		.en	4.011	(05)		0.0		20.0	00.0	20.0	07.0
22Cr-5Ni-3Mo-N		A789		S31803		7/	10H	(25)	-60	90	65	30.0	30.0		
22Cr-5Ni-3Mo-N		A790		S31803	XO		10H	(25)	-60	90	65	30.0	30.0		
22Cr-5Ni-3Mo-N	Wld pipe	A928		S31803			10H	(25)	-60	90	65	30.0	30.0	28.9	27.8
20Cr-18Ni-6Mo	Tube	A249		S31254		$>^3/_{16}$ thk.	8	(8)	-325	95	45	30.0	30.0	29.5	27.3
20Cr-18Ni-6Mo	Tube	A249		S31254	.	\leq ³ / ₁₆ thk.	8	(8)	-325	98	45	30.0	30.0	29.5	27.3
20Cr-18Ni-6Mo	Pipe	A312		S31254		$>^3/_{16}$ thk.	8	(8)	-325	95	45	30.0	30.0	29.5	27.3
20Cr-18Ni-6Mo	Pipe	A312	ے ۔۔	\$31254		$\leq \frac{3}{16}$ thk.	8	(8)	-325	98	45	30.0	30.0	29.5	27.3
26Cr-4Ni-Mo		A789		S32900			10H	(25)	-20	90	70	30.0			
26Cr-4Ni-Mo		A790	\odot	S32900			10H	(25)	-20	90	70	30.0			
46Fe-24Ni-21Cr-6Mo-	Smls. & wld. pipe	A312		N08367		>3/16	45	(26)	-325	95	45	30.0	30.0	29.9	28.6
Cu-N 46Fe-24Ni-21Cr-6Mo-				N08367		>3/16	45	(26)	-325	95	45	30.0	30.0	29.9	28.6
Cu-N 46Fe-24Ni-21Cr-6Mo-	Wld. pipe	A813		N08367		>3/16	45	(26)	-325	95	45	30.0	30.0	29.9	28.6
Cu-N 46Fe-24Ni-21Cr-6Mo- Cu-N	Wld. pipe	A814		N08367		>3/16	45	(26)	-325	95	45	30.0	30.0	29.9	28.6
46Fe-24Ni-21Cr-6Mo- Cu-N	Smls. & wld. pipe	A312		N08367		≤ ³ / ₁₆	45	(26)	-325	100	45	30.0	30.0	30.0	29.6
46Fe-24Ni-21Cr-6Mo- Cu-N	Wld. pipe	A358		N08367		≤³/ ₁₆	45	(26)	-325	100	45	30.0	30.0	30.0	29.6
46Fe-24Ni-21Cr-6Mo- Cu-N	Wld. pipe	A813		N08367		≤ ³ / ₁₆	45	(26)	-325	100	45	30.0	30.0	30.0	29.6
46Fe-24Ni-21Cr-6Mo- Cu-N	Wld. pipe	A814		N08367		≤ ³ / ₁₆	45	(26)	-325	100	45	30.0	30.0	30.0	29.6
21Cr-5Mn-1 ¹ / ₂ Ni-Cu-N	Tube	A789		S32101		>3/16	10H	(25)	-20	94	65	31.3	31.3	29.8	28.5
21Cr-5Mn-1 ¹ / ₂ Ni-Cu-N	Pipe	A790		S32101		>3/16	10H	(25)	-20	94	65	31.3	31.3	29.8	28.5

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350 1	1,400	1,450	1,500	Type/ Grade	Spec. No.
															Stainle	ss Steel	— Р	ipes and	l Tube	s (3)(4a)	(Cont'd)
17.1																					A249
17.1																				V	A 312
23.3	23.3	14.6	12.5	10.7	9.2	7.9	5.9	4.0	2.5											TP443	A268
21.5	20.9	20.6	20.2	19.7	19.1	18.4	17.5	16.4	15.1										Ϋ́. 	TP446-1	A268
22.1	21.2																		5 .	50	A1053
26.7	26.7	26.7	26.7	26.7	26.7	26.7	26.7													CPE20N	A451
22.9	19.2																	7,"			A789
22.9	19.2															D					A790
22.9	19.2															9,				2304	A928
25.2	24.1	23.8	23.6	23.4	23.2	23.0															A813
25.2	24.1	23.8	23.6	23.4	23.2	23.0								<	5.7						A814
														<i>(9)</i> ,						CPCA15	A426
	24.7												1/1/6								A358
	24.7	24.3	24.1	23.9	23.7	22.8						NOW	<u>~</u>								A358
27.2			•••			•••					7	/=									A789
27.2									•••		vO.						•••				A790
	26.9									15,,	¥	•••	•••	•••							A928
25.8		24.3							(•••							A249
25.8		24.3							۸.												A249
25.8		24.3						1	7,												A312
25.8	24.7	24.3	24.1	23.9	23.7	23.0								•••						•••	A312
							J.														A789 A790
27.7	26.2	25.7	25.1	24.7	243	20														•••	A312
	26.2			_Q	72																A358
	26.2		1	2																	A813
27.7	26.2	25 7	25.1	24.7	24.3																A814
	P	× -																			
27.7	26.2	25.7	25.1	24.7	24.3						•••			•••							A312
27.7	26.2	25.7	25.1	24.7	24.3																A358
27.7	26.2	25.7	25.1	24.7	24.3																A813
27.7	26.2	25.7	25.1	24.7	24.3																A814
28.5	28.5																				A789
28.5																					A790

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	ic Allowab ess, S, ksi, Temperat [Note (1)	at ure,
					Class/				Min.		, -	Min.	1 222 ().	
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Size, in.	P-No. (5)	Notes	Temp., °F (6)	Tensile	Vield	Temp. to 100	200 300	400
Stainless Steel — Pipe				1101	remper	****	(0)	Hotes	1 (0)	Tensile	Ticiu	10 100	200 300	100
22Cr-5Ni-3Mo-N	Tube	A789	2205	S32205			10H	(25)	-60	95	70	31.7	31.7 30.6	5 29.4
22Cr-5Ni-3Mo-N	Pipe	A790	2205	S32205			10H	(25)	-60	95	70	31.7	31,730.6	5 29.4
21Cr-5Mn-1 ¹ / ₂ Ni-Cu-N	Tube	A789		S32101		≤ ³ / ₁₆	10H	(25)	-20	101	77	33.7	33.7 32.1	31.0
21Cr-5Mn-1½Ni-Cu-N	Pipe	A790		S32101		≤ ³ / ₁₆	10H	(25)	-20	101	77	33.7	33.7 32.1	31.0
21Cr-3½Ni-1¾Mo-N		A789		S32003		>0.187 thk.	10H	(25)	-60	95	65	31:7	30.7 28.9	28.6
21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N		A790		S32003		>0.187 thk.	10H	(25)	-60	95	65	31.7	30.7 28.9	28.6
21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N	Wld pipe	A928		S32003		>0.187 thk.	10H	(25)	-60	95	65	31.7	30.7 28.9	28.6
22Cr-5Ni-3Mo-N	Wld pipe	A928	2205	S32205			10H	(25)	-60	95	65	31.7	31.7 30.6	5 29.4
24Cr-4Ni-3Mn- 1.5Mo-N	Smls. & wld. tube	A789		S82441		≥0.40 thk.	10H	(25)	-60	99	70	32.9	32.9 32.9	32.9
24Cr-4Ni-3Mn- 1.5Mo-N	Smls. & wld. pipe	A790		S82441		≥0.40 thk.	10H	(25)	-60	99	70	32.9	32.9 32.9	32.9
21Cr-3½Ni-1¾Mo-N		A789		S32003		≤0.187 thk.	10H	(25)	-60	100	70	33.3	32.3 30.4	30.1
21Cr-3½Ni-1¾Mo-N		A790		S32003		≤0.187 thk.	10 P	(25)	-60	100	70	33.3	32.3 30.4	30.1
21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N	Wld. pipe	A928		S32003		≤0.187 thk,	10H	(25)	-60	100	70	33.3	32.3 30.4	30.1
24Cr-4Ni-3Mn- 1.5Mo-N	Smls. & wld. tube	A789		S82441		<0.40 thk.	10H	(25)	-60	107	78	35.8	35.8 35.8	35.8
24Cr-4Ni-3Mn- 1.5Mo-N	Smls. & wld. pipe	A790		S82441	ick to	<0.40 thk.	10H	(25)	-60	107	78	35.8	35.8 35.8	35.8
25Cr-8Ni-3Mo- W-Cu-N		A789		S32760	<u>ن</u>		10H	(25)	-60	109	80	36.3	35.9 34.4	34.0
25Cr-8Ni-3Mo- W-Cu-N		A790		\$32760			10H	(25)	-60	109	80	36.3	35.9 34.4	34.0
29Cr-6.5Ni-2Mo-N	Tube	A789	ري. م	S32906		≥0.40 thk.	10H	(25)	-60	109	80	36.3	36.3 34.0	33.5
29Cr-6.5Ni-2Mo-N	Pipe	A790	<u></u>	S32906		≥0.40 thk.	10H	(25)	-60	109	80	36.3	36.3 34.0	33.5
24Cr-17Ni-6Mn- 4½Mo-N	O	A358		S34565			8	(36)	-325	115	60	38.3	38.1 35.8	34.5
25Cr-7Ni-4Mo-N	Smls. & wld. tube	A789		S32750			10H	(25)	-60	116	80	38.7	38.5 36.4	35.1
25Cr-7Ni-4Mo-N	Smls. & wld. pipe	A790	2507	S32750			10H	(25)	-60	116	80	38.7	38.5 36.4	35.1
25Cr-7Ni-4Mo-N	Wld. pipe		2507	S32750			10H	(25)	-60	116	80	38.7	38.5 36.4	35.1
29Cr-6.5Ni-2Mo-N	Tube	A789		S32906		<0.40 thk.	10H	(25)	-60	116	94	38.7	38.6 36.8	35.6
29Cr-6.5Ni-2Mo-N	Pipe	A790		S32906		<0.40 thk.	10H	(25)	-60	116	94	38.7	38.6 36.8	35.6
Stainless Steel — Plate	es and She	ets (3)f	4a)											
18Cr-11Ni		A240	305	S30500			8	(26)(36) (39)	-325	70	25	16.7		
12Cr-Al		A240	405	S40500			7	(35)	-20	60	25	16.7	15.3 14.8	3 14.5

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350 1	1,400	1,450	1,500	Type/ Grade	Spec. No.
															Stainle	ss Steel	— Pi	pes and	l Tube:	s (3)(4a)	(Cont'd)
28.7	28.4																			2205	A789
28.7	28.4		•••																	2205	A790
30.9	30.9																			~O`	A789
30.9	30.9																				A790
28.6	28.6	28.6																	کر آ		A789
28.6	28.6	28.6																			A790
28.6	28.6	28.6															S				A928
28.7	28.4	28.3														P				2205	A928
32.9	32.8																				A789
32.9	32.8														-OK						A790
	30.1			•••											5~						A789
30.1	30.1	30.1		•••	•••		•••	•••		•••		•••		زرن کا			•••		•••	•••	H/07
30.1	30.1	30.1											W.								A790
30.1	30.1	30.1										N									A928
35.8	35.7										3	16									A789
35.8	35.7									45,,					•••				•••		A790
34.0	34.0								, "C) <u>"</u>											A789
34.0	34.0							O													A790
33.0	33.0						٠,٠														A789
33.0	33.0				711	50															A790
33.8	33.2	33.1	32.7	32.4	32.0																A358
34.5	34.3																				A789
34.5	34.3	حيالي																		2507	A790
34.5	34.3																	•••		2507	A928
35.2	35.2																	•••			A789
35.2	35.2																				A790
																Stainl 	ess St 	eel — F	lates a	and Sheet: 305	s (3)(4a) A240
14.3	14.0	13.8	13.5	13.1	12.6	12.0	11.3	8.4	4.0											405	A240

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	ic Allowa ss, <i>S</i> , ks Temper [Note (1	i, at ature,
Nominal Composition	Product	-	Type/ Grade	UNS	Class/ Condition/ Temper	Size,	P-No.	Notes	Min. Temp., °F (6)	Tensile	Viold	Min. Temp.	200 30	00 400
Composition Stainless Steel — Plat	Form tes and She	No.		No.	remper	in.	(5)	Notes	r (0)	Telisile	rieiu	10 100	200 30	00 400
Stanness Steel Tia	ics und sinc		,											
18Cr-8Ni		A240	304L	S30403			8	(36)	-425	70	25	16.7	16.701	5.7 15.8
16Cr-12Ni-2Mo		A240	316L	S31603			8	(36)	-425	70	25	16.7	16.7 16	5.7 15.7
18Cr-Ti		A240	439	S43035				(35)	-20	60	30	20:0		
18Cr-8Ni		A240	302	S30200			8	(26)(36)	-325	75	30	20.0	20.0 20	0.0 18.6
12Cr-1Ni		A1010	40	S41003			7		-20	66	40	22.0	22.0 22	0 21.5
12Cr-1Ni		A1010	50	S41003			7		-20	70	50	23.3	23.3 23	
									, ŏ					
13Cr		A240	410S	S41008			7	(35)(50)	-20	60	30	20.0	18.4 17	
13Cr		A240	410	S41000	•••		6	(35)	-20	65	30	20.0	18.4 17	
15Cr	•••	A240	429	S42900	•••		6	(35)	-20	65	30	20.0	18.4 17	
17Cr		A240	430	S43000			7	(35)	-20	65	30	20.0	18.4 17	.8 17.4
18Cr-13Ni-3Mo		A240	317L	S31703			18/	(36)	-325	75	30	20.0	20.0 20	0.0 18.9
25Cr-20Ni		A240	310S	S31008	 xO	ijen	8	(28)(31) (35)(36)	-325	75	30	20.0	20.0 20	0.0 20.0
18Cr-10Ni-Ti	Plate, sheet, strip	A240	321	S32100	lick		8	(28)(31) (36)	-325	75	30	20.0	20.0 20	0.0 20.0
23Cr-12Ni		A240	309S	\$30908			8	(28)(35) (36)	-325	75	30	20.0	20.0 20	0.0 20.0
18Cr-10Ni-Cb		A240	347	S34700			8	(36)	-425	75	30	20.0	20.0 20	0.0 20.0
18Cr-10Ni-Cb		A240	348	S34800			8	(36)	-325	75	30	20.0	20.0 20	0.0 20.0
25Cr-20Ni	0	A240	310S	S31008			8	(28)(29) (35)(36)	-325	75	30	20.0	20.0 20	0.0 20.0
18Cr-10Ni-Ti	Plate, sheet, strip	A240	321	S32100			8	(28)(30) (36)	-325	75	30	20.0	20.0 20	0.0 20.0
18Cr-10Ni-Ti	Plate, sheet, strip	A240	321Н	S32109			8	(30)(36)	-325	75	30	20.0	20.0 20	0.0 20.0
16Cr-12Ni-2Mo		A240	316	S31600			8	(26)(28) (36)	-425	75	30	20.0	20.0 20	0.0 19.3
18Cr-13Ni-3Mo		A240	317	S31700			8	(26)(28) (36)	-325	75	30	20.0	20.0 20	0.0 19.3
18Cr-10Ni-Cb		A240	347	S34700			8	(28)(36)	-425	75	30	20.0	20.0 20	0.0 20.0
18Cr-10Ni-Cb		A240	348	S34800			8	(28)(36)	-325	75	30	20.0		0.0 20.0
18Cr-8Ni		A240	304	S30400			8	(26)(28) (36)	-425	75	30	20.0	20.0 20	0.0 18.6

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
									,	,,,,,,,	,	,	,							s (3)(4a)	
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	304L Q	A240
14.8	14.0	13.7	13.5	13.2	12.9	12.7	12.4	12.1	11.8	10.8	10.2	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	316L	A240
																			0) "	
																			5	439	A240
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0									(/ ^V		302	A240
20.8	20.0																CA			40	A1010
22.1			•••					•••			•••									50	A1010
22.1	21.2															Ó				30	A1010
17.2	16.8	16.6	16.2	15.7	15.1	14.4	12.3	8.8	6.4	4.4	2.9	1.8	1.0							410S	A240
17.2	16.8	16.6	16.2	15.7	15.1	14.4	12.3	8.8	6.4	4.4	2.9	1.8	1.0		0°					410	A240
17.2	16.8	16.6	16.2	15.7	15.1	14.4	12.0	9.2	6.5	4.5	3.2	2.4	1.8	11	Υ					429	A240
17.2	16.8	16.6	16.2	15.7	15.1	14.4	12.0	9.2	6.5	4.5	3.2	2.4	1.8	(9),						430	A240
17.7	16.9	16.5	16.2	15.8	15.5	15.2							XUO							317L	A240
												N									
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	15.9	9.9	7.1	5.0	3.6	2.5	1.5	8.0	0.5	0.4	0.3	0.2	310S	A240
											xO	•									
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	321	A240
									Ö	110.											
									. •)											
19.4	18.8	18.5	18.2	18.0	17.7	17.5	17.2	16.9	13.8	10.3	7.6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	0.8	309S	A240
								Ö,													
) 													
20.0		19.0				()	_			12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	347	A240
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	8.0	348	A240
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	16.7	13.8	10.3	7.6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	0.8	310S	A240
				Q_{χ}																	
			15	7																	
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	321	A240
	7	5																			
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	321H	A240
4.5.																					
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	316	A240
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	317	A240
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	347	A240
										17.4		10.5	7.9	5.9	4.4	3.2	2.5	1.8			A240
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	304	A240

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	ic Allowa ess, <i>S</i> , ksi Tempera [Note (1	, at ature,
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200 30	00 400
Stainless Steel — Plate	es and She	ets (3)(4a)		-									
44Fe-25Ni-21Cr-Mo		A240	904L	N08904			45		-325	71	31	20.7	20.7~20	.4 18.7
23Cr-4Ni-Mo-Cu-N		A240	2304	S32304			10H	(25)	-60	87	58	29.0	27.9 26	.1 24.7
22Cr-5Ni-3Mo-N		A240		S31803			10H	(25)	-60	90	65	30.0	300 28	
16Cr-4Ni-6Mn		A240	201LN	S20153			8		-325	95	45	30.0	27.6 24	.7 23.4
20Cr-18Ni-6Mo		A240		S31254		>3/ ₁₆ thk.	8	(8)	-325	95	45	30.0	30.0 29	.5 27.3
20Cr-18Ni-6Mo		A240		S31254		≤ ³ / ₁₆ thk.		(8)	-325	98	45	30.0	30.0 29	.5 27.3
46Fe-24Ni-21Cr-6Mo- Cu-N		A240		N08367		>3/16	45	(26)	-325	95	45	30.0	30.0 29	
46Fe-24Ni-21Cr-6Mo- Cu-N	Sheet & strip	A240		N08367		≤ ³ / ₁₆	45	(26)	-325	100	45	30.0	30.0 30	.0 29.6
21Cr-5Mn-1 ¹ / ₂ Ni-Cu-N		A240		S32101		>3/ ₁₆ thk.	10H	(25)	-20	94	65	31.3	31.3 29	8 28.5
24Cr-4Ni-3Mn-		A240		S82441		≥0.40	10H	(25)	-60	99	70	32.9	32.9 32	
1.5Mo-N						thk.)					
21Cr-5Mn-1½Ni-Cu-N		A240		S32101		\leq ³ / ₁₆ thk.		(25)	-20	101	77	33.7	33.7 32	
22Cr-5Ni-3Mo-N		A240	2205	S32205			10H	(25)	-60	95	65	31.7	31.7 30	
21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N		A240		S32003	•••	>0.187 thk.	10H	(25)	-60	95	65	31.7	30.7 28	.9 28.6
21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N		A240		S32003		≤0.187 thk.	10H	(25)	-60	100	70	33.3	32.3 30	.4 30.1
24Cr-4Ni-3Mn- 1.5Mo-N		A240		S82441		<0.40 thk.	10H	(25)	-60	107	78	35.8	35.8 35	.8 35.8
29Cr-6.5Ni-2Mo-N		A240		S32906		≥0.40 thk.	10H	(25)	-60	109	80	36.3	36.3 34	.5 33.5
29Cr-6.5Ni-2Mo-N		A240		S32906		<0.40 thk.	10H	(25)	-60	116	94	38.7	38.6 36	.8 35.6
				1.										
25Cr-8Ni-3Mo- W-Cu-N		A240		\$32760			10H	(25)	-60	109	80	36.3	36.3 34	.8 34.0
25Cr-7Ni-4Mo-N		A240	2507	S32750			10H	(25)	-60	116	80	38.7	38.5 36	.4 35.1
Stainless Steel — Forg	ings and I	ittings	3)(4a)											
18Cr-13Ni-3Mo		A182	F317L	S31703		≤5 thk.	8	(9)(21a)	-325	70	25	16.7	16.7 16	.7 15.7
18Cr-8Ni		A182	F304L	S30403			8	(9)(21a)	-425	70	25	16.7	16.7 16	.7 15.8
18Cr-8Ni	CHO	A403	WP304L	S30403			8	(32)(37)	-425	70	25	16.7	16.7 16	5.7 15.8
16Cr-12Ni-2Mo		A182	F316L	S31603			8	(9)(21a)	-425	70	25	16.7	167 16	.7 15.7
16Cr-12Ni-2Mo		A403	WP316L	S31603			8	(32)(37)	-425	70	25	16.7		.7 15.7
10C1-12N1-2M0		A403	WF310L	331003			O	(32)(37)	-423	70	23	10.7	10.7 10	/ 13./
20Ni-8Cr		A182	F10	S33100			8	(26)(28) (39)	-325	80	30	20.0		
18Cr-13Ni-3Mo		A403	WP317L	S31703			8	(32)(37)	-325	75	30	20.0	20.0 20	0.0 18.9
25Cr-20Ni		A182	F310H	S31009			8	(9)(35) (39)	-325	75	30	20.0	20.0 20	0.0 20.0
25Cr-20Ni		A403	WP310	S31008			8	(28)(32) (35)(37) (39)	-325	75	30	20.0	20.0 20	0.0 20.0

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
															Stainles	s Steel	— P	lates and	Sheet	ts (3)(4a)	(Cont'd)
17.1																				904L	A240
22.9	19.2																			2304	A240
27.2	26.9																				A240
23.0	22.9	22.8	22.6	22.3	21.8	21.5													C	201LN	A240
25.8	24.7	24.3	24.1	23.9	23.7	23.6													A		A240
25.8	24.7																	0	5		A240
27.7	26.2	25.7	25.1	24.7	24.3		•••											7. V			A240
27.7	26.2	25.7	25.1	24.7	24.3												S				A240
28.5	28.5															12					A240
32.9	32.8														(,	O.					A240
															O						
30.9	30.9														Qv						A240
28.7	28.4					•••	•••				•••	•••		11						2205	A240
28.6	28.6	28.6	•••	•••		•••	•••							KO.							A240
30.1	30.1	30.1							•••		•••		ille					•••			A240
35.8	35.7											1107						•••			A240
											NO.										
33.0	33.0					•••			•••	*			•••								A240
35.2	35.2								(A240
33.9	33.9								7.												A240
33.7	33.7		•••	•••	•••	•••	···	\mathbf{Q}		•••	•••	•••	•••				•••				AZTO
34.5	34.3					(٠,													2507	A240
						\sim									Si	tainless	Stee	l — Forgi	ings a	nd Fitting	
14.8	14.0	13.7	13.5	13.2	12.9	12.7	•••	•••	•••	•••	•••	•••	•••	•••					•••	F317L	A182
14.7	14.0	13.7	13.5	13,3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	F304L	A182
14.7	14.0	13.7	13.5	13.3	13.0	12.8	12.6	12.3	12.0	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	WP304L	A403
		. 1	(V)																		
14.8	14.0	13.7	13.5	13.2	12.9	12.7	12.4	12.1	11.8	10.8	10.2	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	F316L	A182
14.8	14.0	13.7	13.5	13.2	12.9	12.7	12.4	12.1	11.8	10.8	10.2	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	WP316L	A403
	`																				
																				F10	A182
17.7	16.9	16.5	16.2	15.8	15.5	15.2														WP317L	A403
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	15.9	9.9	7.1	5.0	3.6	2.5	1.5	0.8	0.5	0.4	0.3	0.2	F310H	A182
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	15.9	9.9	7.1	5.0	3.6	2.5	1.5	0.8	0.5	0.4	0.3	0.2	WP310	A403

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	ic Allowal ss, <i>S</i> , ksi, Tempera [Note (1)	at ture,
Nominal Composition	Product Form	Spec.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No.	Notes	Min. Temp., °F (6)	Tensile	•	Min. Temp.	200 300	
Stainless Steel — Fe	orgings and	Fittings	(3)(4a)											
18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100		>3/ ₈ thk.	8	(28)	-325	70	25	16.7	16,7 16.	7 16.7
18Cr-10Ni-Ti	Forgings	A182	F321	S32100			8	(9)(21) (28)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100		≤3/ ₈ thk.	8	(28)	-325	75	30	20:0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Wld. fittings	A403	WP321	S32100			8	(28)	-325	75	30	20.0	20.0 20.	0 20.0
23Cr-12Ni		A403	WP309	S30900			8	(28)(32) (35)(37) (39)	-325	75	30	20.0	20.0 20.	0 20.0
25Cr-20Ni		A182	F310H	S31009			8	(9)(21) (29)(35) (39)	-325	75	30	20.0	20.0 20.	0 20.0
25Cr-20Ni		A403	WP310	S31008			8	(28)(29) (32)(35) (37)(39)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A182	F347	S34700			8	(9)(21)	-425	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A403	WP347	S34700			8	(32)(37)	-425	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A182	F348	S34800		,	8	(9)(21)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A403	WP348	S34800			8	(32)(37)	-325	75	30	20.0	20.0 20.	0 20.0
						ile		C X 7						
18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100	140	>3/8 thk.	8	(28)(30)	-325	70	25	16.7	16.7 16.	7 16.7
18Cr-10Ni-Ti	Smls. fittings	A403	WP321H	S32109	HICK	>3/ ₈ thk.	8	(30)	-325	70	25	16.7	16.7 16.	7 16.7
18Cr-10Ni-Ti	Forgings	A182	F321	S32100)		8	(9)(21) (28)(30)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Forgings	A182	F321H	\$32109			8	(9)(21)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Smls. fittings	A403	WP321	\$32100		≤3/ ₈ thk.	8	(28)(30)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Smls. fittings	A403	WP321H	S32109		≤3/ ₈ thk.	8	(30)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Wld.	A403	WP321	S32100			8	(28)(30)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Ti	Wld. fittings	A403	WP321H	S32109			8	(30)	-325	75	30	20.0	20.0 20.	0 20.0
16Cr-12Ni-2Mo	ME	A403	WP316H	S31609			8	(26)(32) (37)	-325	75	30	20.0	20.0 20.	0 19.3
16Cr-12Ni-2Mo		A182	F316H	S31609			8	(9)(21) (26)	-325	75	30	20.0	20.0 20.	0 19.3
18Cr-10Ni-Cb		A403	WP347H	S34709			8	(32)(37)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A182	F347	S34700			8	(9)(21) (28)	-425	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A403	WP347	S34700			8	(28)(32) (37)	-425	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A182	F348	S34800			8	(9)(21) (28)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A403	WP348	S34800			8	(28)(32) (37)	-325	75	30	20.0	20.0 20.	0 20.0
18Cr-10Ni-Cb		A182	F347H	S34709			8	(9)(21)	-325	75	30	20.0	20.0 20.	0 20.0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
									-	-					_					s (3)(4a)	(Cont'd)
16.1	15.2	140	116	142	141	120	120	126	12 5	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	WP3219	A403
10.1	13.2	14.7	14.0	14.5	14.1	13.9	13.0	13.0	13.3	7.0	0.7		3.0	2.0	1.7	1.1	0.0		0.5	0	
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	F321	A182
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	WP321	A403
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	WP321	A403
19.4	18.8	18.5	18.2	18.0	17.7	17.5	17.2	16.9	13.8	10.3	7.6	5.5	4.0	3.0	2.2	1.7	1.3	1.0	0.8	WP309	A403
																. 1	S)				
19.3	18.5	18.2	17.9	17.7	17.4	17.2	16.9	16.7	13.8	10.3	7.6	5.5	4.0	3.0	2.2	¹ ^X	1.3	1.0	8.0	F310H	A182
10.2	18.5	10 2	170	177	174	172	160	167	12 0	10.3	7.6	5.5	4.0	2.0	S	1.7	1.3	1.0	0.8	WP310	A403
19.3	10.5	10.2	17.9	17.7	17.4	17.2	10.9	10.7	13.0	10.5	7.0	5.5	4.0	3.0	\	1./	1.3	1.0	0.0	WP310	A403
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	F347	A182
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.80	3.3	2.2	1.5	1.2	0.9	8.0	WP347	A403
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	8.0	F348	A182
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	8.0	WP348	A403
16.1	15.2	14.9	14.6	14.3	14.1	13.9	13.8	13.6	13.5	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	WP321	A403
16.1	152	140	14.6	142	141	120	12.0	12.6	10.5	127	0.1	6.0	F 4	4.1	2.2	2.5	1.0	1.5	1.1	WD221H	A 402
10.1	15.2	14.9	14.0	14.3	14.1	13.9	13.8	13.0	13.5	18.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	WP321H	A403
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	F321	A182
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	F321H	A182
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	WP321	A403
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	WP321H	A403
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	WP321	A403
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	WP321H	A403
			1	\mathcal{O}																	
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	WP316H	A403
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	F316H	A182
	7																		-10		
20.0	10.2	10.0	107	10 5	102	102	101	101	10 1	171	1/1	10 5	7.0	ΕO	1.4	2.2	2 5	1.0	1 2	WD24711	A 402
									18.1		14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8		WP347H	A403
∠0.0	19.3	19.0	10./	10.5	10.3	10.2	10.1	10.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	F347	A182
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	WP347	A403
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	F348	A182
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	WP348	A403
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	F347H	A182

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Strengt		Stre Metal	ic Allo ss, <i>S</i> , Temp [Note	ksi, a eratu	t
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300	400
Stainless Steel — For	gings and I	Fittings					(-)		(-)						
18Cr-10Ni-Cb		A182	F348H	S34809			8	(9)(21)	-325	75	30	20.0	20.0	20.0	20.0
16Cr-12Ni-2Mo		A182	F316	S31600			8	(9)(21) (26)(28)	-325	75	30	20.0			19.3
16Cr-12Ni-2Mo		A403	WP316	S31600			8	(26)(28) (32)(37)	-425	75	30	20.0	20.0	20.0	19.3
18Cr-13Ni-3Mo	•••	A403	WP317	S31700			8	(26)(28) (32)	-325	75	30	20.0	20.0	20.0	19.3
18Cr-8Ni		A182	F304	S30400			8	(9)(21) (26)(28)	-425	75	30	20.0	20.0	20.0	18.6
18Cr-8Ni		A403	WP304	S30400			8	(26)(28) (32)(37)	-425	75	30	20.0	20.0	20.0	18.6
18Cr-8Ni		A403	WP304H	S30409			8	(26)(32) (37)	325	75	30	20.0	20.0	20.0	18.6
18Cr-8Ni		A182	F304H	S30409			8	(9)(21) (26)	-325	75	30	20.0	20.0	20.0	18.6
44Fe-25Ni-21Cr-Mo		A182	F904L	N08904			450		-325	71	31	20.7	20.7	20.4	18.7
13Cr		A182	F6a	S41000	1	4	6	(35)	-20	70	40	23.3	23.3	22.9	22.5
13Cr		A182	F6a	S41000	2	je	6	(35)	-20	85	55	28.3	28.3	27.8	27.3
20Cr-18Ni-6Mo		A182	F44	S31254	xO		8	(8)	-325	94	44	29.3	29.3	28.9	26.7
20Cr-18Ni-6Mo		A403	WPS31254	S31254	_		8	(8)	-325	94	44	29.3	29.3	28.9	26.7
20Cr-18Ni-6Mo		A403	CRS31254	S31254	Hick		8	(8)	-325	94	44	29.3	29.3	28.9	26.7
23Cr-4Ni-Mo-Cu-N		A182	F68	S32304			10H	(25)	-60	87	58	29.0	27.9	26.1	24.7
22Cr-5Ni-3Mo-N		A182	F51	\$31803			10H	(25)	-60	90	65	30.0	30.0	28.9	27.8
22Cr-5Ni-3Mo-N		A815	WPS31803	\$31803			10H	(25)	-60	90	65	30.0	30.0	28.9	27.8
22Cr-5Ni-3Mo-N		A815	CRS31803	S31803			10H	(25)	-60	90	65	30.0	30.0	28.9	27.8
46Fe-24Ni-21Cr-6Mo- Cu-N	0 0	A182	F62	N08367			45	(26)	-325	95	45	30.0		29.9	
46Fe-24Ni-21Cr-6Mo- Cu-N		A403	WP6XN	N08367			45	(26)	-325	95	45	30.0		29.9	
46Fe-24Ni-21Cr-6Mo- Cu-N	1.7	A403	CR6XN	N08367			45	(26)	-325	95	45	30.0	30.0		
21Cr-5Mn-1½Ni-Cu-N	1	A815		S32101			10H	(25)	-20	94	65	31.3	31.3		
22Cr-5Ni-3Mo-N		A182	F60	S32205		•••	10H	(25)	-60	95	65	31.7	31.7		
22Cr-5Ni-3Mo-N		A815	2205	S32205			10H	(25)	-60	95	65	31.7			29.4
25Cr-8Ni-3Mo- W-Cu-N		A182		S32760			10H	(25)	-60	109	80	36.3	36.3		
25Cr-8Ni-3Mo- W-Cu-N		A815		S32760			10H	(25)	-60	109	80	36.3	36.3	34.8	34.0
13Cr		A182	F6a	S41000	3		6	(35)	-20	110	85	36.7			
13Cr-½Mo		A182	F6b	S41026			6	(35)		110- 135	90	36.7			
25Cr-7Ni-4Mo-N	Forgings	A182	F53	S32750			10H	(25)	-60	116	80	38.7	38.5	36.4	35.1
25Cr-7Ni-4Mo-N	Fittings	A815	WPS32750	S32750			10H	(25)	-60	116	80	38.7	38.5	36.4	35.1

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

500	600	650	700	750	000	050	000	050	1 000	1.050	1 100	1 150	1 200	1 250	1 200	1 250	1 400	1 450	1 500	Type/	Spec.
500	600	050	700	/50	800	850	900	950	1,000	1,050	1,100	1,150	1,200		1,300					Grade s (3)(4a)	No.
20.0	193	19 0	187	18 5	183	18 2	18 1	18 1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	23 anu 1.8	_	F348H	A182
	17.0									15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	F316	A182
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	WP316	A403
18.0	17.0	16.6	16.3	16.1	15.9	15.7	15.6	15.4	15.3	15.1	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	3.	WP317	A403
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	F304	A182
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	WP304	A403
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	WP304H	A403
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	F304H	A182
17.1													~~@							F904L	A182
22.1	21.6	21.2	20.6	20.0	19.2	17.2	12.3	8.8	6.4				<i>\'</i>							F6a Cl. 1	A182
26.9		25.7						8.8	6.4	4.4	2.9	4 .8	1.0							F6a Cl. 2	A182
25.2	24.1	23.8	23.6	23.4	23.2	23.0					۷O Ì									F44	A182
25.2	24.1	23.8	23.6	23.4	23.2	23.0														WPS31254	A403
25.2	24.1	23.8	23.6	23.4	23.2	23.0				JIC.										CRS31254	A403
22.9	19.2																			F68	A182
27.2	26.9							1	1											F51	A182
27.2	26.9							O,												WPS31803	8 A815
27.2	26.9						ر.) <u></u>												CRS31803	A815
27.7	26.2	25.7	25.1	24.7	24.3	50							•••							F62	A182
27.7	26.2	25.7	25.1	24.7	24.3															WP6XN	A403
27.7	26.2	25.7	25.1	24.7	24.3								•••							CR6XN	A403
28.5	28.5	(\																		A815
28.7	28.4																			F60	A182
28.7	28.4																			2205	A815
33.9	33.9																				A182
33.9	33.9																				A815
																				F6a Cl. 3	A182
																				F6b	A182
34.5	34.3																			F53	A182
34.5	34.3																			WPS32750	

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Numbers in										Specifie Streng	d Min.	Basi Stre Metal	ic Allo	wabl ksi, a eratu	ıt
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, in.	P-No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300	400
Stainless Steel — Forg	ings and I	ittings	(3)(4a)												
25Cr-7Ni-4Mo-N	Fittings	A815	CRS32750	S32750		***	10H	(25)	-60	116	80	38.7	38.5	36.4	35.1
13Cr		A182	F6a	S41000	4	•••	6	(35)	-20	130	110	43.3	0		
Stainless Steel — Bar	(3)(4a)											9			
18Cr-8Ni		A479	304	S30400			8	(26)(28)	-425	75	30	20:0	20.0	20.0	18.6
18Cr-8Ni		A479	304H	S30409			8	(26)	-325	75	30	20.0	20.0	20.0	18.7
18Cr-8Ni		A479	304L	S30403			8		-425	70	25	16.7	16.7	16.7	15.8
16Cr-12Ni-2Mo		A479	316	S31600			8	(26)(28)	-325	75	30	20.0	20.0	20.0	19.3
16Cr-12Ni-2Mo		A479	316H	S31609			8	(26)	-325	75	30	20.0	20.0	20.0	19.3
16Cr-12Ni-2Mo		A479	316L	S31603			8		-425	70	25	16.7	16.7	16.7	15.5
18Cr-10Ni-Ti	Bar	A479	321	S32100			8	(28)	-325	75	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Ti	Bar	A479	321	S32100			8	(28)(30)	-325	75 75	30	20.0	20.0		
18Cr-10Ni-Ti	Bar	A479	321 321H	S32100	•••		8	(30)	-325	75 75	30	20.0	20.0		
18Cr-10Ni-Cb		A479	347	S34700	•••		8	(30)	-323 -425	75 75	30	20.0	20.0		
18Cr-10Ni-Cb		A479	347	S34700			8	(28)(30)	-425	75 75	30	20.0	20.0		
18Cr-10Ni-Cb		A479	347H	S34700			8 0		-325	75	30	20.0	20.0		
						. N									
44Fe-25Ni-21Cr-Mo		A479	904L	N08904		::0	45		-325	71	31	20.7	20.7	20.4	18.7
22Cr-5Ni-3Mo-N		A479		S31803		7,	10H	(25)	-60	90	65	30.0	30.0	28.9	27.8
20Cr-18Ni-6Mo		A479		S31254	x O		8	(8)	-325	95	45	30.0	30.0	29.5	27.3
46Fe-24Ni-21Cr-6Mo- Cu-N		A479		N08367	4011		45	(26)	-325	95	45	30.0	30.0	29.9	28.6
21Cr-5Mn-1.5Ni-Cu-N		A479		S32101			10H	(25)	-20	94	65	31.3	31.3	29.8	28.5
22Cr-5Ni-3Mo-N	•••	A479	2205	S32205			10H	(25)	-60	95	65	31.7	31.7	30.6	29.4
24Cr-4Ni-3Mn- 1.5Mo-N		A479	C	\$82441		\geq ⁷ / ₁₆ thk.	10H	(25)	-60	99	70	32.9	32.9	32.9	32.9
22Cr-13Ni-5Mn		A479	XM-19	S20910			8		-20	100	55	33.3	33.1	31.4	30.4
24Cr-4Ni-3Mn- 1.5Mo-N		A479		S82441		$<^{7}/_{16}$ thk.	10H	(25)	-60	107	78	35.8	35.8	35.8	35.8
		5/11.													
29Cr-6.5Ni-2Mo-N		A479		S32906			10H	(25)	-60	109	80	36.3	36.3	34.5	33.5
25Cr-7Ni-4Mo-N		A479		S32750		≤2 thk.	10H	(25)	-60	116	80	38.7	38.5	36.4	35.1
Stainless Steel — Cast	ings (3)(4	a)													
29Ni-20Cr-3Cu-2Mo		A351	CN7M	N08007			45	(9)(30)	-325	62	25	16.7			
35Ni-15Cr-½Mo		A351	HT30	N08603			45	(36)(39)	-325	65	28	18.7			
25Cr-12Ni		A351	CH8	J93400			8	(9)(31)	-325	65	28	18.7	18.7	18.5	18.0
25Cr-20Ni		A351	CK20	J94202			8	(9)(27) (31)(35) (39)	-325	65	28	18.7	18.7	18.5	18.0
16Cr-14Ni-2Mo		A351	CF10MC				8	(30)	-325	70	30	20.0			
18Cr-8Ni		A351	CF3	J92500			8	(9)	-425	70	30	20.0			18.6
18Cr-12Ni-2Mo		A351	CF3M	J92800			8	(9)	-425	70	30	20.0	20.0		
18Cr-8Ni		A351	CF8	J92600			8	(9)(26) (27)(31)	-425	70	30	20.0	20.0	20.0	18.6

Basic Allowable Stress, S, 1	ksi, at Metal Temperature	, °F	Note	(1)]
------------------------------	---------------------------	------	------	------

500	600	650	700	750	900	950	000	050	1 000	1.050	1 100	1 150	1 200	1 250	1 200	1 250	1,400	1.450	1 500	Type/ Grade	Spec. No.
300	000	030	700	730	000	030	900	930	1,000	1,030	1,100	1,130	1,200							s (3)(4a)	
34.5	34.3																			CRS32750	-
																				, 9-)
																				F6a Cl. 4	A182
																		Cha!	.l(C)	V	(2)(4-)
175	16.6	16 2	150	155	15 2	140	116	1/12	14.0	12.4	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8		gel — Bar 304	(3)(4a) A479
	16.4									12.4	9.7	7.7	6.0	4.7	3.7	2.9	2.3	1.8	1.4	304H	A479
14.8	14.0							9.9	7.8	6.3	5.1	4.0	3.2	2.6	2.1	1.7	1.1	1.0	0.9	304L	A479
	17.0									14.5	12.4	9.8	7.4	5.5	4.1	3.1	2,3	1.7	1.3	316	A479
	17.0									14.5	12.4	9.8	7.4	5.5	4.1	3.1	2.3	1.7	1.3	316H	A479
									11.2	10.8	10.2	8.8	6.4	4.7	3.5	2.5	1.8	1.3	1.0	316L	A479
																X	\				
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	9.6	6.9	5.0	3.6	2.6	1.7	1.1	0.8	0.5	0.3	321	A479
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	321	A479
19.3	18.3	17.8	17.5	17.2	16.9	16.7	16.5	16.4	16.2	12.3	9.1	6.9	5.4	4.1	3.2	2.5	1.9	1.5	1.1	321H	A479
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	16.0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	347	A479
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	347	A479
20.0	19.3	19.0	18.7	18.5	18.3	18.2	18.1	18.1	18.1	17.4	14.1	10.5	7.9	5.9	4.4	3.2	2.5	1.8	1.3	347H	A479
												4									
17.1											•	.0								904L	A479
27.2	26.9											1									A479
25.8	24.7	24.3	24.1	23.9	23.7	23.6					×O										A479
27.7	26.2	25.7	25.1	24.7	24.3					1											A479
										ilo.											
28.5	28.5							•••		ر											A479
28.7	28.4								1			•••	•••	•••					•••	2205	A479
22.0	22.0							0	3												4.470
32.9	32.8						T(\mathcal{C}												•••	A479
29.7	29.2	29.0	28.8	28.6	28.3	27.9	27.5	27.0	26.3	25.5	20.4	13.0	8.3							XM-19	A479
35.8	35.7																				A479
					N)															
				0	D.																
33.0	33.0			\bigcirc_{λ}																•••	A479
34.5	34.3		7	<u></u>																	A479
		-	$\langle \rangle$														St	ainless	Steel -	- Castings	(3)(4a)
	(الم																		CN7M	A351
	-																			HT30	A351
	\								11.1	8.5	6.5	5.0	3.8	2.9	2.3	1.8	1.3	0.9	0.8	СН8	A351
									11.3	9.8	8.5	7.3	6.0	4.8	3.5	2.4	1.6	1.1	0.8	CK20	A351
																				CF10MC	A351
	 16.6													•••						CF10MC	A351
	17.0																			CF3M	A351
17.7	17.0	10.0	10.0	10.0	10.0	13.7										•••				31 31-1	11001
17.5	16.6	16.2	15.8	15.5	15.2	14.9	14.6	14.3	12.2	9.5	7.5	6.0	4.8	3.9	3.3	2.7	2.3	2.0	1.7	CF8	A351

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifie Streng		Stre Metal	ic Allo ess, <i>S</i> , Temp [Note	ksi, a eratı	at ure,
Nominal	Product	Spec.	Type/	UNS	Class/ Condition/	Size,	P-No.		Min. Temp.,			Min. Temp.			
Composition	Form	No.	Grade	No.	Temper	in.	(5)	Notes	°F (6)	Tensile	Yield	to 100	200	300	400
Stainless Steel — Cast	ings <mark>(3)(4</mark>	1)													
25Cr-12Ni		A351	CH10	J93401			8	(27)(31) (35)	-325	70	30	20.0	20.0	20.0	20.0
25Cr-12Ni		A351	CH20	J93402			8	(9)(27) (31)(35) (39)	-325	70	30	20.0	20.0	20.0	20.0
18Cr-10Ni-Cb		A351	CF8C	J92710			8	(9)(28)	-325	70	30	20.0	20.0	20.0	19.5
18Cr-12Ni-2Mo		A351	CF8M	J92900			8	(9)(26) (27)(30)	-425	70	30	20.0	20.0	20.0	18.6
$25\text{Cr}-20\text{Ni}-\frac{1}{2}\text{Mo}$		A351	HK40	J94204			8	(35)(36) (39)	-325	62	35	20.7			
25Cr-20Ni- ¹ / ₂ Mo		A351	HK30	J94203			8	(35)(39)	-325	65	35	21.7			
18Cr-8Ni		A351	CF3A	J92500			8	(9)(56)	-425	77	35	23.3	23.3	22.7	21.7
18Cr-8Ni		A351	CF8A	J92600				(9)(26) (56)	-425	77	35	23.3			21.7
25Cr-8Ni-N		A351	CE20N	J92802			18/0	(35)(39)	-325	80	40	26.7	26.7	26.7	26.7
12Cr		A217	CA15	J91150		NON	6	(35)	-20	90	65	30.0	30.0	29.4	28.9
24Cr-10Ni-4Mo-N		A995	2A	J93345		7,	10H	(9)	-60	95	65	31.7	31.6	29.3	28.2
25Cr-8Ni-3Mo-W-Cu- N		A995	6A	J93380	c\ [*] CO		10H	(9)(25)	-60	100	65	33.3	33.2	31.4	30.3
13Cr-4Ni		A487	CA6NM	J91540	À		6	(9)(35)	-20	110	80	36.7	36.7	35.9	35.3
ASI	KNO	21/10	CA6NM	2 km											

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
																Stain	less St	eel —	Casting	s (3)(4a)	(Cont'd)
20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	11.1	8.5	6.5	5.0	3.8	2.9	2.3	1.8	1.3	0.9	8.0	CH10	A351
20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	11.1	8.5	6.5	5.0	3.8	2.9	2.3	1.8	1.3	0.9	0.8	CH20	A351
																				5	
18.8	18.4	183	183	182	18.2	18 1	18 0	18 0	18 0	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	CF8C	A351
	16.6									12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	CF8M	A351
																	2				
																of	S.			HK40	A351
															1	0,					
											•••				20X	•••				HK30	A351
20.4	19.3	18.9	18.5																	CF3A	A351
20.4	19.3	18.9	18.5											M.						CF8A	A351
26.7	26.7	26.7	26.7	26.7	26.7	26.7	26.7					9	Ho							CE20N	A351
28.4	27.7	27.2	26.5	17.5	16.8	14.9	11.0	7.6	5.0	3.3	2.3	21.5	1.0							CA15	A217
	28.2										4									2A	A995
29.8	29.6										NO.									6A	A995
										15	-										
34.8	33.9	33.3	32.4																	CA6NM Cl. A	A487
								0	7.												
							ۍ.	<u>ر</u>													
						20															
				S	14.																
			1	9																	
		1	(\(\cdot\)\)																		
	-	(S)	-																		
	Y	. •																			

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

									Speci Minir Strengt	num
Nominal Composition	Product Form	Spec. No.	UNS No.	Class/ Condition/ Temper	Size Range, in.	P-No. (5)(7)	Notes	Min. Temp., °F (6)	Tensile	Yield
Copper and Copper	r Alloy — I	Pipes and	Tubes							
99.95Cu-P	Pipe	B42	C10200	061		31		-452	30	9
99.9Cu-P	Pipe	B42	C12000	061		31		-452	30	9
99.9Cu-P	Pipe	B42	C12200	061		31		-452	30	9
99.95Cu-P	Tube	B75	C10200	050		31		-452	30	9
99.95Cu-P	Tube	B75	C10200	060		31		-452	30	9
99.9Cu-P	Tube	B75	C12000	050		31		-452	30	9
99.9Cu-P	Tube	B75	C12000	060		31	···	-452	30	9
99.9Cu-P	Tube	B75	C12200	050		31		-452	30	9
99.9Cu-P	Tube	B75	C12200	060		31	S	-452	30	9
99.9Cu-P	Tube	B68	C12200	050		31	(24)	-452	30	9
99.9Cu-P	Tube	B68	C12200	060		31	(24)	-452	30	9
99.9Cu-P	Tube	B88	C12200	050		31	(24)	-452	30	9
99.9Cu-P	Tube	B88	C12200	060		31	(24)	-452	30	9
99.9Cu-P	Tube	B280	C12200	060	 Ç	31	(24)	-452	30	9
85Cu-15Zn	Pipe	B43	C23000	061	" "he	32		-452	40	12
90Cu-10Ni		B467	C70600	W050	>4.5 O.D.	34	(14)	-452	38	13
90Cu-10Ni		B467	C70600	W061	>4.5 O.D.	34	(14)	-452	38	13
90Cu-10Ni		B466	C70600	Annealed 🎺)	34	(14)	-452	38	13
90Cu-10Ni		B467	C70600	W050	≤4.5 O.D.	34	(14)	-452	40	15
90Cu-10Ni		B467	C70600	W061	≤4.5 O.D.	34	(14)	-452	40	15
70Cu-30Ni		B467	C71500	W050	>4.5 O.D.	34	(14)	-452	45	15
70Cu-30Ni		B467	C71500	W061	>4.5 O.D.	34	(14)	-452	45	15
80Cu-20Ni		B466	C71000	Annealed	≤4.5 O.D.	34	(14)	-452	45	16
99.95Cu-P	Pipe	B42	C10200	H55	NPS 2½ thru 12	31	(14)(34)	-452	36	30
99.9Cu-P	Pipe	В42	C12000	H55	NPS 2½ thru 12	31	(14)(34)	-452	36	30
99.9Cu-P	Pipe	B42	C12200	H55	NPS 2½ thru 12	31	(14)(34)	-452	36	30
99.95Cu-P	Tube	B75	C10200	H58		31	(14)(34)	-452	36	30
99.9Cu-P	Tube	B75	C12000	H58		31	(14)(34)	-452	36	30
99.9Cu-P	Tube	B75	C12200	H58		31	(14)(34)	-452	36	30
99.9Cu-P	Tube	B88	C12200	H58		31	(14)(24)(34)	-452	36	30
70Cu-30Ni		B466	C71500	060		34	(14)	-452	52	18
70Cu-30Ni		B467	C71500	W050	≤4.5 O.D.	34	(14)	-452	50	20
70Cu-30Ni		B467	C71500	W061	≤4.5 O.D.	34	(14)	-452	50	20
99.95Cu-P	Pipe	B42	C10200	Н80	NPS ½ thru 2	31	(14)(34)	-452	45	40
99.9Cu-P	Pipe	B42	C12000	Н80	NPS ½ thru 2	31	(14)(34)	-452	45	40
77.76u-1	1.100				111 0 /8 cm a =	31	(11)(31)	132	10	- 0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Min. Temp. to 100	150	200	250	300	350	400	450	500	550	600	650	700	UNS No.	Spec. No.
10 100	100		200	500	550	100	100	500	550				— Pipes a	
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7					C10200	B42
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7					C12000	
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7					C12200	B42
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7				(C10200	B75
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7				*	C10200	B75
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7				~?)\	C12000	B75
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7					C12000	B75
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7			1.	/	C12200	B75
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7			C		C12200	B75
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7		Ç	P		C12200	B68
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7		<i></i> O			C12200	B68
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7		K			C12200	B88
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7	Q`	V			C12200	B88
6.0	5.1	4.9	4.8	4.7	4.0	3.0	2.3	1.7					C12200	B280
								9	10					
8.0	7.9	7.9	7.9	7.9	7.0	5.0	2.0	"HUG				•••	C23000	B43
8.7	8.4	8.2	8.0	7.8	7.7	7.5	7.40	7.3	7.0	6.0			C70600	B467
8.7	8.4	8.2	8.0	7.8	7.7	7.5	7.4	7.3	7.0	6.0			C70600	B467
8.7	8.4	8.2	8.0	7.8	7.7	7.5	7.4	7.3	7.0	6.0			C70600	B466
10.0	9.7	9.5	9.3	9.1	8.9	8.7	8.5	8.0	7.0	6.0			C70600	B467
10.0	9.7	9.5	9.3	9.1	8.9	8.7	8.5	8.0	7.0	6.0			C70600	B467
10.0	9.6	9.4	9.2	9.0	8.8	8.6	8.4	8.2	8.1	8.0	7.9	7.8	C71500	B467
10.0	9.6	9.4	9.2	9.0	8.8	8.6	8.4	8.2	8.1	8.0	7.9	7.8	C71500	B467
10.7	10.6	10.5	10.4	10.2	10.1	9.9	9.6	9.3	8.9	8.4	7.7	7.0	C71000	B466
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C10200	B42
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C12000	B42
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C12200	B42
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C10200	B75
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C12000	B75
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C12200	B75
12.0	11.6	10.9	10.4	10.0	9.8	9.5							C12200	B88
12.0	11.6	11.3	11.0	10.8	10.6	10.3	10.1	9.9	9.8	9.6	9.5	9.4	C71500	B466
13.3	12.9	12.6	12.3	12.0	11.7	11.5	11.2	11.0	10.8	10.7	10.5	10.4	C71500	B467
13.3	12.9	12.6	12.3	12.0	11.7	11.5	11.2	11.0	10.8	10.7	10.5	10.4	C71500	B467
15.0	14.5	13.6	13.0	12.6	12.2	4.3							C10200	B42
15.0	14.5	13.6	13.0	12.6	12.2	4.3							C12000	B42
15.0	14.5	13.6	13.0	12.6	12.2	4.3							C12200	B42

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

					ubies, specifical				Speci Minir Strengt	fied num
Nominal Composition	Product Form	Spec. No.	UNS No.	Class/ Condition/ Temper	Size Range, in.	P-No. (5)(7)	Notes	Min. Temp., °F (6)	Tensile	Yield
Copper and Copper	Alloy — I	Pipes and	Tubes							
99.95Cu-P	Tube	B75	C10200	H80		31	(14)(34)	-452	45	40
99.9Cu-P	Tube	B75	C12000	H80		31	(14)(34)	-452	45	% 10
99.9Cu-P	Tube	B75	C12200	Н80		31	(14)(34)	-452	450	40
Copper and Copper	Alloy — I	Plates and	Sheets						(5)	
99.95Cu-P		B152	C10200	025		31	(14)(24)	452	30	10
99.95Cu-Ag		B152	C10400	025		31	(14)(24)	-452	30	10
99.95Cu-Ag		B152	C10500	025		31	(14)(24)	-452	30	10
99.95Cu-Ag		B152	C10700	025	•••	31	(14)(24)	-452	30	10
99.9Cu-P		B152	C12200	025		31	(14)(24)	-452	30	10
99.9Cu-P		B152	C12300	025		31	(14)(24)	-452	30	10
90Cu-10Ni		B171	C70600		≤2.5 thk.	34	(14)	-452	40	15
97Cu-3Si		B96	C65500	061		33		-452	50	18
70Cu-30Ni		B171	C71500		≤2.5 thk.	34	(14)	-452	50	20
90Cu-7Al-3Fe		B169	C61400	025	≤2.0 thk	35	(13)	-452	70	30
90Cu-7Al-3Fe		B169	C61400	060	<2.0 thk	35	(13)	-452	70	30
					TIEN					
Copper and Copper	Alloy — I	0 0		٠.						
99.9Cu		B283	C11000	L		31	(14)	-452	33	11
97Cu-3Si		B283	C65500	IIO		33	(14)	-452	52	18
60Cu-38Zn-2Pb		B283	C37700	C//		a	(14)	-325	58	23
60Cu-37Zn-2Pb-Sn		B283	C48500			a	(14)	-325	62	24
60Cu-39Zn-Sn		B283	C 46400			32	(14)	-425	64	26
59Cu-39Zn-Fe-Sn		B283	C67500			32	(14)	-325	72	34
Copper and Copper	Alloy — (611	600.600				(0)	225	20	4.4
85Cu-5Sn-5Zn-5Pb		B62	C83600			a	(9)	-325	30	14
57Cu-20Zn-12Ni- 9Pb-2Sn	N. HO	B584	C97300			a	•••	-325	30	15
64Cu-20Ni-8Zn- 4Sn-4Pb		B584	C97600			a	•••	-325	40	17
87Cu-8Sn-4Zn-1Pb		B584	C92300			a		-325	36	16
88Cu-Sn-Zn-Pb		B584	C92200			a		-325	34	16
88Cu-Sn-Zn-Pb		B61	C92200			a	(9)	-325	34	16
88Cu-8Sn-4Zn		B584	C90300			b		-325	40	18
88Cu-10Sn-2Zn		B584	C90500			b		-325	40	18
58Cu-38Zn-1Sn- 1Pb-1Fe		B584	C86400			a	(9)	-325	60	20
66Cu-25Ni-5Sn- 2Pb-2Zn		B584	C97800			a		-325	50	22

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic Allowable Stress, S, ksi, at Metal Temperature, °F [Note (1)] Min. UNS Temp. Spec. to 100 150 200 250 300 350 400 450 500 550 600 650 700 No. No. Copper and Copper Alloy — Pipes and Tubes (Cont'd) 13.0 15.0 14.5 13.6 12.6 12.2 4.3 C10200 B75 15.0 14.5 13.6 13.0 12.6 12.2 4.3 C12000 B75 C12200 B75 15.0 14.5 13.6 13.0 12.6 12.2 4.3 Copper and Copper Alloy – Plates and Sheets C10200 6.7 5.7 5.4 5.3 5.0 4.0 3.0 2.3 1.7 B152 ... 6.7 5.7 5.4 5.3 5.0 4.0 3.0 2.3 1.7 C10400 B152 5.7 5.4 5.3 2.3 C10500 B152 6.7 5.0 4.0 3.0 1.7 6.7 5.7 5.4 5.3 5.0 4.0 3.0 2.3 1.7 C10700 B152 6.7 5.7 5.4 5.3 5.0 2.3 1.7 C12200 4.0 3.0 ... B152 6.7 5.7 5.4 5.3 5.0 4.0 3.0 2.3 1.7 C12300 B152 10.0 9.7 9.5 9.3 9.1 8.9 8.7 8.5 8.0 7.0 6.0 C70600 B171 12.0 12.0 11.9 10.7 6.8 C65500 B96 11.9 11.9 11.0 11.2 10.8 13.3 12.9 12.6 12.3 12.0 11.7 11.5 10.7 10.5 10.4 C71500 B171 20.0 19.9 19.8 19.7 19.5 19.4 19.2 19.0 18.8 C61400 B169 18.8 19.0 20.0 19.2 19.9 19.8 19.7 19.5 19.4 C61400 B169 ... Copper and Copper Alloy — Forgings 2.3 7.3 6.2 6.0 5.8 5.0 4.0 3.0 1.7 B283 ... C11000 12.0 12.0 11.9 11.9 11.9 10.7 6.8 C65500 B283 2.0 15.3 14.5 13.9 13.3 10.5 7.5 C37700 B283 16.0 16.0 16.0 16.0 16.0 16.0 16.0 C48500 B283 17.3 17.3 17.3 17.3 6.3 2.5 C46400 B283 22.7 22.7 22.7 22.7 22.7 22.7 22.7 C67500 B283 Copper and Copper Alloy -**Castings** 9.3 9.3 9.2 B62 8.1 7.7 7.4 7.3 C83600 10.0 C97300 B584 11.3 10.1 9.1 8.7 B584 C97600 10.7 10.7 10.7 10.7 10.7 10.7 C92300 B584 10.7 ... 9.5 10.7 9.6 9.4 9.2 8.9 8.6 C92200 B584 10.7 9.6 9.5 9.4 9.2 8.9 8.3 8.3 C92200 8.6 8.4 B61 12.0 12.0 12.0 12.0 12.0 12.0 12.0 C90300 B584 12.0 12.0 12.0 12.0 12.0 12.0 12.0 C90500 B584 ... 13.3 13.3 13.3 13.3 13.3 13.3 C86400 B584 ... 14.7 14.7 14.7 14.7 14.7 14.7 C97800 B584

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Specified

										Minir Strengt	num
Nominal Composition	Product Form	Spec. No.	UNS No.	Class/ Condition/ Temper	Size Range, in.	P-No. (5)(7)		Notes	Min. Temp., °F (6)	Tensile	Yield
Copper and Coppe	r Alloy — (Castings									
58Cu-39Zn-1Fe- 1Al-1Mn		B584	C86500			b			-325	65	25 %
88Cu-9Al-3Fe		B148	C95200			35	(9)		-425	63	25
89Cu-10Al-1Fe		B148	C95300			35	(9)		-425	2 65	25
90Cu-7Al-3Si		B148	C95600			35			-325	60	28
85Cu-11Al-4Fe		B148	C95400			35			-325	75	30
58Cu-34Zn-2Fe- 2Al-2Mn		B584	C86700			a		ASM	-325	80	32
82Cu-11Al-4Fe- 3Mn		B148	C95500			35	(2, ,	-452	90	40
63Cu-27Zn-4Al- 3Fe-3Mn		B584	C86200			b);;		-325	90	45
61Cu-27Zn-6Al- 3Fe-3Mn		B584	C86300		 \$\frac{1}{2} \cong \frac{1}{2} \cong \	III p			-325	110	60
Copper and Copper	r Alloy — I	Rod			111.						
75Cu-21.5Zn-3Si		B371	C69300	H02	≤1/201	a			-325	85	45
75Cu-21.5Zn-3Si		B371	C69300	H02	> ¹ ⁄ ₂ , ≤1	a			-325	75	35
75Cu-21.5Zn-3Si		B371	C69300	H02 H02	>1, ≤2	a			-325	70	30
			CON								
		Odna	J .								
	40F	7/4									
6	ME										
Ro											

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic Allowable Stress	.S.	ksi.	. at Metal	Temperature.	°F	Note	(1)	1
Dasic Allowable suless		1231	, at Mictai	i chipci atui c,		INOLL		ı

Min. Temp.													UNS	Spec.
to 100	150	200	250	300	350	400	450	500	550	600	650	700	No.	Spec. No.
										Copper	and Cop	per Alloy	— Castings	(Cont'd)
16.7	16.7	16.7	16.7	16.7	16.7								C86500	B584
													100	
													00,	
16.7	15.7	15.2	14.8	14.5	14.3	14.2	14.1	14.1	11.7	7.4			C95200	B148
16.7	16.7	16.7	16.7	16.7	16.7	16.7	16.7	16.7	16.7	16.7			2 95300	B148
18.7												& 2	C95600	B148
20.0	19.0	18.7	18.5	18.5	18.5	18.5	16.0	13.9			<		C95400	B148
24.0	24.0	24.2	24.2	24.0	24.2						- M		006700	DE0.4
21.3	21.3	21.3	21.3	21.3	21.3						S.	•••	C86700	B584
26.7	26.7	26.7	26.7	26.7	26.7	26.7	26.7	26.7			Υ		C95500	B148
										200				
30.0	30.0	30.0	30.0	30.0	30.0					O,'''			C86200	B584
									ill P	•				
36.7	36.7	36.7	36.7	36.7	36.7						•••		C86300	B584
								0,						
								N THE			Co	nner and	Copper Allo	v — Rod
28.3	25.9	25.4	25.4	25.4				7					C69300	B371
23.3	20.2	19.8	19.8	19.8	•••	•••	jie						C69300	B371
20.0	17.3	17.0	17.0	17.0		🔽	0						C69300	B371
20.0	27.0	27.0	27.0	17.0		1						•••	407000	20,1
						ilo,								
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		70	•											
	N													
•	W.		25.4 19.8 17.0											
	7													

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

		Turchen	eses Refer to	7 110103 1	01 11	рреник	Trables,	Specific Mir Strengt	fied 1.		ic Allo	owable		ss, <i>S</i> , 1	ksi, at	Meta	l
			Class/	Size	P-		Min.			Min.							
Nominal Composition	Spec. No.	UNS No.	Condition/ Temper	Range, in.	No. (5)	Notes	Temp., °F (6)	Tensile	Yield	Temp. to 100	200	300	400	500	600	650	700
Nickel and Nic					(0)	110100	- (0)	10110110		10 100			100	500		000	
99.0Ni-Low C	B161		Annealed	>5 O.D.	41		-325	50	10	6.7	6.4	6.3	6.3	6.3	6.3	6.2	6.2
99.0Ni-Low C	B725	N02201	Annealed	>5 O.D.	41		-325	50	10	6.7	6.4	6.3	6.3	6.3	6.3	6.2	6.2
99.0Ni	B161	N02200	Annealed	>5 O.D.	41		-325	55	12	8.0	8.0	8.0	8.0	8.0	8.0	1/5)
99.0Ni	B725	N02200	Annealed	>5 O.D.	41		-325	55	12	8.0	8.0	8.0	8.0	8.0	8.0	کر ا	
99.0Ni-Low C	B161	N02201	Annealed	≤5 O.D.	41		-325	50	12	8.0	7.7	7.5	7.5	7.5	7.5	7.5	7.4
99.0Ni-Low C	B725	N02201	Annealed	≤5 O.D.	41		-325	50	12	8.0	7.7	7.5	7.5	7.5	7.5	7.5	7.4
99.0Ni	B161	N02200	Annealed	≤5 O.D.	41		-325	55	15	10.0	10.0	10.0	10.0	10.0	10.0		
99.0Ni	B725	N02200	Annealed	≤5 O.D.	41		-325	55	15	10.0	10.0	10.0	10.0	10.0	10.0		
67Ni-30Cu	B165	N04400	Annealed	>5 O.D.	42		-325	70	25	16.7	14.6	13.6	13.2	13.1	13.1	13.1	13.0
67Ni-30Cu	B725		Annealed	>5 O.D.	42		-325	70	25	16.7	- X		13.2				
33Ni-42Fe- 21Cr	B407	N08800	H.F. or H.F. ann.		45		-325	65	25	16.7	96.7	16.7	16.7	16.7	16.7	16.7	16.7
72Ni-15Cr- 8Fe	B167	N06600	H.F. or H.F. ann.	>5 O.D.	43		-325	75	25	16.7	16.7	16.7	16.7	16.7	16.7	16.7	16.7
33Ni-42Fe- 21Cr	B407	N08810	C.D. sol. ann. or H.F. ann.		45	(62)	-325	65	25	16.7	16.7	16.7	16.7	16.7	16.5	16.1	15.7
33Ni-42Fe- 21Cr	B514	N08810	Annealed		45	(62)	-325	N 65	25	16.7	16.7	16.7	16.7	16.7	16.5	16.1	15.7
33Ni-42Fe- 21Cr-Al-Ti	B407	N08811	C.D. sol. ann. or H.F. ann.		45	(62)	-325	65	25	16.7	16.7	16.7	16.7	16.7	16.5	16.1	15.7
						i,cX											
67Ni-30Cu	B165	N04400	Annealed	≤5 O.D.	42	$O_{II_{a}}$	-325	70	28	18.7	16.4	15.2	14.7	14.7	14.7	14.7	14.6
67Ni-30Cu	B725	N04400	Annealed	≤5 O.D.	42		-325	70	28	18.7	16.4	15.2	14.7	14.7	14.7	14.7	14.6
26Ni-22Cr- 5Mo-Ti	B619	N08320	Sol. ann.	~O	45		-325	75	28	18.7	18.7	18.7	18.7	18.7	18.6	18.2	17.8
26Ni-22Cr- 5Mo-Ti	B622	N08320	Sol. ann.	ر.	45		-325	75	28	18.7	18.7	18.7	18.7	18.7	18.6	18.2	17.8
99.0Ni-Low C	B161	N02201	Str. rel		41		-325	60	30	20.0	20.0	19.8	19.8	19.7	19.0		
99.0Ni-Low C	B725	N02201	Str. rel.		41		-325	60	30	20.0	20.0	19.8	19.8	19.7	19.0		
33Ni-42Fe- 21Cr	B514	N08800	Annealed		45		-325	75	30	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0
72Ni-15Cr- 8Fe	B167	N06600	H.F. or H.F. ann.	≤5 O.D.	43		-325	80	30	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0
72Ni-15Cr- 8Fe	B167	N06600	C.D. ann.	>5 O.D.	43		-325	80	30	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0
33Ni-42Fe-	B407	N08800	C.D. ann.		45	(61)	-325	75	30	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0
21Cr 31Ni-31Fe-			Sol. ann.		45		-325	73	31	20.7			20.7				
29Cr-Mo	B668																10.3
99.0Ni	B161	N02200			41		-325	65	40	21.7			21.6				
99.0Ni	B725	N02200			41		-325	65	40	21.7			21.6				
35Ni-35Fe- 20Cr-Cb	B464		Annealed		45		-325	80	35	23.3			23.3				
35Ni-35Fe- 20Cr-Cb	B474	N08020	Annealed		45		-325	80	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	1,550	1,600	1,650	UNS No.	Spec. No.
														Nicke	el and	Nickel	Alloy -	— Pipes	and Tub	es (4a)
6.1	6.0	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2										N02201	B161
6.1	6.0	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2								•••		N02201	B725
																		20	N02200	B161
											•••						•••	(V	N02200	B725
7.3	7.2	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2									' 5	N02201	B161
7.3	7.2	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2		•••		•••				~G)		N02201 N02200	B725
									•••							· · · · ·	O ii		N02200	B161 B725
																NK		•••	NU2200	D/23
12.9	12.7	11.0	8.0												C				N04400	B165
	12.7		8.0											<u>k</u>	Y				N04400	B725
	16.7				16.6	16.3	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	0.8				N08800	B407
														X						
16.7	16.7	16.7	16.0	10.6	7.0	4.5	3.0	2.2	2.0				(२)						N06600	B167
15.3	15.0	14.7	14.5	14.2	14.0	13.8	11.6	9.3	7.4	5.9	4.7	3.8	3.0	2.4	1.9	1.4	1.1	0.86	N08810	B407
												e)								
15.3	15.0	14.7	14.5	14.2	14.0	13.8	11.6	9.3	7.4	5.9	4.7	3.8	3.0	2.4	1.9	1.4	1.1	0.86	N08810	B514
10.0	10.0	11.,	11.0	11.2	11.0	15.0	11.0	7.0	7.1	. 0	14	5.0	5.0	2.1	1.7	1.1	1.1	0.00	1100010	DOTT
15.3	15.0	14.7	14.5	14.2	14.0	13.8	12.9	10.4	8.3	6.7	5.4	4.3	3.4	2.7	2.2	1.6	1.2	0.91	N08811	B407
									X	Ò										
								.*.	St.											
14.5	14.3	11.0	8.0						,										N04400	B165
14.5	14.3	11.0	8.0					٠											N04400	B725
17.5	17.2						CO!												N08320	B619
						C	O_{i}													
17.5	17.2					C.	<i>.</i>												N08320	B622
					_(5													N02201	B161
					On														N02201	B725
20.0	20.0	20.0	20.0	20.0	19.9	17.0	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	0.8				N08800	B514
			. (2																
20.0	20.0	20.0	16.0	10.6	7.0	4.5	3.0	2.2	2.0										N06600	B167
20.0	20.0	20.0	16.0	10.6	7.0	45	3.0	22	2.0										N06600	R167
20.0	20.0	5	10.0	10.0	7.0	1.5	5.0	2.2	2.0			•••		•••	•••				1400000	DIO
	P																			
20.0	20.0	20.0	20.0	20.0	19.9	17.0	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	8.0				N08800	B407
	4=0	4																		D. ((0
17.7	17.2	16.7		•••					•••					•••	•••				N08028	8668
																			N02200	B161
																			N02200	B725
23.2	22.7																		N08020	B464
																				- · · ·
23.2	22.7																		N08020	B474

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

								Speci: Mir Strengt	1.	Bas	ic Allo			ss, <i>S</i> , I			1
Nominal Composition	Spec. No.	UNS No.	Class/ Condition/ Temper	Size Range, in.	P- No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300	400	500	600	650	700
Nickel and Ni		ov — Pipe		s (4a)	.,												
35Ni-35Fe- 20Cr-Cb	B729		Annealed		45		-325	80	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
42Ni-21.5Cr- 3Mo-2.3Cu	B163	N08825	Annealed		45		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
42Ni-21.5Cr- 3Mo-2.3Cu	B423	N08825	C.D. ann.		45		-325	85	35	23.3	23.3	23.3	23.3	23.3	2 3.3	23.3	23.3
42Ni-21.5Cr- 3Mo-2.3Cu	B474	N08825	Annealed		45		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
42Ni-21.5Cr- 3Mo-2.3Cu	B704	N08825	Annealed		45		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
42Ni-21.5Cr- 3Mo-2.3Cu	B705	N08825			45		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
47Ni-22Cr- 19Fe-6Mo	B619	N06007	Sol. ann.		45		-325	90	35	23.3	23.3	23.3	23.3	23.3	22.7	22.4	22.2
47Ni-22Cr- 19Fe-6Mo	B622	N06007	Sol. ann.		45		-325	90	35	23.3	23.3	23.3	23.3	23.3	22.7	22.4	22.2
40Ni-29Cr- 15Fe-5Mo	B619	N06030	Sol. ann.		45		-325	85	35	23.3	23.3	23.3	23.2	22.1	21.3	20.9	20.5
40Ni-29Cr- 15Fe-5Mo	B622	N06030	Sol. ann.		45		-325	85	35	23.3	23.3	23.3	23.2	22.1	21.3	20.9	20.5
40Ni-29Cr- 15Fe-5Mo	B626	N06030	Sol. ann.		45		-325	85	35	23.3	23.3	23.3	23.2	22.1	21.3	20.9	20.5
							×O										
72Ni-15Cr- 8Fe	B167	N06600	C.D. ann.	≤5 O.D.	43	Click	-325	80	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
72Ni-15Cr- 8Fe	B517	N06600	C.D. ann.		43		-325	80	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
58Ni-29Cr- 9Fe	B163	N06690	C.D. ann.	≤3 O.D.	43		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
58Ni-29Cr- 9Fe	B167	N06690	C.D. ann.	≤5 O.D.	43		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3	23.3	23.3
37Ni-33Fe- 25Cr	B163	N08120	Sol. ann.		45		-325	90	40	26.7	26.7	26.7	26.7	25.1	24.4	23.3	22.9
37Ni-33Fe- 25Cr	B407	N08120	Sol. ann.		45		-325	90	40	26.7	26.7	26.7	26.7	25.1	24.4	23.3	22.9
37Ni-33Fe- 25Cr	B514	N08120	Sol. ann.		45		-325	90	40	26.7	26.7	26.7	26.7	25.1	24.4	23.3	22.9
37Ni-33Fe- 25Cr	B515	N08120	Sol. ann.		45		-325	90	40	26.7	26.7	26.7	26.7	25.1	24.4	23.3	22.9
61Ni-16Mo- 16Cr	B619	N06455	Sol. ann.		43		-325	100	40	26.7	26.7	26.7	26.7	26.7	26.7	26.7	26.5

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	1,550	1,600		JNS No.	Spec. No.
]	Nickel a	nd Nick	cel Allo	ру — 1	Pipes a	nd Tubes ((4a) (Cont'd)
23.2	22.7																	NO	8020	B729
																		7/9	5	
23.2	23.0	22.9	22.8	22.6	22.3													ONO	8825	B163
23.2	23.0	22.9	22.8	22.6	22.3												0	NO NO	8825	B423
23.2	23.0	22.9	22.8	22.6	22.3											7	\$ 3	N0	8825	B474
23.2	23.0	22.9	22.8	22.6	22.3										c	W		N0	8825	B704
23.2	23.0	22.9	22.8	22.6	22.3									<u>k</u>	P			NO	8825	B705
22.0	21.8	21.7	20.0	19.5	18.9									()				NO	06007	B619
22.0	21.8																	NO	6007	B622
20.1	19.7											9	"" "					NO	6030	B619
20.1	19.7										7,4%							N0	06030	B622
20.1	19.7									-ije	5/11							NO	06030	B626
									×	0										
23.3	23.3	23.3	16.0	10.6	7.0	4.5	3.0	2.2	2.0									NO	06600	B167
23.3	23.3	23.3	16.0	10.6	7.0	4.5	3.0	2.2	2.0									NO	06600	B517
23.3	23.3	23.3	23.3				$\Theta_{b_{ij}}$											NO	06690	B163
23.3	23.3	23.3	23.3			<u>ر</u>	J											NO	06690	B167
)														
22.6	22.4	22.2	22.1	22.0	21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4 NO	8120	B163
22.6	22.4	22.2	22.1	22.0	21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4 NO	8120	B407
22.6	22.4	22.2	22.1	22.0	21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4 NO	8120	B514
22.6	22.4	22.2	22.1	22.0	21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4 NO	8120	B515
26.2	25.8																	N0	6455	B619

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

					••					Specia Mir Strengt	1.	s	tress, Te	S, ks mper	owabl i, at M ature, e (1)]	letal	
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size Range, in.	P- No. (5)	Notes	Min. Temp., °F (6)	Tensile		Min. Temp. to 100	200	300	400	500	600
Nickel and Nickel Allo	y — Pipe	s and	Tubes (4a)														
47Ni-22Cr-9Mo-18Fe		B619		N06002	Sol. ann.		43		-325	100	40	26.7	26.7	26.7	26.7	25.5	24.2
47Ni-22Cr-9Mo-18Fe		B622		N06002	Sol. ann.		43		-325	100	40	26.7	26.7	26.7	26.7	25.5	24.2
31Ni-33Fe-27Cr- 6.5Mo-Cu-N		B619		N08031	Annealed		45		-325	94	40	26.7	26.7	26.7	24.7	23.3	22.2
31Ni-33Fe-27Cr- 6.5Mo-Cu-N		B622		N08031	Annealed		45		-325	94	40	26.7	26.7	26.7	24.7	23.3	22.2
61Ni-16Mo-16Cr		B622		N06455	Sol. ann.		43		-325	100	40	26.7	26.7	26.7	26.7	26.7	26.7
54Ni-16Mo-15Cr		B619		N10276	Sol. ann.		43		-325	100	41	27,3	27.3	27.3	27.3	26.9	25.2
54Ni-16Mo-15Cr		B622		N10276	Sol. ann.		43		-325	100 👣	41	27.3	27.3	27.3	27.3	26.9	25.2
54Ni-16Mo-15Cr		B626			Sol. ann.		43		-325	100	41	27.3	27.3	27.3	27.3	26.9	25.2
67Ni-30Cu		B165		N04400	Str. rel		42	(54)	-325	85	55	28.3	28.3	28.3	28.3	28.3	
67Ni-30Cu		B725		N04400				(54)	-325	85	55	28.3			28.3		
46Fe-24Ni-21Cr-6Mo- Cu-N		B675			Annealed	>3/16	45	· .	-325	95	45	30.0			28.6		
46Fe-24Ni-21Cr-6Mo- Cu-N		B690		N08367	Annealed	>3/16	45	we'	-325	95	45	30.0	30.0	29.9	28.6	27.7	26.2
46Fe-24Ni-21Cr-6Mo- Cu-N		B804		N08367	Annealed	>3/16	45		-325	95	45	30.0	30.0	29.9	28.6	27.7	26.2
46Fe-24Ni-21Cr-6Mo- Cu-N		B675		N08367	Annealed	≤³∕16	45		-325	100	45	30.0	30.0	30.0	29.6	27.7	26.2
46Fe-24Ni-21Cr-6Mo- Cu-N		B690		N08367	Annealed	≤3/16	45		-325	100	45	30.0	30.0	30.0	29.6	27.7	26.2
46Fe-24Ni-21Cr-6Mo- Cu-N		B804		N08367	Annealed	≤³/ ₁₆	45		-325	100	45	30.0	30.0	29.9	28.6	27.7	26.2
55Ni-21Cr-13.5Mo		B619		N06022	Sol. ann.		43		-325	100	45	30.0	30.0	30.0	30.0	29.0	27.6
55Ni-21Cr-13.5Mo		B622		N06022	Sol. ann.		43		-325	100	45	30.0	30.0	30.0	30.0	29.0	27.6
58Ni-33Cr-8Mo		B619	(N06035	Sol. ann.		43		-325	85	35	23.3	23.3	23.3	22.2	20.6	19.7
58Ni-33Cr-8Mo		B622	··· C	N06035	Sol. ann.		43		-325	85	35	23.3	23.3	23.3	22.2	20.6	19.7
58Ni-33Cr-8Mo		B626		N06035	Sol. ann.		43		-325	85	35	23.3	23.3	23.3	22.2	20.6	19.7
59Ni-23Cr-16Mo		B619	Θ	N06059	Sol. ann.		43		-325	100	45	30.0	30.0	30.0	30.0	29.7	28.2
59Ni-23Cr-16Mo		B622		N06059	Sol. ann.		43		-325	100	45	30.0	30.0	30.0	30.0	29.7	28.2
59Ni-23Cr-16Mo		B626		N06059	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	29.7	28.2
59Ni-23Cr-16Mo- 1.6Cu	CHIC	B619		N06200	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	28.6	26.9
59Ni-23Cr-16Mo- 1.6Cu	1/2	B622		N06200	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	28.6	26.9
59Ni-23Cr-16Mo- 1.6Cu		B626			Sol. ann.	All	43		-325	100	45	30.0			30.0		
62Ni-22Mo-15Cr		B619			Sol. ann.	All	43		-325	105	45	30.0			30.0		
62Ni-22Mo-15Cr	•••	B622			Sol. ann.	All	43		-325	105	45	30.0			30.0		
62Ni-22Mo-15Cr		B626			Sol. ann.	All	43		-325	105	45	30.0			30.0		
62Ni-28Mo-5Fe		B619			Sol. ann.		44		-325	100	45	30.0			30.0		
62Ni-28Mo-5Fe		B622			Sol. ann.		44		-325	100	45	30.0			30.0		
65Ni-28Mo-2Fe		B619			Sol. ann.		44		-325	110	51	34.0			34.0		
65Ni-28Mo-2Fe		B622			Sol. ann.		44		-325	110	51	34.0			34.0		
65Ni-29.5Mo-2Fe-2Cr		B619			Sol. ann.		44		-325	110	51	34.0			34.0		
65Ni-29.5Mo-2Fe-2Cr	•••	B622			Sol. ann.		44		-325	110	51	34.0			34.0		
65Ni-29.5Mo-2Fe-2Cr		B626		N106/2	Sol. ann.		44		-325	110	51	34.0	34.0	34.0	34.0	34.0	34.0

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

	650	700	750	800	850	900	950	1.000	1.050	1.100	1.150	1.200	1.250	1.300	1.350	1,400	1,450	1.500	1.550	1.600	1.650	UNS No. or Grade	Spec. No.
-	000	700	700	000	050	700	750	1,000	1,050	1,100	1,150	1,200	1,250	1,500	1,550	1,100						and Tub	
	23.7	23.3	22.9	22.7	22.5	19.6	19.5	19.3	19.3	17.5	14.1	11.3	9.3	7.7	6.1	4.8	3.8	3.0				N06002	B619
						19.6		19.3	19.3	17.5	14.1	11.3	9.3	7.7	6.1	4.8	3.8	3.0			N	N06002	B622
			8.9																		O	N08031	B619
																				0	V		
:	21.7	11.1	8.9	7.2																S		N08031	B622
	26.7	26.5	26.1	25.8															<i>,.</i> \			N06455	B622
:	24.6	24.0	23.5	23.1	22.8	22.6	22.4	22.3	18.5	15.0	12.2	9.8	7.8						(/			N10276	B619
																		CH					
:	24.6	24.0	23.5	23.1	22.8	22.6	22.4	22.3	18.5	15.0	12.2	9.8	7.8				<i>C</i>					N10276	B622
:	24.6	24.0	23.5	23.1	22.8	22.6	22.4	22.3	18.5	15.0	12.2	9.8	7.8				1 12					N10276	B626
																4	O.						
																O _X						N04400	B165
) Y						N04400	B725
:	25.6	25.1	24.7	24.3	23.9	23.6																N08367	B675
:	25.6	25.1	24.7	24.3	23.9	23.6								بر ان								N08367	B690
		. . .	a. -																				2001
-	25.6	25.1	24.7	24.3	23.9	23.6							N									N08367	B804
:	25.6	25.1	24.7	24.3	23.9	23.6						į	6									N08367	B675
:	25.6	25.1	24.7	24.3	23.9	23.6					بلخي .											N08367	B690
:	25.6	25.1	24.7	24.3						Ċ,												N08367	B804
	27.0	26.5	26.1	25.7					1													N06022	B619
	27.0	26.5	26.1	25.7																		N06022	B622
	19.4	19.2	19.0	18.8				(N06035	B619
:	19.4	19.2	19.0	18.8				Ci	-													N06035	B622
	19.4	19.2	19.0	18.8				γ														N06035	B626
:	27.5	26.8	26.1	25.5			\bigcirc															N06059	B619
:	27.5	26.8	26.1	25.5		1	1															N06059	B622
:	27.5	26.8	26.1	25.5		(=,																N06059	B626
	26.2	25.7	25.4	25.2	7)																N06200	B619
:	26.2	25.7	25.4	25.2																		N06200	B622
:	26.2	25.7	25.4	25.2																		N06200	B626
:	27.3	27.0	26.7	26.4																		N10362	B619
:	27.3	27.0	26.7	26.4																		N10362	B622
:	27.3	27.0	26.7	26.4																		N10362	B626
	30.0	30.0	30.0	29.9																		N10001	B619
	30.0	30.0	30.0	29.9																		N10001	B622
	34.0	34.0	34.0	34.0																		N10665	B619
	34.0	34.0	34.0	34.0																		N10665	B622
	34.0	34.0	33.9	33.5																		N10675	B619
	34.0	34.0	33.9	33.5																		N10675	B622
	34.0	34.0	33.9	33.5																		N10675	B626

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specif Min Strengtl	١.	S	tress, Te	S, ks mper	owabl i, at M ature, e (1)]	letal	
Nominal Composition	Product Form	Spec.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size Range, in.	P- No. (5)	Notes	Min. Temp., °F (6)	Tensile	Vield	Min. Temp. to 100	200	300	400	500	600
Nickel and Nickel Allo					Temper		(0)	110105	. (0)	10110110	11014	100		000	100	500	
60Ni-22Cr-9Mo-3.5Cb		B444	1	N06625	Annealed		43	(64)(70)	-325	120	60	40.0	40.0	39.6	39.2	38.6	37.8
60Ni-22Cr-9Mo-3.5Cb		B705	1	N06625	Annealed		43	(64)(70)	-325	120	60	40.0	40.0	39.6	39.2	38.6	37.8
57Ni-22Cr-14W-2Mo- La		B619		N06230	Sol. ann.		43		-325	110	45	30.0	30.0	30.6	30.0	30.0	29.6
57Ni-22Cr-14W-2Mo- La		B622		N06230	Sol. ann.		43		-325	110	45	30.0	30.0	30.0	30.0	30.0	29.6
57Ni-22Cr-14W-2Mo- La		B626		N06230	Sol. ann.		43		-325	110	45	30.0	30.0	30.0	30.0	30.0	29.6
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B619		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9	28.1	26.1	24.7	23.8
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B622		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9	28.1	26.1	24.7	23.8
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B626		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9	28.1	26.1	24.7	23.8
Nightal and Nightal Alla	Dlat	aa and	Chaota (4a	a				61									
Nickel and Nickel Allog 99.0Ni-Low C	y — Piat Plate	es and B162	•	•	H.R. ann.		41	0,	-325	50	12	8.0	7.7	7.5	7.5	7.5	7.5
99.0Ni-Low C	Plate	B162			H.R. as R.	•••	41	W.	-325	50	12	8.0	7.7	7.5	7.5	7.5	7.5
99.0Ni	Plate	B162		N02201	H.R. ann.		41		-325	55	15	10.0			10.0		
99.0Ni	Plate	B162		N02200	H.R. as R.		41		-325	55	20	13.3			13.3		
33Ni-42Fe-21Cr		B409		N08810	Annealed	All	45		-325	65	25	16.7			16.7		
33Ni-42Fe-21Cr-Al-Ti		B409			Annealed	All	45		-325	65	25	16.7			16.7		
26Ni-22Cr-5Mo-Ti		B620		N08320	Sol. ann.	All	45		-325	75	28	18.7	18.7	18.7	18.7	18.7	18.6
67Ni-30Cu	Plate	B127			H.R. ann.		42		-325	70	28	18.7	16.4	15.2	14.7	14.7	14.7
47Ni-22Cr-19Fe-6Mo		B582		N06007	Sol. ann.	>3/4	45		-325	85	30	20.0	20.0	20.0	20.0	20.0	19.5
33Ni-42Fe-21Cr		B409		N08800	Annealed	All	45		-325	75	30	20.0	20.0	20.0	20.0	20.0	20.0
31Ni-31Fe-29Cr-Mo		B709	(N08028	Sol. ann.		45		-325	73	31	20.7	20.7	20.7	20.7	20.7	19.5
42Ni-21.5Cr-3Mo- 2.3Cu		B424		N08825	Annealed		45		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3
35Ni-35Fe-20Cr-Cb		B463	\bigcirc	N08020	Annealed	All	45		-325	80	35	23.3	23.3	23.3	23.3	23.3	23.3
40Ni-29Cr-15Fe-5Mo		B582		N06030	Sol. ann.	All	45		-325	85	35	23.3	23.3	23.3	23.2	22.1	21.3
47Ni-22Cr-19Fe-6Mo	·:·C	B582		N06007	Sol. ann.	≤3/4	45		-325	90	35	23.3	23.3	23.3	23.3	23.3	22.7
47Ni-22Cr-9Mo-18Fe	EM	B435		N06002	H.R. sol. ann.	All	43		-325	95	35	23.3	23.3	23.3	23.3	22.3	21.2
72Ni-15Cr-8Fe	Plate	B168		NUEEUU	H.R. ann.		43		-325	80	35	23.3	23.3	233	23.3	233	23.3
72Ni-15Cr-8Fe	Plate	B168			H.R. as R.		43		-325	85	35	23.3			23.3		
58Ni-29Cr-9Fe	Plate	B168			Annealed	 ≥³/ ₁₆	43		-325	85	35	23.3			23.3		
58Ni-29Cr-9Fe	Sheet	B168			Annealed	0.018- 0.250	43		-325	85	35	23.3			23.3		
67Ni-30Cu	Plate	B127		N04400	H.R. as R.		42		-325	75	40	25.0	25.0	24.7	23.9	23.4	23.1
37Ni-33Fe-25Cr		B409		N08120	Sol. ann.	All	45		-325	90	40	26.7	26.7	26.7	26.7	25.1	24.4
31Ni-33Fe-27Cr- 6.5Mo-Cu-N		B625		N08031	Annealed	All	45		-325	94	40	26.7	26.7	26.7	24.7	23.3	22.2
61Ni-16Mo-16Cr		B575		N06455	Sol. ann.	All	43		-325	100	40	26.7	26.7	26.7	26.7	26.7	26.7
54Ni-16Mo-15Cr		B575		N10276	Sol. ann.	All	43		-325	100	41	27.3	27.3	27.3	27.3	26.9	25.2
60Ni-22Cr-9Mo-3.5Cb	Plate	B443	1	N06625	Annealed	All	43	(64)(70)	-325	110	55	36.7	36.7	36.3	35.9	35.4	34.7

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	1,550	1,600	1,650	UNS No. or Grade	Spec. No.
															Nickel	and N	ickel Al	loy —	Pipes a	ınd Tub	es (4a) (Cont'd)
37.4	37.0	36.6	36.3	36.1	35.8	35.4	31.2	31.2	23.1	21.0	13.2										N06625	B444
37.4	37.0	36.6	36.3	36.1	35.8	35.4	31.2	31.2	23.1	21.0	13.2									~~^	N06625	B705
29.1	28.7	28.4	28.2	28.2	28.2	28.2	28.2	28.2	23.2	19.0	15.6	12.9	10.6	8.5	6.7	5.3	4.1	2.9	2.1	115	N06230	B619
																			C) .		
29.1	28.7	28.4	28.2	28.2	28.2	28.2	28.2	28.2	23.2	19.0	15.6	12.9	10.6	8.5	6.7	5.3	4.1	2.9	2.1	1.5	N06230	B622
29 1	28 7	7 28 4	28.2	28.2	28.2	282	28.2	28.2	23.2	19.0	15.6	12.9	10.6	8.5	6.7	5.3	4.1	2	2.1	1.5	N06230	B626
27.1	20.7	20.1	20.2	20.2	20.2	20.2	20.2	20.2	20.2	17.0	15.0	12.7	10.0	0.5	0.7	5.5	1.1	√ .~	2.1	1.0	1100230	DOLO
																	S					
23.5	23.1	22.9	22.6													6	5				R20033	B619
																6						
23.5	23.1	22.9	22.6													Θ,					R20033	B622
23.5	23 1	22.9	22.6																		R20033	B626
25.5	20.1	. 22.)	22.0											···· <	\mathcal{V}						1120033	D020
														11.								
													K	D,		Nick	el and l	Nickel	Alloy -	- Plates	and Shee	ets (4a)
7.5	7.4	7.4	7.2	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2		Q _N	٠							N02201	B162
7.5	7.4	7.4	7.2	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2		0.								N02201	B162
												SH									N02200	B162
												(0									N02200	B162
16.2	15.8	15.5	15.1	14.9	14.6	14.3	14.0	13.8	11.6	9.3	7.4	5.9	4.7	3.8	3.0	2.4	1.9	1.4	1.1	0.86	N08810	B409
16.1	15.7	15.3	15.0	14.7	14.5	14.2	14.0	13.7	12.9	10.4	8.3	6.7	5.4	4.3	3.4	2.7	2.2	1.6	1.2	0.91	N08811	B409
										CY	•											
18.2	17.8	17.5	17.2																		N08320	B620
14.7	14.6	14.5	14.3	11.0	8.0				٠.,												N04400	B127
19.2	19.0	18.8	18.7	18.6	18.5	18.4	18.3														N06007	B582
20.0	20.0	20.0	20.0	20.0	20.0	20.0	19.9	17.0	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	8.0				N08800	B409
18.9	18.3	17.7	17.2	16.7			, ,)													N08028	B709
23.3	23.3	23.2	23.0	22.9	22.8	22.6	22.3														N08825	B424
22.2	22.		22.7			7)														NOOOOO	D462
		23.2 20.1													•••						N08020	B463
		22.0		•	20.0	105	 18.9														N06030 N06007	B582 B582
		22.0			20.0	17.3	10.9		•••						•••			•••			N06007	B435
20.7	20.0	20.1		7	•••				•••						•••			•••			1100002	D 100
		•	Vr																			
23.3	23.3	23.3	23.3	23.3	16.0	10.6	7.0	4.5	3.0	2.2	2.0										N06600	B168
23.3	23.3	1						4.5		2.2	2.0										N06600	B168
23.3	23.3	23.3	23.3	23.3	23.3																N06690	B168
23.3	23.3	23.3	23.3	23.3	23.3																N06690	B168
		20.0																			N04400	B127
							21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4	N08120	B409
21.7	21.3	20.9	20.5																		N08031	B625
26.7	26 5	26.1	25 Q																		N06455	B575
								18.5	 15.0	 12.2	 9.8	 7.8									N10276	
24.0	4T.(. 23.3	23.1	22.0	22.0	22.T	22.3	10.5	13.0	14.4	7.0	7.0				•••			•••		11102/0	טוטע
34.9	33 (1 32 6	33 3	22 1	32.0	32 5	31 2	31.2	22.1	21.0	122										N06625	R4.4.2
54.5	55.5	55.0	55.5	55.1	32.0	34.3	31.4	31.4	43.1	21.0	13.4	•••			•••	•••		•••			1100023	CPFU

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specif Min		s	tress,	S, ks	owabl i, at M ature	Ietal	
										Strengtl	h, ksi		°F	[Note	e (1)]		
					Cl /	C!			341			Min.					
Nominal	Product	Spec.	Type/	UNS	Class/ Condition/	Size Range.	P- No.		Min. Temp.,			Temp. to					
Composition	Form	No.	Grade	No.	Temper	in.	(5)	Notes	°F (6)	Tensile	Yield	100	200	300	400	500	600
Nickel and Nickel Allo	y — Plate	es and	Sheets (4a)													
57Ni-22Cr-14W-2Mo- La		B435		N06230	Sol. ann.	All	43		-325	110	45	30.0	30.0	30.0	30.0	30.0	29.6
55Ni-21Cr-13.5Mo	Sheet	B575		N06022	Sol. ann.	< ³ / ₁₆	43		-325	100	45	30.0	30.0	30.0	30.0	29.0	27.6
58Ni-33Cr-8Mo		B575		N06035	Sol. ann.	All	43		-325	85	35	23.3	23.3	23.3	22.2	20.6	19.7
46Fe-24Ni-21Cr-6Mo- Cu-N		B688		N08367	Annealed	>3/16	45		-325	95	45	30.0	30.0	29.9	28.6	27.7	26.2
46Fe-24Ni-21Cr-6Mo- Cu-N		B688		N08367	Annealed	≤³/ ₁₆	45		-325	100	45	30.0	30.0	30.0	29.6	27.7	26.2
59Ni-23Cr-16Mo		B575		N06059	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	29.6	28.1
59Ni-23Cr-16Mo-		B575		N06200	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	28.6	26.9
1.6Cu										Š	•						
62Ni-22Mo-15Cr		B575		N10362	Sol. ann.	All	43		-325	105	45	30.0	30.0	30.0	30.0	28.9	27.7
62Ni-28Mo-5Fe	Plate	B333		N10001	Sol. ann.	$\geq \frac{3}{16}$, $\leq 2\frac{1}{2}$	44		-325	100	45	30.0	30.0	30.0	30.0	30.0	30.0
62Ni-28Mo-5Fe	Sheet	B333		N10001	Sol. ann.	<³/ ₁₆	44		-325	115	50	33.3	33.3	33.3	33.3	33.3	33.3
65Ni-28Mo-2Fe		B333		N10665	Sol. ann.	All	44	<i>(N</i>)	-325	110	51	34.0	34.0	34.0	34.0	34.0	34.0
65Ni-29.5Mo-2Fe-2Cr		B333		N10675	Sol. ann.	All	44	we.	-325	110	51	34.0	34.0	34.0	34.0	34.0	34.0
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B625		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9	28.1	26.1	24.7	23.8
Nickel and Nickel Allo	y — Forg	ings a	nd Fittings	(4a)		7.											
99.0Ni-Low C		B160		N02201	Annealed,	All	41	(9)(9a)	-325	50	10	6.7	6.4	6.3	6.3	6.3	6.3
99.0Ni-Low C		B366		N02201	Annealed	All	41	(32)(74)	-325	50	10	6.7	6.4	6.3	6.3	6.3	6.3
99.0Ni		B366		N02200	Annealed	All	41	(32)(74)	-325	55	15	10.0	10.0	10.0	10.0	10.0	10.0
33Ni-42Fe-21Cr		B564			Annealed		45		-325 -325	65	25	16.7	16.7				
33Ni-42Fe-21Cr-Al-Ti	•••	B564			Annealed		45	7.7	-325 -325	65	25	16.7	16.7				
33Ni-42Fe-21Cr 33Ni-42Fe-21Cr		B366		~ _	Annealed	 All		(9)(74)	-325 -325	65	25	16.7	16.7				
33Ni-42Fe-21Cr-Al-Ti	•••	В366			Annealed	All		(9)(74)	-325 -325	65	25	16.7	16.7				
67Ni-30Cu		B564			Annealed		42		-325 -325	70	25	16.7	14.6				
67Ni-30Cu		B366	\circ		Annealed	 All		(32)(74)	-325 -325	70	25	16.7	14.6				
07NI-30Cu		ВЗОО	,	N04400	Aimealeu	All	42	(32)(74)	-323	70	23	10.7	14.0	13.0	13.2	13.1	13.1
72Ni-15Cr-8Fe	ΞC	B366		N06600	Annealed	All	43	(32)(74)	-325	75	25	16.7	16.7				
40Ni-29Cr-15Fe-5Mo	1P	B366		N06030	Sol. ann.	All	45	(74)	-325	85	35	23.3	23.3	23.3	23.2	22.1	21.3
40Ni-29Cr-15Fe-5Mo	V	B462		N06030	Sol. ann.	All	45		-325	85	35	23.3	23.3	23.3	23.2	22.1	21.3
33Ni-42Fe-21Cr		B366		N08800	C.D. ann.	All	45	(74)	-325	75	30	20.0	20.0	20.0	20.0	20.0	20.0
33Ni-42Fe-21Ci		B564		N08800	Annealed		45	(9)	-325	75	30	20.0	20.0	20.0	20.0	20.0	20.0
35Ni-35Fe-20Cr-Cb		B366		N08020	Annealed	All	45	(74)	-325	80	35	23.3	23.3	23.3	23.3	23.3	23.3
35Ni-35Fe-20Cr-Cb		B462		N08020	Annealed		45		-325	80	35	23.3	23.3				
72Ni-15Cr-8Fe		B564		N06600	Annealed	All		(9)	-325	80	35	23.3	23.3				
42Ni-21.5Cr-3Mo- 2.3Cu		B366		N08825	C.D. ann.	All	45	(74)	-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3
42Ni-21.5Cr-3Mo- 2.3Cu		B564		N08825	Annealed		45	•••	-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3
58Ni-29Cr-9Fe	Forg.	B564		N06690	Annealed	All	43	(9)	-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Basic Allowable Stress, S, ksi, at Metal Temperature, °F [Note (1)]

650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	1,550	1,600	1,650	UNS No. or Grade	Spec. No.
]	Nickel a	nd Nic	kel Allo	oy — I	Plates a	nd She	ets (4a) (Cont'd)
29.1	28.7	28.4	28.2	28.2	28.2	28.2	28.2	28.2	23.2	19.0	15.6	12.9	10.6	8.5	6.7	5.3	4.1	2.9	2.1	1.5	N 06230	B435
27.0	26.5	26.1	25.7																	0	N06022	B575
			18.8																0	1	N06035	B575
																			N:)		
25.6	25.1	24.7	24.3	23.9	23.6													. 0	3-)		N08367	B688
25.6	25.1	24.7	24.3	23.9	23.6													(-)			N08367	B688
27.5	26.7	26.1	25.6														C				N06059	B575
26.2	25.7	25.4	25.2													7 .5	>				N06200	B575
27 2	27.0	26.7	26.4													0					N10362	B575
			29.8		•••	•••			•••						Ä	•••	•••				N10001	B333
30.0	50.0	50.0	29.0		•••									<)\						NIOUUI	Б333
33.3	33.3	33.3	33.2											11.							N10001	B333
34.0	34.0	34.0	34.0										🗴	D.							N10665	B333
34.0	34.0	33.9	33.5										S								N10675	B333
23.5	23.1	22.9	22.6									W,	 (1)								R20033	B625
											i	6										
											\sim	•			Ni	ckel ar	nd Nick	el Allo	oy — Fo	rgings	and Fittin	gs (4a)
6.2	6.2			5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2										N02201	B160
6.2	6.2	6.1	6.0	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2										N02201	B366
									C),												2011
																					N02200	B366
			15.0				14.0	13.8	•	9.3	7.4	5.9	4.7	3.8	3.0	2.4	1.9	1.4	1.1	0.86	N08810	B564
			15.0				14.0	13.8	12.9	10.4	8.3	6.7	5.4	4.3	3.4	2.7	2.2	1.6	1.2	0.91	N08811	B564
			15.0				14.0	√ 13.8 13.8	11.6 12.9	9.3	7.4 8.3	5.9	4.7	3.8	3.0	2.4 2.7	1.9 2.2	1.4	1.1 1.2	0.86 0.91	N08810	B366 B366
			12.7			14.4	14.0	13.0		10.4		6.7	5.4	4.3	3.4			1.6			N08811	
			12.7		8.0 8.0	S)	<i></i>										•••				N04400 N04400	B564 B366
				•	2	7.				•••						•••	•••				N04400	D300
			16.7		15.9	10.6	7.0	4.5	3.0	2.2	2.0										N06600	B366
			19.7																		N06030	B366
			19.7																		N06030	B462
		_	20.0				19.9	17.0	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	8.0				N08800	B366
20.0	20.0	20.0	20.0	20.0	20.0	20.0	19.9	17.0	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	0.8				N08800	B564
			22.7																		N08020	
			22.7																		N08020	
23.3	23.3	23.3	23.3	23.3	16.0	10.6	7.0	4.5	3.0	2.2	2.0										N06600	B564
23.3	23.3	23.2	23.0	22.9	22.8	22.6	22.3														N08825	B366
23.3	23.3	23.2	23.0	22.9	22.8	22.6	22.3														N08825	B564
23.3	23.3	23.3	23.3	23.3	23.3																N06690	B564

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifi Min		s	Basic Al Stress, S, ks Tempe	si, at M	1etal	
										Strength			°F [No			
					Class/	Size	P-		Min.			Min. Temp.				
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Range, in.	No. (5)	Notes	Temp., °F (6)	Tensile	Yield	to 100	200 300	400	500	600
Nickel and Nickel Allo	y — Forg	gings ar	nd Fittings	(4a)	<u> </u>											
37Ni-33Fe-25Cr		B366		N08120	Sol. ann.	All	45		-325	90	40	26.7	26.7 26.7	26.7	25 .1	24.4
37Ni-33Fe-25Cr		B564		N08120	Sol. ann.	All	45		-325	90	40	26.7	26.7 26.7	26.7	25.1	24.4
47Ni-22Cr-9Mo-18Fe		B366		N06002	Sol. ann.	All	43	(32)	-325	100	40	26.7	26.7 26.7	26.7	25.5	24.2
31Ni-33Fe-27Cr- 6.5Mo-Cu-N	•••	B366		N08031	Sol. ann.	All	45	(74)	-325	94	40	26.7	26.7 26.7	24.7	23.3	22.2
31Ni-33Fe-27Cr- 6.5Mo-Cu-N		B564		N08031	Annealed H.W.	All	45		-325	94	40	26.7	26.7 26.7	24.7	23.3	22.2
54Ni-16Mo-15Cr		B366		N10276	Sol. ann.	All	43	(74)	-325	100	41	27.3	27.3 27.3	27.3	26.9	25.2
54Ni-16Mo-15Cr		B462		N10276	Sol. ann.	All	43	(9)	-325	100	41	27.3	27.3 27.3	27.3	26.9	25.2
54Ni-16Mo-15Cr		B564		N10276	Sol. ann.	All	43	(9)	-325	100	41	27.3	27.3 27.3	27.3	26.9	25.2
62Ni-28Mo-5Fe		B366		N10001	Sol. ann.	All	44	(32)	-325	100	45	30.0	30.0 30.0	30.0	30.0	30.0
55Ni-21Cr-13.5Mo		B366		N06022	Sol. ann.	All	43	(32)(74)	-325	100	45	30.0	30.0 30.0	30.0	29.0	27.6
55Ni-21Cr-13.5Mo		B462		N06022	Sol. ann.	All	43		-325	100	45	30.0	30.0 30.0	30.0	30.0	27.6
55Ni-21Cr-13.5Mo		B564		N06022	Sol. ann.	All	43	O _(Q)	-325	100	45	30.0	30.0 30.0	30.0	29.0	27.6
58Ni-33Cr-8Mo		B366		N06035	Sol. ann.	All	•	(32)(74)	-325	85	35	23.3	23.3 23.3	22.2	20.6	19.7
58Ni-33Cr-8Mo		B462		N06035	Sol. ann.	All _	43	(9)	-325	85	35	23.3	23.3 23.3	22.2	20.6	19.7
58Ni-33Cr-8Mo		B564		N06035	Sol. ann.	All	43	(9)	-325	85	35	23.3	23.3 23.3	22.2	20.6	19.7
59Ni-23Cr-16Mo		B366		N06059	Sol. ann.	All	43	(74)	-325	100	45	30.0	30.0 30.0	30.0	29.7	28.2
59Ni-23Cr-16Mo	•••	B564		N06059	H.W. sol. ann.	All	43		-325	100	45	30.0	30.0 30.0	30.0	29.7	28.2
59Ni-23Cr-16Mo- 1.6Cu		B366		N06200	Søl. ann.	All	43	(74)	-325	100	45	30.0	30.0 30.0	30.0	28.6	26.9
59Ni-23Cr-16Mo- 1.6Cu		B462		N06200	Sol. ann.	All	43		-325	100	45	30.0	30.0 30.0	30.0	28.6	26.9
59Ni-23Cr-16Mo- 1.6Cu		B564		N06200	Sol. ann.	All	43		-325	100	45	30.0	30.0 30.0	30.0	28.6	26.9
62Ni-22Mo-15Cr		B366	<u>ک</u>	N10362	Sol. ann.	All	43	(9)	-325	105	45	30.0	30.0 30.0	30.0	28.9	27.7
62Ni-22Mo-15Cr	•••	B462	\sim	N10362	Sol. ann.	All	43	(9)	-325	105	45	30.0	30.0 30.0	30.0	28.9	27.7
62Ni-22Mo-15Cr		B564		N10362	Sol. ann.	All	43	(9)	-325	105	45	30.0	30.0 30.0	30.0	28.9	27.7
60Ni-22Cr-9Mo-3.5Cb		B564		N06625	Annealed	≤4	43	(9)(64)	-325	120	60	40.0	40.0 39.6	39.2	38.6	37.8
)`														
65Ni-28Mo-2Fe	N	B366		N10665	Sol. ann.	All	44	(74)	-325	110	51	34.0	34.0 34.0			
65Ni-29.5Mo-2Fe-2Cr	//	B366			Sol. ann.	All		(74)	-325	110	51	34.0	34.0 34.0			
65Ni-29.5Mo-2Fe-2Ci		B462			Sol. ann.	All	44		-325	110	51	34.0	34.0 34.0			
65Ni-29.5Mo-2 Fe-2 Cr		B564			Sol. ann.	All	44		-325	110	51	34.0	34.0 34.0			
57Ni-22Cr-14W-2Mo- La	•••	B564		N06230	Sol. ann.	All	43		-325	110	45	30.0	30.0 30.0	30.0	30.0	29.6
57Ni-22Cr-14W-2Mo- La		B366		N06230	Sol. ann.	All	43	(74)	-325	110	45	30.0	30.0 30.0	30.0	30.0	29.6
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B366		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9 28.1	26.1	24.7	23.8
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B462		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9 28.1	26.1	24.7	23.8
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B564		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9 28.1	26.1	24.7	23.8

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Basic Allowable Stress, S, ksi, at Metal Temperature, °F [Note (1)]

																					UNS	
650	700	750	900	050	000	050	1 000	1 050	1 100	1 150	1 200	1 250	1 200	1 250	1 400	1 450	1 500	1 550	1 600	1 650	No. or	Spec.
650	700	/50	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300		1,400						Grade gs (4a) (No.
23.3	22.9	22.6	22.4	22.2	22.1	22.0	21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0		N08120	B366
							21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4	N08120	B564
			22.7				19.3	19.3	17.5	14.1	11.3	9.3	7.7	6.1	4.8	3.8	3.0			O	N06002	B366
21.7	21.3	20.9	20.5																0)	N08031	B366
																		,	1			
21.7	21.3	20.9	20.5															0). D.		N08031	B564
																		6. Y				
24.6	24.0	23.5	23.1	22.8	22.6	22.4	22.3	18.5	15.0	12.2	9.8	7.8					Co.	X			N10276	B366
							22.3	18.5	15.0	12.2	9.8	7.8				6	(S)				N10276	B462
24.6	24.0	23.5	23.1	22.8	22.6	22.4	22.3	18.5	15.0	12.2	9.8	7.8				<u> </u>					N10276	B564
															1	0,						
30.0	30.0	30.0	29.9												W.						N10001	B366
														. <								
27.0	26.5	26.1	25.7											111							N06022	B366
27.0	26.5	26.1	25.7										×	6							N06022	B462
27.0	26.5	26.1	25.7										NO.								N06022	B564
19.4	19.2	19.0	18.8									7,	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>								N06035	B366
			18.8									07									N06035	B462
			18.8								-7										N06035	B564
			25.5								(O										N06059	B366
27.5	26.8	26.1	25.5			•••		•••		4											N06059	B564
26.2	25.7	25.4	25.2						(10											N06200	B366
									. •)												
26.2	25.7	25.4	25.2		•••				<u></u>												N06200	B462
26.2	25.7	25.4	25.2					·O`													N06200	B564
								"כ														
27.3	27.0	26.7	26.4				⟨ ∪.														N10362	B366
			26.4			2	ノ														N10362	B462
			26.4		7																N10362	B564
37.4	37.0	36.6	36.3	36.1	35.8	35.4	31.2	31.2	23.1	21.0	13.2										N06625	B564
) `																****	2011
	34.0		()	7		•••			•••		•••		•••					•••			N10665	B366
	34.0 34.0	-	33.5		•••	•••			•••							•••					N10675 N10675	B366
			33.5		•••																	B462 B564
	,	Y .			 28 2		 28.2	 28 2	23.2	 19.0	 15.6	 12.9	10.6	 8.5	 6.7	5.3	4.1	 2.9	2.1	 1.5	N10675 N06230	B564
27.1	20.7	20.1	20.2	20.2	20.2	20.2	20.2	20.2	25.2	17.0	15.0	12.7	10.0	0.5	0.7	5.5	1.1	2.7	2.1	1.0	1100230	D501
29.1	28.7	28.4	28.2	28.2	28.2	28.2	28.2	28.2	23.2	19.0	15.6	12.9	10.6	8.5	6.7	5.3	4.1	2.9	2.1	1.5	N06230	B366
22 5	22.1	22 Q	22.6																		R20033	B366
23.3	20.1	,	22.0																		1120000	2500
23.5	23.1	22.9	22.6																		R20033	B462
20.5	22.4	20.0	20.4																		Daccas	DEC.
23.5	23.1	22.9	22.6																		R20033	B564

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

										Specifi Min.		s	tress, S Ten	S, ksi ipera	ature,	letal ,	
										Strength	, ksi		°F	Note	(1)]		
Nominal	Product	-	Type/	UNS	Class/ Condition/	Size Range,	P- No.		Min. Temp.,			Min. Temp. to					
Composition	Form	No.	Grade	No.	Temper	in.	(5)	Notes	°F (6)	Tensile Y	lield	100	200	300	400	500	600
Nickel and Nickel Allo	•			Nonana	77.747	4.11	4.1	(0)	225	60	15	10.0	100		1004	~ 0 0	10.0
99.0Ni		B160		N02200		All		(9)	-325	60 55	15	10.0 10.0	10.0 1			7)	
99.0Ni	•••	B160		NU2200	Annealed	All	41	(9)	-325	55	15	10.0	10.0	10.0	9.00	,10.0	10.0
67Ni-30Cu		B164		N04400	Ann. forg.	All	42	(13)	-325	70	25	16.7	14.6	13.6	13.2	13.1	13.1
33Ni-42Fe-21Cr	Bar	B408		N08810	Sol. tr. or ann.		45		-325	65	25	16.7	16.7 1	16.7	16.7	16.7	16.5
33Ni-42Fe-21Cr-Al-Ti	Bar	B408		N08811	Sol. tr. or ann.		45		-325	65	25	16.7	16.7	16.7	16.7	16.7	16.5
33Ni-42Fe-21Cr	Bar	B408		N08800	H.F.		45		-325	75 \ \	30	20.0	20.0 2	20.0	20.0	20.0	20.0
26Ni-22Cr-5Mo-Ti		B621		N08320	Sol. ann.	All	45		-325	75	28	18.7	18.7	18.7	18.7	18.7	18.6
47Ni-22Cr-19Fe-6Mo		B581		N06007	Sol. ann.	>3/4	45		-325	85	30	20.0	20.0	20.0	20.0	20.0	19.5
42Ni-21.5Cr-3Mo- 2.3Cu		B425			Annealed		45	ne)	-325	85	35	23.3	23.3				
58Ni-29Cr-9Fe	Bar	B166		N06690	H.R.	>3	43		-325	85	35	23.3	23.3	23.3	23.3	23.3	23.3
58Ni-29Cr-9Fe	Bar	B166		N06690	H.R or C.D. ann.	All	43		-325	85	35	23.3	23.3 2	23.3	23.3	23.3	23.3
47Ni-22Cr-19Fe-6Mo		B581		N06007	Sol. ann. 🤸	3 / ₄	45		-325	90	35	23.3	23.3	23.3	23.3	23.3	22.7
40Ni-29Cr-15Fe-5Mo		B581		N06030	Sol. ann.	All	45		-325	85	35	23.3	23.3 2	23.3	23.2	22.1	21.3
37Ni-33Fe-25Cr		B408		N08120	Sol. ann.	All	45		-325	90	40	26.7	26.7	26.7	26.7	25.1	24.4
31Ni-33Fe-27Cr- 6.5Mo-Cu-N		B649		Ola	Ånnealed	All	45		-325	94	40	26.7	26.7				
67Ni-30Cu		B164	() کرک	N04400	H.W.	All except hex.	42		-325	80	40	26.7	25.8 2	24.8	23.9	23.4	23.1
			\sim			>21/8											
58Ni-33Cr-8Mo		B574	<u>)</u>		Sol. ann.	All		(9)	-325	85	35	23.3	23.3				
61Ni-16Mo-16Cr		B574	·		Sol. ann.	All		(9)	-325	100	40	26.7	26.7				
54Ni-16Mo-15Cr 62Ni-22Mo-15Cr		B574 B574			Sol. ann. Sol. ann.	All	43	 (9)	-325 -325	100 105	41	27.3	27.3 2				
60Ni-22Cr-9Mo-3.5Cb		В446			Annealed	All >4 to 10		7.7	-325	110	45 50	30.0	30.0 3 33.3 3				
60Ni-22Cr-9Mo-3.5Cb		B446	1	N06625	Annealed	≤4	43	(9)(64) (70)	-325	120	60	40.0	40.0	40.0	40.0	38.3	38.0
57Ni-22Cr-14W-2Mo- La		B572		N06230	Sol. ann.	All	43		-325	110	45	30.0	30.0	30.0	30.0	30.0	29.6
59Ni-23Cr-16Mo		B574		N06059	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	29.7	28.2
59Ni-23Cr-16Mo- 1.6Cu		B574		N06200	Sol. ann.	All	43		-325	100	45	30.0	30.0	30.0	30.0	28.6	26.9
65Ni-29.5Mo-2Fe-2Cr		B335		N10675	Sol. ann.	All	44		-325	110	51	34.0	34.0	34.0	34.0	34.0	34.0
33Cr-31Ni-32Fe- 1.5Mo-0.6Cu-N		B649		R20033	Sol. ann.	All	45		-325	109	55	36.3	30.9 2	28.1	26.1	24.7	23.8

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Basic Allowable Stress, S, ksi, at Metal Temperature, °F [Note (1)]

650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450				1,650		Spec. No.
																	Nickel	and N	ickel A	lloy — l	Rod and Ba	
						•••															N02200	B160
																				On	N02200	B160
																				、レ		
13.1	13.0	12.9	12.7	11.0	8.0														No. 3)	N04400	B164
																			٠,/,			
																		. &)			
16.1	15.7	15.3	15.0	14.7	14.5	14.2	14.0	13.8	11.6	9.3	7.4	5.9	4.7	3.8	3.0	2.4	1.9	1.4	1.1	0.86	N08810	B408
16.1	157	153	15.0	147	145	14 2	14.0	13.7	12.9	10.4	8.3	6.7	5.4	4.3	3.4	2.7	(22	1.6	1.2	0.91	N08811	B408
10.1	13.7	13.3	13.0	11.7	14.5	17.2	14.0	13.7	12.7	10.1	0.5	0.7	5.1	1.5	5.1	2.,		1.0	1.2	0.71	1100011	D-100
20.0	20.0	20.0	20.0	20.0	20.0	20.0	19.9	17.0	13.0	9.8	6.6	4.2	2.0	1.6	1.1	1.0	0.8				N08800	B408
															1	Ο,						
100	450	455	450												\sim						1100000	D/04
18.2	17.8	17.5	17.2											<							N08320	B621
														11.								
19.2	19.0	18.8	18.7	18.6	18.5	18.4	18.3						🗴	<i>(7)</i> ,							N06007	B581
23.3	23.3	23.2	23.0	22.9	22.8	22.6	22.3						O _~	٠							N08825	B425
													9,									
		23.3										N									N06690	B166
23.3	23.3	23.3	23.3	23.3	23.3						((O.)									N06690	B166
22.4	22.2	22.0	21.0	217	20.0	10.5	10.0														N06007	B581
		20.1			20.0	19.5	18.9														N06007 N06030	B581
20.9	20.5	20.1	19.7			•••				·C	• •••										NUOUSU	D301
									<u> </u>	111-												
				22.2	22.1	22.0	21.9	21.9	17.9	14.2	12.3	9.4	7.6	6.2	5.0	4.0	3.2	2.6	2.0	1.4	N08120	B408
21.7	21.3	20.9	20.5		•••	•••															N08031	B649
22.0	22.7	20.0	115	0 5	4.0	1.9		.O`													N04400	B164
22.7	22.7	20.0	14.5	0.5	4.0	1.5	(٦			•••					•••	•••	•••	•••	•••	N04400	D104
							C.															
						\sim																
		19.0			1						•••						•••	•••			N06035	B574
		26.1				4															N06455	B574
					22.6	22.4	22.3	18.5	15.0	12.2	9.8	7.8									N10276	B574
		26.7	~ ~ ~																		N10362	B574
33.3	33.3	33.3	33.3	33.1	32.8	32.5	31.2	31.2	23.1	21.0	13.2										N06625	B446
37.7	37.4	374	37.4	37.4	37.4	37.4	37.4	37.4	37.4	27.7	21.0	13.2									N06625	B446
0,,,	\$		0,	0,	0,11	0,	07.11	0711	07.1	_,,,	21.0	10.2									1100020	2110
29.1	28.7	28.4	28.2	28.2	28.2	28.2	28.2	28.2	23.2	19.0	15.6	12.9	10.6	8.5	6.7	5.3	4.1	2.9	2.1	1.5	N06230	B572
27.5	26.8	26.1	25.5																		N06059	B574
26.2	25.7	25.4	25.2																		N06200	B574
34.0	34.0	33.9	33.5																		N10675	B335
23.5	23.1	22.9	22.6																		R20033	B649

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

Basic Allowable Stress, S, ksi, at Metal Temperature, °F [Note (1)]																						
650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	1,550	1,600	1,650	UNS No. or Grade	Spec. No.
																	Ni	ckel an	d Nick	el Alloy	— Casting	gs (4a)
24.0	24.0	24.0	24.0	24.0	24.0	24.0	22.8														CW12MW	A494
24.0	24.0	24.0	24.0	24.0	24.0	24.0	22.8													OP	CW6M	A494
																			()	CX2MW	A494
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Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

	i i arentneses keier ti	<u> </u>	ppenum	145165, 50			2 0 111 0 11		Specifie Streng	d Min.
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	P-No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield
Titanium and Ti	tanium Alloy — Pipes	and Tubes								
Ti	Smls. & wld. tube	B338	1	R50250	Annealed	51		-75	35	20
Ti	Smls. pipe	B861	1	R50250	Annealed	51		-75	35	20
Ti	Wld. pipe	B862	1	R50250	Annealed	51		-75	35	20
Ti	Smls. & wld. tube	B338	2	R50400	Annealed	51		-75	250	40
Ti	Smls. & wid. tube	B861	2	R50400	Annealed	51		-75 -75	50	40
	• •							-/3	•	
Ti	Wld. pipe	B862	2	R50400	Annealed	51		-43	50	40
Ti	Smls. & wld. tube	B338	3	R50550	Annealed	52	المير	-75	65	55
Ti	Smls. pipe	B861	3	R50550	Annealed	52	S.	-75	65	55
Ti	Wld. pipe	B862	3	R50550	Annealed	52	/ Y	-75	65	55
Ti-Pd	Smls. & wld. tube	B338	7	R52400	Annealed	51		-75	50	40
Ti-Pd	Smls. pipe	B861	7	R52400	Annealed Q	51		-75	50	40
Ti-Pd	Wld. pipe	B862	7	R52400	Annealed	51		-75	50	40
11 1 4	wid. pipe	5002	,	N32 100	7 minicules.	31		73	50	10
Ti-0.3Mo-0.8Ni	Smls. & wld. tube	B338	12	R53400	Annealed	52		-75	70	50
Ti-0.3Mo-0.8Ni	Smls. pipe	B861	12	R53400	Annealed	52		-75	70	50
Ti-0.3Mo-0.8Ni	Wld. pipe	B862	12	R53400	Annealed	52		-75	70	50
Titanium and Ti	tanium Alloy — Plates	s Sheets and	Strine X	0						
Ti		в В265	our po	R50250	Annealed	51		-75	35	20
Ti		B265		R50400	Annealed	51		-75	50	40
Ti		B265	3	R50550	Annealed	52		-75	65	55
Ti-Pd		B265	7	R52400	Annealed	51		-75	50	40
Ti-0.3Mo-0.8Ni		B265	12	R53400	Annealed	52		-75	70	50
11 0.5140 0.0141		C 10 B203	12	1133 100	Timearea	52		73	70	30
Titanium and Ti	tanium Alloy — Forgi	ngs and Fitti	ngs							
Ti	Fittings	B363	WPT1	R50250	Annealed	51		-75	35	20
Ti	Forgings	B381	F-1	R50250	Annealed	51		-75	35	20
Ti	Fittings	B363	WPT2	R50400	Annealed	51		-75	50	40
Ti	Forgings	B381	F-2	R50400	Annealed	51		-75	50	40
Ti	Fittings	B363	WPT3	R50550	Annealed	52		-75	65	55
Ti	Forgings	B381	F-3	R50550	Annealed	52		-75	65	55
Ti-Pd	Fittings	B363	WPT7	R52400	Annealed	51		-75	50	40
Ti-Pd	Forgings	B381	F-7	R52400	Annealed	51		-75	50	40
Ti-0.3Mo-0.8Ni	Fittings	B363	WPT12	R53400	Annealed	52		-75	70	50
Ti-0.3Mo-0.8Ni	Forgings	B381	F-12		Annealed	52		-75	70	50
Titaning 1 m	tanium Alless B									
Titanium and Ti	tanium Alloy — Bars	B348	1	R50250	Annealed	51		-75	35	20
Ti		B348	2	R50400	Annealed	51		-75 -75	50	40
Ti		B348	3	R50550	Annealed	52		-75	65	55
			-			-				

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

		Basic	Allowa	ble Stres	ss, S, ks	i, at Meta	al Temp	erature,	°F [Not	te (1)]			_	
Min.														
Temp. to 100	150	200	250	300	350	400	450	500	550	600	650	700	UNS No.	Spec. No.
										Titaniuı	m and T	itanium	Alloy — Pipe	s and Tubes
11.7	10.7	9.3	8.2	7.2	6.3	5.5	4.7	4.2	3.8	3.5			R50250	B338
11.7	10.7	9.3	8.2	7.2	6.3	5.5	4.7	4.2	3.8	3.5			R50250	B861
11.7	10.7	9.3	8.2	7.2	6.3	5.5	4.7	4.2	3.8	3.5			R50250	B862
													2	
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R50400	B338
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R50400	B861
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6		<	R50400	B862
21.7	20.0	10 /	166	140	13.5	121	11.0	9.9	9.3	8.6		N	R50550	B338
21.7 21.7	20.0	18.4 18.4	16.6 16.6	14.9 14.9	13.5	12.1 12.1	11.0	9.9	9.3	8.6	" C	1/2:	R50550	В330
21.7	20.0	18.4	16.6	14.9	13.5	12.1	11.0	9.9	9.3	8.6	c P		R50550	B862
21.7	20.0	10.4	10.0	14.7	13.3	12.1	11.0	9.9	7.3	0.0	0	•••	K30330	D002
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R52400	B338
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R52400	B861
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R52400	B862
									S/O					
23.3	22.6	21.8	20.4	18.9	17.8	16.7	16.0	15.2	14.8	14.4			R53400	B338
23.3	22.6	21.8	20.4	18.9	17.8	16.7	16.0	15.2	14.8	14.4			R53400	B861
23.3	22.6	21.8	20.4	18.9	17.8	16.7	16.0	15.2	14.8	14.4			R53400	B862
							×0 ⁷							
											tanium	Alloy —	· Plates, Sheet	_
11.7	10.7	9.3	8.2	7.2	6.3	5.5	4.7	4.2	3.8	3.5			R50250	B265
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R50400	B265
21.7	20.0	18.4	16.6	14.9	13.5	12.1	11.0	9.9	9.3	8.6	•••		R50550	B265
16.7	15.6	14.5	13.3	12.1	$Q_{7.8}^{11.2}$	10.3	9.6	8.9	8.2	7.6			R52400	B265
23.3	22.6	21.8	20.4	18.9	77.8	16.7	16.0	15.2	14.8	14.4	•••		R53400	B265
				Δ0.					Tita	nium an	d Titani	um Allo	y — Forgings	and Fittings
11.7	10.7	9.3	8.2	7.2	6.3	5.5	4.7	4.2	3.8	3.5			R50250	В363
11.7	10.7	9.3	8.2	7.2	6.3	5.5	4.7	4.2	3.8	3.5			R50250	B381
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R50400	B363
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R50400	B381
21.7	20.0	18.4	16.6	14.9	13.5	12.1	11.0	9.9	9.3	8.6			R50550	B363
21.7	20.0	18.4	16.6	14.9	13.5	12.1	11.0	9.9	9.3	8.6			R50550	B381
	P													
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R52400	B363
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R52400	B381
23.3	22.6	21.8	20.4	18.9	17.8	16.7	16.0	15.2	14.8	14.4			R53400	B363
23.3	22.6	21.8	20.4	18.9	17.8	16.7	16.0	15.2	14.8	14.4			R53400	B381
													1 min	
117	10.7	0.3	0.3	7.0	()		4.77	4.3	2.0	2.5			nd Titanium A	•
11.7 16.7	10.7 15.6	9.3	8.2 13.3	7.2 12.1	6.3 11.2	5.5 10.3	4.7 9.6	4.2 8.9	3.8 8.2	3.5 7.6			R50250	B348
21.7	20.0	14.5 18.4	13.3	12.1 14.9	13.5	10.3	9.6	8.9 9.9	9.3	7.6 8.6			R50400 R50550	B348 B348
41./	20.0	10.4	10.0	エサ.フ	13.3	14.1	11.0	2.7	1.3	0.0			いつりつつり	D340

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

									Specifie Streng	
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	P-No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield
	anium Alloy — Bars					(-)		(-)		
Ti-Pd		B348	7	R52400	Annealed	51		-75	50	40
Ti-0.3Mo-0.8Ni		B348	12	R53400	Annealed	52		-75	70	$\frac{50}{6}$
Titanium and Tit	anium Alloy — Castings								00	
Ti		B367	C-2	R52550		51	(14)(44)	-75	C ₂ 50	40
Ti		B367	C-3	R52550		52	(14)(44)	-75	65	55
Ti-Pd		B367	C-7	R52700		51	(14)(44)	3 75	50	40
Zirconium and Zi	irconium Alloy — Pipes ar	d Tubes					No.			
99.2Zr		B523		R60702		61	5	-75	55	30
99.2Zr		B658		R60702		61	£ 1	-75	55	30
95.5Zr + 2.5Cb		B523		R60705		62	(73)	-75	80	55
95.5Zr + 2.5Cb		B658		R60705	/)	62	(73)	-75	80	55
30.0EF 1 2.00D		2000		1100700	SUIL	٥ -	(, 5)	. 0		
Zirconium and Zi	irconium Alloy — Plates a	nd Sheets			0,					
99.2Zr		B551		R60702	No	61		-75	55	30
95.5Zr + 2.5Cb		B551		R60705		62	(73)	-75	80	55
Zirconium and Zi	irconium Alloy — Forgings	and Bar		Tile						
99.2Zr	, , ,	B493	🗡	R60702		61		-75	55	30
99.2Zr		B550	110x	R60702		61		-75	55	30
05.55 0.50		D400 *	O,	D.COEOE		60	(50)		70	
95.5Zr + 2.5Cb		B493		R60705		62	(73)	-75	70	55
95.5Zr + 2.5Cb		B550	•••	R60705		62	(73)	-75	80	55
	MENORMDOC.									

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

		Basic	Allowa	ble Stre	ss, <i>S</i> , ksi	, at Meta	al Temp	erature,	°F [Not	e (1)]				
Min.														
Temp. to 100	150	200	250	300	350	400	450	500	550	600	650	700	UNS No.	Spec. No.
-												d Titaniu	ım Alloy — Ba	
16.7	15.6	14.5	13.3	12.1	11.2	10.3	9.6	8.9	8.2	7.6			R52400	B348
23.3	22.6	21.8	20.4	18.9	17.8	16.7	16.0	15.2	14.8	14.4			R53400	B348
													~	O
											Titaniu	m and T	itanium Alloy	_
16.7	15.2	13.8	12.6	11.4	10.4	9.5	8.7	7.9					R 525 50	B367
21.7	20.0	18.4	16.6	14.9	13.5	12.1	11.0	9.9		•••			R52550	B367
16.7	15.2	13.8	12.6	11.4	10.4	9.5	8.7	7.9				; Q	R52700	B367
									7:		. and 7:	N/	Allan Dina	a and Tubas
18.3	17.2	15.4	13.6	12.0	10.6	9.3	8.3	7.4	6.6	6.0	5.6	5.2	Alloy — Pipe R60702	B523
18.3	17.2	15.4	13.6	12.0	10.6	9.3	8.3	7.4	6.6	6.0	5.6	5.2	R60702	B658
10.5	17.2	15.1	15.0	12.0	10.0	7.5	0.5	7.1	0.0	0.0	0	3.2	100702	D030
26.7	24.4	22.1	20.4	18.9	17.7	16.7	15.8	15.0	14.4	13.9	13.5	13.2	R60705	B523
26.7	24.4	22.1	20.4	18.9	17.7	16.7	15.8	15.0	14.4	13.9	13.5	13.2	R60705	B658
									11					
									Zir	conium	and Ziro	conium A	Alloy — Plates	and Sheets
18.3	17.2	15.4	13.6	12.0	10.6	9.3	8.3	7.4	6.6	6.0	5.6	5.2	R60702	B551
26.7	24.4	22.1	20.4	18.9	17.7	16.7	15.8	15.0	14.4	13.9	13.5	13.2	R60705	B551
							i.	Q ²						
							_v 0						Alloy — Forgi	_
18.3	17.2	15.4	13.6	12.0	10.6	9.3	8.3	7.4	6.6	6.0	5.6	5.2	R60702	B493
18.3	17.2	15.4	13.6	12.0	10.6	9.8	8.3	7.4	6.6	6.0	5.6	5.2	R60702	B550
26.7	24.4	22.1	20.4	10.0	177*	O .	150	15.0	111	120	12.5	122	DC0705	D402
26.7 26.7	24.4 24.4	22.1 22.1	20.4 20.4	18.9 18.9	17.7	16.7 16.7	15.8 15.8	15.0 15.0	14.4 14.4	13.9 13.9	13.5 13.5	13.2 13.2	R60705 R60705	B493 B550
20.7	24.4	22.1	20.4	10.9	Q _x	10.7	13.0	13.0	14.4	13.9	13.3	13.2	K00703	D330
)									
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	P	22.1												

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

									Speci Mii Strengt	ı.	Basio Metal	: Allo					
											Min.			,			
Nominal Composition	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size or Thickness Range, in.	P- No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Temp. to 100	150	200	250	300	350	400
Aluminum Allo	oy — Se	amless Pipes ar	nd Tubes	-	-												
Al-Mn-Cu	B210	Alclad 3003	A83003	0		21	(14)(33)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
Al-Mn-Cu	B210	Alclad 3003	A83003	H112		21	(14)(33)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
Al-Mn-Cu	B241	Alclad 3003	A83003	0		21	(14)(33)	-452	13	4.5	3.0	2.9	2.8	2,7	2.5	1.9	1.5
Al-Mn-Cu	B241	Alclad 3003	A83003	H112		21	(14)(33)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
Al-Mn-Cu	B210	Alclad 3003	A83003	H14		21	(14)(33)	-452	19	16	6.3	6.3	6.3	6.1	4.3	3.0	2.3
Al-Mn-Cu	B210	Alclad 3003	A83003	H18		21	(14)(33)	-452	26	23	8.7	8.7	8.7	8.4	4.3	3.0	2.3
99.60Al	B210	1060	A91060	0		21	(14)(33)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2	1.1	0.8
99.60Al	B210	1060	A91060	H112		21	(14)(33)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2	1.1	8.0
99.60Al	B210	1060	A91060	H113		21	(14)(33)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2	1.1	8.0
99.60Al	B241	1060	A91060			21	(14)(33)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2	1.1	8.0
99.60Al	B241	1060	A91060	H112		21	(14)(33)	-452	8.5	2.5	1.7	1.7	1.6	1.4		1.1	0.8
99.60Al	B241	1060	A91060	H113		21	(14)(33)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2		0.8
99.60Al	B210	1060	A91060	H14		21	(14)(33)	-452	12	10	4.0	4.0	4.0	4.0	2.7	1.8	1.1
99.0Al-Cu	B241	1100	A91100			21	(14)(33)	-452	11	3	2.0	2.0	2.0	1.9	1.7	1.3	1.0
99.0Al-Cu	B241	1100	A91100	H112		21	(14)(33)	-452	11	3	2.0	2.0	2.0	1.9	1.7	1.3	1.0
99.0Al-Cu	B210	1100	A91100	H113		21	(14)(33)	-452	11	3.5	2.3	2.3	2.3	2.3	1.7	1.3	1.0
99.0Al-Cu	B210	1100	A91100	H14		21	(14)(33)	-452	16	14	5.3	5.3	5.3	4.9	2.8	1.9	1.1
	D040	2002	100000	0	10	24	(4.42(00)	450		_	0.0	0.0	0.4	0.0	0.5	4.0	4.5
Al-Mn-Cu	B210	3003	A93003			21	(14)(33)	-452	14	5	3.3	3.2	3.1	3.0	2.7	1.9	1.5
Al-Mn-Cu Al-Mn-Cu	B210 B241	3003 3003	A93003 A93003		-1110	21 21	(14)(33)	-452 -452	14 14	5 5	3.3	3.2	3.1	3.0	2.7 2.7		1.5 1.5
Al-Mn-Cu	B241	3003	A93003		<i>-</i>	21	(14)(33) (14)(33)	-452 -452	14	5	3.3	3.2	3.1	3.0		1.9	1.5
Al-Mn-Cu	B491	3003	A93003			21	(14)(33)	-452	14	5	3.3	3.2	3.1	3.0		1.9	1.5
Al-Mn-Cu	B491	3003	A93003			21	(14)(33)	-452	14	5	3.3	3.2	3.1	3.0		1.9	1.5
III IIII Gu	<i>D</i> 171	3003		Ö			(11)(33)	132	11	5	5.5	5.2	5.1	5.0	2.7	1.7	1.5
Al-Mn-Cu	B210	3003	A93003	H14		21	(14)(33)	-452	20	17	6.7	6.7	6.5	4.8	4.3	3.0	2.3
Al-Mn-Cu	B210	3003	A93003	H18		21	(14)(33)	-452	27	24	9.0	9.0	8.7	8.0	5.3	3.5	2.5
Al-Mn-Cu	B241	3003	A93003	H18		21	(14)(33)	-452	27	24	9.0	9.0	8.7	8.0	5.3	3.5	2.5
Al-2.5Mg	B210	5052	A95052	0		22	(14)	-452	25	10	6.7	6.7	6.7	6.6	6.1	4.1	2.3
Al-2.5Mg	B241	5052	A95052	0		22	(14)	-452	25	10	6.7					4.1	
Al-2.5Mg	B210	5052	A95052	H32		22	(14)(33)	-452	31	23	10.3	10.3	10.3	10.3	6.1	4.1	2.3
Al-2.5Mg	B210	5052	A95052	H34		22	(14)(33)	-452	34	26	11.3	11.3	11.3	11.3	6.1	4.1	2.3
Al-4.4Mg-Mn	B210	5083	A95083	0		25	(33)	-452	39	16	10.7	10.7					
Al-4.4Mg-Mn	B210	5083	A95083			25	(33)	-452 -452	39	16		10.7					
Al-4.4Mg-Mn	B241	5083	A95083			25	(33)	-452	39	16	10.7						
Al-4.4Mg-Mn	B241	5083	A95083			25	(33)	-452	39	16	10.7						
Al-4.0Mg-Mn	B210	5086	A95086	0		25	(33)	-452	35	14	9.3	9.3					
Al-4.0Mg-Mn	B210	5086	A95086			25	(33)	-452	35	14	9.3	9.3					
Al-4.0Mg-Mn	B241	5086	A95086			25	(33)	-452	35	14	9.3	9.3					
Al-4.0Mg-Mn	B241	5086	A95086			25	(33)	-452	35	14	9.3	9.3					
Al-4.0Mg-Mn	B210	5086	A95086				(33)	-452	40	28	13.3	13.3					

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

							•		Speci Min Strengt	n.		c Allo l Tem					
				Class/	Size or	P-		Min.		·	Min. Temp.		-	-			
Nominal Composition	Spec. No.	Type/ Grade	UNS No.	Condition/ Temper	Thickness Range, in.	No. (5)	Notes	Temp., °F (6)	Tensile	Yield	to 100	150	200	250	300	350	400
		amless Pipes and				(-)		- (0)									
Al-4.0Mg-Mn	B210	5086	A95086	-		25	(33)	-452	44	34	14.7	14.7					
Al-3.5Mg	B210	5154	A95154	0		22		-452	30	11	7.3	7.3		N 2)		
Al-3.5Mg	B210	5154	A95154	H34		22	(33)	-452	39	29	13.3	13.0	20)			
												O	`V				
Al-2.7Mg-Mn	B241	5454	A95454	0		22	(33)	-452	31	12	8.0	8.0	8.0	7.4	5.5	4.1	3.0
Al-2.7Mg-Mn	B241	5454	A95454	H112		22	(33)	-452	31	12	8.0	8.0	8.0	7.4	5.5	4.1	3.0
Al-5.1Mg-Mn	B210	5456	A95456	0		25	(33)	-452	41	19	12.7	12.7					
Al-5.1Mg-Mn	B210	5456	A95456	H112		25	(33)	-452	41	19	12.7	12.7					
Al-5.1Mg-Mn	B241	5456	A95456	0		25	(33)	-452	41	19	12.7	12.7					
Al-5.1Mg-Mn	B241	5456	A95456	H112		25	(33)	-452	of t	19	12.7	12.7					
Al-Mg-Si-Cu	B210	6061	A96061	T4 wld.		23	(22)(63)	452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B210	6061	A96061	T6 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B241	6061	A96061	T4 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B241	6061	A96061	T6 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
						S	~©										
Al-Mg-Si-Cu	B241	6061	A96061	T4		23	(33)(63)	-452	26	16	8.7	8.7	8.7	8.7	8.3	7.4	5.2
Al-Mg-Si-Cu	B210	6061	A96061	T4		23	(33)	-452	30	16	10.0	10.0	10.0	9.9	9.5	8.4	5.2
Al-Mg-Si-Cu	B241	6061	A96061	T6	1/2	23	(33)(63)	-452	38	35	12.7	12.7	12.7	12.3	10.5	8.1	5.2
Al-Mg-Si-Cu	B210	6061	A96061	T6	×O	23	(33)	-452	42	35	14.0	14.0	14.0	13.6	11.7	8.9	5.2
					.K												
Al-Mg-Si	B210	6063	A96063	T4 wld.	``	23		-452	17		5.7	5.7	5.6	5.3	4.8	3.8	2.0
Al-Mg-Si	B210	6063	A96063	T5 wld		23		-452	17		5.7	5.7	5.6	5.3	4.8	3.8	2.0
Al-Mg-Si	B210	6063		T6 wld.		23		-452	17		5.7	5.7	5.6	5.3	4.8	3.8	2.0
Al-Mg-Si	B241	6063	(T4 wld.		23		-452	17		5.7	5.7	5.6	5.3	4.8	3.8	2.0
Al-Mg-Si	B241	6063		T5 wld.		23		-452	17		5.7	5.7	5.6	5.3	4.8	3.8	2.0
Al-Mg-Si	B241	6063	A96063	T6 wld.		23		-452	17		5.7	5.7	5.6	5.3	4.8	3.8	2.0
Al-Mg-Si	B241	6063	A96063	T4	≤0.500	23	(33)	-452	19	10	6.3	6.3	6.3	6.3	5.8	3.9	1.5
Al-Mg-Si	B210	6063	A96063			23	(33)	-452	22	10	6.7	6.5	6.5	6.3	6.3	4.5	1.7
Al-Mg-Si	B241	6063	A96063		≤0.500	23	(33)	-452	22	16	7.3	7.3	7.3	7.3	7.1	3.8	2.0
Al-Mg-Si	B241		A96063				(33)	-452	30	25	10.0	10.0					
Al-Mg-Si	B210		A96063				(33)	-452	33	28		11.0					
•	V																
Aluminum Alt	oy — W	elded Pipes and	Tubes														
Al-4.4Mg-Mn	B547	5083	A95083	0		25		-452	40	18	12.0	12.0					
Aluminum Alle	oy — Stı	ructural Tubes															
Al-Mn-Cu	B221	Alclad 3003	A83003	0		21	(33)(69)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
Al-Mn-Cu	B221	Alclad 3003	A83003	H112		21	(33)(69)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
99.0Al	B221	1060	A91060	0		21	(33)(69)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2	1.1	0.8
99.0Al	B221	1060	A91060	H112		21	(33)(69)	-452	8.5	2.5	1.7	1.7	1.6	1.4	1.2	1.1	8.0
99.0Al-Cu	B221	1100	A91100	0		21	(33)(69)	-452	11	3	2.0	2.0	2.0	1.9	1.7	1.3	1.0
99.0Al-Cu	B221	1100	A91100	H112		21	(33)(69)	-452	11	3	2.0	2.0	2.0	1.9	1.7	1.3	1.0

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

		i ai entileses i					, opee		Speci Mi Strengt	fied n.	Basi	c Allo l Tem	wabl	e Str	ess, <i>S</i> ,	, ksi,	
				Cl /	6'			341			Min.						
Nominal	Spec.	Type/	UNS	Class/ Condition/	Size or Thickness	P- No.		Min. Temp.,			Temp. to						
Composition	No.	Grade	No.	Temper	Range, in.	(5)	Notes	°F (6)	Tensile	Yield	100	150	200	250	300	350	400
Aluminum Alle	oy — Stı	ructural Tubes	(Cont'd)														
Al-Mn-Cu	B221	3003	A93003	0		21	(33)(69)	-452	14	5	3.3	3.2	3.1	3.0	$-\mathbf{o}$	1.9	1.5
Al-Mn-Cu	B221	3003	A93003	H112		21	(33)(69)	-452	14	5	3.3	3.2	3.1	3.0	2.7) 1.9	1.5
Al-2.5Mg	B221	5052	A95052	0		22	(69)	-452	25	10	6.7	6.7	6.7	6.6	6.1	4.1	2.3
Al-4.4Mg-Mn	B221	5083	A95083			25	(69)	-452	39	16	10.7	10.7)			
Al-4.0Mg-Mn	B221	5086	A95086	0		25	(69)	-452	35	14	9.3	9.3					
Al-3.5Mg	B221	5154	A95154	0		22	(69)	-452	30	11	7.3	7.3					
Al-2.7Mg-Mn	B221	5454	A95454	0		22	(69)	-452	31	12 🧷	8.0	8.0	8.0	7.4	5.5	4.1	3.0
Al-5.1Mg-Mn	B221	5456	A95456	0		25	(69)	-452	41	19	12.7	12.7					
Al-Mg-Si-Cu	B221	6061	A96061	T4 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B221	6061	A96061	T6 wld.		23	(69) (22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B221	6061	A96061	T4		23	(69) (33)(63)	-452	26	16	8.7	8.7	8.7	8.7	8.3	7.4	5.2
Al-Mg-Si-Cu	B221	6061	A96061	Т6		23	(69) (33)(63) (69)	-452	38	35	12.7	12.7	12.7	12.3	10.5	8.1	5.2
Al M- C:	D221	(0(2	10000	T4] J		23	((0)	452	17		F 7	- 7	F.(F 2	4.0	2.0	2.0
Al-Mg-Si	B221 B221	6063 6063		T4 wld. T5 wld.		23	(69) (69)	-452 -452	17 17		5.7 5.7	5.7 5.7	5.6 5.6	5.3 5.3	4.8 4.8		2.0
Al-Mg-Si Al-Mg-Si	B221	6063		T6 wld.	'\ XO	23	(69)	-452	17		5.7	5.7	5.6	5.3	4.8		2.0
Al-Mg-Si	B221	6063	A96063		≤0.500	23	(13)(33) (69)	-452	19	10	6.3	6.3	6.3	6.3		3.9	1.5
Al-Mg-Si	B221	6063	A96063	T5	≤0.500	23	(13)(33)	-452	22	16	7.3	7.3	7.3	7.3	7.1	3.8	2.0
Al-Mg-Si	B221	6063	A96063	TON		23	(69) (33)(69)	-452	30	25	10.0	10.0	10.0	9.1	7.2	3.4	2.0
A1 A11	DI	ata a a di Charata		\mathbf{O}													
	оу — Ра В209	ates and Sheets Alclad 3003	A83003	0	0.006.0.400	21	(66)	452	12	4.5	2.0	2.9	2.0	27	2 5	1.0	1 5
Al-Mn-Cu Al-Mn-Cu	B209	Alclad 3003	A83003		0.006-0.499 0.500-3.000	21 21	(66) (68)	-452 -452	13 14	4.5 5	3.0	3.2	2.8	2.7 3.0		1.9 1.9	1.5 1.5
Al-Mn-Cu	B209	Alclad 3003	A83003		0.500-2.000		(33)(66)	-452	15	6	4.0	3.9	3.7	3.6		1.9	1.5
Al-Mn-Cu	B209	Alclad 3003	A83003		0.017-0.499		(33)(66)	-452	16	11	5.3	5.3		4.9		3.0	2.3
Al-Mn-Cu	B209	Alclad 3003	A83003		0.500-2.000		(33)(68)	-452	17	12	5.7				4.3	3.0	2.3
Al-Mn-Cu	B209	Alclad 3003	A83003		0.009-0.499	21	(33)(66)	-452	19	16	6.3	6.3	6.3		4.3		
Al-Mn-Cu	6	Alclad 3003	A83003	H14	0.500-1.000	21	(33)(68)	-452	20	17	6.7	6.7	6.7	6.5	4.3	3.0	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004	0	0.006-0.499	22	(66)	-452	21	8	5.3	5.3	5.3	5.3	5.3	3.8	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004		0.500-3.000	22	(68)	-452	22	8.5	5.7	5.6	5.6	5.6		3.8	
Al-Mn-Mg	B209	Alclad 3004	A83004	H112	0.250-0.499	22	(33)(66)	-452	22	8.5	5.7	5.6	5.6	5.6	5.6	3.8	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004	H112	0.500-3.000	22	(33)(68)	-452	23	9	6.0	6.0	6.0	6.0	5.7	3.8	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004	H32	0.017-0.499	22	(33)(66)	-452	27	20	9.0	9.0	9.0	9.0	5.7	3.8	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004	H32	0.500-2.000	22	(33)(68)	-452	28	21	9.3	9.3	9.3	9.3	5.7	3.8	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004	H34	0.009-0.499	22	(33)(66)	-452	31	24	10.3	10.3	10.3	10.3	5.7	3.8	2.3
Al-Mn-Mg	B209	Alclad 3004	A83004	H34	0.500-1.000	22	(33)(68)	-452	32	25	10.7	10.7	10.7	10.7	5.7	3.8	2.3
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T4 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T6 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

									Speci Mir Strengt	n.			wable perat				
Nominal Composition	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size or Thickness Range, in.	P- No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	150	200	250	300	350	400
Aluminum Allo	oy — Pla	ates and Sheets	(Cont'd)														
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T4		23	(33)(66)	-452	27	14	9.0	9.0	9.0	8.9	8.6	7.6	5.2
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T451	0.250-0.499	23	(33)(66)	-452	27	14	9.0	9.0	_	8.9	8.6	7.6	5.2
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T451	0.500-3.000	23	(33)(68)	-452	30	16	9.0	9.0	9.0	8.9	8.5	8.4	5.2
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	Т6		23	(33)(66)	-452	38	32	12.7	12.7	12.7	12.3	10.6	8.1	5.2
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T651	0.250-0.499	23	(33)(66)	-452	38	32	12.7	12.7	12.7	12.3	10.6	8.1	5.2
Al-Mg-Si-Cu	B209	Alclad 6061	A86061	T651	0.500-4.000	23	(33)(68)	-452	42	35	14.0	14.0	14.0	13.6	11.7	8.9	5.2
99.60Al	B209	1060	A91060	0		21		-452	8 (2.5	1.7	1.6	1.6	1.4	1.2	1.1	0.8
99.60Al	B209	1060	A91060	H112	0.500-1.000	21	(13)(33)	-452	10	9 ₅	3.3	3.2	2.9	2.5	2.0	1.5	0.9
99.60Al	B209	1060	A91060	H12		21	(33)	-452	11	9	3.7	3.7	3.4	3.1	2.7	1.8	1.1
99.60Al	B209	1060	A91060	H14		21	(33)	-452	12	10	4.0	4.0	4.0	4.0	2.7	1.8	1.1
99.0Al-Cu	B209	1100	A91100	0		21		-452	11	3.5	2.3	2.3	2.3	2.3	1.7	1.3	1.0
99.0Al-Cu	B209	1100	A91100		0.500-2.000	21	(13)(33)	-452	12	5	3.3	3.3	3.3	3.2		1.7	1.0
99.0Al-Cu	B209	1100	A91100			21	(33)	-452	14	11	4.7	4.7	4.6	3.8		1.9	1.1
99.0Al-Cu	B209	1100	A91100				(3)	-452	16	14	5.3	5.3	5.3	4.9		1.9	1.1
						N	O.										
Al-Mn-Cu	B209	3003	A93003			21		-452	14	5	3.3	3.2	3.1	3.0	2.7		1.5
Al-Mn-Cu	B209	3003	A93003		0.500-2.000	21	(13)(33)	-452	15	6	4.0	3.9	3.7	3.6		1.9	1.5
Al-Mn-Cu	B209	3003	A93003		X O	21	(33)	-452	17	12	5.7	5.7	5.6	5.2		3.0	2.3
Al-Mn-Cu	B209	3003	A93003	H14	<i>*</i>	21	(33)	-452	20	17	6.7	6.7	6.7	6.5	4.3	3.0	2.3
Al-Mn-Mg	B209	3004	A93004	0		22		-452	22	8.5	5.7	5.7	5.7	5.7	5.7	3.8	2.3
Al-Mn-Mg	B209	3004	A93004	H112		22	(33)	-452	23	9	6.0	6.0	6.0	6.0	5.8	3.8	2.3
Al-Mn-Mg	B209	3004	A93004	H32		22	(33)	-452	28	21	9.3	9.3	9.3	9.3	5.7	3.8	2.3
Al-Mn-Mg	B209	3004	A93004	H34		22	(33)	-452	32	25	10.7	10.7	10.7	10.7	5.7	3.8	2.3
Al-1.5Mg	B209	5050	A95050	0		21		-452	18	6	4.0	4.0	4.0	4.0	4.0	2.8	1.4
Al-1.5Mg	B209	5050	A95050			21	(33)	-452	20	8	5.3	5.3	5.3	5.2	5.2		1.4
Al-1.5Mg	B209	5050	A95050			21	(33)	-452	22	16	7.3	7.3	7.3	7.3		2.8	1.4
Al-1.5Mg	B209	5050	A95050	H34		21	(33)	-452	25	20	8.3	8.3	8.3	7.8	5.3	2.8	1.4
Al-2.5Mg	B209	5052	A95052	0		22		-452	25	9.5	6.3	6.3	6.3	6.2	6.1	4.1	2.3
Al-2.5Mg	B209	5052	A95052		0.500-3.000	22	(13)(33)	-452	25	9.5	6.3		6.3			4.1	
Al-2.5Mg	B209	5052	A95052			22	(33)	-452	31	23	10.3		10.3			4.1	
Al-2.5Mg	B209	5052	A95052	H34		22	(33)	-452	34	26	11.3	11.3	11.3	11.3	6.1	4.1	2.3
Al-4.4Mg-Mn	B209	5083	A95083	0	0.051-1.500	25	(13)	-452	40	18	12.0	12.0					
Al-4.4Mg-Mn	B209	5083	A95083		0.188-1.500	25	(13)(33)	-452	44	31	14.7	14.7					
Al-4.0Mg-Mn	B209	5086	A95086			25		-452	35	14	9.3	9.3					
Al-4.0Mg-Mn	B209	5086	A95086		0.500-1.000	25	(13)(33)	-452	35	16	9.3	9.3					
Al-4.0Mg-Mn	B209	5086	A95086			25	(33)	-452	40	28		13.3					
Al-4.0Mg-Mn	B209	5086	A95086			25		-452	44	34		14.7					
Al-3.5Mg	B209	5154	A95154	0		22		-452	30	11	7.3	7.3					
Al-3.5Mg	B209	5154	A95154		0.500-3.000		(13)(33)	-452	30	11	7.3	7.3					
111 0.01/15	5207	5101	11/3134	.1112	5.500 5.000		(10)(00)	132	50	11	,.5	,.5					

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

	.010 111	Parentheses R			, , , , , , , , , , , , , , , , , , ,	4010	s, opeon		Speci Mir Strengt	fied n.	Basi	c Allo	wabl	e Str	ess, S	, ksi,	
Nominal	Spec.	Type/	UNS	Class/ Condition/	Size or Thickness	P- No.		Min. Temp.,	burenge	, 1131	Min. Temp.		реги	tur c,	. [occ	<u> </u>
Composition	No.	Grade	No.	Temper	Range, in.	(5)	Notes	°F (6)	Tensile	Yield	100	150	200	250	300	350	400
Aluminum Allo	oy — Pla	ates and Sheets	(Cont'd)														
Al-3.5Mg	B209	5154	A95154	H32		22	(33)	-452	36	26	12.0	12.0					
Al-3.5Mg	B209	5154	A95154	H34		22	(33)	-452	39	29	13.0	13.0			1/2)	
Al-3.5Mg	B209	5254	A95254	0		22		-452	30	11	7.3	7.3	<u>()</u>	\V	·		
Al-3.5Mg	B209	5254	A95254	H112	0.500-3.000	22	(13)(33)	-452	30	11	7.3	7.3	N)			
Al-3.5Mg	B209	5254	A95254	H32		22	(33)	-452	36	26	12.0	12.0)`				
Al-3.5Mg	B209	5254	A95254	H34		22	(33)	-452	39	29	13.0	13.0					
Al-2.7Mg-Mn	B209	5454	A95454	0		22		-452	31	12 C	8.0	8.0	8.0	7.4	5.5	4.1	3.0
Al-2.7Mg-Mn	B209	5454	A95454	H112	0.500-3.000	22	(13)(33)	-452	31	12	8.0	8.0	8.0	7.4	5.5	4.1	3.0
Al-2.7Mg-Mn	B209	5454	A95454	H32		22	(33)	-452	36	26	12.0	12.0	12.0	7.5	5.5	4.1	3.0
Al-2.7Mg-Mn	B209	5454	A95454	H34		22	(33)	-452	39	29	13.0	13.0	13.0	7.5	5.5	4.1	3.0
Al-5.1Mg-Mn	B209	5456	A95456	0	0.051-1.500	25	(13)	-452	42	19	12.7	12.7					
Al-5.1Mg-Mn	B209	5456	A95456	H32	0.188-0.499	25	(13)(33)	-452	46	33	15.3	15.3					
Al-2.5Mg	B209	5652	A95652	0		22	,	-452	25	9.5	6.3	6.3	6.3	6.2	6.1	4.1	2.3
Al-2.5Mg	B209	5652	A95652	H112	0.500-3.000	22	(13)(33)	-452	25	9.5	6.3	6.3	6.3	6.3	6.1	4.1	2.3
Al-2.5Mg	B209	5652	A95652	H32		22	(33)	-452	31	23	10.3	10.3	10.3	10.3	6.1	4.1	2.3
Al-2.5Mg	B209	5652	A95652	H34		22	(33)	-452	34	26	11.3	11.3	11.3	11.3	6.1	4.1	2.3
Al-Mg-Si-Cu	B209	6061	A96061	T4 wld.		23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B209	6061	A96061	T6 wld.	, X O	23	(22)(63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B209	6061	A96061	T4		23	(33)(63)	-452	30	16	10.0	10.0	10.0	9.9	9.5	8.4	5.2
Al-Mg-Si-Cu	B209	6061	A96061	T6 (23	(33)	-452	42	35	14.0	14.0	14.0	13.6	11.7	8.9	5.2
Al-Mg-Si-Cu	B209	6061	A96061	T651	0.250-4.000	23	(13)(33)	-452	42	35	14.0	14.0	14.0	13.6	11.7	8.9	5.2
Aluminum Alle	ov — Fo	rgings and Fittir	1gs	ON													
Al-Mn-Cu	B361	WP Alclad 3003	-	6		21	(13)(14)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
			-0	•			(32)(33) (66)										
Al-Mn-Cu	B361	WP Alclad 3003	A83003	H112		21	(13)(14) (32)(33)	-452	13	4.5	3.0	2.9	2.8	2.7	2.5	1.9	1.5
99.60Al	B361	WP1060	A91060	0		21	(66) (13)(14) (32)(33)	-452	8	2.5	1.7	1.6	1.6	1.4	1.2	1.1	0.8
99.60Al	B361	WP1060	A91060	H112		21	(13)(14) (32)(33)	-452	8	2.5	1.7	1.6	1.6	1.4	1.2	1.1	0.8
99.0Al-Cu	B361	WP1100	A91100	0		21	(13)(14) (32)(33)	-452	11	3	2.0	2.0	2.0	1.9	1.7	1.3	1.0
99.0Al-Cu	B361	WP1100	A91100	H112		21	(13)(14) (32)(33)	-452	11	3	2.0	2.0	2.0	1.9	1.7	1.3	1.0
Al-Mn-Cu	B247	3003	A93003		•••	21	(9)(45)	-452	14	5	3.3	3.2			2.7		
Al-Mn-Cu	B247	3003		H112 wld.		21	(9)(45)	-452	14	5	3.3	3.2		3.0			1.5
Al-Mn-Cu	B361	WP3003	A93003	0		21	(13)(14) (32)(33)	-452	14	5	3.3	3.2	3.1	3.0	2.7	1.9	1.5
Al-Mn-Cu	B361	WP3003	A93003	H112		21	(13)(14) (32)(33)	-452	14	5	3.3	3.2	3.1	3.0	2.7	1.9	1.5
Al-Mn-Cu	B247	5083	A95083	0		25	(9)(32) (33)	-452	39	16	10.7	10.7					

Table A-1 Basic Allowable Stresses in Tension for Metals (Cont'd)

					•		•		Speci Mi Strengt	n.	Basic Metal	c Allo l Tem				, ,	
Nominal Composition	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size or Thickness Range, in.	P- No. (5)	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	150	200	250	300	350	400
Aluminum Allo	oy — Fo	rgings and Fit	tings (Cont	t'd)													
Al-Mn-Cu	B247	5083	A95083	H112		25	(9)(32) (33)	-452	39	16	10.7	10.7		, 6			
Al-Mn-Cu	B247	5083	A95083	H112 wld.		25	(9)(32) (33)	-452	39	16	10.7	10.7	7	5			
Al-4.4Mg-Mn	B361	WP5083	A95083	0		25	(13)(32) (33)	-452	39	16	10.7	10.7					
Al-4.4Mg-Mn	B361	WP5083	A95083	H112		25	(13)(32) (33)	-452	39	16	10.7	10.7					
Al-3.5Mg	B361	WP5154	A95154	0		22	(32)(33)	-452	30	11	7.3	7.3					
Al-3.5Mg	B361	WP5154	A95154	H112		22	(32)(33)	-452	30	11	7.3	7.3					
Al-Mg-Si-Cu	B247	6061	A96061	T6 wld.		23	(9)(22)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B361	WP6061	A96061	T4 wld.		23	(22)(32) (63)	452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B361	WP6061	A96061	T6 wld.		23	(22)(32) (63)	-452	24		8.0	8.0	8.0	8.0	7.7	6.9	5.1
Al-Mg-Si-Cu	B361	WP6061	A96061	T4		23	(13)(32) (33)(63)	-452	26	16	8.7	8.7	8.7	8.7	8.3	7.4	5.2
Al-Mg-Si-Cu	B247	6061	A96061	T6		23	(9)(33)	-452	38	35	12.7	12.7	12.7	12.3	10.5	8.1	5.2
Al-Mg-Si-Cu	B361	WP6061	A96061	Т6	" jie	23	(13)(32) (33)(63)	-452	38	35	12.7	12.7	12.7	12.3	10.5	8.1	5.2
Al-Mg-Si	B361	WP6063	A96063	T4 wld	*0	23	(32)	-452	17		5.7	5.7	5.7	5.7	5.5	3.8	2.0
Al-Mg-Si	B361	WP6063	A96063		*	23	(32)	-452	17		5.7	5.7	5.7	5.7	5.5	3.8	2.0
Al-Mg-Si	B361	WP6063	A96063			23	(13)(32) (33)	-452	18	9	6.0	5.9	5.8	5.7		3.7	1.4
Al-Mg-Si	B361	WP6063	A96063	To		23	(13)(32) (33)	-452	30	25	10.0	10.0	10.0	9.1	7.2	3.4	2.0
Aluminum Allo	oy — Ca	stings	C).														
Al-Si-Mg	B26	356.0	A03560	T71		26	(9)(43)	-452	25	18	8.3	8.3	8.3	8.1	7.3	5.5	2.4
Al-Si-Mg	B26	356.0	A03560	T6		26	(9)(43)	-452	30	20	10.0	10.0	10.0	8.4			
Al-Si	B26	443.0	A04430	F			(9)(43)	-452	17	7	4.7	4.7	4.7	4.7	4.7	4.7	3.5

(18) Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Notes	Min. Temp., °C (6)	Min. Tensile Strgth., MPa	Min. Yield Strgth., MPa	Max. Use Temp., °C
1	Fe	Castings	A48	20	F11401		(8e)(48)	-29	138		204
2	Fe	Castings	A278	20	F11401		(8e)(48)	-29	138		204
	Fe	Castings	A126	Α	F11501		(8e)(9)(48)	-29	145		204
							(-)(-)				0.
4	Fe	Castings	A48	25	F11701		(8e)(48)	-29	172		204
5	Fe	Castings	A278	25	F11701		(8e)(48)	-29	172	()	204
										. ന ്	
6	Fe	Castings	A48	30	F12101		(8e)(48)	-29	207	0	204
7	Fe	Castings	A278	30	F12101		(8e)(48)	-29	207	ر ا	204
8	Fe	Castings	A126	В	F12102		(8e)(9)(48)	-29	214		204
									MIL		
9	Fe	Castings	A48	35	F12401		(8e)(48)	-29	241		204
10		Castings	A278	35	F12401		(8e)(48)	-29	241		204
		33.33					(00)(10)	N. O.			
11	Fe	Castings	A48	40	F12801		(8e)(9)(48)	-29	276		204
12		Castings	A126	С	F12802		(8e)(9)(48)	-29	283		204
13		Castings	A278	40	F12803		(8e)(9)(53)	-29	276		343
		33.33					Costo				
14	Fe	Castings	A48	45	F13101		(8e)(48)	-29	310		204
		dustings	7110	10	110101		(00)(10)	2,	510	•••	201
15	Fo	Castings	A48	50	F13501	:.0	(8e)(48)	-29	345		204
16	_	Castings	A278	50	F13501	7,	(8e)(53)	-29	345		343
10	re	Castiligs	AZ/O	30	F13302	×O	(06)(33)	-29	343		343
17	Eo	Coatings	A 4 O		F13801		(00)(40)	20	379		204
17	re	Castings	A48	55	F13801		(8e)(48)	-29	3/9		204
4.0	F	o .:	4.40	60.4	F1.44.04		(0.)(40)	20	44.4		204
18		Castings	A48	60	F14101		(8e)(48)	-29	414		204
19	Fe	Castings	A278	60	F14102		(8e)(53)	-29	414		343
	_	_		O_{-}							
20	Fe	Castings	A197) · ···	F22000		(8e)(9)	-29	276	207	343
			20								
21	Fe	Castings	A47	32510	F22200		(8e)(9)	-29	345	224	343
		0									
22	Fe	Castings	A395	60-40-18	F32800		(8d)(9)	-29	414	276	343
		7									
23	Fe	Castings	A571	D-2M	F43010	1	(8d)	-29	448	207	40
	51										
24	Fe	Castings	A536	65-45-12	F33100		(8d)(9)	-29	448	310	260

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units)

	Numbers in	- u. ondi		llowable S			_					mult	
	Min.								-				
Line No.	Temp. to 40	65	100	125	150	175	200	225	250	275	300	325	350
1	13.8	13.8	13.8	13.8	13.8	13.8	13.8	13.8					
2	13.8	13.8	13.8	13.8	13.8	13.8	13.8	13.8					
3	13.8	13.8	13.8	13.8	13.8	13.8	13.8	13.8					
4	17.2	17.2	17.2	17.2	17.2	17.2	17.2	17.2				- 1	6
5	17.2	17.2	17.2	17.2	17.2	17.2	17.2	17.2					
	20.5		22.5	20.5	20.7	20.7	00.7				K	پ	
6		20.7	20.7	20.7	20.7	20.7	20.7	20.7			~?°)		
7	20.7	20.7	20.7	20.7	20.7	20.7	20.7	20.7					
8	20.7	20.7	20.7	20.7	20.7	20.7	20.7	20.7		100			
9	24.1	24.1	24.1	24.1	24.1	24.1	24.1	24.1		VS,			
10	24.1	24.1	24.1	24.1	24.1	24.1	24.1	24.1	" ŏ				
11	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	O _X				
12	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6					
13		27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6	27.6
								© `					
14	31.0	31.0	31.0	31.0	31.0	31.0	31.0	31.0					
							CN.						
15	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5					
16	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5
17	37.9	<i>37.9</i>	37.9	37.9	37.9	37.9	37.9	<i>37.</i> 9					
					· O,								
18	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4					
19	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4	41.4
20	55.2	55.2	55.2	55.2	55.2	<i>55.2</i>	<i>55.2</i>	55.2	55.2	55.2	55.2	55.2	55.2
			~0										
21	68.9	68.9	68,9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
22	137	133	128	125	122	119	116	112	109	106	103	98.0	93.5
23	138												
	Sh												
24	149	149	149	149	149	149	148	148	148	147			

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Cond./ Temper	Size, mm	P-No. (5)	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
1	Carbon steel	Pipe & tube	A134					1	(8b)(57)	В	310	165	482
2	Carbon steel	Pipe & tube	A672	A45	K01700			1	(57)(59)(67)	В	310	165	593
3	Carbon steel	Pipe & tube	API 5L	A25				1	(8a)(77)	-29	310	172	204
4	Carbon steel	Pipe & tube	API 5L	A25				1	(57)(59)(77)	В	310	172	204
5	Carbon steel	Pipe & tube	A179		K01200			1	(57)(59)	-29	324	179	593
6	Carbon steel	Pipe & tube	A53	Α	K02504			1	(8a)	-70) 331	207	204
7	Carbon steel	Pipe & tube	A139	Α				1	(8b)	A	331	207	149
8	Carbon steel	Pipe & tube	A587		K11500			1	(57)(59)	-29	331	207	454
9	Carbon steel	Pipe & tube	A53	Α	K02504			1	(57)(59)	В	331	207	593
10	Carbon steel	Pipe & tube	A106	Α	K02501			1	(57)	В	331	207	593
11	Carbon steel	Pipe & tube	A135	Α				1	(57)(59)	В	331	207	593
12	Carbon steel	Pipe & tube	A369	FPA	K02501			1	(57)	В	331	207	593
13	Carbon steel	Pipe & tube	API 5L	A			 Ç	JIX	(57)(59)	В	331	207	593
14	Carbon steel	Pipe & tube	A134				2	1	(8b)(57)	В	345	186	482
15	Carbon steel	Pipe & tube	A672	A50	K02200		77	1	(57)(59)(67)	В	345	186	593
16		D: 0 . 1	4104			:(0)		4	(01.)(57)		270	207	400
16	Carbon steel	Pipe & tube	A134			1,		1	(8b)(57)	A	379	207	482
17	Carbon steel Carbon steel	Pipe & tube	A524 A333	II 1	K02104 K03008			1	(57)	-29	379	207	538
18 19	Carbon steel	Pipe & tube	A334	1 1	K03008			1	(57)(59)	-46 -46	379	207 207	593 593
20	Carbon steel	Pipe & tube Pipe & tube	A671	CA55	/,			1 1	(57)(59) (50)(67)	-40 A	379 379	207	593
21	Carbon steel	Pipe & tube	A672	A55	K02801			1	(59)(67) (57)(59)(67)	A	379	207	593
22	Carbon steel	Pipe & tube	A672	C55	K02801	•••		1	(57)(59)(67)	C	379	207	593
	Carbon steer	-						1	(37)(07)	C	379	207	393
23	Carbon steel	Pipe & tube	A671	CC60	K02100			1	(57)(67)	С	414	221	538
24	Carbon steel	Pipe & tube	A671	CB60	K02401			1	(57)(67)	В	414	221	593
25	Carbon steel	Pipe & tube	A672	B60	K02401			1	(57)(67)	В	414	221	593
26	Carbon steel	Pipe & tube	A672	C60	K02100			1	(57)(67)	С	414	221	593
27	Carbon steel	Pipe & tube	A139	В	K03003			1	(8b)	A	414	241	149
28	Carbon steel	Pipe & tube	A135	В	K03018			1	(57)(59)	В	414	241	538
29	Carbon steel	Pipe & tube	A524	I	K02104			1	(57)	-29	414	241	538
	•	P											
30	Carbon steel	Pipe & tube	A53	В	K03005			1	(57)(59)	В	414	241	593
31	Carbon steel	Pipe & tube	A106	В	K03006			1	(57)	В	414	241	593
32	Carbon steel	Pipe & tube	A333	6	K03006			1	(57)	-46	414	241	593
33	Carbon steel	Pipe & tube	A334	6	K03006			1	(57)	-46	414	241	593
34	Carbon steel	Pipe & tube	A369	FPB	K03006			1	(57)	-29	414	241	593
35	Carbon steel	Pipe & tube	A381	Y35				1		Α	414	241	593
36	Carbon steel	Pipe & tube	API 5L	В				1	(57)(59)(77)	В	414	241	593

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	lumbers	1 6	0.11011						a, at M									······	
	Min.				710 11110	· · · · · · · · · · · · · · · · · · ·	541 655	, 0, 1.11	u, ut 1-1		прога		<u> </u>	(1)	(9)1			
	Temp.		4.5.5														-		
No.	to 40	65	100	150	200	250	300	325	350	375	400	425	450	475	500	525	550	575	600
1	103	103	101	97.5	94.6	90.8	86.1	83.6	81.1	78.6	73.3	64.0	55.8	43.9	40.7				
2	103	103	101	97.5	94.6	90.8	86.1	83.6	81.1	78.6	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
3	103	103	103	102	98.5													0-	
4	103	103	103	102	98.5												 ص	2/20	
5	108	108	108	106	102	98.3	93.3	90.6	87.8	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
6	110	110	110	110	110											0,0			
7	110	110	110	110											×.	, Y			
8	110	110	110	110	110	110	108	105	97.0	84.3	73.3	64.0	55.8	54.5	Sur.			•••	
9	110	110	110	110	110	110	108	105	97.0	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
10	110	110	110	110	110	110	108	105	97.0	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
11	110	110	110	110	110	110	108	105	97.0	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
12	110	110	110	110	110	110	108	105	97.0	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
13	110	110	110	110	110	110	108	105	97.0	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
14	115	115	113	110	106	102	96.9	94.1	91.2	84.3	7313	64.0	55.8	43.9	40.7				
15	115	115	113	110	106	102	96.9	94.1	91.2	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
16	126	126	126	122	118	113	108	105	-	98.3	89.0	75.3	62.1	45.0	40.7				
17	126	126	126	122	118	113	108	105		98.3	89.0	75.3	62.1	45.0	31.7	21.4	17.2		
18	126	126	126	122	118	113	108	105	101	98.3	89.0	75.3	62.1	45.0	31.7	21.4	14.2	9.40	6.89
19	126	126	126	122	118	113	108	105	101	98.3	89.0	75.3	62.1	45.0	31.7	21.4	14.2	9.40	6.89
20 21	126 126	126 126	126 126	122 122	118 118	113	108 108	105 105	101 101	98.3 98.3	89.0 89.0	75.3 75.3	62.1 62.1	45.0 45.0	31.7 31.7	21.4 21.4	14.2 14.2	9.40 9.40	6.89 6.89
22	126 126	126	126	122	118	113 113	108	105	101	98.3	89.0	75.3	62.1	45.0 45.0	31.7	21.4	14.2	9.40	6.89
					_ (9.40	0.09
23	138	138	134	130	126		115	111	108	105	95.1	79.5	62.6	45.0	31.7	21.4	17.2		
24	138	138	134	130	126	121	115	111	108	105	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
25	138	138	134	130	126	121	115	111	108	105	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
26	138	138	134		126	121	115	111	108	105	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
27	138	138	138	138														•••	
28	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	17.2		
29	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	17.2		
30	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
31	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
32	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
33	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
34	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
35	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
36	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Cond./ Temper	Size, mm	P-No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
37	Carbon steel	Pipe & tube	A139	С	K03004			1	(8b)	Α	414	290	149
38	Carbon steel	Pipe & tube	A139	D	K03010			1	(8b)	Α	414	317	149
39	Carbon steel	Pipe & tube	API 5L	X42				1	(55)(77)	Α	414	290	204
		•											
40	Carbon steel	Pipe & tube	A381	Y42				1		A	414	290	204
41	Carbon steel	Pipe & tube	A381	Y48				1		A	427	331	343
42	Carbon steel	Pipe & tube	API 5L	X46				1	(55)(77)	A) 434	317	204
43	Carbon steel	Pipe & tube	A381	Y46				1		A	434	317	204
		-							•	VI			
44	Carbon steel	Pipe & tube	A381	Y50				1	, PS	A	441	345	343
45	Carbon steel	Pipe & tube	A671	CC65	K02403			1	(57)(60)	В	448	241	538
46	Carbon steel	Pipe & tube	A671	CB65	K02800			1	(57)(67)	Α	448	241	593
47	Carbon steel	Pipe & tube	A672	B65	K02800			1	(57)(67)	Α	448	241	593
48	Carbon steel	Pipe & tube	A672	C65	K02403			1	(57)(67)	В	448	241	593
		•					ç	n.					
49	Carbon steel	Pipe & tube	A139	Е	K03012		0	1	(8b)	Α	455	359	149
50	Carbon steel	Pipe & tube	API 5L	X52				1	(55)(77)	Α	455	359	204
51	Carbon steel	Pipe & tube	A381	Y52		N.		1		A	455	359	204
-						ile.							
52	Carbon steel	Pipe & tube	A671	CC70	K02700			1	(57)(67)	В	483	262	538
53	Carbon steel	Pipe & tube	A671	CB70	K08101			1	(57)(67)	A	483	262	593
54	Carbon steel	Pipe & tube	A672		K03101			1	(57)(67)	A	483	262	593
55	Carbon steel	Pipe & tube	A672	C70	K02700			1	(57)(67)	В	483	262	593
56	Carbon steel	Pipe & tube	A106	\ C	K03501			1	(57)	В	483	276	427
57	Carbon steel	Pipe & tube	A671	CD70	K12437		 ≤64	1	(67)	D	483	345	371
58	Carbon steel	Pipe & tube	A672	D70	K12437		≤64	1	(67)	D	483	345	371
59	Carbon steel	Pipe & tube	A691	CMSH-	K12437		≤64	1	(67)	D	483	345	371
37	carbon seer	Tipe & tube	AOJI	70	K12437		201	1	(07)	D	103	343	371
60	Carbon steel	Pipe & tube	API 5L	X56				1	(51)(55)(71) (77)	A	490	386	204
61	Carbon steel	Pipe & tube	A381	Y56				1	(51)(55)(71)	Α	490	386	204
62	Carbon steel		A671	CK75	 К02803		 >25	1	(57)(67)	A	517	276	593
63	Carbon steel		A672	N75	K02803		>25	1	(57)(67)	A	517	276	593
64	Carbon steel	Pipe & tube	A691		K02803		>25	1	(57)(67)	A	517	276	593
04	Carbonisteer	ripe & tube	A071	CM3-73	K02003		-23	1	(37)(07)	А	317	270	393
65	Carbon steel	Pipe & tube	A671	CK75	K02803		≤25	1	(57)(67)	Α	517	290	371
66	Carbon steel	Pipe & tube	A672	N75	K02803		≤25	1	(57)(67)	Α	517	290	371
67	Carbon steel	Pipe & tube	A691		K02803		≤25	1	(57)(67)	A	517	290	371
									(3.)(3.)				
68	Carbon steel	Pipe & tube	API 5L	X60				1	(51)(55)(71) (77)	A	517	414	204
69	Carbon steel	Pipe & tube	API 5L	X65				1	(51)(55)(71) (77)	A	531	448	204
70	Carbon steel	Pipe & tube	API 5L	X70				1	(51)(55)(71) (77)	A	565	483	204

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	unibers	, 111 1 0	Спин						a, at M								.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
	Min.													. , ,					
	Temp.	6 F	100	150	200	250	300	325	350	375	400	425	450	475	500	525	550	-7 -	600
No. 37	to 40	65 138	138	138														575	600
38	138	138	138	138															
39	138	138	138	138	 138														
3,	150	150	150	100	100	•••			•••	•••		•••		•••	•••		•••		
40	138	138	138	138	138													7/8	
41	142	142	142	142	142	142	142	142	129								(2)		
42	145	145	145	145	145											0 ,5			
43	145	145	145	145	145										1	Y			
44	147	147	147	147	147	147	147	147	129					C	Mr				
														& P					
45	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	47.7	32.5	21.4	17.2		
46	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	47.7	32.5	21.4	14.2	9.40	6.89
47	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	47.7	32.5	21.4	14.2	9.40	6.89
48	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	47.7	32.5	21.4	14.2	9.40	6.89
49	152	152	152	152							୍ଡ `								
50	152	152	152	152	152					٠, ×	7,"								
51	152	152	152	152	152				 !!	N.S.									
52	161	161	159	154	150	144	136	132	128	122	101	83.8	66.8	50.3	33.2	21.4	17.2		
53	161	161	159	154	150	144	136	132	128	122	101	83.8	66.8	50.3	33.2	21.4	14.2	9.40	6.89
54	161	161	159	154	150	144	136	132	128	122	101	83.8	66.8	50.3	33.2	21.4	14.2	9.40	6.89
55	161	161	159	154	150	144	136	132	128	122	101	83.8	66.8	50.3	33.2	21.4	14.2	9.40	6.89
56	161	161	161	161	158	151	144	139	135	122	101	83.8	82.7						
57	161	161	161	157	156	156	156	154	148	126									
58	161	161	161	157	156	156	156	154	148	126									
59	161	161	161	157	56	156	156	154	148	126									
60	163	163	163	163	163														
61	163	163	163	163	163														
62	172	172	168	163	158	151	144	139	135	131	107	88.0	67.3	50.3	33.2	21.4	14.2	9.40	6.89
63	172	172	168	163	158	151	144	139	135	131	107	88.0	67.3	50.3	33.2	21.4	14.2	9.40	6.89
64	172	172	168	163	158	151	144	139	135	131	107	88.0	67.3	50.3	33.2	21.4	14.2	9.40	6.89
65	172	172	172	171	165	159	151	146	142	131									
66	172	172	172	171	165	159	151	146	142	131									
67	172	172	172	171	165	159	151	146	142	131									
68	172	172	172	172	172														
69	177	177	177	177	177														
70	188	188	188	188	188														

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Cond./ Temper	Size, mm	P-No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
71	Carbon steel	Pipe & tube	API 5L	X80				1	(51)(55)(71) (77)	A	621	552	204
72	Carbon steel	Pina & tuha	A381	Y60				1	(51)(71)	A	517	414	204
72	car bon steer	Tipe & tube	A301	100				1	(31)(71)	А	317	117	5
73	Carbon steel	Pipe	A134					1	(8a)(8c)	-29	311	165	204
74	Carbon steel	Pipe	A134					1	(8a)(8c)	-29	338	207	204
75	Carbon steel	Pipe	A134					1	(8a)(8c)	29	345	186	149
76	Carbon steel	Pipe	A134					1	(8a)(8c)	-29	359	228	204
77	Carbon steel	Pipe	A134					1	(8a)(8d)	-29	365	248	204
78	Carbon steel	Pipe	A134					1	(8a)(8c)	-29	379	276	204
79	Carbon steel	Pipe	A134				k		(8a)(8c)	-29	400	248	204
80	Carbon steel	Pipe	A134				100	1	(8a)(8c)	-29	414	228	149
81	Carbon steel	Pipe	A134			W.		1	(8a)(8c)	-29	414	310	204
						ile							
82	Carbon steel	Pipe	A134		1/0			1	(8a)(8c)	-29	448	345	204
83	Carbon steel	Plate, bar, shps., sheet	A285	A	K01700			1	(57)(59)	В	310	165	593
84	Carbon steel	Plate, bar, shps., sheet	A285	V B	K02200			1	(57)(59)	В	345	186	593
85	Carbon steel	Plate, bar, shps., sheet	A516	55	K01800			1	(57)	С	379	207	454
86	Carbon steel	Plate, bar, shps., sheet	A285	С	K02801			1	(57)(59)	A	379	207	593
87	Carbon steel	Plate, bar, shps, sheet	A516	60	K02100			1	(57)	С	414	221	454
88	Carbon steel	Plate, bar, shps., sheet	A515	60	K02401			1	(57)	В	414	221	538
89	Carbon steel	Plate, bar, shps., sheet	A696	В	K03200			1	(57)	A	415	240	371
90	Carbon steel	Plate, bar, shps., sheet	A516	65	K02403			1	(57)	В	448	241	454
91	Carbon stee			65	K02800			1	(57)	A	448	241	538
92	Carbon steel	Plate, bar, shps., sheet	A516	70	K02700			1	(57)	В	483	262	454
93	Carbon steel	Plate, bar, shps., sheet		70	K03101			1	(57)	A	483	262	538
94	Carbon steel	Plate, bar, shps., sheet	A696	С	K03200			1	(57)	A	485	275	371
95	Carbon steel	Plate, bar, shps., sheet	A537		K12437	1	≤64	1		D	483	345	371
96	Carbon steel	Plate, bar, shps., sheet		A	K02803		>25	1	(57)	A	517	276	593
97	Carbon steel	Plate, bar, shps., sheet	A299	A	K02803		≤25	1	(57)	A	517	290	593
98	Carbon steel	Plate, bar, shps., sheet	A283	Α	K01400			1	(8c)(57)	A	310	165	399

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	lumbers	, 111 1 0	ii Ciltili			wable											**13C 1	iuitall	-u
	Min.													. , ,					
	Temp. to 40	6E	100	150	200	250	300	325	350	275	400	425	450	475	500	525	EEO	E7E	600
No. 71	207	65 207	207	207	207					375				4/3			550	575 	000
, 1	207	207	207	207	207														
72	172	172	172	172	172													 O	
73	103	103	101	97.5	94.6												<u>"</u>	7	
74	113	113	113	113	113											- CZ	ري` ري`		
75	115	115	113	110											K	ر کی			
76	120	120	120	120	120									C	Sh.				
77	122	122	122	122	122								<u> </u>	5 ¹					
78	126	126	126	126	126							"6)						
79	133	133	133	133	133	•••						71							
80	138	138	138	134						×	<u>,</u>								
81	138	138	138	138	138					en									
82	149	149	149	149	149			,	0										
83	103	103	101	97.5	94.6	90.8	86.1	83.6	81.1	78.6	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
84	115	115	113	110	106	102	96.9	94.1	91.2	84.3	73.3	64.0	55.8	43.9	31.7	21.4	14.2	9.40	6.89
85	126	126	126	122	118	113	108	105	101	98.3	89.0	75.3	62.1	60.0					
86	126	126	126	122	118	113	108	105	101	98.3	89.0	75.3	62.1	45.0	31.7	21.4	14.2	9.40	6.89
87	138	138	134	130	126	121	115	111	108	105	95.1	79.5	62.6	60.0					
88	138	138	134	130	126	121	115	111	108	105	95.1	79.5	62.6	45.0	31.7	21.4	17.2		
89	138	138	138	138	138	132	125	122	118	115									
90	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	62.1					
91	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	47.7	32.5	21.4	17.2		
92	161	161	159	154	150	144	136	132	128	122	101	83.8	66.8	64.1					
93	161	161	159	154	150	144	136	132	128	122	101	83.8	66.8	50.3	33.2	21.4	17.2		
94 95	161 161	161 161	161 161	161 157	158 <i>156</i>	151 156	144 156	139 154	135 148	131 126									
96	172	172	168	163	158	151	144	139	135	131	107	88.0	67.3	50.3	33.2	21.4	14.2	9.40	6.89
97	172	172	172	171	165	159	151	146	142	131	107	88.0	67.3	50.3	33.2	21.4	14.2	9.40	6.89
98	103	103	101	97.5	94.6	90.8	86.1	83.6	81.1	78.6	73.8								

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Cond./ Temper	Size, mm	P-No. (5)	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
99	Carbon steel	Plate, bar, shps., sheet	A1011	30	K02502			1	(8c)(57)	Α	338	207	399
100	Carbon steel	Plate, bar, shps., sheet	A283	В	K01702			1	(8c)(57)	A	345	186	399
101	Carbon steel	Plate, bar, shps., sheet	A1011	33	K02502			1	(8c)(57)	A	359	228	399
102	Carbon steel	Plate, bar, shps., sheet	A1011	36	K02502			1	(8c)(57)	A	365	248	399
103	Carbon steel	Plate, bar, shps., sheet	A283	С	K02401			1	(8c)(57)	Α	379	207	399
104	Carbon steel	Plate, bar, shps., sheet		40	K02502			1	(8c)(57)	A	1379	276	399
		,,,							(00)(01)	~~	3		
105	Carbon steel	Plate, bar, shps., sheet	A36		K02600			1	(8c)	NEA C	400	248	371
106	Carbon steel	Plate, bar, shps., sheet	A283	D	K02702			1	(8c)(57)	Α	414	228	399
107	Carbon steel	Plate, bar, shps., sheet	A1011	45	K02507			1	(8c)(57)	A	414	310	399
		•							40				
108	Carbon steel	Plate, bar, shps., sheet		50	K02507			1	(8c)(57)	A	448	344	399
109	Carbon steel	Plate, bar, shps., sheet	A992					1	(8c)(57)	A	448	344	427
110	Carbon steel	Forgings & fittings	A350	LF1	K03009		٤		(9)(57)(59)	-29	414	207	538
111	Carbon steel	Forgings & fittings	A181		K03502	60	<u>~</u> @	1	(9)(57)(59)	Α	414	207	593
112	Carbon steel	Forgings & fittings	A420	WPL6	K03006	ilen*	 77 .	1	(57)	-46	414	241	538
113	Carbon steel	Forgings & fittings	A234	WPB	K03006			1	(57)(59)	В	414	241	593
114	Carbon steel	Forgings & fittings	A694	F42	K03014			1	(9)	-29	415	290	260
115	Carbon steel	Forgings & fittings	A707	L1	K02302	1		1	(9)	-29	415	290	260
116	Carbon steel	Forgings & fittings	A707	L2	K03301	1		1	(9)	-46	415	290	260
117	Carbon steel	Forgings & fittings	A707	L3	K12510	1		1	(9)	-46	415	290	260
118	Carbon steel	Forgings & fittings	A860	WPHY				1		-46	415	290	260
		OC).	42									
119	Carbon steel	Forgings & fittings	A694	F46	K03014			1	(9)	-29	435	317	260
120	Carbon steel	Forgings & fittings	A860	WPHY 46				1		-46	435	317	260
121	Carbon steel	Forgings & fittings	A694	F52	K03014			1	(9)	-29	455	360	260
122	Carbon steel	Forgings & fittings	A707	L1	K02302	2		1	(9)	-29	455	360	260
123	Carbon steel	Forgings & fittings	A707	L2	K03301	2		1	(9)	-46	455	360	260
124	Carbon steel	Forgings & fittings	A707	L3	K12510	2		1	(9)	-46	455	360	260
125	Carbon steel	Forgings & fittings	A860	WPHY 52			•••	1		-46	455	360	260
126	Carbon steel	Forgings & fittings	A350	LF2	K03011	1		1	(9)(57)	-46	483	248	538
127	Carbon steel	Forgings & fittings	A350	LF2	K03011	2		1	(9)(57)	-18	483	248	538
				D. 2		-							
128	Carbon steel	Forgings & fittings	A105		K03504			1	(9)(57)(59)	-29	483	248	593
129	Carbon steel	Forgings & fittings	A181		K03502	70		1	(9)(57)(59)	A	483	248	593
130	Carbon steel	Forgings & fittings	A234	WPC	K03501			1	(57)(59)	В	483	276	427

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	umbers								a, at M		_								
	Min.										-			. ,		,,			
Line	Temp.																		
No.	to 40	65	100	150	200	250	300	325	350	375	400	425	450	475	500	525	550	575	600
99	113	113	113	113	113	113	108	105	97.0	84.3	73.8								
100	115	115	113	110	106	102	96.9	94.1	91.2	84.3	73.8								
101	120	120	120	120	120	120	118	115	97.0	84.3	73.8								
																		0-	
102	122	122	122	122	122	122	122	122	97.0	84.3	73.8							V.0	
																	<u> </u>	2.	
103	126	126	126	122	118	113	108	105	101	98.3	89.6						02	/	
104	126	126	126	126	126	126	126	126	124	105	89.6					N			
																2	•		
105	133	133	133	133	133	133	129	125	122	108					1,	V			
106	138	138	138	134	130	125	118	115	111	108	95.8			C					
107	138	138	138	138	138	138	138	138	135	113	95.8			· P'					
10,	100	100	100	100	100	100	100	100	100	110	70.0			7	•••			•••	•••
108	149	149	149	149	149	149	149	149	135	113	95.8		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \						
100	142	142	142	142	142	142	142	142	121	108	90.3	7 5.6	59.9	•••	•••			•••	•••
107	142	172	172	172	172	172	172	172	121	100	70.5	1,4,4	37.7	•••	•••			•••	•••
110	138	130	126	122	118	113	108	105	101	98.3	05 (1)	79.5	62.6	45.0	31.7	21.4	172		
																21.4	17.2		
111	138	130	126	122	118	113	108	105	101	98.3	95/1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
										la.	··				a. -				
112	138	138	138	138	138	132	126	122	118	2113	95.1	79.5	62.6	45.0	31.7	21.4	17.2	•••	
									7.										
113	138	138	138	138	138	132	126	122	118	113	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
								الي.	•										
114	138	138	138	138	138	137	132						•••	•••					
115	138	138	138	138	138	137	132												
116	138	138	138	138	138	137	132												
117	138	138	138	138	138	137	132												
118	138	138	138	138	138	137	132												
					\sim \sim \sim														
)														
119	145	145	145	145	145	145	144							•••		•••	•••		
120	145	145	145	145	145	145	144												
101	450	450	O_{λ}	150	150	450	450												
121	150	~ ~	150	150	150	150	150												
122	150	150	150	150	150	150	150	•••	•••			•••	•••	•••		•••	•••		
123		150	150	150	150	150	150												
124		150	150	150	150	150	150												
125	150	150	150	150	150	150	150					•••				•••	•••		
100	100	151	151	1.40	1.40	100	100	105	100	110	101	00.0		F0.0	20.0	24.4	450		
126	161	156	151	146	142	136	129	125	122	118	101	83.8	66.8	50.3	33.2	21.4	17.2		
127	161	156	151	146	142	136	129	125	122	118	101	83.8	66.8	50.3	33.2	21.4	17.2		
128	161	156	151	146	142	136	129	125	122	118	101	83.8	66.8	50.3	33.2	21.4	14.2	9.40	6.89
129	161	156	151	146	142	136	129	125	122	118	101	83.8	66.8	50.3	33.2	21.4	14.2	9.40	6.89
130	161	161	161	161	158	151	144	139	135	122	101	83.8	82.7						

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Cond./ Temper	Size, mm	P-No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
	0 0	A694	F56				1		-29	490		260
		A694	F60						-29	515		260
	0 0	A707	L2		3				-46	515		260
		A707		K12510	3							
Carbon steel	Forgings & fittings	A860	WPHY 60				1		-46	_ *	415	260
Carbon steel	Forgings & fittings	A694	F65	K03014			1	(9)	-29		450	260
Carbon steel	Forgings & fittings	A860	WPHY 65				1		-46	530	450	260
Carbon steel	Forgings & fittings	A694	F70	K03014			1	(9)(79)	N	565	485	204
Carbon steel	Forgings & fittings	A860	WPHY 70				1	C	-46	565	485	204
Carbon steel	Castings	A216	WCA	J02502			1	(57)	-29	414	207	593
Carbon steel	Castings	A352	LCB	J03003			1	(9)(57)	-46	448	241	593
Carbon steel	Castings	A352	LCC	J02505		 Ç	11/4	(9)	-46	483	276	371
Carbon steel	Castings	A216	WCB	J03002		ZO.	1	(9)(57)	-29	483	248	593
Carbon steel	Castings	A216	WCC	J02503	~/	<i>"</i>	1	(9)(57)	-29	483	276	538
ASI	IENORMDOC		"V	ilck to	TION.							
	Carbon steel	Carbon steel Forgings & fittings Carbon steel Carbings & fittings Carbon steel Castings Carbon steel Castings Carbon steel Castings Carbon steel Castings	Carbon steel Forgings & fittings A694 Carbon steel Forgings & fittings A707 Carbon steel Forgings & fittings A707 Carbon steel Forgings & fittings A707 Carbon steel Forgings & fittings A860 Carbon steel Castings A350 Carbon steel Castings A352 Carbon steel Castings A352 Carbon steel Castings A216 Carbon steel Castings A216 Carbon steel Castings A216	Carbon steel Forgings & fittings A694 F60 Carbon steel Forgings & fittings A707 L2 Carbon steel Forgings & fittings A707 L3 Carbon steel Forgings & fittings A707 L3 Carbon steel Forgings & fittings A860 WPHY 60 Carbon steel Forgings & fittings A694 F65 Carbon steel Forgings & fittings A860 WPHY 65 Carbon steel Forgings & fittings A860 WPHY 65 Carbon steel Forgings & fittings A860 WPHY 70 Carbon steel Forgings & fittings A860 WPHY 70 Carbon steel Castings A216 WCA Carbon steel Castings A352 LCB Carbon steel Castings A216 WCB Carbon steel Castings A216 WCC	Carbon steel Forgings & fittings A694 F56 K03014 Carbon steel Forgings & fittings A707 L2 K03301 Carbon steel Forgings & fittings A707 L3 K12510 Carbon steel Forgings & fittings A860 WPHY Carbon steel Forgings & fittings A694 F65 K03014 Carbon steel Forgings & fittings A707 L3 K12510 Carbon steel Forgings & fittings A860 WPHY Carbon steel Castings A369 WPHY Carbon steel Castings A352 LCB J03003 Carbon steel Castings A352 LCB J02505 Carbon steel Castings A216 WCB J03002 Carbon steel Castings A216 WCB J03002 Carbon steel Castings A216 WCC J02503	Nominal CompositionProduct FormSpec. No.Type/ GradeCond./ GradeCond./ TemperCarbon steel Carbon steel Carbon steel Carbon steel Forgings & fittings Carbon steel Carbon steel Forgings & fittings Carbon steel Forgings & fittings Forgings & fittings Carbon steel Forgings & fittings Carbon steel Forgings & fittings Carbon steel Forgings & fittings Forgings & fittings Carbon steel Forgings & fittings Carbon steel Forgings & fittings Carbon steel Forgings & fittings Forgings & fittings Carbon steel Forgings & fittings Carbon steel Forgings & fittings Carbon steelA694 F65 A694 F70 A860 WPHY F70 WCAWOA WPHY WCAWOA WPHY WCAWOA WPHY WCAWOA WPHY WCAWOA WPHY WCACarbon steel Carbon steelCastings Carbon steelA352 Carbon steelLCB WCAJ03003 J03003 J03002 J02503WCA WCACarbon steel Carbon steelCastingsA216 CastingsWCB WCBJ03002 J02503WWW WCC	Nominal Composition Product Form Spec. No. Type Grade Grad	Nominal Composition	Nominal Composition	Nominal Composition	Nominal Carbon steel Forgings & fittings A694 F56 K03014 1 (9)	Nominal Carbon steel Forgings & fittings A694 F56 K03014 1 (9)

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

131	to 40	65	100	150	200	250	300	325	350	375	400	425	450	475	500	525	550	575	600
	163	163	163	163	163	163	163												
132	172	172	172	172	172	172	172												
133	172	172	172	172	172	172	172											·C-	
134	172	172	172	172	172	172	172											100	
135	172	172	172	172	172	172	172)	
136	177	177	177	177	177	177	177										<u>ن</u> ز		
137	177	177	177	177	177	177	177									^{റ്റ} ്റ			
138	188	188	188	188	188	188									4	,			
	188	188	188	188	188	188									NI				
														, P.)				
140	138	130	126	122	118	113	108	105	101	98.3	95.1	79.5	62.6	45.0	31.7	21.4	14.2	9.40	6.89
141	149	149	147	142	138	132	126	122	118	113	95.1	79.5	64.4	47.7	32.5	21.4	14.2	9.40	6.89
	161	161	161	161	158	151	139	137	136	132									
												.							
143	161	156	151	146	142	136	129	125	122	118	101	83.8	66.8	50.3	33.2	21.4	14.2	9.40	6.89
144	161	161	161	161	158	151	144	139	135	122	101	83.8	66.8	50.3	33.2	21.4	17.2		
					142		V . C	ick	<i>`</i> 0,										

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line	Nominal	Product	Spec.	Type/	UNS	Class/ Condition/	Size,	P-No.	MISTINE MISTINE	Min. Temp.,	Min. Tensile Str.,	Min. Yield Str.,	Max. Use Temp.,
No.	Composition	Form	No.	Grade	No.	Temper	mm	(5)	Notes	°C (6)	MPa	MPa	°C
	¹ / ₂ Cr- ¹ / ₂ Mo	Pipe	A335	P2	K11547			3		-29	379	207	538
2	½Cr−½Mo	Pipe	A691	½CR	K12143			3	(11)(67)	-29	379	228	538
3	$C-\frac{1}{2}Mo$	Pipe	A335	P1	K11522			3	(58)	-29	379	207	593
	$C-\frac{1}{2}Mo$	Pipe	A369	FP1	K11522			3	(58)	-29	379	207	7 593
	¹/ ₂ Cr−¹/ ₂ Mo	Pipe	A369	FP2	K11547			3		-29	379	207	593
6	1Cr− ¹ ⁄ ₂ Mo	Pipe	A691	1CR	K11757			4	(11)(67)	-29	379	228	649
7	¹/₂Cr−¹/₂Mo	Pipe	A426	CP2	J11547			3	(10)	-29	414	207	593
	$1\frac{1}{2}Si-\frac{1}{2}Mo$	Pipe	A335	P15	K11578			3		-29 <	2414	207	593
9	C− ¹ ⁄ ₂ Mo−Si	Pipe	A426	CP15	J11522			3	(10)	-29	414	207	593
10	1Cr-½Mo	Pipe	A426	CP12	J11562			4	(10)	S-29	414	207	649
11	5Cr-1½Si- ½Mo	Pipe	A426	CP5b	J51545			5B	(10)	-29	414	207	649
12	3Cr-Mo	Pipe	A426	CP21	J31545			5A	(10)	-29	414	207	649
13	³ / ₄ Cr- ³ / ₄ Ni-Cu- Al	Pipe	A333	4	K11267			(4)		-101	414	241	40
14	2Cr- ¹ / ₂ Mo	Pipe	A369	FP3b	K21509		X	S 4		-29	414	207	649
15	1Cr−½Mo	Pipe	A335	P12	K11562		0,10	4		-29	414	221	649
16	1Cr- ¹ / ₂ Mo	Pipe	A369	FP12	K11562	V		4		-29	414	221	649
17	1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si	Pipe	A335	P11	K11597	1		4	•••	-29	414	207	649
	1½Cr-½Mo-Si	Pipe	A369	FP11	K11597	Jic."		4		-29	414	207	649
19	1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si	Pipe	A691	11/4CR	K11789			4	(11)(67)	-29	414	241	649
	5Cr−½Mo	Pipe	A691	5CR	K41545			5B	(11)(67)	-29	414	207	649
21	5Cr−½Mo	Pipe	A335	P5	K41545			5B		-29	414	207	649
	5Cr-½Mo-Si	Pipe	A335	P5b	K51545			5B		-29	414	207	649
	5Cr−½Mo−Ti	Pipe	A335	P5c	K41245			5B		-29	414	207	649
24	5Cr- ¹ / ₂ Mo	Pipe	A369	FP5	K41545			5B		-29	414	207	649
25	9Cr-1Mo	Pipe	A335	Р9	K90941			5B		-29	414	207	649
	9Cr-1Mo	Pipe	A369	FP9	K90941			5B		-29	414	207	649
27	9Cr-1Mo	Pipe	A691	9CR	K90941			5B	(11)(67)	-29	414	207	649
28	3Cr-1Mo	Pipe	A335	P21	K31545			5A		-29	414	207	649
29	3Cr-1Mo	Pipe	A369	FP21	K31545			5A		-29	414	207	649
30	3Cr-1Mo	Pipe	A691	3CR	K31545			5A	(11)(67)	-29	414	207	649
31	2 ¹ / ₄ Cr-1Mo	Pipe	A691	2 ¹ / ₄ CR	K21590			5A	(11)(67)(72) (75)	-29	414	207	649
	2 ¹ / ₄ Cr-1Mo	Pipe	A369	FP22	K21590			5A	(72)(75)	-29	414	207	649
	2 ¹ / ₄ Cr-1Mo	Pipe	A335	P22	K21590			5A	(72)(75)	-29	414	207	649
	2Ni-1Cu	Pipe	A333	9	K22035			9A		-73	434	317	40
35	2Ni-1Cu	Pipe	A334	9	K22035	•••		9A		-73	434	317	40

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Nulli	Ders	111 1	ai cii	tilest												°C [Not				Tiller	WISC	inuica	iteu	
	Min.						Jusic	7111011	ubic	ou co.	,, 0, 1.1	<i>1 u, u</i>	·····	1 1011	треги	ture,	C [MOC	C3 (1)	unu (,					
Line	Temp.																								
No.	to 40																450		500			575	600	625	650
1	126											112		108			100	97.1	74.4				•••		
2	126	126	126	126	126	126	126	126	126	126	125	123	121	119	116	114	110	107	74.4	49.9	40.7		•••		
3	126															103			68.0						
4	126															103			68.0				16.5		
5	126												110				100		93.5)		
6	126	126	123	122	122	122	122	121	120	118	116	115	114	112	110	109	106	104	92.1	61.1	40.4	26.4	17.4	11.6	7.58
7	120	122	120	126	124	122	120	110	117	115	111	112	110	100	100	102	100	07.1	74.4	40.0	1)	16 5		
7 8	138 138															103 107			74.4 74.7	`'	7				
9																107			74.7						
,	150	133	12)	127	123	124	122	121	120	110	11/	113	114	112	110	107	103	00.4	N.	33.7	33.0	23.2	10.5		•••
10	138	120	124	120	117	115	112	110	100	107	106	105	103	102	100	087	7 96.8	946	92.0	61 1	40.4	26.4	17.4	116	7.58
10	150	12)	124	120	117	113	112	110	107	107	100	103	103	102	100	70.7	70.0	. 43.0) ,2.0	01.1	70.7	20.4	17.4	11.0	7.30
11	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	80.6	617	46.4	34.7	25.5	17 R	11 4	6.89
11	150	12)	124	122	120	11)	11)	110	110	117	11/	110	114	112	110	100	103	00.0	01.7	70.7	34.7	23.3	17.0	11.7	0.09
12	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	89.2	68.8	54.2	43.4	34.0	25.1	17.1	10.3
															-	X									
13	138														ال										
														_0											
14	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	118	74.7	53.3	36.0	24.6	15.5	9.21	6.89
													4												
15	138											4	$\mathbf{\mathcal{C}}$			105		101					17.4		7.58
16	138	138	132	128	125	122	120	118	116	114	113	HX	110	109	107	105	103	101	92.1	61.1	40.4	26.4	17.4	11.6	7.58
17	120	121	126	124	101	110	116	115	110	444	400	107	100	104	100	00.6	07.0	045	50.5	5 2.0	26.2	25.2	45.6	40.0	0.25
17										. •. C	10						97.2								8.27
18	138	131	120	124	121	119	110	115	113	111	109	107	100	104	102	99.0	97.2	94.3	/3./	52.0	30.3	23.2	17.0	12.3	8.27
19	138	120	130	120	120	12Ω	136	12/	121	120	127	125	122	121	110	116	112	104	73 7	52 N	363	25.2	17.6	122	8.27
20									7,							106							17.8		6.89
20	150	12)	127	122	120	117		9	110	117	117	110	111	112	110	100	103	00.0	01.7	10.1	34.7	25.5	17.0	11.7	0.07
21	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	80.6	617	46.4	34 7	25.5	17.8	114	6.89
22													114				103						17.8		6.89
23						\sim							114				103						17.8		6.89
24					. 17.7											106	103						17.8		6.89
				X																					
25	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	98.3	83.2	60.2	42.9	29.9	20.6	14.4	10.3
26	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	98.3	83.2	60.2	42.9	29.9	20.6	14.4	10.3
27	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	98.3	83.2	60.2	42.9	29.9	20.6	14.4	10.3
	7	O .																							
28																122							25.1		
29	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	89.2	68.8	54.2	43.4	34.0	25.1	17.1	10.3
30	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	89.2	68.8	54.2	43.4	34.0	25.1	17.1	10.3
31																122							23.5		9.65
			-	-	-									·	-					-			-	-	
32	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	99.6	80.9	63.3	47.5	34.2	23.5	15.3	9.65
33	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	99.6	80.9	63.3	47.5	34.2	23.5	15.3	9.65
2.4	1 4 5																								
34																				•••					
35	145																			•••					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers in 1				·-PP	11 140	, -pt			U			M
Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
36	2 ¹ / ₄ Ni	Pipe	A333	7	K21903			9A		-73	448	241	593
	2 ¹ / ₄ Ni	Pipe	A334	7	K21903			9A		-73	448	241	593
38	3 ¹ / ₂ Ni	Pipe	A333	3	K31918			9B		-101	448	241	593
	3½Ni	Pipe	A334	3	K31918			9B		-101	448	241	593
	2	•										~	V
40	C- ¹ / ₂ Mo	Pipe	A426	CP1	J12521			3	(10)(58)	-29	448	241	593
41	C-1/2Mo	Pipe	A672	L65	K11820			3	(11)(58)(67)	-29	448	255	593
	C-½Mo	Pipe	A691	CM-65	K11820			3	(11)(58)(67)	-29	2448	255	593
	_	•								4.	V		
43	2 ¹ / ₄ Ni	Pipe	A671	CFB70	K22103			9A	(11)(65)(67)	-29	483	276	40
	3½Ni	Pipe	A671	CFE70	K32018			9B	(11)(65)(67)	-29	483	276	40
									٤.	/			
45	C-1/2Mo	Pipe	A672	L70	K12020			3	(11)(58)(67)	-29	483	276	593
46	C-½Mo	Pipe	A691	CM-70	K12020			3	(11)(58)(67)	-29	483	276	593
47	1 ¹ / ₄ Cr- ¹ / ₂ Mo	Pipe	A426	CP11	J12072			4	(10)	-29	483	276	649
48	2 ¹ / ₄ Cr-1Mo	Pipe	A426	CP22	J21890			5A	(10)(72)	-29	483	276	649
49	C-1/2Mo	Pipe	A672	L75	K12320		, X	3	(11)(58)(67)	-29	517	296	593
50	C-1/2Mo	Pipe	A691	CM-75	K12320		SN	3	(11)(58)(67)	-29	517	296	593
						j							
51	9Cr-1Mo-V	Pipe	A335	P91	K90901	wO	≤75	15E		-29	586	414	649
52	9Cr-1Mo-V	Pipe	A691	91	K90901	1	≤75	15E	(11)(67)	-29	586	414	649
						lio,							
53	5Cr-½Mo	Pipe	A426	CP5	J42045	J		5B	(10)	-29	621	414	649
54	9Cr-1Mo	Pipe	A426	CP9	J82090			5B	(10)	-29	621	414	649
					U.								
	9Ni	Pipe	A333	8	⊀81340			11A	(47)	-196	689	517	93
	9Ni	Pipe	A334	7 8.	K81340			11A	***	-196	689	517	93
	¹/ ₂ Cr−¹/ ₂ Mo	Plate	A387	2	K12143	1		3		-29	379	228	538
	1Cr-½Mo	Plate	A387	12	K11757	1		4		-29	379	228	649
59	9Cr-1Mo	Plate	A387	9	K90941	1		5B		-29	414	207	649
		1											
	1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si	Plate	A387	11	K11789	1		4		-29	414	241	649
	5Cr-½Mo	Plate	A387	5	K41545	1		5B		-29	414	207	649
	3Cr-1Mo	Plate	A387	21	K31545	1		5A		-29	414	207	649
63	2 ¹ / ₄ Cr-1Mo	Plate	A387	22	K21590	1		5A	(72)	-29	414	207	649
	a1. vv				*****								=00
	2 ¹ / ₄ Ni 3 ¹ / ₂ Ni	Plate	A203	A	K21703			9A	(12)(65)	-29	448	255	538
65	37 ₂ N1	Plate	A203	D	K31718		•••	9B	(12)(65)	-29	448	255	538
6.6	C-½Mo	Plate	A204	A	K11820			3	(58)	-29	448	255	593
	С- / ₂ мо 1Cr- ¹ / ₂ Мо	Plate	A204 A387	12	K11820 K11757	 2	•••	4	(58)	-29 -29	448	255	593 649
07	1G1 - /2IVIU	1 iate	A30/	14	KII/J/	4		4		-49	770	2/0	U*7
60	2 ¹ / ₄ Ni	Plate	A203	В	K22103			9A	(12)(65)	-29	483	276	538
	3½Ni	Plate	A203	E	K22103 K32018			9A 9B	(12)(65)	-29 -29	483	276	538
0,7			00	-	1102010			,,,	(12)(00)		.55	_,0	230
	I												

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Hum	DCIS	111 1	ai cii	tilest													es (1)			other	wise i	Haica	ıcu	
	Min.						Jusic	7111011	ubic	ou co.	,, 0, 1.1	<i>1 u, u</i>	. meta	1 TCII	треги	ur c,	G [MO	.03 (1)	unu (10)]					
Line	Temp.																								
No.	to 40	65	100	125	150	175	200	225	250	275	300	325	350	375			450	475	500	525	550	575	600	625	650
36	149					140											64.4				14.2		6.89		
37	149	149	147	144	142	140	138	135	132	128	124	119	113	107	95.1	79.5	64.4	48.8	35.4	22.6	14.2	9.40	6.89		
38	149																					9.48			
39	149	149	147	144	142	140	138	135	132	128	124	119	113	107	95.1	79.5	64.4	48.8	35.4	22.6	14.2	9.48	7.96		
																						00			
40	149	149	149	148	145	143	140	138	137	135	133	131	129	126	123	120	117	109	68.0	42.3	30.5	23 2	16.5		
																					N)			
41	149														131			109		~	"	23.2			
42	149	149	149	149	149	149	148	146	144	142	140	138	136	133	131	127	124	109	68.0	42.3	30.5	23.2	16.5		
																			11-						
43	161	•••					•••																		
44	161					•••			•••				•••	•••		•••		. P		•••	•••				
45	161	1.11	161	161	1.61	1.11	161	150	150	154	150	140	1.47	111	1 4 1	120	124	100	60.0	40.0	20.5	22.2	465		
45	161																134				30.5		16.5		
46	161	101	101	101	101	101	101	130	136	154	132	149	147	144	141	130	134	109	00.0	42.3	30.5	23.2	16.5		
47	161	161	161	161	161	150	155	152	150	1/10	116	1/12	1/1	120	136	122	120	104	72 7	E2 0	262	25.2	176	122	8.27
48	161														156	• *		119				30.0			8.27
10	101	101	100	157	150	150	150	150	150	150	150	150	150	0	120	150	150	11,	00.1	01.0	11.0	30.0	17.7	12.0	0.27
49	172	172	172	172	172	172	172	170	168	165	163	161	158	155	152	148	144	109	68.0	423	30.5	23.2	165		
50													- 1		152			109				23.2			
50	1,2	1,2	1,2	172	1,2	172	1,2	170	100	100	105	101	2	155	152	110		107	00.0	12.0	50.5	25.2	10.0	•••	
51	195	195	195	195	195	195	195	195	194	193	192	190	187	183	178	172	165	156	147	137	115	87.0	64.7	45.1	29.6
52											X,	_			178			156				87.0			
											7														
53	207	207	205	202	200	199	199	199	198	198	196	194	191	187	182	176	169	80.6	61.7	46.4	34.7	25.5	17.8	11.4	6.89
54	207														182			160	87.5	61.2	42.9	29.9	20.6	14.4	10.3
									7																
55	230	230	230				'م	Ö.																	
56	230	230	230				٠, ڀ)																	
						7																			
57	126	126	126	126	126	126	126	126	126	126	125	123	121	119	116	114	110	107	74.4	49.9	40.7				
58	126	126	123	122	122	122	122	121	120	118	116	115	114	112	110	109	106	104	92.1	61.1	40.4	26.4	17.4	11.6	7.58
59	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	98.3	83.2	60.2	42.9	29.9	20.6	14.4	10.3
			2																						
60	138	138	138	138	138	138	136	134	131	129	127	125	123	121	119	116	113	104	73.7	52.0	36.3	25.2	17.6	12.3	8.27
61		13													110							25.5			6.89
62	138																					34.0			
63	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	99.6	80.9	63.3	47.5	34.2	23.5	15.3	9.65
64																		48.8					•••		
65	149	149	149	149	149	148	146	143	140	136	131	126	120	113	95.1	79.5	64.4	48.8	35.4	22.6	17.2				
	4.40	1.40	110	4.40	4.40	4.40	140	1.4		1.40	1.40	100	100	100	101	105	101	100		40.0	20.5	22.2	46 =		
66																	124					23.2			
67	149	149	146	144	144	144	144	144	144	143	141	139	138	136	134	132	129	126	92.1	01.1	40.4	26.4	1/.4	11.6	7.58
(0	161	161	161	161	161	160	150	155	151	147	142	127	120	112	05.4	705	: 64 4	40.0	25.4	22.6	170				
68 69																		48.8							
09	101	101	101	101	101	100	130	199	131	14/	147	130	130	144	101	03.0	, 00.6	47.4	33.4	22.0	17.2				

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

					FF		, - <u>F</u>		MISTRIC TISTIN		Min.	Min.	Max.
Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)	Notes	Min. Temp., °C (6)	Tensile Str., MPa	Yield Str., MPa	мах. Use Temp., °С
	¹ / ₂ Cr- ¹ / ₂ Mo	Plate	A387	2	K12143	2		3		-29	483	310	538
	$C-\frac{1}{2}Mo$	Plate	A204	В	K12020			3	(58)	-29	483	276	593
72	$Mn-\frac{1}{2}Mo$	Plate	A302	A	K12021			3		-29	517	310	538
73	C-1/2Mo	Plate	A204	С	K12320			3	(58)	-29	517	296	} 593
												0,	
	1½Cr-½Mo-Si	Plate	A387	11	K11789	2		4		-29	517 517	310	649
	5Cr-½Mo 3Cr-1Mo	Plate Plate	A387 A387	5 21	K41545	2 2		5B 5A		-29 -29	517	310 310	649 649
	$2\frac{1}{4}$ Cr-1Mo	Plate	A387	22	K31545 K21590	2		5A	 (72)		2517	310	649
,,	27401 1110	Tiate	11307	22	R21370	2	•••	311	(72)		9 17	310	047
78	$Mn-\frac{1}{2}Mo$	Plate	A302	В	K12022			3		-29	552	345	538
79	$Mn - \frac{1}{2}Mo - \frac{1}{2}Ni$	Plate	A302	С	K12039	•••		3		-29	552	345	538
80	$Mn^{-1}/_{2}Mo^{-3}/_{4}Ni$	Plate	A302	D	K12054			3	<u>ç</u>	-29	552	345	538
81	9Cr-1Mo-V	Plate	A387	91	K90901	2	≤75	15E	OOK	-29	586	414	649
82	8Ni	Plate	A553	II	K71340			11A	(47)	-171	689	586	40
83	5Ni- ¹ / ₄ Mo	Plate	A645	A	K41583			11A		-171	655	448	93
	9Ni	Plate	A553	I	K81340			11A	(47)	-196	689	586	93
85	9Ni	Plate	A353		K81340		0,10	11A	(47)	-196	689	517	93
06	C- ¹ / ₂ Mo	Γ 0 ft-	1224	M/D1	1/12021	1		2	(50)	-29	379	207	F02
00	C- /2IMO	Forg. & ftg.	A234	WP1	K12821	, KO	•••	3	(58)	-29	3/9	207	593
87	1Cr−½Mo	Forg. & ftg.	A182	F12	K11562	· C 1		4	(9)	-29	414	221	649
	1Cr−½Mo	Forg. & ftg.		WP12	K12062	1		4		-29	414	221	649
		0 0											
89	1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si	Forg. & ftg.	A182	F11	K11597	1		4	(9)	-29	414	207	649
90	$1\frac{1}{4}$ Cr $-\frac{1}{2}$ Mo $-$ Si	Forg. & ftg.	A234	WP11	K11597	1		4		-29	414	207	649
				C_{i}									
	2½Cr-1Mo	Forg. & ftg.		F22	K21590	1		5A	(9)(72)(75)	-29	414	207	649
92	21/4Cr-1Mo	Forg. & ftg.	A234	WP22	K21590	1		5A	(72)	-29	414	207	649
		\sim	11.										
93	5Cr- ¹ / ₂ Mo	Forg. & ftg.	A234	WP5	K41545			5B		-29	414	207	649
		1											
94	9Cr-1Mo	Forg. & ftg.	A234	WP9	K90941			5B		-29	414	207	649
	S	7.											
95	3½Ni	Forg. & ftg.	A420	WPL3	K31918			9B		-101	448	241	343
	· ·												
96	$3\frac{1}{2}Ni$	Forg. & ftg.	A350	LF3	K32025			9B	(9)	-101	483	259	343
	¹⁄₂Cr−¹⁄₂Mo	Forg. & ftg.	A182	F2	K12122	•••		3	(9)	-29	483	276	538
98	C-1/2Mo	Forg. & ftg.	A182	F1	K12822			3	(9)(58)	-29	483	276	593
	1Cr-½Mo	Forg. & ftg.		F12	K11564	2		4	(9)	-29	483	276	649
100	1Cr-½Mo	Forg. & ftg.	A234	WP12	K12062	2		4		-29	483	276	649

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	wuiii	DEI 3	шР	ai Eil	uiest												_	tes (1)			Juiel	W13C	mulca	ıcu	
	Min.								2010		, 0, 1,1	- w, ut			-pera		5 [110	-50 (1)		-~,]					
Line	Temp.	. -	400	40=	450	4	200	205	252	255	200	20=	252	255	400	40=	4=0	4	F 00	F0=				60 =	C.E.O.
No.	to 40															425		475	500		550	575	600	625	650
70	161									161					159		151	146			40.7	 23.2			
71	161	101	101	161	161	101	101	158	156	154	152	149	147	144	141	138	134	109	68.0	42.3	30.5	23.2	10.5		
72	172	172	172	172	172	172	172	172	172	172	172	172	171	160	165	160	154	104	68 N	123	33.1				
73																148		104				23.2	165		•••
73	172	1/2	1/2	1/2	1/2	1/2	1/2	170	100	105	103	101	130	133	132	140	111	107	00.0	12.5	30.3	23.2	10		
74	172	172	172	172	172	172	172	172	169	166	164	161	159	156	153	149	146	104	73.7	52.0	36.3	252	17.6	12.3	8.27
75	172												159				104						17.8		6.89
76	172												167				167				N .		20.6		8.96
77	172	172	171	168	167	167	167	167	167	167	167	167	167	167	167	167	167	119		~``	つ		19.7		8.27
																				/					
78	184	184	184	184	184	184	184	184	184	184	184	184	184	184	183	178	172	104	68.0	42.3	33.1				
79	184	184	184	184	184	184	184	184	184	184	184	184	184	184	183	178	172	104	68.0	42.3	33.1				
80	184	184	184	184	184	184	184	184	184	184	184	184	184	184	183	178	172	104	68.0	42.3	33.1				
																	, (5)							
81	195	195	195	195	195	195	195	195	194	193	192	190	187	183	178	172	165	156	147	137	115	87.0	64.7	45.1	29.6
																0)								
82	230															\ \									
83	218	218	218												$\langle O \rangle$										
														. ~0											
84	230	230	230											11.											
85	230	230	230										4												
												ii.	0												
86	126	126	126	126	124	122	120	119	117	115	114	112	110	108	106	103	100	97.1	68.0	42.3	30.5	23.2	16.5		
											` X														
87	138	129	124	120	117	115	112	110	109	107	106	105	103	102	100	98.7	96.8	94.6	92.0	61.1	40.4	26.4	17.4	11.6	7.58
88	138	138	132	128	125	122	120	118	116	114	113	112	110	109	107	105	103	101	92.1	61.1	40.4	26.4	17.4	11.6	7.58
89	138	131	126	124	121	119	116	115	113	111	109	107	106	104	102	99.6	97.2	94.5	73.7	52.0	36.3	25.2	17.6	12.3	8.27
90	138	131	126	124	121	119	116	115	113	111	109	107	106	104	102	99.6	97.2	94.5	73.7	52.0	36.3	25.2	17.6	12.3	8.27
							- (,																	
91	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	99.6	80.9	63.3	47.5	34.2	23.5	15.3	9.65
92	138	132	128	126	125	124	124	124	124	124	124	124	124	124	123	122	121	99.6	80.9	63.3	47.5	34.2	23.5	15.3	9.65
				_ <	U,																				
93	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	80.6	61.7	46.4	34.7	25.5	17.8	11.4	6.89
			1	O																					
94	138	129	124	122	120	119	119	118	118	117	117	116	114	112	110	106	103	98.3	87.5	61.2	42.9	29.9	20.6	14.4	10.3
		U.																							
0.5			4.45		4.40	4.40	100	405	400	400	404	440	440												
95	149	149	147	144	142	140	138	135	132	128	124	119	113												
96	161	160	157	155	152	150	148	145	142	137	133	128	122												
97	161	161	161	161	161	161	161	158	156	154	152	149	147	144	141	138	134	129	93.5	49.9	40.7				
98	161	161	161	161	161	161	161	158	156	154	152	149	147	144	141	138	134	109	68.0	42.3	30.5	23.2	16.5		
99	161	161	157	155	155	153	150	147	145	143	141	139	138	136	134	132	129	126	92.1	61.1	40.4	26.4	17.4	11.6	7.58
100																	129						17.4		7.58
·																									

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C
101	1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si	Forg. & ftg.	A182	F11	K11572	2		4	(9)	-29	483	276	649
102	1 ¹ / ₄ Cr- ¹ / ₂ Mo-Si	Forg. & ftg.	A234	WP11	K11572	2		4		-29	483	276	649
103	5Cr- ¹ / ₂ Mo	Forg. & ftg.	A182	F5	K41545		•••	5B	(9)	-29	483	276	649
104	3Cr-1Mo	Forg. & ftg.	A182	F21	K31545			5A	(9)	-29	517	310	649
105	2½Cr-1Mo	Forg. & ftg.	A182	F22	K21590	3		5A	(9)(72)	-29	517	310	649
106	2½Cr-1Mo	Forg. & ftg.	A234	WP22	K21590	3		5A	(72)	-29	517	310	649
										<	S ₂		
107	9Cr-1Mo	Forg. & ftg.	A182	F9	K90941			5B	(9)	-29	586	379	649
108	9Cr-1Mo-V	Forg. & ftg.	A182	F91	K90901		≤75	15E		-29	586	414	649
109	9Cr-1Mo-V	Forg. & ftg.	A234	WP91	K90901		≤75	15E	6	-29	586	414	649
110	5Cr−½Mo	Forg. & ftg.	A182	F5a	K42544			5B	(9)	-29	621	448	649
111	9Ni	Forg. & ftg.	A420	WPL8	K81340			11A	(47)	-196	689	517	93
									\sim				
112	C−½Mo	Castings	A352	LC1	J12522			3	(9)(58)	-59	448	241	371
113	C-½Mo	Castings	A217	WC1	J12524			3)	(9)(58)	-29	448	241	593
114	2½Ni	Castings	A352	LC2	J22500			O 9A	(9)	-73	483	276	343
115	3½Ni	Castings	A352	LC3	J31550		, X	9B	(9)	-101	483	276	343
							N						
116	1Ni-½Cr-½Mo	Castings	A217	WC4	J12082		(0	4	(9)	-29	483	276	538
117	3/4Ni-1Mo-3/4Cr	Castings	A217	WC5	J22000	" O"		4	(9)	-29	483	276	593
118	1½Cr-½Mo	Castings	A217	WC6	J12072			4	(9)	-29	483	276	649
119	2 ¹ / ₄ Cr–1Mo	Castings	A217	WC9	J21890	lick		5A	(9)	-29	483	276	649
120	5Cr−½Mo	Castings	A217	C5	J42045			5B	(9)	-29	621	414	649
121	9Cr-1Mo	Castings	A217	C12	182090			5B	(9)	-29	621	414	649
	ASI	KENOP!	MD	C12 C.									

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

-	Num	bers	III P	aren	tnese												_	tes (1)			Juner	wise	inuica	itea	
	Min.						Jusic		шыс	Ju C33	, 0, 1.1	1 4, 4	ricu	ı ıcıı	реги	iui c,	C [NO	(1)	unu (,					
Line	Temp.		400	40.	450	4	000		250		200		0.50		400	40=	450		=00					60 	C = 0
No.	to 40																	475		525	550	575	600	625	650
101	161											143						104			36.3			12.3	8.27
102	161	101	101	101	101	130	155	133	150	140	140	143	141	130	130	133	130	104	/3./	32.0	30.3	23.2	17.6	12.3	8.27
102	161	161	160	157	156	155	155	155	151	151	150	151	140	116	112	127	121	90.6	617	16.1	247	25.5	170	11.4	6.00
103	161	101	100	15/	130	155	133	155	154	134	155	151	149	140	142	137	151	00.0	01.7	40.4	34.7	25.5	17.8	11.4	6.89
104	172	172	172	160	160	167	166	166	165	165	161	161	162	161	150	155	152	00.2	72 5	E47	40.6	20.2	20.6	152	8.96
104	172	1/2	1/2	109	100	107	100	100	103	103	104	164	102	101	150	155	132	90.2	/3.3	34.7	40.0	292	20.0	15.2	0.90
105	172	172	171	160	167	167	167	167	167	167	167	167	167	167	167	167	167	119	00 1	64.0	112	30.0	19.7	12 0	8.27
103	172											167						119			N .		19.7		8.27
100	1/2	1/2	1/1	100	107	107	107	107	107	107	107	107	107	107	107	107	107	117	00.4	(2)	5 4.0	30.0	17.7	12.0	0.27
107	195	105	101	101	1.00	1 2 2	1 0 0	1 2 2	127	197	126	184	1Ω1	177	172	166	150	151	032	60.2	42 Q	20 0	20.6	14.4	10.3
108	195											190					165		. //				64.7		
109	195											190					165	156					64.7		
110	207																	80.6						11.4	6.89
111	230	230															,(3							
																	(
112	149	149	149	148	145	143	140	138	137	135	133	131	129	127		0)								
113	149	149	149	148	145	143	140	138	137	135	133	131	129	126	123	120	117	109	68.0	42.3	30.5	23.2	16.5		
															$\langle \mathcal{O} \rangle$										
114	161	161	161	161	161	160	158	155	151	147	142	136	131	2											
115	161	161	161	161	161	160	158	155	151	147	142	136	131												
													4												
116	161	161	161	161	161	161	161	161	159	158	156	154	152	149	146	142	137	131	74.4	49.9	40.7				
117	161	161	161	161	161	161	161	161	159	158	156	154	152	149	146	142	137	131	74.4	49.9	34.3	23.2	16.5		
118	161	161	161	161	161	158	155	153	150	148	146	143	141	138	136	133	130	104	73.7	52.0	36.3	25.2	17.6	12.3	8.27
119	161	161	160	157	156	156	156	156	156	156	156	156	156	156	156	156	156	119	88.4	64.0	44.6	30.0	19.7	12.8	8.27
120	207	207	205	202	200	199	199	199	198	198	196	194	191	187	182	176	169	80.6	61.7	46.4	34.7	25.5	17.8	11.4	6.89
121	207	207	205	202	200	199	199	199	198	198	196	194	191	187	182	176	169	160	83.2	60.2	42.9	29.9	20.6	14.4	10.3
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Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
1	18Cr-10Ni-Ti	Smls. pipe	A312	TP321	S32100		>10	8
2	18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100		>10	8
		PP						8
3	18Cr-8Ni	Tube	A213	TP304L	S30403		\sim 0'	8
4	18Cr-8Ni	Tube	A269	TP304L	S30403			8
5	18Cr-8Ni	Tube	A270	TP304L	S30403	,	 	8
6	18Cr-8Ni	Smls. & wld. pipe	A312	TP304L	S30403	ഹ് `		8
7	18Cr-8Ni	Wld. pipe	A358	304L	S30403			8
		• •				N		
8	16Cr-12Ni-2Mo	Tube	A213	TP316L	S31603			8
9	16Cr-12Ni-2Mo	Tube	A269	TP316L	S31603			8
10	16Cr-12Ni-2Mo	Tube	A270	TP316L	\$31603			8
11	16Cr-12Ni-2Mo	Smls. & wld. pipe	A312	TP316L	S31603			8
12	16Cr-12Ni-2Mo	Wld. pipe	A358	316L	S31603			8
13	16Cr-12Ni-2Mo-Ti	Tube	A213	TP316Ti	S31635			8
				60.				
14	18Cr-10Ni-Ti	Smls. pipe	A312 💉	TP321	S32100		>10	8
15	18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100		>10	8
16	18Cr-10Ni-Ti	Smls. pipe	A312	TP321H	S32109		>10	8
17	18Cr-10Ni-Ti	Smls. pipe	A376	TP321H	S32109		>10	8
		×O						
18	25Cr-12Ni	Pipe & tube	A451	СРН8	J93400			8
19	25Cr-20Ni	Pipe & tube	A451	CPK20	J94202			8
		Smls. pipe Pipe & tube Pipe & tube Tube						
20	11Cr-Ti	Tube	A268	TP409	S40900			7
21	18Cr-Ti	Tube	A268	TP430Ti	S43036			7
22	16Cr-14Ni-2Mo	Pipe & tube	A451	CPF10MC	J92971			8
23	16Cr-8Ni-2Mo	Pipe	A376	16-8-2H	S16800			8
		.00						
24	12Cr-Al	Tube	A268	TP405	S40500			7
25	13Cr	Tube	A268	TP410	S41000			6
26	17Cr	Tube	A268	TP430	S43000			7
27	18Cr-13Ni-3Mo	Smls. & wld. pipe	A312	TP317L	S31703			8
28	25Cr-20Ni	Smls. & wld. pipe	A312	TP310	S31009			8
29	25Cr-20Ni	Wld. pipe	A358	310S	S31008			8
30	25Cr-20Ni	Pipe	A409	TP310S	S31008			8
31	18Cr-10Ni-Ti	Smls. pipe	A312	TP321	S32100		≤10	8
32	18Cr-10Ni-Ti	Wld. pipe	A312	TP321	S32100			8
33	18Cr-10Ni-Ti	Wld. pipe	A358	321	S32100			8
34	18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100		≤10	8
35	18Cr-10Ni-Ti	Wld. pipe	A409	TP321	S32100			8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	umbers in rarentieses							owable				
								Ten	nperati	ıre,		
				Min.			°C [Notes (1), (3),	and (4	b)]	
Line		Min. Temp.,	Min. Tensile Strength,	Yield Strength,	Max. Use Temp.,	Min. Temp.						
No.	Notes	°C (6)	MPa	MPa	°C	to 40	65	100	125	150	175	200
1	(28)	-254	485	170	816	115	115	115	115	115	115	115
2	(28)(36)	-254	485	170	816	115	115	115	115	115	115	115
											- 1	b
3	(14)(36)	-254	483	172	816	115	115	115	115	115	114	110
4	(14)(36)	-254	483	172	816	115	115	115	115	115	114	110
5	(14)	-254	483	172	816	115	115	115	115	115.	114	110
6		-254	483	172	816	115	115	115	115	115	114	110
7	(36)	-254	483	172	816	115	115	115	115	115	114	110
								2	110			
	(14)(36)	-254	483	172	816	115	115	115	115	115	113	109
	(14)(36)	-254	483	172	816	115	115	115	115	115	113	109
	(14)	-254	483	172	816	115	115		115	115	113	109
11		-254	483	172	816	115	115	115	115	115	113	109
	(36)	-254	483	172	816	115	115	115	115	115	113	109
13	(30)	-254	517	207	816	138	138	138	138	138	138	134
1.4	(20)(20)	254	405	170	816	115	115	115	115	115	115	115
	(28)(30)	-254	485	170 170	816	115	115	115	115	115	115	115
	(28)(30)(36)	-254 -198	485 485	170	816	115 115	115	115	115 115	115 115	115 115	115 115
	(30) (30)(36)	-196 -198	485	170	816	115	115 115	115 115	115	115	115	115
17	(30)(30)	-190	403	×O	010	113	113	113	113	113	113	113
18	(26)(28)(35)	-198	448	193	816	129	129	129	129	127	125	124
	(12)(28)(35)(39)	-198	448	193	816	129	129	129	129	127	125	124
			Ċ									
20	(35)	-29	414	207	40	138						
	(35)(49)	-29	414	276	40	138						
	(28)	-198	483	207	40	138						
23	(26)(31)(35)	-198	517	207	40	138						
		0										
24	(35)	-29	414	207	538	138	138	138	137	135	134	133
	(35)	-29	414	207	649	138	138	138	137	135	134	133
26	(35)(49)	-29	414	241	649	138	138	138	137	135	134	133
27	cN	-198	517	207	454	138	138	138	138	138	136	131
	No.											
	(35)(39)	-198	517	207	816	138	138	138	138	138	138	138
	(28)(35)(36)	-198	517	207	816	138	138	138	138	138	138	138
30	(28)(31)(35)(36)	-198	517	207	816	138	138	138	138	138	138	138
	(28)	-254	515	205	816	138	138	138	138	138	138	138
	(28)	-254	515	205	816	138	138	138	138	138	138	138
	(28)(36)	-254	515	205	816	138	138	138	138	138	138	138
	(28)(36)	-254	515	205	816	138	138	138	138	138	138	138
35	(28)(36)	-254	515	205	816	138	138	138	138	138	138	138

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				Ва	sic Allow			a, at Meta), and (4	-	erature,			
Line													
No.	225	250	275	300	325	350	375	400	425	450	475	500	525
1	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
2	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
													_V&
3	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
4	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
5	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
6	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	3 5.6	83.7
7	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
											Chir		
8	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5
9	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5
10	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5
11	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5
12 13	106	103	100	98.1	96.1	94.3	92.6	90.9	89. 3	87.6	85.9	84.2	82.5
13	129	124	120	117	115	113	112	111	THO	109	108	107	106
14	115	112	109	106	104	102	100	99.00	97.0	96.3	95.3	94.4	93.6
15	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
16	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
17	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
							χO						
18	124	123	121	119	117	115	112	109	106	103	100	96.9	93.7
19	124	123	121	119	117	115	112	109	106	103	100	96.9	93.7
20					W.								
21					~Ö.`								
22				····	<u> </u>								
23				0									
				\mathcal{I}									
24	132	131	130	129	127	124	121	118	114	109	103	70.1	38.8
25	132	131	130	129	127	124	121	118	114	109	92.5	68.4	51.1
26	132	131	130	129	127	124	121	118	114	109	88.7	69.8	52.6
0.7	405		100	440	445	440		100	405	405	400		
27	127	S 123	120	118	115	113	111	109	107	105	103		
20	127	124	121	120	127	125	122	122	120	110	117	116	04.0
28 29	137 1	134 134	131	129	127	125 125	123	122	120 120	119	117 117	116	84.9 84.9
30	137	134	131	129	127		123	122		119		116	
30	13/	134	131	129	127	125	123	122	120	119	117	116	84.9
31	138	135	131	128	125	122	120	119	117	115	114	113	112
32	138	135	131	128	125	122	120	119	117	115	114	113	112
33	138	135	131	128	125	122	120	119	117	115	114	113	112
34	138	135	131	128	125	122	120	119	117	115	114	113	112
35	138	135	131	128	125	122	120	119	117	115	114	113	112

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

		1 41 611 6			Allowable	Stress, S, M	IPa, at Me	tal Tempei		- SE COMOI V		
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
1	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
2	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
3	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
4	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
5	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
6	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
7	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
8	80.8	79.3	77.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
9	80.8	79.3	77.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
10	80.8	79.3	77.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
11	80.8	79.3	77.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
12	80.8	73.0	67.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
13	106	101	80.3	65.5	50.4	38.6	29.6	23.0	17.7	13.4	10.4	8.05
14	92.7	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
15	92.7	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
16	92.7	76.5	58.7	46.0	36.8	287	23.0	18.4	14.5	11.5	9.02	6.83
17	92.7	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
18	68.1	53.5	42.1	33.2	25.9	20.3	16 5	12.2	10.1	7.35	5.89	5.52
19	73.2	64.4	56.5	49.0	41.0	33.5	16.5 25.4	13.2 18.3	12.8	9.01	6.59	5.52
	73.2	04.4	30.3	45.0	· Carro	33.3	23.4	10.3	12.0	9.01	0.39	3.32
20				O.M.								
21				\mathcal{O}		•••					•••	
22			C)			•••					•••	
23			NOO									
24	27.6	26.2	47.0			•••					•••	
25	37.4	26.3	17.8	11.4	6.89	•••					•••	
26	38.1	() ·	20.6	15.9	12.4		•••					•••
27	RSI	•			•••		•••					•••
28	59.0	43.5	31.9	23.6	16.9	10.7	6.10	3.90	2.99	2.36	1.73	1.38
29	59.0	43.5	31.9	23.6	16.9	10.7	6.10	3.90	2.99	2.36	1.73	1.38
30	59.0	43.5	31.9	23.6	16.9	10.7	6.10	3.90	2.99	2.36	1.73	1.38
31	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
32	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
33	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
34	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
35	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line			Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Nominal Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
36	23Cr-12Ni	Smls. & wld. pipe	A312	TP309				8
37	23Cr-12Ni	Wld. pipe	A358	309S	S30908			8
								b
38	18Cr-8Ni	Pipe & tube	A451	CPF8	J92600		00	8
20	100 - 10N: Ch	Cula 0 11 dia	4242	TD2.47	624700	, C) (0
	18Cr-10Ni-Cb	Smls. & wld. pipe	A312	TP347	S34700 S34700			8
	18Cr-10Ni-Cb	Wld. pipe	A358	347		. & ³		8
	18Cr-10Ni-Cb	Pipe	A376	TP347	S34700			8
	18Cr-10Ni-Cb	Pipe	A409	TP347	S34700	4		8
	18Cr-10Ni-Cb 18Cr-10Ni-Cb	Smls. & wld. pipe Wld. pipe	A312 A358	TP348 348	S34800 S34800			8
					\$34800			8
	18Cr-10Ni-Cb	Pipe	A376	TP348	S34800 S34800			8
46	18Cr-10Ni-Cb	Pipe	A409	TP348	334800			8
47	25Cr-12Ni	Pipe & tube	A451	СРН10	J93402			8
	25Cr-12Ni	Pipe & tube	A451	CPH20	J93402			8
10	2301 12111	Tipe & tube	11131	0) 33 TO Z	•••		O
49	25Cr-20Ni	Smls. & wld. pipe	A312	TP310H	S31009			8
	25Cr-20Ni	Wld_nine	A358	310S	S31008			8
		- Company	110.					
51	18Cr-10Ni-Cb	Pipe & tube	A451	CPF8C	J92710			8
		X			,			
52	18Cr-10Ni-Ti	Pipe & tube Smls. pipe Wld. pipe	A312	TP321	S32100		≤10	8
53	18Cr-10Ni-Ti	Wld. pipe	A312	TP321	S32100			8
54	18Cr-10Ni-Ti	Wld. pipe	A358	321	S32100			8
55	18Cr-10Ni-Ti	Smls. pipe	A376	TP321	S32100		≤10	8
56	18Cr-10Ni-Ti	Wld. pipe	A409	TP321	S32100			8
57	18Cr-10Ni-Ti	Smls. pipe	A312	TP321H	S32109		≤10	8
58	18Cr-10Ni-Ti	Wld. pipe	A312	TP321H	S32109			8
59	18Cr-10Ni-Ti	Wld. pipe	A358	321H	S32109			8
60	18Cr-10Ni-Ti	Smls. pipe	A376	TP321H	S32109		≤10	8
	.20							
61	16Cr-12Ni-2M6	Tube	A213	TP316	S31600			8
62	16Cr-12Ni-2Mo	Tube	A269	TP316	S31600			8
63	16Cr-12Ni-2Mo	Tube	A270	TP316	S31600			8
	\							
64	16Cr-12Ni-2Mo	Smls. & wld. pipe	A312	TP316	S31600			8
65	16Cr-12Ni-2Mo	Wld. pipe	A358	316	S31600			8
66	16Cr-12Ni-2Mo	Pipe	A376	TP316	S31600			8
67	16Cr-12Ni-2Mo	Pipe	A409	TP316	S31600			8
68	18Cr-13Ni-3Mo	Smls. & wld. pipe	A312	TP317	S31700			8
69	18Cr-13Ni-3Mo	Pipe	A409	TP317	S31700			8
70	16Cr-12Ni-2Mo	Pipe	A376	TP316H	S31609			8
71	16Cr-12Ni-2Mo	Smls. & wld. pipe	A312	TP316H	S31609			8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

- N	umbers in Parentheses	s keier to	Notes for App	enaix A Ta	Dies; Specii		s Are AS asic Allo					
						Ва	isic Allo		stress, mperati		at met	al
				Min.			°C [(1), (3),	-	b)]	
		Min.	Min. Tensile	Yield	Max. Use	Min.						
Line No.	Notes	Temp., °C (6)	Strength, MPa	Strength, MPa	Temp., °C	Temp. to 40	65	100	125	150	175	200
	(28)(35)(39)	-198	517	207	816	138	138	138	138	138	138	138
37	(28)(31)(35)(36)	-198	517	207	816	138	138	138	138	138	138	138
37	(20)(31)(33)(30)	-190	317	207	010	130	130	130	130	130	130	h
38	(26)(28)	-254	483	207	816	138	138	138	138	138	134	129
30	(20)(20)	231	105	207	010	150	130	150	150	130	T	12)
39		-254	517	207	816	138	138	138	138	138	138	138
40	(30)(36)	-254	517	207	816	138	138	138	138	138	138	138
	(30)(36)	-254	517	207	816	138	138	138	138	138	138	138
	(30)(36)	-254	517	207	816	138	138	138	138	138	138	138
43		-198	517	207	816	138	138	138	138	138	138	138
44	(30)(36)	-198	517	207	816	138	138 💪	138	138	138	138	138
45	(30)(36)	-198	517	207	816	138	1380	138	138	138	138	138
46	(30)(36)	-198	517	207	816	138	138	138	138	138	138	138
						0	V					
47	(12)(14)(28)(35)(39)	-198	483	207	816	138	138	138	138	137	135	134
48	(12)(14)(28)(35)(39)	-198	483	207	816	138	138	138	138	137	135	134
					"VO							
49	(29)(35)(39)	-198	517	207	816	138	138	138	138	138	138	138
50	(28)(29)(35)(36)	-198	517	207	816	138	138	138	138	138	138	138
				~ 7.								
51	(28)	-198	483	207	816	138	138	138	138	138	134	129
				C/F								
	(28)(30)	-254	515	205	816	138	138	138	138	138	138	138
	(28)(30)	-254	515	205	816	138	138	138	138	138	138	138
	(28)(30)(36)	-254	515	205	816	138	138	138	138	138	138	138
	(28)(30)(36)	-254	515	205	816	138	138	138	138	138	138	138
	(28)(30)(36)	-254	515	205	816	138	138	138	138	138	138	138
	(30)	-198	515	205	816	138	138	138	138	138	138	138
	(30)	198	515	205	816	138	138	138	138	138	138	138
	(30)(36)	-198	515	205	816	138	138	138	138	138	138	138
60	(30)(36)	-198	515	205	816	138	138	138	138	138	138	138
61	(14)(26)(28)(31)(36)	-254	517	207	016	138	120	120	138	138	120	134
	(14)(26)(28)(31)(36)	-254 -254	517	207	816 816	138	138 138	138 138	138	138	138 138	134
	(14)(26)(28)	-254 -254	517	207	816	138	138	138	138	138	138	134
03	(14)(20)(20)	-234	317	207	010	130	130	130	130	130	130	134
64	(26)(28)	-254	517	207	816	138	138	138	138	138	138	134
	(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	138	134
	(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	138	134
	(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	138	134
	(26)(28)	-198	517	207	816	138	138	138	138	138	138	134
	(26)(28)(31)(36)	-198	517	207	816	138	138	138	138	138	138	134
	(26)(31)(36)	-198	517	207	816	138	138	138	138	138	138	134
71	(26)	-198	517	207	816	138	138	138	138	138	138	134
Į.												

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				Ва	sic Allow			a, at Met B), and (4	al Tempe	erature,			
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
36	138	135	133	131	129	127	125	124	122	121	119	117	108
37	138	135	133	131	129	127	125	124	122	121	119	117	108
38	125	122	119	116	113	111	109	107	105	103	101	99.1	94.4
39	138	138	137	135	132	130	128	127	126	126	125	125.	125
40	138	138	137	135	132	130	128	127	126	126	125	125	125
41	138	138	137	135	132	130	128	127	126	126	125	125	125
42	138	138	137	135	132	130	128	127	126	126	125	125	125
43	138	138	137	135	132	130	128	127	126	126	C ₁₂₅	125	125
44	138	138	137	135	132	130	128	127	126	126	125	125	125
45	138	138	137	135	132	130	128	127	126	126	125	125	125
46	138	138	137	135	132	130	128	127	126	126	125	125	125
47	133	131	129	128	125	123	120	117	114	111	107	104	100
48	133	131	129	128	125	123	120	117	114	111	107	104	100
49	137	134	131	129	127	125	123	122	120	119	117	116	108
50	137	134	131	129	127	125	123	122	120	119	117	116	108
30	137	134	131	129	127	123	123	122	120	117	117	110	100
51	125	122	119	116	113	111	1 09	107	105	103	101	99.1	97.3
52	138	135	131	128	125	122	120	119	117	115	114	113	112
53	138	135	131	128	125	122	120	119	117	115	114	113	112
54	138	135	131	128	125	122	120	119	117	115	114	113	112
55	138	135	131	128	125	122	120	119	117	115	114	113	112
56	138	135	131	128	125	122	120	119	117	115	114	113	112
57	138	135	131	128	125	122	120	119	117	115	114	113	112
58	138	135	131	128	125	122	120	119	117	115	114	113	112
59	138	135	131	128	125	122	120	119	117	115	114	113	112
60	138	135	131	128	125	122	120	119	117	115	114	113	112
61	129	125	122	119	116	114	112	111	110	109	108	107	106
62	129	125	122	119	116	114	112	111	110	109	108	107	106
63	129	125	122	119	116	114	112	111	110	109	108	107	106
64	129	125	122	119	116	114	112	111	110	109	108	107	106
65	129	125	122	119	116	114	112	111	110	109	108	107	106
66	129	125	122	119	116	114	112	111	110	109	108	107	106
67	129	125	122	119	116	114	112	111	110	109	108	107	106
68	129	125	122	119	116	114	112	111	110	109	108	107	106
69	129	125	122	119	116	114	112	111	110	109	108	107	106
70	129	125	122	119	116	114	112	111	110	109	108	107	106
71	129	125	122	119	116	114	112	111	110	109	108	107	106

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				Basic .		Stress, S, N		tal Temper	ature,			
					<u> </u>	itotes (1),	(S), and (
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
36	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
37	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
											8	
38	75.3	60.4	49.0	40.1	32.8	27.2	23.4	19.6	16.8	14.7	12.8	11.7
39	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
40	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
41	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
42	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
43	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
44	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4 💃	8.97	7.08	5.89	5.52
45	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
46	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
47	68.1	53.5	42.1	33.2	25.9	20.3	16.5	13.2	10.1	7.35	5.89	5.52
48	68.1	53.5	42.1	33.2	25.9	20.3	16.5	13.2	10.1	7.35	5.89	5.52
49	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
50	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
30	03.7	04.0	40.5	30.3	27.3	1/6	13.7	12.3	7.07	7.03	3.77	3.17
51	95.5	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
52	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
53	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
54	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
55	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
56	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
57	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
58	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
59	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
60	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
61	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
62	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
63	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
64	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
65	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
66	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
67	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
68	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
69	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
70	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
71	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line			Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Nominal Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
72	18Cr-10Ni-Cb	Pipe	A376	TP347H	S34709			8
73	18Cr-10Ni-Cb	Smls. & wld. pipe	A312	TP347	S34700			8
74	18Cr-10Ni-Cb	Wld. pipe	A358	347	S34700		O_{Ω}	8
75	18Cr-10Ni-Cb	Pipe	A376	TP347	S34700	(L.V	8
76	18Cr-10Ni-Cb	Pipe	A409	TP347	S34700		J	8
77	18Cr-10Ni-Cb	Smls. & wld. pipe	A312	TP348	S34800	85°5		8
	18Cr-10Ni-Cb	Wld. pipe	A358	348	S34800	\(\frac{1}{2}\)		8
79	18Cr-10Ni-Cb	Pipe	A376	TP348	S34800	W.		8
80	18Cr-10Ni-Cb	Pipe	A409	TP348	S34800			8
					& P			
81	18Cr-10Ni-Cb	Smls. & wld. pipe	A312	TP347H	\$34709			8
82	18Cr-10Ni-Cb	Smls. & wld. pipe	A312	TP348H	S34809			8
	18Cr-8Ni	Tube	A213	TP304	S30400			8
	18Cr-8Ni	Tube	A269	TP304	S30400			8
	18Cr-8Ni	Tube	A270	FP304	S30400			8
	18Cr-8Ni	Smls. & wld. pipe	A312	TP304	S30400			8
	18Cr-8Ni	Wld. pipe	A358	304	S30400			8
	18Cr-8Ni	Pipe	A376	TP304	S30400			8
	18Cr-8Ni	Pipe	A376	TP304H	S30409			8
	18Cr-8Ni	Pipe	A409	TP304	S30400			8
	18Cr-8Ni	Smls. & wld. pipe	A312	TP304H	S30409			8
92	18Cr-12Ni-2Mo	Pipe & tube	A451	CPF8M	J92900			8
93	44Fe-25Ni-21Cr-Mo	Wld. tube	A249		N08904			45
94	44Fe-25Ni-21Cr-Mo	Smls. & wld. pipe	A312		N08904			45
95	20Cr-Cu	Tube	A268	TP443	S44300			a
96	27Cr	Tube	A268	TP446-1	S44600			10I
		•						
97	12Cr	Wld. pipe	A1053	50	S41003			7
98	25Cr-8Ni-N	Pipe & tube	A451	CPE20N	J92802			8
	CM.							
99	23Cr-4Ni-Mo-Cu-N	Smls. & wld. tube	A789		S32304			10H
100	23Cr-4Ni-Mo-Cu-N	Smls. & wld. pipe	A790		S32304			10H
101	23Cr-4Ni-Mo-Cu-N	Pipe & tube	A928	2304	S32304			10H
102	20Cr-18Ni-6Mo	Pipe & tube	A813		S31254			8
103	20Cr-18Ni-6Mo	Pipe & tube	A814		S31254			8
104	13Cr	Pipe & tube	A426	CPCA15	J91150			6
	20Cr-18Ni-6Mo	Wld. pipe	A358		S31254		>5.0	8
106	20Cr-18Ni-6Mo	Wld. pipe	A358		S31254		≤5.0	8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

					bles; Specif			owable	-	S, MPa,	at Met	al
							۰c		nperati	ıre, and <mark>(4</mark>	h)]	
Line		Min. Temp.,	Min. Tensile Strength,	Min. Yield Strength,	Max. Use Temp.,	Min. Temp.		[Notes	<u>(1), (3),</u>	anu (4	<u> </u>	
No.	Notes	°C (6)	MPa	MPa	°C	to 40	65	100	125	150	175	200
72	(30)(36)	-198	517	207	816	138	138	138	138	138	138	138
	(28)	-254	517	207	816	138	138	138	138	138	138	
	(28)(30)(36)	-254	517	207	816	138	138	138	138	138	138	138
	(28)(30)(36)	-254	517	207	816	138	138	138	138	138	138	138
	(28)(30)(36)	-254	517	207	816	138	138	138	138	138	138	138
	(28)	-198	517	207	816	138	138	138	138	138	138	138
	(28)(30)(36)	-198	517	207	816	138	138	138	138	138	138	138
	(28)(30)(36)	-198	517	207	816	138	138	138	138	138	138	138
	(28)(30)(36)	-198	517	207	816	138	138	138	138	138	138	138
00	(20)(30)(30)	-170	317	207	010	130	130		130	130	130	130
81		-198	517	207	816	138	138	138	138	138	138	138
82		-198	517	207	816	138	138	138	138	138	138	138
						Q'	V					
83	(14)(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	134	129
84	(14)(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	134	129
85	(14)(26)(28)	-254	517	207	816	138	138	138	138	138	134	129
86	(26)(28)	-254	517	207	816	138	138	138	138	138	134	129
87	(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	134	129
88	(20)(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	134	129
89	(26)(31)(36)	-198	517	207	816	138	138	138	138	138	134	129
90	(26)(28)(31)(36)	-254	517	207	816	138	138	138	138	138	134	129
	(26)	-198	517	207	816	138	138	138	138	138	134	129
92	(26)(28)	-254	483	207	816	138	138	138	138	130	124	118
93	(26)	-198	490	220	260	143	143	143	143	141	135	130
94	(26)	-198	490	220	260	143	143	143	143	141	135	130
0.5	(7)(25)	200	402	276	5 20	161	161	161	1.61	161	161	1.61
0.0	(7)(35)	-29 -29	483	276	538	161	161	161	161	161	161	161
96	(35) (35)(39)	-29	483	276	538	161	161	161	158	155	153	152
97		-29	485	350	316	162	162	162	162	162	161	159
98	(35)(39)	-198	552	276	482	184	184	184	184	184	184	184
	Chil											
99	(25)	-51	600	400	316	200	200	191	185	180	175	171
100	(25)	-51	600	400	316	200	200	191	185	180	175	171
101	(25)	-51	600	400	316	200	200	191	185	180	175	171
102	(8)	-198	650	300	454	202	202	202	202	199	192	185
103		-198	650	300	454	202	202	202	202	199	192	185
10.	(10)(25)	20	(04	440	40	207						
104	(10)(35)	-29	621	448	40	207			•••	•••		
105		-198	655	310	475	207	207	207	207	203	196	189
106		-198	690	310	475	207	207	207	207	203	196	189

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]												
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
72	138	138	137	135	132	130	129	127	126	126	125	125	125
73	138	138	137	135	132	130	129	127	126	126	125	125	125
74	138	138	137	135	132	130	128	127	126	126	125	125	125
75	138	138	137	135	132	130	128	127	126	126	125	125	125
76	138	138	137	135	132	130	128	127	126	126	125	125.	125
77	138	138	137	135	132	130	128	127	126	126	125	1 25	125
78	138	138	137	135	132	130	128	127	126	126	125	125	125
79	138	138	137	135	132	130	128	127	126	126	125	125	125
80	138	138	137	135	132	130	128	127	126	126	125	125	125
										﴿ بِي	~		
81	138	138	137	135	132	130	129	127	126	126	125	125	125
82	138	138	137	135	132	130	129	127	126	126	125	125	125
									_,(Υ)	~			
83	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
84	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
85	125	122	119	116	113	111	109	107		103	101	99.1	97.3
86	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
87	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
88	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
89	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
90	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
91	125	122	119	116	113	(1)(1	109	107	105	103	101	99.1	97.3
92	114	110	107	104	102	101	99.3	98.1	97.0	95.9	94.7	93.3	91.5
0.0	405	100	44.5		Oh,								
93	125	120	116	(
94	125	120	116	_()									
05	161	161	161	\sim	161	07.0	04.2	5 0.0	64.0	55.0	42.0	24.5	24.4
95	161	161	161	161	161	97.0	84.3	73.3	64.0	55.8	43.9	31.7	21.4
96	150	149	147	145	144	141	139	136	132	128	122	116	109
0.7	150	154	O_{r_2}	140	146								
97	156 184	154 184	152	149	146								
98	184	184	184	184	184	184	184	184	184	184	184	184	
99	166	5 161	153	143	111								
	Y	*										•••	
100	166	161	153	143	111								
101	166	161	153	143	111								
102	180	175	171	168	165	164	162	161	160	159	158		
103	180	175	171	168	165	164	162	161	160	159	158		
103	100	1/3	1/1	100	103	101	102	101	100	10)	130	•••	
104												•••	
	**									-			
105	184	179	175	172	169	167	165	165	164	163	161		
106	184	179	175	172	169	167	165	165	164	163	161		
1	-	-	-			-			-		•		

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]											
-												
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
72	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
73	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
74	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
75	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
76	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
77	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	146	10.9	8.96
78	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8 /	14.6	10.9	8.96
79	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
80	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18,8	14.6	10.9	8.96
81	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
82	125	112	90.6	69.6	53.8	41.4 41.4	31.8	24.0	18.8	14.6	10.9	8.96
02	125	112	90.0	09.0	33.0	41.4	31.0	24:0	10.0	14.0	10.9	0.90
83	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
84	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
85	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
86	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
87	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
88	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
89	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
90	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
91	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
92	89.1	72.7	57.7	46.0	36.9	30.1	24.3	20.3	17.0	14.3	12.1	11.0
				ON								
93				$C_{i}^{O_{i}}$								
94			C						•••			
95	17.2											
96	104	05										
0.7		,0/										
97		EN							•••			
98			•••					•••	•••	•••	•••	
99	S,											
100	Y											
101												
102												
103						•••		•••	•••	•••	•••	
104												
105												
106		•••	•••	•••								
100												

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						Class/		
Line			Spec.	Type/		Condition/	Size,	P-No.
No.	Nominal Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
107	22Cr-5Ni-3Mo-N	Smls. & wld. tube	A789		S31803			10H
	22Cr-5Ni-3Mo-N	Smls. & wld. pipe	A790		S31803			2 0Н
	22Cr-5Ni-3Mo-N	Pipe & tube	A928		S31803			10H
		•					~~~	
110	20Cr-18Ni-6Mo	Pipe & tube	A249		S31254	,	>5.00	8
111	20Cr-18Ni-6Mo	Pipe & tube	A249		S31254	~?)`	≤5.00	8
112	20Cr-18Ni-6Mo	Pipe & tube	A312		S31254	\(\lambda_{}\)	>5.00	8
113	20Cr-18Ni-6Mo	Pipe & tube	A312		S31254		≤5.00	8
					C			
114	26Cr-4Ni-Mo	Smls. & wld. tube	A789		S32900			10H
115	26Cr-4Ni-Mo	Smls. & wld. pipe	A790		\$32900			10H
					X			
116	46Fe-24Ni-21Cr-6Mo-	Smls. & wld. pipe	A312	(Q\	N08367		>5.0	45
445	Cu-N	TATE I	4050	1111	NOOOG		5 0	4.5
11/	46Fe-24Ni-21Cr-6Mo- Cu-N	Wld. pipe	A358	X	N08367		>5.0	45
118	46Fe-24Ni-21Cr-6Mo-	Wld. pipe	A813		N08367		>5.0	45
	Cu-N	• •	<i>a</i> .					
119	46Fe-24Ni-21Cr-6Mo-	Wld. pipe	A814		N08367		>5.0	45
	Cu-N		7					
120	46Fe-24Ni-21Cr-6Mo- Cu-N	Smls. & wld. pipe	A312		N08367		≤5.0	45
121	46Fe-24Ni-21Cr-6Mo-	Smls. & wld. pipe Wld. pipe	A358		N08367		≤5.0	45
121	Cu-N	wid. pipe	A330		1400307		33.0	43
122	46Fe-24Ni-21Cr-6Mo-	Wld. pipe	A813		N08367		≤5.0	45
	Cu-N	Oly						
123	46Fe-24Ni-21Cr-6Mo-	Wld. pipe	A814		N08367		≤5.0	45
	Cu–N	℃ .						
124	21Cr-5Mn-1½Ni-Cu-N	Smls. & wld. tube	A789		S32101		>5.0	10H
	21Cr-5Mn-1½Ni-Cu-N	Smls. & wld. tube	A790		S32101 S32101		>5.0	10H
	24Cr-4Ni-3Mn-1.5Mo-N	Smls. & wld. pipe	A789		S82441		≥10.0	10H
	24Cr-4Ni-3Mn-1.5Mo-N	Smls. & wld. tube	A790		S82441		≥10.0	10H
	21Cr-5Mn-1 ¹ / ₂ Ni-Cu-N	Smls. & wld. tube	A789		S32101		≤5.0	10H
	21Cr-5Mn-1 ½Ni-Cu-N	Smls. & wld. pipe	A790		S32101		≤5.0	10H
	N. T.	Siller to with paper						
130	21Cr-3½Ni-1¾Mo-N	Smls. & wld. tube	A789		S32003		>5.00	10H
	21Cr-3½Ni-1¾Mo-N	Smls. & wld. pipe	A790		S32003		>5.00	10H
	21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N	Pipe & tube	A928		S32003		>5.00	10H
	22Cr-5Ni-3Mo-N	Pipe & tube	A928	2205	S32205			10H
134	21Cr-3½Ni-1¾Mo-N	Smls. & wld. tube	A789		S32003		≤5.00	10H
	21Cr-3½Ni-1¾Mo-N	Smls. & wld. pipe	A790		S32003		≤5.00	10H
136	21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N	Pipe & tube	A928		S32003		≤5.00	10H
137	24Cr-4Ni-3Mn-1.5Mo-N	Smls. & wld. tube	A789		S82441		<10.0	10H
138	24Cr-4Ni-3Mn-1.5Mo-N	Smls. & wld. pipe	A790		S82441		<10.0	10H

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

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137 (25)

138 (25)

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]												
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
													_
107	190	188	187	186	185								
108	190	188	187	186	185								~ V.50
109	190	188	187	186	185								<i>O</i>
110	184	179	175	172	169	167	166	165	164	163	161	رث _ر ک	
111	184	179	175	172	169	167	166	165	164	163	161	0	
111	184	179	175	172	169	167	166	165	164	163	161	₹ ³	
											NY/	•••	
113	184	179	175	172	169	167	166	165	164	163	161		
114										7 ي	٠		
115										. 0			
110										<	•••		
116	195	192	188	184	179	176	173	170	167	166			
117	195	192	188	184	179	176	173	170	167	166			
118	195	192	188	184	179	176	173	170	167	166			
119	195	192	188	184	179	176	173	170	167	166			
120	199	194	188	184	179	176	773	170	167	166			
121	199	194	188	184	179	Q,400,	173	170	167	166			
122	199	194	188	184	179	• 176	173	170	167	166			
123	199	194	188	184	179	176	173	170	167	166			
				20	•								
124	199	199	199	199	199								
125	199	199	199	199	199								
126	227	227	227	227	227								
127	227	227	227	227	227								
128	214	214	214	214	214								
129	214	214	214	214	214		•••						
130	197	197	197	197	197	197							
131	197	197	197	197	197	197	•••		•••	•••	•••	•••	
131	197 197	197 197	197 197	197 197	197 197								
						197 105							
133	201	199	197	196	196	195					•••		
134	207	207	207	207	207	207							
135	207	207	207	207	207	207							
136	207	207	207	207	207	207					•••		•••
137	247	247	247	247	247								
138	247	247	247	247	247		•••			•••		•••	•••
130	41/	47/	47/	411	471			•••					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]											
Line				.	6 2 0							
No.	550	575	600	625	650	675	700	725	750	775	800	825
107												
108											.8	
109											20/10	
110										. V.		
111										000		
112										, `		
113									CM.			
114									No.			
115								Č				•••
113								~				
116								80				
117							ike full					
118							Me.					
119						Jien,						
120					X							
121					Cijio							
122				ON	•							
123			 _()	Ċ.								
124			200									
125			Ur.									
126												
127												
128		/										
129	SN											
130												
131												
132												
133			•••									
134												
135												
136											•••	
137												
138												

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
120	25Cr-8Ni-3Mo-W-Cu-N	Smls. & wld. tube	A789		S32760			10H
	25Cr-8Ni-3Mo-W-Cu-N	Smls. & wld. tube	A790		S32760			1 011
110		omor ca vital pipe	11, 50		002700		~O^	3011
141	29Cr-6.5Ni-2Mo-N	Smls. & wld. tube	A789		S32906		≥10	10H
142	29Cr-6.5Ni-2Mo-N	Smls. & wld. pipe	A790		S32906		•≥10	10H
						<i>∞</i> , 2000.		
143	24 Cr -17 Ni -6 Mn $-4\frac{1}{2}$ Mo $-$ N	Pipe & tube	A358		S34565			8
	25Cr-7Ni-4Mo-N	Smls. & wld. tube	A789		S32750	W.		10H
145	25Cr-7Ni-4Mo-N	Smls. & wld. pipe	A790	2507	S32750			10H
146	25Cr-7Ni-4Mo-N	Pipe & tube	A928	2507	S32750			10H
					, O,			
	29Cr-6.5Ni-2Mo-N	Smls. & wld. tube	A789	0	S32906		<10	10H
148	29Cr-6.5Ni-2Mo-N	Smls. & wld. pipe	A790		S32906		<10	10H
				1/1/13				
	18Cr-11Ni	Plate & sheet	A240	305	S30500			8
150	12Cr–Al	Plate & sheet	A240	405	S40500			7
4-4	100 000		· her	22.4	200.400			
151	18Cr-8Ni	Plate & sheet	A240	304L	S30403			8
152	16Cr-12Ni-2Mo	Plate & sheet Plate & sheet	A240	316L	S31603			8
132	1001-12141-21410	Trace & sirect	AZ-TO	310L	331003			U
153	18Cr-Ti	Plate & sheet	A240	439	S43035			
		, 0,						
154	18Cr-8Ni	Plate & sheet	A240	302	S30200			8
		COV.						
155	12Cr-1Ni	Plate, sheet, strip	A1010	40	S41003			7
156	12Cr-1Ni	Plate, sheet, strip	A1010	50	S41003			7
		•0						
157	13Cr	Plate & sheet	A240	410S	S41008			7
158	13Cr	Plate & sheet	A240	410	S41000			6
	15Cr	Plate & sheet	A240	429	S42900			6
160	17Cr	Plate & sheet	A240	430	S43000			7
	CW.							
161	18Cr-13Ni-3Mo	Plate & sheet	A240	317L	S31703			8
	,							
162	25Cr-20Ni	Plate & sheet	A240	310S	S31008			8
162	10Cm 10N; T;	Dlata about atrin	A240	221	C22100			8
103	18Cr-10Ni-Ti	Plate, sheet, strip	A240	321	S32100			O
164	23Cr-12Ni	Plate & sheet	A240	309S	S30908			8
101	2001 12111	The de shoet	11210	3075	330700			J
165	18Cr-10Ni-Cb	Plate & sheet	A240	347	S34700			8
	18Cr-10Ni-Cb	Plate & sheet	A240	348	S34800			8
	-							

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

N	umbers in Parentheses	s keier to	notes for App	enaix A Ta	bies; Specii							
						Ďζ	isit All	owable Ter	stress, nperati		at met	aı
				Min.			°C	[Notes (-	-	b)]	
		Min.	Min. Tensile	Yield	Max. Use	Min.						
Line No.	Notes	Temp., °C (6)	Strength, MPa	Strength, MPa	Temp., °C	Temp. to 40	65	100	125	150	175	200
139	(25)	-51	750	550	316	250	250	248	243	238	236	234
140	(25)	-51	750	550	316	250	250	248	243	238	236) 234
											oo'	
	(25)	-51	750	550	316	251	251	249	243	238	235	231
142	(25)	-51	750	550	316	251	251	249	243	238	235	231
4.40	(0.0)	400	505		405	0.4	0.4	260	~~)	0.40	200
	(36)	-198	795	415	427	264	264	260	253 257	247	242	238
	(25)	-51 -51	800 800	550 550	316 316	267 267	265 265	264 264	257	251 251	247 247	243
	(25) (25)	-51 -51	800	550	316	267 267	265 (264	257 257	251 251	247 247	243 243
140	(23)	31	000	JJ2	310	207	200	207	23/	4 J1	41/	47J
147	(25)	-51	800	650	316	267	267	265	259	253	250	246
	(25)	-51	800	650	316	267	267	265	259	253	250	246
						111						
149	(26)(36)(39)	-198	483	172	40	115						
150	(35)	-29	414	172	538	115	109	105	103	102	101	100
					N							
151	(36)	-254	483	172	816	115	115	115	115	115	114	110
152	(36)	-254	483	172	816	115	115	115	115	115	113	109
102	(33)	201	100	45	010	115	115	110	110	115	110	10)
153	(35)	-29	414	207	40	138						
154	(26)(36)	-198	517	207	538	138	138	138	138	138	134	129
		(~O`									
155		-29_	455	275	316	152	152	152	152	152	151	149
156		~20	485	350	316	162	162	162	162	162	161	159
157	(35)(50)	-29	414	207	649	138	130	126	124	122	121	120
	(35)	-29	448	207	649	138	130	126	124	122	121	120
	(35)	-29	448	207	649	138	130	126	124	122	121	120
	(35)	-29	448	207	649	138	130	126	124	122	121	120
	(35)(50) (35) (35) (35) (36)											
161	(36)	-198	517	207	454	138	138	138	138	138	136	131
	•											
162	(28)(31)(35)(36)	-198	517	207	816	138	138	138	138	138	138	138
4.55	(00)(04)(06)	400	F4.	205	011	400	400	400	400	400	400	400
163	(28)(31)(36)	-198	515	205	816	138	138	138	138	138	138	138
164	(28)(35)(36)	-198	517	207	816	138	138	138	138	138	138	138
104	(20)(33)(30)	-170	J1/	207	010	130	130	130	130	130	130	130
165	(36)	-254	517	207	816	138	138	138	138	138	138	138
	(36)	-198	517	207	816	138	138	138	138	138	138	138

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]												
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
139	233	233	233	233	233						•••	•••	
140	233	233	233	233	233								78
141	230	228	228	228	228							_C	V
142	230	228	228	228	228							2	
143	235	234	232	231	229	228	226	223	221	218	/,	\$	
144	241	238	237	237	236								
145	241	238	237	237	236						5		
146	241	238	237	237	236					¢			
147	245	243	243	242	242					%	•••	•••	
148	245	243	243	242	242				"				
149									(I)				
150	99.7	99.1	98.4	97.5	96.2	94.7	92.6	901	87.0	83.4	79.2	70.1	38.8
151	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
152	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5
153						Cijo.							
154	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
155	147	145	142	140	137								
156	156	154	152	149	146								
157	120	119	118	117	115	114	111	108	104	100	92.5	68.4	51.1
158	120	119	118	117	115	114	111	108	104	100	92.5	68.4	51.1
159	120	119	118	117	115	114	111	108	104	100	88.7	69.8	52.6
160	120	119	118	117	115	114	111	108	104	100	88.7	69.8	52.6
161	127	2 ₁₂₃	120	118	115	113	111	109	107	105	103		
162	137	134	131	129	127	125	123	122	120	119	117	116	84.9
163	138	135	131	128	125	122	120	119	117	115	114	113	112
164	138	135	133	131	129	127	125	124	122	121	119	117	108
165	138	138	137	135	132	130	128	127	126	126	125	125	125
166	138	138	137	135	132	130	128	127	126	126	125	125	125

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]											
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
120												
139 140											0/8	
141										O	V	
142										23		
143										\Q		
144							•••		M			
145									D.			
146	•••					•••		¢				•••
147								OX.				
148								Q V				
149												
150	27.6						He .					
151	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
152	80.8	73.0	67.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
153					Cijo							
154	96.4			MOS	•		•••			•••		
155			c	<u> </u>								•••
156			1000									
157	37.4	26.3	17.8	11.4	6.89							
158	37.4	26.3	17.8	11.4	6.89							
159 160	38.1 38.1	27.6 27.6	20.6 20.6	15.9 15.9	12.4 12.4							
161	RSN											
162	59.0	43.5	31.9	23.6	16.9	10.7	6.10	3.90	2.99	2.36	1.73	1.38
163	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
164	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
165	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
166	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
167	25Cr-20Ni	Plate & sheet	A240	310S	S31008			8
168	18Cr-10Ni-Ti	Plate, sheet, strip	A240	321	S32100			8
169	18Cr-10Ni-Ti	Plate, sheet, strip	A240	321H	S32109		00	8
						(3 V	
	16Cr-12Ni-2Mo	Plate & sheet	A240	316	S31600	0	•	8
1/1	18Cr-13Ni-3Mo	Plate & sheet	A240	317	S31700	, & J		8
172	18Cr-10Ni-Cb	Plate & sheet	A240	347	S34700	N		8
	18Cr-10Ni-Cb	Plate & sheet	A240	348	S34800	<i>b</i>		8
1.0	1001 10111 00	That a sheet	112 10	0.10	, P			Ü
174	18Cr-8Ni	Plate & sheet	A240	304	\$30400			8
175	44Fe-25Ni-21Cr-Mo	Plate & sheet	A240	904L	N08904			45
176	23Cr-4Ni-Mo-Cu-N	Plate & sheet	A240	2304	S32304			10H
177	22Cr-5Ni-3Mo-N	Plate & sheet	A240		S31803	***		10H
178	16Cr-4Ni-6Mn	Plate & sheet	A240	201LN	S20153			8
179	20Cr-18Ni-6Mo	Plate	A240		S31254		>5.0	8
180	20Cr-18Ni-6Mo	Sheet	A240		S31254		≤5.0	8
181	46Fe-24Ni-21Cr-6Mo-	Plate	A240		N08367		>5.0	45
182	Cu-N 46Fe-24Ni-21Cr-6Mo- Cu-N	Sheet & strip	A240		N08367		≤5.0	45
183	21Cr-5Mn-1.5Ni-Cu-N	Plate & sheet	A240		S32101		>5.0	10H
184	24Cr-4Ni-3Mn-1.5Mo-N	Plate & sheet	A240		S82441		≥10.0	10H
185	21Cr-5Mn-1.5Ni-Cu-N	Plate & sheet	A240		S32101		≤5.0	10H
		~C.						
	21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N	Plate & sheet	A240		S32003		>5.00	10H
	21Cr-3 ¹ / ₂ Ni-1 ³ / ₄ Mo-N	Plate & sheet	A240		S32003		≤5.00	10H
188	24Cr-4Ni-3Mn-1.5Mo-N	Plate & sheet	A240		S82441	***	<10.0	10H
100	200m 6 EN; 2Ma N	Diata 9 shoot	1240		C22006		>100	1011
	29Cr-6.5Ni-2Mø-N 29Cr-6.5Ni-2Mo-N	Plate & sheet Plate & sheet	A240 A240		S32906 S32906		≥10.0 ≤10.0	10H 10H
190	29C1 -0.3N1-2M0-N	riate & Sileet	A240		332900		≥10.0	1011
191	25Cr-8Ni-3Mo-W-Cu-N	Plate & sheet	A240		S32760			10H
	25Cr-7Ni-4Mo-N	Plate & sheet	A240	2507	S32750			10H
193	18Cr-13Ni-3Mo	Forgings & fittings	A182	F317L	S31703	•••	≤125	8
	18Cr-8Ni	Forgings & fittings	A182	F304L	S30403	•••		8
195	18Cr-8Ni	Forgings & fittings	A403	WP304L	S30403			8
100	16Cr 12N; 2Ma	Forgings & fittings	A102	E216I	C21602			0
	16Cr-12Ni-2Mo 16Cr-12Ni-2Mo	Forgings & fittings Forgings & fittings	A182	F316L WP316I	S31603		•••	8
17/	1001-17MI-7M0	rorgings & numgs	A403	WP316L	S31603			8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

(9)(21a)

195 (32)(37)

196 (9)(21a)

197 (32)(37)

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-254

-254

-254

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]												
Line						_							
No.	225	250	275	300	325	350	375	400	425	450	475	500	525
167	137	134	131	129	127	125	123	122	120	119	117	116	108
168	138	135	131	128	125	122	120	119	117	115	114	113	192
169	138	135	131	128	125	122	120	119	117	115	114	113	112
10)	150	100	101	120	120	122	120	117	11,	110	111	110	
170	129	125	122	119	116	114	112	111	110	109	108	107	106
171	129	125	122	119	116	114	112	111	110	109	108	107	106
172	138	138	137	135	132	130	128	127	126	126	125	125	125
173	138	138	137	135	132	130	128	127	126	126	125	125	125
454	405	400	440	446	440		100	405	405	100	101	00.4	0.7.0
174	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
175	125	120	116),			
176	166	161	153	 143	 111								
177	190	188	187	186	185								
178	160	159	158	158	158	157	156	154	152	149	146		
179	184	179	175	172	169	167	166	165	164	163	161		
180	184	179	175	172	169	167	166	165	164	163	161		
181	195	192	188	184	179	176	173	170	167	166			
182	199	194	188	184	179	176	173	170	167	166			
102	199	194	100	104	1/9	1/07	1/3	170	107	100			
						Q,							
183	199	199	199	199	199	•							
184	227	227	227	227	227								
185	214	214	214	214	214								
186	197	197	197	197	197	197							
187	207	207	207	207	207	207	•••	•••	•••	•••	•••	•••	•••
188	247	247	247	247	247								
100	217	217	Or	217	21,		•••		•••		•••		
189	230	228	228	228	228								
190	245	243	243	242	242								
	7	5											
191	233	233	233	233	233								
192	241	238	237	237	236								
100	100	102	100	00.1	06.1	043	02.6	00.0	00.2	07.6	05.0		
193	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9		
194	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
195	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7
196	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5
197	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	82.5

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

-	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]											
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
167	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
10.	00.7	0 1.0	10.0	50.0			20.7	12.0	7.07	7.00	0.57	0.17
168	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9,02	6.83
169	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
										0-	V	
170	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
171	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	1333	10.4	8.96
172	125	112	00.6	(0.6	5 2.0	41.4	21.0	24.0	10.0	14.6	10.0	0.06
172 173	125 125	112 112	90.6 90.6	69.6 69.6	53.8 53.8	41.4 41.4	31.8 31.8	24.0 24.0	18.8 18.8	14.6 14.6	10.9 10.9	8.96 8.96
1/3	123	112	90.0	09.0	33.0	41.4	31.0	24.0	75,0	14.0	10.9	0.90
174	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
								N.				
175							,	QV				
176							11.5					
177							C. XO.					
178	•••						No.				•••	•••
179						1/2						
180 181	•••					TIO.				•••		•••
181					 *	0						
182					cjick t							
183				. ا	•							
184				-Ola								
185				Q								
406			20	•								
186	•••		30								***	***
187 188			115									
100		.0				•••						
189		7									•••	
190	EN.											
191	P											
192												
193												
194	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
195	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21
196	80.8	73.0	67.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89
197	80.8	73.0	67.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7.99	6.89

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
198	20Ni-8Cr	Forgings & fittings	A182	F10	S33100			8
199	18Cr-13Ni-3Mo	Forgings & fittings	A403	WP317L	S31703		20	8
200	25Cr-20Ni	Forgings & fittings	A182	F310H	S31009		5	8
201	25Cr-20Ni	Forgings & fittings	A403	WP310	S31008	~?)`		8
						4		
202	18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100	W.	>10	8
203	18Cr-10Ni-Ti	Forgings	A182	F321	S32100			8
204	18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100		≤10	8
205	18Cr-10Ni-Ti	Wld. fittings	A403	WP321	\$32100			8
		_			•			
206	23Cr-12Ni	Forgings & fittings	A403	WP309	S30900			8
207	25Cr-20Ni	Forgings & fittings	A182	F310H	S31009			8
208	25Cr-20Ni	Forgings & fittings	A403 💉	WP310	S31008			8
			187					
209	18Cr-10Ni-Cb	Forgings & fittings	A182	F347	S34700			8
210	18Cr-10Ni-Cb	Forgings & fittings	A403	WP347	S34700			8
211	18Cr-10Ni-Cb	Forgings & fittings	A182	F348	S34800			8
212	18Cr-10Ni-Cb	Forgings & fittings	A403	WP348	S34800			8
		cjiO.						
213	18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100		>10	8
214	18Cr-10Ni-Ti	Smls. fittings	A403	WP321H	S32109		>10	8
215	18Cr-10Ni-Ti	Forgings	A182	F321	S32100			8
216	18Cr-10Ni-Ti	Forgings	A182	F321H	S32109			8
217	18Cr-10Ni-Ti	Smls. fittings	A403	WP321	S32100		≤10	8
218	18Cr-10Ni-Ti	Smls. fittings	A403	WP321H	S32109		≤10	8
219	18Cr-10Ni-Ti	Wid. fittings	A403	WP321	S32100			8
220	18Cr-10Ni-Ti	Wld. fittings	A403	WP321H	S32109			8
	,0'	-						
221	16Cr-12Ni-2M	Forgings & fittings	A403	WP316H	S31609			8
	16Cr-12Ni-2Mo	Forgings & fittings	A182	F316H	S31609			8
	5							
223	18Cr-10Ni-Cb	Forgings & fittings	A403	WP347H	S34709			8
	18Cr-10Ni-Cb	Forgings & fittings	A182	F347	S34700			8
225	18Cr-10Ni-Cb	Forgings & fittings	A403	WP347	S34700			8
	18Cr-10Ni-Cb	Forgings & fittings	A182	F348	S34800			8
	18Cr-10Ni-Cb	Forgings & fittings	A403	WP348	S34800	•••		8
		0 0 0-		-				
228	18Cr-10Ni-Cb	Forgings & fittings	A182	F347H	S34709			8
	18Cr-10Ni-Cb	Forgings & fittings	A182	F348H	S34809			8
		0 0	~-			***		-
230	16Cr-12Ni-2Mo	Forgings & fittings	A182	F316	S31600			8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						Basic Allowable Stress, S, MPa, at Metal Temperature,								
				Min.			°C		(1), (3),		· b)]			
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Strength, MPa	Yield Strength, MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200		
		- (-)												
198	(26)(28)(39)	-198	552	207	40	138						ა		
199	(32)(37)	-198	517	207	454	138	138	138	138	138	136	131		
200	(9)(35)(39)	-198	517	207	816	138	138	138	138	138	138	138		
	(28)(32)(35)(37)(39)	-198	517	207	816	138	138	138	138	138	138	138		
202	(28)	-198	485	170	816	115	115	115	115	115	115	115		
	(9)(21)(28)	-198	515	205	816	138	138	138	138	138	138	138		
	(28)	-198	515	205	816	138	138	138	138	138	138	138		
	(28)	-198	515	205	816	138	138		138	138	138	138		
206	(28)(32)(35)(37)(39)	-198	517	207	816	138	138	138	138	138	138	138		
207	(9)(21)(29)(35)(39)	-198	517	207	816	138	138	138	138	138	138	138		
	(28)(29)(32)(35)(37) (39)	-198	517	207	816	138	138	138	138	138	138	138		
209	(9)(21)	-254	517	207	816	138	138	138	138	138	138	138		
210	(32)(37)	-254	517	207	816	138	138	138	138	138	138	138		
211	(9)(21)	-198	517	207	816	138	138	138	138	138	138	138		
212	(32)(37)	-198	517	207	816	138	138	138	138	138	138	138		
212	(28)(30)	-198	485	170	816	115	115	115	115	115	115	115		
	(30)	-198	485	170	816	115	115	115	115	115	115	115		
	(9)(21)(28)(30)	-198	515	205	816	138	138	138	138	138	138	138		
	(9)(21)	-198	515	205	816	138	138	138	138	138	138	138		
	(28)(30)	-198	515	205	816	138	138	138	138	138	138	138		
	(30)	198	515	205	816	138	138	138	138	138	138	138		
	(28)(30)	-198	515	205	816	138	138	138	138	138	138	138		
220	(30)		515	205	816	138	138	138	138	138	138	138		
221	(30) (26)(32)(37) (9)(21)(26)	-198	517	207	816	138	138	138	138	138	138	134		
222	(9)(21)(26)	-198	517	207	816	138	138	138	138	138	138	134		
223	(32)(37)	-198	517	207	816	138	138	138	138	138	138	138		
224	(9)(21)(28)	-254	517	207	816	138	138	138	138	138	138	138		
	(28)(32)(37)	-254	517	207	816	138	138	138	138	138	138	138		
	(9)(21)(28)	-198	517	207	816	138	138	138	138	138	138	138		
	(28)(32)(37)	-198	517	207	816	138	138	138	138	138	138	138		
228	(9)(21)	-198	517	207	816	138	138	138	138	138	138	138		
	(9)(21)	-198	517	207	816	138	138	138	138	138	138	138		
230	(9)(21)(26)(28)	-198	517	207	816	138	138	138	138	138	138	134		

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]												
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
198													<u>.</u> %
199	127	123	120	118	115	113	111	109	107	105	103		10,
200	137	134	131	129	127	125	123	122	120	119	117	116.	84.9
201	137	134	131	129	127	125	123	122	120	119	117	1 16	84.9
												Ø	
202	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
203	138	135	131	128	125	122	120	119	117	115	114	113	112
204	138	135	131	128	125	122	120	119	117	115	114	113	112
205	138	135	131	128	125	122	120	119	117	115	114	113	112
										X			
206	138	135	133	131	129	127	125	124	122	121	119	117	108
207	137	134	131	129	127	125	123	122	120	119	117	116	108
208	137	134	131	129	127	125	123	122	120	119	117	116	108
209	138	138	137	135	132	130	128	127	126	126	125	125	125
210	138	138	137	135	132	130	128	127	126	126	125	125	125
211	138	138	137	135	132	130	128	127	126	126	125	125	125
212	138	138	137	135	132	130	128	127	126	126	125	125	125
212	150	150	157	133	132	130	120	127	120	120	123	125	123
213	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
214	115	112	109	106	104	102	100	99.0	97.0	96.3	95.3	94.4	93.6
215	138	135	131	128	125	122	120	119	117	115	114	113	112
216	138	135	131	128	125	122	120	119	117	115	114	113	112
217	138	135	131	128	125	122	120	119	117	115	114	113	112
218	138	135	131	128	125	122	120	119	117	115	114	113	112
219	138	135	131	128	125	122	120	119	117	115	114	113	112
220	138	135	131	128	125	122	120	119	117	115	114	113	112
			O										
221	129	125	122	119	116	114	112	111	110	109	108	107	106
222	129	125 125	122	119	116	114	112	111	110	109	108	107	106
	0	3 .											
223	138	138	137	135	132	130	129	127	126	126	125	125	125
224	138	138	137	135	132	130	128	127	126	126	125	125	125
225	138	138	137	135	132	130	129	127	126	126	125	125	125
226	138	138	137	135	132	130	128	127	126	126	125	125	125
227	138	138	137	135	132	130	128	127	126	126	125	125	125
						·				4 = 1			
228	138	138	137	135	132	130	129	127	126	126	125	125	125
229	138	138	137	135	132	130	129	127	126	126	125	125	125
230	129	125	122	119	116	114	112	111	110	109	108	107	106

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]											
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
198												
199											20/20	
200	59.0	43.5	31.9	23.6	16.9	10.7	6.10	3.90	2.99	2.36	1.73	1.38
201	59.0	43.5	31.9	23.6	16.9	10.7	6.10	3.90	2.99	2.36	1.73	1.38
										, V		
202	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
203	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
204	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
205	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
206	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
207	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
208	83.7	64.0	48.5	36.3	27.3	21.0	15.9	12.5	9.87	7.65	5.97	5.17
						~,						
209	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
210	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
211	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
212	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
242	02.7	76 F	50.5	46.0	Cha	20.5	22.0	10.4	145	11.5	0.02	6.00
213 214	92.7	76.5 76.5	58.7 58.7	46.0 46.0	36.8 36.8	28.7 28.7	23.0 23.0	18.4 18.4	14.5 14.5	11.5 11.5	9.02 9.02	6.83 6.83
214	92.7 100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
216	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
217	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
218	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
219	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
220	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
		~\O,										
221	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
222	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
223	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
224	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
225	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
226	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
227	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
228	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
229	125	112	90.6	69.6	53.8	41.4 41.4	31.8	24.0	18.8	14.6	10.9	8.96
22)	123	114	70.0	07.0	33.0	11.7	51.0	21.0	10.0	1110	10.7	0.70
230	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
231	16Cr-12Ni-2Mo	Forgings & fittings	A403	WP316	S31600			8
232	18Cr-13Ni-3Mo	Forgings & fittings	A403	WP317	S31700			8
233	18Cr-8Ni	Forgings & fittings	A182	F304	S30400		00	8
234	18Cr-8Ni	Forgings & fittings	A403	WP304	S30400) <u>レ</u>	8
235	18Cr-8Ni	Forgings & fittings	A403	WP304H	S30409	25		8
236	18Cr-8Ni	Forgings & fittings	A182	F304H	S30409			8
237	44Fe-25Ni-21Cr-Mo	Forgings	A182	F904L	N08904			45
238	13Cr	Forgings & fittings	A182	F6a	\$41000	1		6
239	13Cr	Forgings & fittings	A182	F6a	S41000	2		6
240	20Cr-18Ni-6Mo	Forgings	A182	F44	S31254			8
241	20Cr-18Ni-6Mo	Fittings	A403	WP\$31254	S31254			8
242	20Cr-18Ni-6Mo	Fittings	A403	CRS31254	S31254			8
243	23Cr-4Ni-Mo-Cu-N	Forgings	A182	F68	S32304			10H
	22Cr-5Ni-3Mo-N		A182	F51	S31803			10H
	22Cr-5Ni-3Mo-N	Fittings	A815	WPS31803	S31803			10H
	22Cr-5Ni-3Mo-N	Fittings	A815	CRS31803	S31803			10H
247	46Fe-24Ni-21Cr-6Mo-Cu- N	Forgings Fittings Fittings Forgings	A182	F62	N08367			45
248	46Fe-24Ni-21Cr-6Mo-Cu-N	Fittings	A403	WP6XN	N08367			45
249	46Fe-24Ni-21Cr-6Mo-Cu-N	Fittings	A403	CR6XN	N08367			45
250	21Cr-5Mn-1½Ni-Cu-N	Fittings	A815		S32101			10H
251	25Cr-8Ni-3Mo-W-Cu-N	Forgings & fittings	A182		S32760			10H
252	25Cr-8Ni-3Mo-W-Cu-N	Forgings & fittings	A815		S32760			10H
253	13Cr	Forgings & fittings	A182	F6a	S41000	3		6
	13Cr- ¹ / ₂ M6	Forgings & fittings	A182	F6b	S41026			6
255	25Cr-7Ni-4Mo-N	Forgings & fittings	A182	F53	S32750			10H
256	25Cr-7Ni-4Mo-N	Forgings & fittings	A815	WPS32750	S32750			10H
	25Cr-7Ni-4Mo-N	Forgings & fittings	A815	CRS32750	S32750			10H
258	13Cr	Forgings & fittings	A182	F6a	S41000	4		6
259	18Cr-8Ni	Bar	A479	304	S30400			8
260	18Cr-8Ni	Bar	A479	304H	S30409			8
261	18Cr-8Ni	Bar	A479	304L	S30403			8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM Unless Otherwise Indicated

Basic Allowable Stress, S, MPa, at Metal

			••			Basic Allowable Stress, S, MPa, at Metal								
							°C []		1) (3)	re, and <mark>(4</mark>	h)]			
		Min.	Min. Tensile	Min. Yield	Max. Use	Min.	υ į.	totes (<u> </u>	unu (1	<u>., </u>			
Line No.	Notes	Temp., °C (6)	Strength, MPa	Strength, MPa	Temp., °C	Temp. to 40	65	100	125	150	175	200		
	(26)(28)(32)(37)	-254	517	207	816	138	138	138	138	138	138	134		
	(26)(28)(32)	-198	517	207	816	138	138	138	138	138	138	134		
											19	b		
233	(9)(21)(26)(28)	-254	517	207	816	138	138	138	138	138	134	129		
234	(26)(28)(32)(37)	-254	517	207	816	138	138	138	138	138	134	129		
									(2				
	(26)(32)(37)	-198	517	207	816	138	138	138	138	138	134	129		
236	(9)(21)(26)	-198	517	207	816	138	138	138	138	138	134	129		
227	(26)	-198	490	220	260	143	143	143	143	141	135	130		
237	(20)	170	470	220	200	143	143	F 30	143	171	133	130		
238	(35)	-29	483	276	538	161	161	161	160	158	156	155		
	(35)	-29	586	379	649	195	195	195	194	191	190	188		
						. (2)								
240	(8)	-198	650	300	454	202	202	202	202	199	192	185		
241		-198	650	300	454	202	202	202	202	199	192	185		
242	(8)	-198	650	300	454	202	202	202	202	199	192	185		
242	(05)	F.4	600	400	N	200	200	404	405	400	455	4.774		
	(25)	-51	600	400 450	316 316	200	200	191	185	180	175	171		
	(25) (25)	-51 -51	620 620	450	316	207 207	207 207	207 207	204 204	199 199	196 196	193 193		
	(25)	-51 -51	620	450	316	207	207	207	204	199	196	193		
210	(23)	51	020	G 150	310	207	207	207	201	1,,,	150	175		
247	(26)	-198	655	310	427	207	207	207	207	206	202	198		
240	(26)	-198	655	310	427	207	207	207	207	206	202	198		
240	(20)	-190	0000	310	427	207	207	207	207	200	202	170		
249	(26)	-198	655	310	427	207	207	207	207	206	202	198		
		\sim		.=.										
250	(25)	-29	650	450	316	217	217	215	211	206	203	199		
251	(25)	-51	750	550	316	250	250	248	243	238	236	234		
	(25)	-51	750	550	316	250	250	248	243	238	236	234		
	(35)	-29	758	586	40	253								
	(35)		760-930	620	40	253								
255	(05)	5 4	000	550	24.6	0.67	265	264	0.55	254	0.47	0.40		
	(25)	-51	800	550	316	267	265	264	257	251 251	247	243		
	(25)	-51 -51	800 800	550 550	316 316	267 267	265 265	264 264	257 257	251 251	247 247	243		
43/	(25)	-91	000	550	310	20/	265	204	4 3/	231	247	243		
258	(35)	-29	896	758	40	299								
	(26)(28)	-254	517	207	816	138	138	138	138	138	134	129		
	(26)	-198	517	207	816	138	138	138	138	138	134	129		
261		-254	483	172	816	115	115	115	115	115	114	110		

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]												
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
231	129	125	122	119	116	114	112	111	110	109	108	107	106
232	129	125	122	119	116	114	112	111	110	109	108	107	106
233	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
234	125	122	119	116	113	111	109	107	105	103	101	99.13	97.3
235	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
236	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
237	125	120	116							,	SMI		
238	154	153	152	150	148	145	142	137	133	125	92.5	68.4	51.1
239	187	186	184	182	180	176	172	167	161	125	92.5	68.4	51.1
240	180	175	171	168	165	164	162	161	160	159	158		
241	180	175	171	168	165	164	162	161	160	159	158		
242	180	175	171	168	165	164	162	161	160	159	158		
243	166	161	153	143	111			<i>"</i> "					
244	190	188	187	186	185		11/2						
245	190	188	187	186	185		×O						
246	190	188	187	186	185	CIICK		•••		•••			
247	195	192	188	184	179	176	173	170	167	166			
248	195	192	188	184	179	176	173	170	167	166			
249	195	192	188	184	179	176	173	170	167	166			
250	199	199	199	199	199								
251	233	233	233	233	233								
252	233	233	233	233	233						•••		
253		W.											
254	🗸	3/2								•••			
255	241	238	237	237	236								
256	241	238	237	237	236		•••						
257	241	238	237	237	236								
258													
259	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
260	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
261	106	103	99.9	97.7	95.7	94.1	92.6	91.3	90.0	88.7	87.3	85.6	83.7

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1), (3), and (4b)]											
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
231	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
232	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
233	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
234	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
235	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	141	11.2	9.65
236	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
									- M			
237								SK O	ASMI			
238	44.1							, Ö				
239	37.4	26.3	17.8	11.4	6.89			ODX				
240							11.					
241							XO					
242							Me.					
243						No:						
244						71,						
245					X	.						
246					Click							
247					•							
248				COM								
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250			ND									
251		S.										
252		1										
253		/										
254	RSP											
255												
256												
257												
258												
259	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
260	95.5	78.9	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	9.65
261	81.4	40.4	33.2	26.7	21.9	18.2	15.0	12.4	8.87	7.20	6.58	6.21

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
	16Cr-12Ni-2Mo	Bar	A479	316	S31600			8
	16Cr-12Ni-2Mo	Bar	A479	316H	S31609			8
	16Cr-12Ni-2Mo	Bar	A479	316L	S31603			%
							~O)	
265	18Cr-10Ni-Ti	Bar	A479	321	S32100		21	8
266	18Cr-10Ni-Ti	Bar	A479	321	S32100		 	8
267	18Cr-10Ni-Ti	Bar	A479	321H	S32109	್ದ್ರಾ		8
268	18Cr-10Ni-Cb	Bar	A479	347	S34700	\(\frac{1}{2}\)		8
269	18Cr-10Ni-Cb	Bar	A479	347	S34700			8
270	18Cr-10Ni-Cb	Bar	A479	347H	S34709			8
					& P			
271	44Fe-25Ni-21Cr-Mo	Bar	A479	904L	N08904			45
272	22Cr-5Ni-3Mo-N	Bar	A479	0	S31803			10H
273	20Cr-18Ni-6Mo	Bar	A479	Q	S31254			8
274	46Fe-24Ni-21Cr-6Mo-	Bar	A479		N08367			45
275	Cu-N	Dan	A 470	0	C22101			1011
2/5	21Cr-5Mn-1.5Ni-Cu-N	Bar	A479		S32101			10H
276	24Cr-4Ni-3Mn-1.5Mo-N	Bar	A479		S82441		≥11.0	10H
	22Cr-13Ni-5Mn	Bar	A479	XM-19	S20910			8
	24Cr-4Ni-3Mn-1.5Mo-N	Bar	A479		S82441		<11.0	10H
		Bar Bar						
279	29Cr-6.5Ni-2Mo-N	Bar	A479		S32906			10H
280	25Cr-7Ni-4Mo-N	Bar	A479		S32750		≤50	10H
		<i>d</i> .						
281	29Ni-20Cr-3Cu-2Mo	Castings	A351	CN7M	N08007			45
282	35Ni-15Cr- ¹ / ₂ Mo	Castings	A351	HT30	N08603			45
283	25Cr-12Ni	Castings	A351	CH8	J93400			8
284	25Cr-20Ni	Castings	A351	CK20	J94202	•••		8
	1							
285	16Cr-14Ni-2Mo	Castings	A351	CF10MC				8
286	18Cr-8Ni	Castings	A351	CF3	J92500			8
287	18Cr-12Ni-2Mo	Castings	A351	CF3M	J92800	•••		8
	CMI							
288	18Cr-8Ni	Castings	A351	CF8	J92600			8
200	050 4000		1051	01110	100101			0
	25Cr-12Ni	Castings	A351	CH10	J93401	•••	•••	8
290	25Cr-12Ni	Castings	A351	CH20	J93402	•••		8
201	18Cr-10Ni-Cb	Castings	A351	CF8C	J92710			8
	18Cr-12Ni-2Mo	Castings	A351	CF8M	J92710 J92900			8
<u> </u>	1001-12141-71410	Gasungs	U221	GI OM	J 2 2 3 0 0	•••		U
293	25Cr-20Ni-½Mo	Castings	A351	HK40	J94204			8
2,5	2001 20111 /2110		11001		, , 1201			J
294	25Cr-20Ni-½Mo	Castings	A351	HK30	J94203			8
	-	=						

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers in Parentneses Refer to Notes for Appendix A Tables; Specifications are ASTM Offices Otherwise indicated													
						Basic Allowable Stress, S, MPa, at Metal Temperature,								
				Min.			°C [-	and (4)	b)]			
		Min.	Min. Tensile	Yield	Max. Use	Min.								
Line No.	Notes	Temp., °C (6)	Strength, MPa	Strength, MPa	Temp., °C	Temp. to 40	65	100	125	150	175	200		
	(26)(28)	-198	517	207	816	138	138	138	138	138	138	134		
	(26)	-198	517	207	816	138	138	138	138	138	138	134		
264		-254	483	172	816	115	115	115	115	115		b 109		
201		254	403	1/2	010	113	113	113	113	113				
265	(28)	-198	515	205	816	138	138	138	138	138	138	138		
266	(28)(30)	-198	515	205	816	138	138	138	138	138	138	138		
	(30)	-198	515	205	816	138	138	138	138	138	138	138		
268		-254	517	207	816	138	138	138	138	138	138	138		
269	(28)(30)	-254	517	207	816	138	138	138	138	138	138	138		
270		-198	517	207	816	138	138	138	138	138	138	138		
							ķ	P						
271	(26)	-198	490	220	260	143	143	143	143	141	135	130		
272	(25)	-51	620	450	316	207 🏑	207	207	204	199	196	193		
273	(8)	-198	655	310	454	207	207	207	207	203	196	190		
274	(26)	-198	655	310	427	207	207	207	207	206	202	198		
275	(25)	-29	650	450	316	217	217	215	211	206	203	199		
276	(25)	-51	680	480	316	227	227	227	227	227	227	227		
277		-29	690	380	649	230	230	227	221	217	213	210		
	(25)	-51	740	540	316	247	247	247	247	247	247	247		
270	(23)	31	7 10	1	310	217	217	217	217	217	217	217		
279	(25)	-51	750	550	316	251	251	249	243	238	235	231		
	(25)	-51	800	550	316	267	265	264	257	251	247	243		
200	(23)	51	W .	330	510	20,	200	201	207	201	217	210		
281	(9)(30)	-198	427	172	40	115								
282	(36)(39)	-198	448	193	40	129								
283	(9)(31)	-198	448	193	816	129	129	129	129	127	125	124		
284	(9)(27)(31)(35)(39)	198	448	193	816	129	129	129	129	127	125	124		
	(30)	-198	483	207	40	138								
286		-254	483	207	427	138	138	138	138	138	134	129		
287	(9)	-254	483	207	454	138	138	138	138	138	138	133		
288	(9)(26)(27)(31)	-254	483	207	816	138	138	138	138	138	134	129		
289	(27)(31)(35)	-198	483	207	816	138	138	138	138	138	138	138		
290	(9)(27)(31)(35)(39)	-198	483	207	816	138	138	138	138	138	138	138		
291	(9)(28)	-198	485	205	816	138	138	138	138	138	138	135		
	(9)(26)(27)(30)	-254	483	207	816	138	138	138	138	138	134	129		
,	(-)(-)(-)(00)	-51	130	-57	010	200	200	100	100	100		/		
293	(35)(36)(39)	-198	427	241	40	142								
294	(35)(39)	-198	448	241	40	149								

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						vable Stre	ess, <i>S</i> , MP		al Tempe			i wise mur	
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
262	129	125	122	119	116	114	112	111	110	109	108	107	106
263	129	125	122	119	116	114	112	111	110	109	108	107	106
264	106	103	100	98.1	96.1	94.3	92.6	90.9	89.3	87.6	85.9	84.2	825
201	100	103	100	70.1	70.1	71.5	72.0	70.7	07.5	07.0	03.7	01.2	0/25
265	138	135	131	128	125	122	120	119	117	115	114	113	112
266	138	135	131	128	125	122	120	119	117	115	114	113.5	112
267	138	135	131	128	125	122	120	119	117	115	114	113	112
268	138	138	137	135	132	130	128	127	126	126	125	125	125
269	138	138	137	135	132	130	128	127	126	126	125	125	125
270	138	138	137	135	132	130	128	127	126	126	C ₁₂₅	125	125
270	130	150	157	155	132	150	120	127	120	120	32 3	123	123
271	125	120	116							o Š	•		
271	190	188	187	 186	 185		•••			√ ∪			
273	184	179	175	172	169	 167	 166	 165	164	163	 161		
273	195	192	188	184	179	176	173	170	167	166			
2/4	193	172	100	104	1/9	170	1/3	170	E THE	100			
275	199	199	199	199	199			THE					
276	227	227	227	227	227			<i>1</i>					
277	207	205	204	202	201	200	199	197	195	193	191	188	183
278	247	247	247	247	247		<u>، ۲</u>						
						V							
279	230	228	228	228	228	Silo,							
280	241	238	237	237	236	O,							
					1	•							
281					Ola.								
282				(
283	124	123	121	119)	117	115	112	109	106	103	100	96.9	93.7
284	124	123	121	119	117	115	112	109	106	103	100	96.9	93.7
			1										
285			07/2										
286	125	122	Q ₁₉	116	113	111	109	107	105	103			
287	129	125	122	119	116	114	112	111	109	108	 107		
207	12)		122	117	110	111	112	111	107	100	107	•••	•••
288	125	9 122	119	116	113	111	109	107	105	103	101	99.1	94.4
200	120	120	120	120	120	120	120	120	120	120	120	120	120
289	138	138	138	138	138	138	138	138	138	138	138	138	138
290	138	138	138	138	138	138	138	138	138	138	138	138	138
291	132	130	128	127	127	126	126	126	125	125	124	124	124
291	125	122	119	116	113	111	109	107	105	103	101	99.1	97.3
<u> </u>	143	144	117	110	113	111	107	107	103	103	101	99.1	91.3
293													
294													

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	s in Tarent	neses keie		Allowable	Stress, S, N		tal Tempe		iess otherv	visc mulca	icu
-					<u> </u>	Notes (1),	(3), and (-	 				
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
262	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
263	105	97.8	80.8	65.0	50.4	38.6	29.6	23.0	17.4	13.3	10.4	8.96
264	80.8	73.0	67.9	58.0	43.6	33.0	25.3	18.8	14.0	10.4	7,99	6.89
											0/10	
265	88.7	59.2	44.0	32.9	24.5	18.3	12.5	8.49	6.19	4.28	2.75	1.74
266	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	11.5	9.02	6.83
267	100	76.5	58.7	46.0	36.8	28.7	23.0	18.4	14.5	1105	9.02	6.83
268	97.6	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
269	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18.8	14.6	10.9	8.96
270	125	112	90.6	69.6	53.8	41.4	31.8	24.0	18,8	14.6	10.9	8.96
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271								" Ó				
272												
273												
274												
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275							NO					
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276						.01						
277	179	174	132	83.6	56.1	117						
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279												
280												
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281				٥٠, ١								
282				9								
283	68.1	53.5	42.1	33.2	25.9	20.3	16.5	13.2	10.1	7.35	5.89	5.52
284	73.2	64.4	56.5	49.0	41.0	33.5	25.4	18.3	12.8	9.01	6.59	5.52
		~	110									
285		- K										
286		1										
287		()		•••						•••		
	-CN											
288	75.3	60.4	49.0	40.1	32.8	27.2	23.4	19.6	16.8	14.7	12.8	11.7
289	68.1	53.5	42.1	33.2	25.9	20.3	16.5	13.2	10.1	7.35	5.89	5.52
290	68.1	53.5	42.1	33.2	25.9	20.3	16.5	13.2	10.1	7.35	5.89	5.52
291	98.3	77.2	57.7	39.9	30.0	23.2	16.3	11.2	8.93	7.08	5.77	5.32
292	95.5	75.9	57.2	40.2	30.3	23.2	16.2	11.4	8.97	7.08	5.89	5.52
200												
293												
20.4												
294					•••							

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
205	10Cm ON:	Contingo	A 2 E 1	CE2 A	102500			O
	18Cr-8Ni 18Cr-8Ni	Castings	A351 A351	CF3A CF8A	J92500 J92600			8
		Castings				•••	~	
297	25Cr-8Ni-N	Castings	A351	CE20N	J92802		200	8
298	12Cr	Castings	A217	CA15	J91150		 	6
299	24Cr-10Ni-4Mo-N	Castings	A995	2A	J93345	<u>ഏ</u> ം`		10H
300	25Cr-8Ni-3Mo-W-Cu-N	Castings	A995	6A	J93380	K		10H
301	13Cr-4Ni	Castings	A487	CA6NM	J91540			6
	ASMENOR	Castings Castings Castings Castings	o jien i	ine full.				

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			Notes for ripp		, - #			owable		S, MPa,		al
				Min.			°C	[Notes (b)]	
		Min.	Min. Tensile	Yield	Max. Use	Min.						
Line	••	Temp.,	Strength,	Strength,	Temp.,	Temp.		400	40.	4=0	4	200
No.	Notes	°C (6)	MPa	MPa	°C	to 40	65	100	125	150	175	200
205	(0)(5()	254	F24	241	271	171	161	1.61	160	150	150	151
	(9)(56)	-254	531	241	371	161	161	161	160	156	153	151
	(9)(26)(56)	-254	531	241	371	161	161	161	160	156	153	0151
297	(35)(39)	-198	552	276	482	184	184	184	184	184	184	184
200	(25)	20	(21	440	(40	207	207	207	205	203.	201	100
	(35)	-29	621	448	649	207	207	207			201	199
299		-51	655	448	316	218	218	216	208	201	197	195
300	(9)(25)	-51	689	448	316	230	230	227	221	216	212	209
								.65	7/			
301	(9)(35)	-29	758	552	371	253	253	253	251	248	245	244
	(9)(35) (9)(35)							1,				
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Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						vable Stre	ess, <i>S</i> , MF tes (1), (3	a, at Met	al Temp			or wise man	
Line No.	225	250	275	300	325	350	375	400	425	450	475	500	525
295	146	142	138	135	132	130	127						
296	146	142	138	135	132	130	127						2
297	184	184	184	184	184	184	184	184	184	184	184	184	0'
											82.1	က	V
298	198	197	195	193	190	187	182	120	116	105	82.1	59.9	41.8
299	194	194	194	194	194							Ø ₂	
300	207	206	205	204	204						~		
201	0.40	240	222	006			004				CMIL		
301	242	240	238	236	232	228	224						
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Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				Basic	Allowable °C		MPa, at Me (3), and (4		rature,			
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
295												
296											2	
297											JO,	
298	28.7	20.1	14.3	9.77	6.89					0.00		
299										25		
300					6.89					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
301									BA			
								Z 0				
								ODK				
							11.	X				
							Le XO					
						, n'	a,					
						jiez						
					X	9						
					Click							
				٨.								
				COM								
			C	0								
			100°									
		0	Mr									
		40,										
	d											
	PSI	-										
	•											

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	UNS No.	Class/ Condition/ Temper	Size,	P-No. (5)(7)	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa
1	99.95Cu-P	Pipe	B42	C10200	061		31		-269	207	62
	99.9Cu-P	Pipe	B42	C12000	061		31		-269	207	62
	99.9Cu-P	Pipe	B42	C12200	061		31		-269	207	62
	99.95Cu-P	Tube	B75	C10200	050		31		-269	207	62
	99.95Cu-P	Tube	B75	C10200	060		31		-269	207	62
	99.9Cu-P	Tube	B75	C12000	050		31		-269	207	62
	99.9Cu-P	Tube	B75	C12000	060		31		-269	207	62
	99.9Cu-P	Tube	B75	C12200	050		31		-269	207	62
	99.9Cu-P	Tube	B75	C12200	060		31		-269 ⁾	207	62
	99.9Cu-P	Tube	B68	C12200	050		31	(24)	-269	207	62
	99.9Cu-P	Tube	B68	C12200	060		31	(24)	-269	207	62
	99.9Cu-P	Tube	B88	C12200	050		31	(24)	-269	207	62
	99.9Cu-P	Tube	B88	C12200	060		31	(24)	-269	207	62
	99.9Cu-P	Tube	B280	C12200	060		31	(24)	-269	207	62
							~	<i>y</i> ,			
15	85Cu-15Zn	Pipe	B43	C23000	061		32		-269	276	83
		•				(1)					
16	90Cu-10Ni	Pipe & tube	B467	C70600	W050	>114 O.D.	34	(14)	-269	262	90
17	90Cu-10Ni	Pipe & tube	B467	C70600	W061	>114.0.D.	34	(14)	-269	262	90
18	90Cu-10Ni	Pipe & tube	B466	C70600	Annealed	N	34	(14)	-269	262	90
19	90Cu-10Ni	Pipe & tube	B467	C70600	W050	≤114 O.D.	34	(14)	-269	276	103
20	90Cu-10Ni	Pipe & tube	B467	C70600	W061	≤114 O.D.	34	(14)	-269	276	103
21	70Cu-30Ni	Pipe & tube	B467	C71500	W050	>114 O.D.	34	(14)	-269	310	103
22	70Cu-30Ni	Pipe & tube	B467	C71500	W061	>114 O.D.	34	(14)	-269	310	103
23	80Cu-20Ni	Pipe & tube	B466	C71000	Annealed	≤114 O.D.	34	(14)	-269	310	110
24	99.95Cu-P	Pipe	B42	610200	Н55	DN 64 thru	31	(14)(34)	-269	248	207
25	99.9Cu-P	Pipe	B42	C12000	Н55	300 DN 64 thru 300	31	(14)(34)	-269	248	207
26	99.9Cu-P	Pipe	B42	C12200	H55	DN 64 thru 300	31	(14)(34)	-269	248	207
27	99.95Cu-P	Tube	B75	C10200	H58		31	(14)(34)	-269	248	207
28	99.9Cu-P	Tube	B75	C12000	H58		31	(14)(34)	-269	248	207
29	99.9Cu-P	Tube	B75	C12200	H58		31	(14)(34)	-269	248	207
30	99.9Cu-P	Tube	B88	C12200	Н58		31	(14)(24) (34)	-269	248	207
31	70Cu-30Ni	Pipe & tube	B466	C71500	060	•••	34	(14)	-269	359	124
	70Cu-30Ni	Pipe & tube	B467	C71500	W050	≤114 O.D.	34	(14)	-269	345	138
	70Cu-30Ni	Pipe & tube	B467	C71500	W061	≤114 O.D.	34	(14)	-269	345	138
		•		-							
34	99.95Cu-P	Pipe	B42	C10200	H80	DN 6 thru 50	31	(14)(34)	-269	310	276
	99.9Cu-P	Pipe	B42	C12000	H80	DN 6 thru 50	31	(14)(34)	-269	310	276
	99.9Cu-P	Pipe	B42	C12200	H80	DN 6 thru 50	31	(14)(34)	-269	310	276
	99.95Cu-P	Tube	B75	C10200	Н80		31	(14)(34)	-269	310	276
	99.9Cu-P	Tube	B75	C12000	H80		31	(14)(34)	-269	310	276

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	ın rarei	nuieses							erature, '				muicate	<u>u </u>
	Max. Use	Min.		Dasic	Anowab	ne stress	s, s, MPa	, at Meta	и тетр	erature,	C [NOTE:	s (1) and	ı (4UJ)		
Line	Temp.,	Temp.													
No.	°C	to 40	65	100	125	150	175	200	225	250	275	300	325	350	375
1	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
2	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
3	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
4	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6			. 95	
5	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6		(10	
6	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6		?	·	
7	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6		ૣૢઌૺ૽		
8	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6	<u>C</u>	·		
9	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6	\mathcal{S}			
10	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6	\			
11	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
12	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
13	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
14	260	41.4	34.9	33.5	32.9	32.2	28.0	21.7	16.7	12.9	11.6				
									Ó	O,					
15	232	55.2	54.7	54.7	54.7	54.7	54.7	36.4	17.5	13.8					
									(11)						
16	316	59.8	58.0	56.1	54.9	53.8	52.9	52.0	51.2	50.4	49.7	45.1	39.3		
17	316	59.8	58.0	56.1	54.9	53.8	52.9	52.0	51.2	50.4	49.7	45.1	39.3		
18	316	59.8	58.0	56.1	54.9	53.8	52.9	52.0	51.2	50.4	49.7	45.1	39.3		
19	316	68.9	67.0	65.1	63.7	62.4	61.1	60.0	59.1	58.3	51.3	45.1	39.3		
20	316	68.9	67.0	65.1	63.7	62.4	61.1	60.0	59.1	58.3	51.3	45.1	39.3		
21	371	68.9	66.6	64.6	63.2	61.9	60.7	59.5	58.4	57.4	56.2	55.5	54.9	54.3	53.8
22	371	68.9	66.6	64.6	63.2	61.9	60.7	59.5	58.4	57.4	56.2	55.5	54.9	54.3	53.8
23	371	73.5	72.8	72.1	71.4	70.6	69.6	68.3	66.6	64.7	62.4	60.0	56.2	51.9	48.3
					1										
24	204	82.7	80.0	74.1	71.3	69.2	67.4	65.7	65.3						
0.5	20.4	00 T		G	74.0				- F 0						
25	204	82.7	80.0	74.1	71.3	69.2	67.4	65.7	65.3				•••		
26	204	82.7	80.0) 74.1	71.3	69.2	67.4	65.7	65.3						
20	201	02.7		, 1.1	71.0	07.2	07.11	00.7	00.0	•••	•••	•••	•••		•••
27	204	82.7	80.0	74.1	71.3	69.2	67.4	65.7	65.3						
28	204	82.7	80.0	74.1	71.3	69.2	67.4	65.7	65.3						
29	204	82.7	80.0	74.1	71.3	69.2	67.4	65.7	65.3						
30	204	82.7	80.0	74.1	71.3	69.2	67.4	65.7	65.3						
	~S`														
	~														
31	371	82.7	79.8	77.5	75.9	74.3	72.9	71.5	70.2	68.9	67.8	66.8	65.9	65.3	64.8
32	371	91.9	88.7	86.1	84.3	82.6	81.0	79.4	78.0	76.6	75.3	74.2	73.2	72.5	71.7
33	371	91.9	88.7	86.1	84.3	82.6	81.0	79.4	78.0	76.6	75.3	74.2	73.2	72.5	71.7
ı															
34	204	103	100	92.6	89.1	86.5	84.3	35.8	29.6						
35	204	103	100	92.6	89.1	86.5	84.3	35.8	29.6						
36	204	103	100	92.6	89.1	86.5	84.3	35.8	29.6						
37	204	103	100	92.6	89.1	86.5	84.3	35.8	29.6						
38	204	103	100	92.6	89.1	86.5	84.3	35.8	29.6						

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line	Nominal	Product	Spec.	PF	Class/ Condition/	Size,	P-No.		Min. Temp.,	Min. Tensile Str.,	Min. Yield Str.,
No.	Composition	Form	No.	UNS No.	Temper	mm	(5)(7)	Notes	°C (6)	MPa	MPa
39	99.9Cu-P	Tube	B75	C12200	Н80		31	(14)(34)	-269	310	276
40	99.95Cu-P	Plate & sheet	B152	C10200	025		31	(14)(24)	-269	207	69
41	99.95Cu-Ag	Plate & sheet	B152	C10400	025		31	(14)(24)	-269	207	69
42	99.95Cu-Ag	Plate & sheet	B152	C10500	025		31	(14)(24)	-269	207	69
43	99.95Cu-Ag	Plate & sheet	B152	C10700	025		31	(14)(24)	-269	207	69
44	99.9Cu-P	Plate & sheet	B152	C12200	025		31	(14)(24)	-269	207	69
45	99.9Cu-P	Plate & sheet	B152	C12300	025		31	(14)(24)	-269	207	69
46	90Cu-10Ni	Plate & sheet	B171	C70600		≤64 thk.	34	(14)	-269	276	103
47	97Cu-3Si	Plate & sheet	B96	C65500	061		33		-269	345	124
48	70Cu-30Ni	Plate & sheet	B171	C71500		≤64 thk.	34	(14)	-269	345	138
49	90Cu-7Al-3Fe	Plate & sheet	B169	C61400	025	≤50 thk.	35	(13)	-269	483	207
50	90Cu-7Al-3Fe	Plate & sheet	B169	C61400	060	≤50 thk.	35	(13)	-269	483	207
51	99.9Cu	Forgings	B283	C11000			31	(14)	-269	228	76
52	97Cu-3Si	Forgings	B283	C65500		(1)	33	(14)	-269	359	124
53	60Cu-38Zn-2Pb	Forgings	B283	C37700		"Lej	a	(14)	-198	400	159
54	60Cu-37Zn- 2Pb-Sn	Forgings	B283	C48500		M	a	(14)	-198	427	165
55	60Cu-39Zn-Sn	Forgings	B283	C46400	7,		32	(14)	-254	441	179
56	59Cu-39Zn-Fe- Sn	Forgings	B283	C67500	ick to vie		32	(14)	-198	496	234
57	85Cu-5Sn-5Zn- 5Pb	Castings	B62	C83600			a	(9)	-198	207	97
58	57Cu-20Zn- 12Ni-9Pb-2Sn	Castings	B584	C97300			a		-198	207	103
59	64Cu-20Ni-8Zn- 4Sn-4Pb	Castings	B584	C97600			a		-198	276	117
60	87Cu-8Sn-4Zn- 1Pb	Castings	B584	C92300			a		-198	248	110
61	88Cu-Sn-Zn-Pb	Castings	B584	C92200			a		-198	234	110
	88Cu-Sn-Zn-Pb		B61	C92200			a	(9)	-198	234	110
	88Cu-8Sn-4Zn	_	B584	C90300			b		-198	276	124
	88Cu-10Sn-2Zn	_	B584	C90500			b		-198	276	124
	58Cu-38Zn-	Castings	B584	C86400			a	(9)	-198	414	138
	1Sn-1Pb-1Fe 66Cu-25Ni-5Sn-	-	B584	C97800	•••	•••	a		-198	345	152
	2Pb-2Zn	Ü				•••					
6/	58Cu-39Zn- 1Fe-1Al-1Mn	Castings	B584	C86500		•••	b		-198	448	172
68	88Cu-9Al-3Fe	Castings	B148	C95200			35	(9)	-254	448	172
	89Cu-10Al-1Fe	Castings	B148	C95300			35	(9)	-254	448	172

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

		s in Pare	nuieses						al Tempe					murcate	:u
	Max. Use	Min.		Dasic	Allowan	ne stres	5, 5, MI a	, at Met	ai Tempe	rature,	C [Note	5 (1) and	ı (T D)]		
Line	Temp.,	Temp.													
No.	°C	to 40	65	100	125	150	175	200	225	250	275	300	325	350	375
39	204	103	100	92.6	89.1	86.5	84.3	35.8	29.6						
40	260	46.0	39.1	37.1	36.5	34.2	28.0	21.7	16.7	12.9	11.6				
41	260	46.0	39.1	37.1	36.5	34.2	28.0	21.7	16.7	12.9	11.6			<u> </u>	
42	260	46.0	39.1	37.1	36.5	34.2	28.0	21.7	16.7	12.9	11.6			NO	
43	260	46.0	39.1	37.1	36.5	34.2	28.0	21.7	16.7	12.9	11.6		<u> </u>	2	
44	260	46.0	39.1	37.1	36.5	34.2	28.0	21.7	16.7	12.9	11.6		2	•	•••
45	260	46.0	39.1	37.1	36.5	34.2	28.0	21.7	16.7	12.9	11.6		\ . <u>"</u>		•••
43	200	10.0	37.1	37.1	30.3	34.2	20.0	21.7	10.7	12.7	11.0	⟨ 2))		
46	316	68.9	67.0	65.1	63.7	62.4	61.1	60.0	59.1	58.3	51.3	45.1	39.3		
47	204	82.7	82.7	82.7	82.7	82.7	75.4	50.8	31.9		C				
48	371	91.9	88.7	86.1	84.3	82.6	81.0	79.4	78.0	76.6	75.3	74.2	73.2	72.5	71.7
49	260	138	137	136	135	135	134	133	131	130	130				
50	260	138	137	136	135	135	134	133	131	130	130				
٣1	260	F0.6	42.0	40.0	40.2	24.2	20.0	24.7	16.7	12.0	11.6				
51 52	260 204	50.6 82.7	42.8 82.7	40.8 82.7	40.2 82.7	34.2 82.7	28.0 75.4	21.7 50.8	31.9	12.9	11.6				
									~ ~				•••		
53	204	106	99.8	94.5	91.1	71.4	52.8	17.0	13.8						
54	204	110	110	110	110	110	110	110	110						
							ile	9							
55	204	120	120	120	120	118	118	20.0	17.2						
56	204	156	156	156	156	156	156	156	156		•••		•••		
						ZIIC,									
57	232	64.4	64.4	62.6	59.1•	55.7	53.0	51.2	50.3	50.1					
37	232	01.1	01.1	02.0	33.1	33.7	33.0	31.2	50.5	50.1	•••		•••		
58	40	68.9		(O_{IZ}										
59	149	78.1	69.6	64,9	62.5	60.3									
39	147	70.1	09.0	04.9	02.3	00.3									•••
60	204	73.5	73.5	73.5	73.5	73.5	73.5	73.5	73.5						
			5 Mi.												
		O_{ϵ}													
61	204	73.5	66.4	65.3	64.6	63.3	61.5	59.6	58.1						
62	288	73.5	66.4	65.3	64.6	63.3	61.5	59.6	58.1	57.5	57.5	57.3			
63	204	82.7	82.7	82.7	82.7	82.7	82.7	82.7	82.7		•••				
64	204	82.7	82.7	82.7	82.7	82.7	82.7	82.7	82.7		•••				
65	177	91.9	91.9	91.9	91.9	91.9	91.9	91.9							
66	177	101	101	101	101	101	101	101							•••
67	177	115	115	115	115	115	115	115							
•															
68	316	115	108	104	102	99.8	98.6	97.8	97.5	074	97.4	65.9	127		
69										97.4 115			43.7		
09	316	115	115	115	115	115	115	115	115	115	115	115	115		

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line	Nominal	Product	Spec.		Class/ Condition/	Size,	P-No.		Min. Temp.,	Min. Tensile Str.,	Min. Yield Str.,
No.	Composition	Form	No.	UNS No.	Temper	mm	(5)(7)	Notes	°C (6)	MPa	MPa
70	90Cu-7Al-3Si	Castings	B148	C95600			35		-198	414	193
71	85Cu-11Al-4Fe	Castings	B148	C95400			35		-198	517	207
72	58Cu-34Zn- 2Fe-2Al-2Mn	Castings	B584	C86700			a		-198	552	221
73	82Cu-11Al-4Fe- 3Mn	Castings	B148	C95500		•••	35		-269	621	276
74	63Cu-27Zn-4Al- 3Fe-3Mn	Castings	B584	C86200			b		-198 N	621	310
75	61Cu_277n_6Al_	Castings	B584	C86300			b		-198	758	414
76	75Cu-21.5Zn- 3Si	Rod	B371	C69300	Н02	≤12	a	of ASI	-198	585	310
77	75Cu-21.5Zn- 3Si	Rod	B371	C69300	H02	>12, ≤25	a	O.	-198	515	240
78	75Cu-21.5Zn- 3Si	Rod	B371	C69300	H02	>25, ≤50	(a)		-198	480	205
	ASM	Rod Rod Rod	S.		jick to vie	enthe.					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Max.	-						, at Meta							
Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225	250	275	300	325	350	375
40	129													
260	138	131	128	128	128	128	128	128	101	95.8				
177	147	147	147	147	147	147	147						2	
260	184	184	184	184	184	184	184	184	184	184)	
177	207	207	207	207	207	207	207					, <u>; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;</u>		
177	253	253	253	253	253	253	253				EB			
149	195	179	176	176	176					BS.				
149	161	139	137	137	137				K O					
149	138	119	117	117	117				V					
ASM	ENOS	2,410	5°.	OW.	click	yo vie								
	Use Temp., °C 40 260 177 260 177	Use Temp. °C Min. Temp. to 40 40 129 260 138 177 147 260 184 177 207	Use Temp. °C Min. Temp. to 40 65 40 129 260 138 131 177 147 147 260 184 184 177 207 207	Use Temp., °C Min. Temp. to 40 65 100 40 129 260 138 131 128 177 147 147 147 260 184 184 184 177 207 207 207	Use Temp., °C Min. Temp. to 40 65 100 125 40 129 260 138 131 128 128 177 147 147 147 147 260 184 184 184 184 177 207 207 207 207	Use Temp., °C Min. Temp. to 40 65 100 125 150 40 129 260 138 131 128 128 128 177 147 147 147 147 147 260 184 184 184 184 184 177 207 207 207 207 207 177 352 352 353 353 353 353	Use Temp., °C Min. Temp. to 40 65 100 125 150 175 40 129	Use Temp., °C Min. Temp. to 40 65 100 125 150 175 200 40 129	Use Temp., °C Min. Temp. to 40 65 100 125 150 175 200 225 40 129	Use Temp., °C Min. Temp. to 40 65 100 125 150 175 200 225 250 40 129	Use Temp., °C Min. Temp. to 40 65 100 125 150 175 200 225 250 275 40 129	Use Temp., °C Min. Temp., to 40 65 100 125 150 175 200 225 250 275 300 40 129	Use Temp., °C Min. Temp. to 40 65 100 125 150 175 200 225 250 275 300 325 40 129	Use Temp., °C Min. Temp., to 40 65 100 125 150 175 200 225 250 275 300 325 350 40 129

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line			Spec.		Type/		Class/ Condition/	Size,	P-No.
No.	Nominal Composition	Product Form	No.		Grade	UNS No.	Temper	mm	(5)
1	99.0Ni-Low C	Pipe & tube	B161			N02201	Annealed	>125	41
2	99.0Ni-Low C	Pipe & tube	B725			N02201	Annealed	>125	41
3	99.0Ni	Pipe & tube	B161			N02200	Annealed	>125	40
4	99.0Ni	Pipe & tube	B725			N02200	Annealed	>125	41
5	99.0Ni-Low C	Pipe & tube	B161			N02201	Annealed	≤125	41
6	99.0Ni-Low C	Pipe & tube	B725			N02201	Annealed	≤125	41
7	99.0Ni	Pipe & tube	B161			N02200	Annealed	≤125	41
8	99.0Ni	Pipe & tube	B725			N02200	Annealed	≤125	41
							M		
9	67Ni-30Cu	Pipe & tube	B165			N04400	Annealed	>125	42
10	67Ni-30Cu	Pipe & tube	B725			N04400	Annealed	>125	42
11	33Ni-42Fe-21Cr	Pipe & tube	B407			N08800	H.F. or H.F.		45
						X	ann.		
12	72Ni-15Cr-8Fe	Pipe & tube	B167		"LEV	N06600	H.F. or H.F. ann.	>125	43
13	33Ni-42Fe-21Cr	Pipe & tube	B407	 ~e	SOL.	N08810	C.D. sol. ann. or H.F. ann.		45
14	33Ni-42Fe-21Cr	Pipe & tube	B514	O)		N08810	Annealed		45
15	33Ni-42Fe-21Cr-Al-Ti	Pipe & tube	B407			N08811	C.D. sol. ann. or H.F.		45
		×					ann.		
1.0	(7N: 20C.	Dina 8 tuka	D165			NO4400	Annealed	≤125	42
	67Ni-30Cu 67Ni-30Cu	Pipe & tube Pipe & tube	D105			N04400 N04400	Annealed	≤125 ≤125	42 42
	26Ni-22Cr-5Mo-Ti	Pipe & tube	B619			N04400 N08320	Sol. ann.		45
	26Ni-22Cr-5Mo-Ti	Pipe & tube	B622			N08320	Sol. ann.		45
	99.0Ni-Low C	Pipe & tube	B161			N02201			43
21	99.0Ni-Low C	Pipe & tube	B725			N02201			41
22	33Ni-42Fe-21Cr	Pipe & tube	B514			N08800	Annealed		45
23		Pipe & tube	B167			N06600	H.F. or H.F.	 ≤125	43
23	72NI-13CI-01-6	The & tube	D107			NOOOOO	ann.	5125	43
24	72Ni-15Cr-8Fe	Pipe & tube	B167			N06600	C.D. ann.	>125	43
	140	·							
25	33Ni-42Fe-21Cr	Pipe & tube	B407			N08800	C.D. ann.		45
	31Ni-31F6-29Cr-Mo	Pipe & tube	B668			N08028	Sol. ann.		45
		Pipe & tube	B161			N02200	Str. rel.		41
28	99.0Ni	Pipe & tube	B725			N02200	Str. rel.		41
	35Ni-35Fe-20Cr-Cb	Pipe & tube	B464			N08020	Annealed		45
	35Ni-35Fe-20Cr-Cb	Pipe & tube	B474			N08020	Annealed		45
	35Ni-35Fe-20Cr-Cb	Pipe & tube	B729			N08020	Annealed		45
32	42Ni-21.5Cr-3Mo-2.3Cu	Smls. tube	B163			N08825	Annealed		45
33	42Ni-21.5Cr-3Mo-2.3Cu	Pipe & tube	B423			N08825	C.D. ann.		45
34	42Ni-21.5Cr-3Mo-2.3Cu	Pipe & tube	B474			N08825	Annealed		45
35	42Ni-21.5Cr-3Mo-2.3Cu	Wld. tube	B704			N08825	Annealed		45

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				•	•	Basic All	owable S	tress, S,		Metal T [4b]]	empera	iture,°C	[Notes	(1) and
Line	N	Min. Temp.,	Min. Tensile Str.,	Min. Yield Str.,	Max. Use Temp.,	Min. Temp. to	. -	400	405	450	455	200	005	250
No.	Notes	°C (6)	MPa	MPa	°C	40	65	100	125	150	175	200	225	250
1		-198	345	69	649	46.0	44.7	43.9	43.6	43.3	43.2	43.2	43.2	43.2
2		-198	345	69	649	46.0	44.7	43.9	43.6	43.3	43.2	43.2	43.2	43.2
3		-198	379	83	316	55.2	55.2	55.2	55.2	55.2	55.2	55.2	5 5.2	55.2
4 5		-198 -198	379	83 83	316 649	55.2	55.2 53.8	55.2 52.8	55.2 52.3	55.2 51.9	55.2	55.2 51.6	55.2 51.6	55.2 51.6
			345			55.2					51.7	7		
6		-198	345	83	649	55.2	53.8	52.8 68.9	52.3 68.9	51.9	5 1. 7 68.9	51.6 68.9	51.6	51.6
7		-198 100	379	103	316	68.9	68.9			68.9	68.9		68.9	68.9
8		-198	379	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
9		-198	483	172	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4	90.4
10		-198	483	172	482	115	106	99.7	96,2	93.6	91.9	90.9	90.4	90.4
11		-198	448	172	816	115	115	115	115	115	115	115	115	115
12		-198	517	172	649	115	115	115	115	115	115	115	115	115
13	(62)	-198	448	172	899	115	(115	115	115	115	115	115	115	115
						~	ું ડ							
14	(62)	-198	448	172	899	1115	115	115	115	115	115	115	115	115
	(62)	-198	448	172	899	115	115	115	115	115	115	115	115	115
					707									
16		-198	483	193	482	129	119	112	108	105	103	102	101	101
17		-198	483	193	482	129	119	112	108	105	103	102	101	101
18		-198	517	193	427	129	129	129	129	129	129	129	129	129
19		-198	517	193	427	129	129	129	129	129	129	129	129	129
20		-198	414	207	316	138	138	138	137	137	137	137	137	136
21		-198	414	207	316	138	138	138	137	137	137	137	137	136
22		-198	3 17	207	816	138	138	138	138	138	138	138	138	138
23		-198	552	207	649	138	138	138	138	138	138	138	138	138
24		-198	552	207	649	138	138	138	138	138	138	138	138	138
25	(61)	-198	517	207	816	138	138	138	138	138	138	138	138	138
26	col.	-198	505	215	454	143	143	143	143	143	143	143	143	143
27	\	-198	448	276	316	149	149	149	149	149	149	149	149	148
28		-198	448	276	316	149	149	149	149	149	149	149	149	148
29		-198	552	241	427	161	161	161	161	161	161	161	161	161
30		-198	552	241	427	161	161	161	161	161	161	161	161	161
31		-198	552	241	427	161	161	161	161	161	161	161	161	161
32		-198	585	240	538	161	161	161	161	161	161	161	161	161
33		-198	585	240	538	161	161	161	161	161	161	161	161	161
34		-198	585	240	538	161	161	161	161	161	161	161	161	161
35		-198	585	240	538	161	161	161	161	161	161	161	161	161
	I '	_,,			- 50									

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			Basic A	Allowable	Stress, S	, MPa, at	Metal Ten	ıperatur	e, °C [<mark>Not</mark>	es (1) an	d (4b)]		
Line No.	275	300	325	350	375	400	425	450	475	500	525	550	575
1	43.2	43.2	43.1	42.9	42.6	42.1	41.5	40.7	33.1	27.4	22.8	18.7	15.6
2	43.2	43.2	43.1	42.9	42.6	42.1	41.5	40.7	33.1	27.4	22.8	18.7	15.6
3	55.2	55.2	55.2										2
4	55.2	55.2	55.2									🔿	0,,
5	51.6	51.6	51.6	51.5	51.2	50.7	49.9	41.4	33.1	27.4	22.8	18.7	15.6
6	51.6	51.6	51.6	51.5	51.2	50.7	49.9	41.4	33.1	27.4	22.8	18.7	15.6
7	68.9	68.9	68.9									ල <u>`</u>	
8	68.9	68.9	68.9								NEX		
9	90.4	90.4	90.4	90.4	89.8	89.0	88.0	79.7	59.9	55.2	W.		
10	90.4	90.4	90.4	90.4	89.8	89.0	88.0	79.7	59.9	55.2			•••
11	115	115	115	115	115	115	115	115	115	115	 115	 113	 107
11	113	113	113	113	113	113	113	113	113	113	113	113	107
12	115	115	115	115	115	115	115	115	115	84.8	58.4	39.7	27.0
13	115	115	113	110	108	106	104	102	100	98.6	97.1	95.7	91.8
								No.					
14	115	115	113	110	108	106	104	102	100	98.6	97.1	95.7	91.8
15	115	115	113	110	108	106	104	102	100	98.6	97.1	95.7	92.5
16	101	101	101	101	100	99.6	98.6	79.7	59.9	55.2			
17	101	101	101	101	100	99.6	98.6	79.7	59.9	55.2			
18	129	129	127	125	122	121	119	119					
19	129	129	127	125	122	121	119	119					
20	135	133	130	()								
21	135	133	130	رن.									
22	138	138	138	138	138	138	138	138	138	138	138	136	107
23	138	138	138	138	138	138	138	138	138	84.8	58.4	39.7	27.0
24	138	138	138	138	138	138	138	138	138	84.8	58.4	39.7	27.0
25	138	138	138	138	138	138	138	138	138	138	138	136	107
26	140	137	133	130	125	122	119	116	113				
27	146	144	141										
28	146	144	141										
29	161	161	161	161	161	160	157	156					
30	161	161	161	161	161	160	157	156					
31	161	161	161	161	161	160	157	156					
32	161	161	161	161	161	160	159	158	157	156	155	153	
33	161	161	161	161	161	160	159	158	157	156	155	153	
34	161	161	161	161	161	160	159	158	157	156	155	153	
35	161	161	161	161	161	160	159	158	157	156	155	153	

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

-			Basic A	Allowable	Stress, S	, MPa, at	Metal Te	mperatur	e, °C [<mark>Not</mark>	es (1) an	d (4b)]		
ine Io.	600	625	650	675	700	725	750	775	800	825	850	875	90
1	12.9	10.0	8.27										
2	12.9	10.0	8.27										
3													
4												-0/	
5			 9.27	•••								الم	
	12.9	10.0	8.27								O) [*]	•••
6	12.9	10.0	8.27								0,		
7										,	$\phi_{\mathcal{O}}$		
8											,		
9										SM.			
10									ç				
11	83.8	63.9	44.7	29.8	15.5	11.7	8.68	7.20	6.25	5.11			
12	19.2	15.0	13.8), "				
13	75.7	62.6	50.6	41.2	33.6	27.7	22.6	18.3	15.0	11.9	9.03	7.35	5.8
							we						
14	75.7	62.6	50.6	41.2	33.6	27.7	22.6	18.3	15.0	11.9	9.03	7.35	5.8
15	84.5	69.5	56.7	46.8	38.5	31.5	25.5	20.7	17.0	13.9	11.2	9.33	7.5
16 17					Cilic								
18					•								
				N									
19	•••			رق کی							•••	•••	
20				O									
21) *									
22	83.8	63.9	44.7	29.8	15.5	11.7	8.68	7.20	6.25	5.11			
23	19.2	15.0	13.8										
24	19.2	15.0	13.8										
25	83.8	63.9	44.7	29.8	15.5	11.7	8.68	7.20	6.25	5.11			
26	5												
27	>												
28													
29													
30													••
31				•••			•••	•••			•••	•••	
32													
33								•••				•••	
34													

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

							Class/		
Line No.	Nominal Composition	Product Form	Spec. No.		Type/ Grade	UNS No.	Condition/ Temper	Size, mm	P-No. (5)
36	42Ni-21.5Cr-3Mo-2.3Cu	Pipe & tube	B705			N08825			45
37	47Ni-22Cr-19Fe-6Mo	Pipe & tube	B619			N06007	Sol. ann.	1	45
38	47Ni-22Cr-19Fe-6Mo	Pipe & tube	B622			N06007	Sol. ann.		45
39	40Ni-29Cr-15Fe-5Mo	Pipe & tube	B619			N06030	Sol. ann.		45
40	40Ni-29Cr-15Fe-5Mo	Pipe & tube	B622			N06030	Sol. ann.	, j	45
41	40Ni-29Cr-15Fe-5Mo	Pipe & tube	B626			N06030	Sol. ann		45
42	72Ni-15Cr-8Fe	Pipe & tube	B167			N06600	C.D. ann.	≤125	43
43	72Ni-15Cr-8Fe	Pipe & tube	B517			N06600	C.D. ann.		43
44	58Ni-29Cr-9Fe	Tube	B163			N06690	Annealed	≤75	43
45	58Ni-29Cr-9Fe	Pipe & tube	B167			N06690	C.D. ann.	≤125	43
46	37Ni-33Fe-25Cr	Pipe & tube	B163			N08120	Sol. ann.		45
47	37Ni-33Fe-25Cr	Pipe & tube	B407		. ?`	N08120	Sol. ann.		45
48	37Ni-33Fe-25Cr	Pipe & tube	B514			N08120	Sol. ann.		45
49	37Ni-33Fe-25Cr	Pipe & tube	B515		XO.	N08120	Sol. ann.		45
50	61Ni-16Mo-16Cr	Pipe & tube	B619	Ne)	N06455	Sol. ann.		43
51	47Ni-22Cr-9Mo-18Fe	Pipe & tube	B619			N06002	Sol. ann.		43
52	47Ni-22Cr-9Mo-18Fe	Pipe & tube	B622			N06002	Sol. ann.		43
53	31Ni-33Fe-27Cr-6.5Mo- Cu-N	Pipe & tube	В619			N08031	Annealed		45
54	31Ni-33Fe-27Cr-6.5Mo- Cu-N	Pipe & tube Pipe & tube Pipe & tube	B622			N08031	Annealed		45
55	61Ni-16Mo-16Cr	Pipe & tube	B622			N06455	Sol. ann.		43
56	54Ni-16Mo-15Cr	Pipe & tube	B619			N10276	Sol. ann.		43
57	54Ni-16Mo-15Cr	Pipe & tube	B622			N10276	Sol. ann.		43
58	54Ni-16Mo-15Cr	Pipe & tube	B626			N10276	Sol. ann.		43
59	67Ni-30Cu	Pipe & tube	B165			N04400	Str. rel.		42
	67Ni-30Cu	Pipe & tube	B725			N04400	Str. rel.		42
00	07141-30Cd	Tipe & tube	D7 23			1104400	Str. rei.		72
61	46Fe-24Ni-21Cr-6Mo- Cu-N	Pipe & tube	B675			N08367	Annealed	>5	45
62	46Fe-24Ni-21Cr-6Mo- Cu-N	Pipe & tube	B690			N08367	Annealed	>5	45
63	46Fe-24Ni-21Cr-6Mo- Cu-N	Pipe & tube	B804			N08367	Annealed	>5	45
64	46Fe-24Ni-21Cr-6Mo- Cu-N	Pipe & tube	B675			N08367	Annealed	≤5	45
65	46Fe-24Ni-21Cr-6Mo- Cu-N	Pipe & tube	B690			N08367	Annealed	≤5	45
66	46Fe-24Ni-21Cr-6Mo- Cu-N	Pipe & tube	B804			N08367	Annealed	≤5	45
67	55Ni-21Cr-13.5Mo	Pipe & tube	B619			N06022	Sol. ann.		43

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	in rarentine.	ses Refer to r	10103 101 11	урсник т		owable St		MPa, at					
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225	250
36		-198	585	240	538	161	161	161	161	161	161	161	161	161
		1,0	555	2.0	555	101	101	101	101	101	101	101	101	101
37		-198	621	241	538	161	161	161	161	161	161	161	2 161	161
38		-198	621	241	427	161	161	161	161	161	161	161	161	161
39		-198	586	241	427	161	161	161	161	161	161	161	157	154
40		-198	586	241	427	161	161	161	161	161	161	161	157	154
41		-198	586	241	427	161	161	161	161	161	161	161	157	154
42		-198	552	241	649	161	161	161	161	161	2 161	161	161	161
43		-198	552	241	649	161	161	161	161	161	161	161	161	161
44		-198	586	241	482	160	160	160	160	160	160	160	160	160
45		-198	586	240	482	160	160	160	160	160	160	160	160	160
									3					
46		-198	621	276	899	184	184	184	184	184	184	184	180	175
47		-198	621	276	899	184	184	184	184	184	184	184	180	175
48		-198	621	276	899	184	184	184	184	184	184	184	180	175
49		-198	621	276	899	184	184	184	184	184	184	184	180	175
50		-198	689	276	427	184	² 184	184	184	184	184	184	184	184
						181								
51		-198	689	276	816	184	184	184	184	184	184	184	184	178
52		-198	689	276	816		184	184	184	184	184	184	184	178
53		-198	648	276	427	184	184	184	184	184	177	171	166	162
00		170	0.10	2.0	./- <u>.</u>	101	101	101	101	101			100	102
54		-198	648	276	427	184	184	184	184	184	177	171	166	162
				.0										
55		-198	689	276	427	184	184	184	184	184	184	184	184	184
			_c C											
56		-198	689	283	677	188	188	188	188	188	188	188	188	187
57		-198	689 *	283	677	188	188	188	188	188	188	188	188	187
58		-198	689	283	677	188	188	188	188	188	188	188	188	187
		and the same of th	V											
	(54)	-198	586	379	260	195	195	195	195	195	195	195	195	195
60	(54)	-198	586	379	260	195	195	195	195	195	195	195	195	195
61	M	-198	655	310	427	207	207	207	207	206	202	198	195	192
62	S.	-198	655	310	427	207	207	207	207	206	202	198	195	192
02	Y	-190	033	310	427	207	207	207	207	200	202	190	195	192
63		-198	655	310	427	207	207	207	207	206	202	198	195	192
64		-198	689	310	427	207	207	207	207	206	202	198	195	192
65		-198	689	310	427	207	207	207	207	206	202	198	195	192
		400		0.10	40-	0.0-	0.5-	0.0-	0.0-	0.5.5	0		4	400
66		-198	689	310	427	207	207	207	207	206	202	198	195	192
67		-198	689	310	427	207	207	207	207	207	207	207	204	202
67		-130	007	210	44/	207	207	407	207	207	207	207	204	202

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

										es (1) and			
-			Dasic A	mowabie	Ju 535, 3	, mra, al	1-1-ctal 161	mperatur	e, e [NOL	vs (1) all	ı (TUJ]		
Line													
No.	275	300	325	350	375	400	425	450	475	500	525	550	575
36	161	161	161	161	161	160	159	158	157	156	155	153	
													Co
37	160	158	156	154	153	152	151	150	149	136	132	130	V.50
38	160	158	156	154	153	152	151	150					>
39	151	148	146	143	141	138	136	136				્જો	
40	151	148	146	143	141	138	136	136				3/	
41	151	148	146	143	141	138	136	136				20.7	
42	161	161	161	161	161	161	161	161	161	84.8	58.4	39.7	27.0
43 44	161 160	161 160	161 160	161 160	161	161 160	161 160	161 160	161 160	84.8 160	58.4	39.7	27.0
					160					1	<i></i>		
45	160	160	160	160	160	160	160	160	160	160			
46	170	166	163	160	158	156	154	153	153	152	151	151	151
47	170	166	163	160	158	156	154	153	153	152	151	151	151
48	170	166	163	160	158	156	154	153	153	152	151	151	151
49	170	166	163	160	158	156	154	153	153	152	151	151	151
50	184	184	184	184	183	180	178	178					
30	104	104	104	104	103	100	170	Histo				•••	
51	173	169	165	162	160	158	157	155	154	135	134	133	129
52	173	169	165	162	160	158	157	155	154	135	134	133	129
53	158	155	152	149	74.2	61.1	9 50.3	49.6					
						40:							
54	158	155	152	149	74.2	61.1	50.3	49.6					
55	184	184	184	184	182	180	178	178					
	101	101	10.	101	Off.	100	1.0	1,0					
56	183	177	172	169 🤇	165	162	159	157	156	155	154	143	118
57	183	177	172	169	165	162	159	157	156	155	154	143	118
58	183	177	172	169	165	162	159	157	156	155	154	143	118
5 0	105		ON!										
59	195												
60	195		O										
61	188	183	179	176	172	170	160	167					
01	100	1900	1/9	176	173	170	168	107					
62	188	183	179	176	173	170	168	167					
	•												
63	188	183	179	176	173	170	168	167					
C 4	100	102	170	176	172	170	160	167					
64	188	183	179	176	173	170	168	167					
65	188	183	179	176	173	170	168	167					
	400	400	450	454	450	450	4.00	4.5					
66	188	183	179	176	173	170	168	167					
67	197	193	189	185	182	180	177	177					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

-			Basic A	Allowable	Stress, S	, MPa, at	Metal Te	emperatur	e, °C [Not	tes (1) an	d (4b)]		
Line No.	600	625	650	675	700	725	750	775	800	825	850	875	900
36													
37												\&)
38												~O,/	
39											0		
40											, , , ;) 	
41											~ე``		
42	19.2	15.0	13.8							(,	V		
43	19.2	15.0	13.8										
44										5			
45													
46	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
47	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
48	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
49	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
50							*10	3					
51	115	94.2	77.3	64.9	54.7	44.7.	36.1	29.2	23.6	20.7			
52	115	94.2	77.3	64.9	54.7	44.7	36.1	29.2	23.6	20.7		•••	
53					34.7	×O						•••	
33	•••					F	•••	•••					
54					Clic								
55				ال									
56	99.1	81.6	67.0	54.6	42.2								
57	99.1	81.6	67.0	54.6	42.2								
58	99.1	81.6	67.0	54.6	42.2								
59													
60	•••	.0			•••		•••	•••				•••	•••
		4					•••						
61	Call												
62	جي. کي.												
	•												
63													
64													
65													
66													
67													

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line			Spec.	Type/		,	Size,	P-No.
No.	Nominal Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
68	55Ni-21Cr-13.5Mo	Pipe & tube	B622		N06022	Sol. ann.		43
69	58Ni-33Cr-8Mo	Pipe & tube	B619		N06035	Sol. ann.		43
	58Ni-33Cr-8Mo	Pipe & tube	B622		N06035	Sol. ann.	/	43
71	58Ni-33Cr-8Mo	Pipe & tube	B626		N06035	Sol. ann.	2.JO	43
72	59Ni-23Cr-16Mo	Pipe & tube	B619		N06059	Sol. ann.	·	43
73	59Ni-23Cr-16Mo	Pipe & tube	B622		N06059	Sol. ann		43
74	59Ni-23Cr-16Mo-1.6Cu	Pipe & tube	B619		N06200	Sol. ann.	All	43
75	59Ni-23Cr-16Mo-1.6Cu	Pipe & tube	B622		N06200	Sol. ann.	All	43
76	59Ni-23Cr-16Mo-1.6Cu	Pipe & tube	B626		N06200	Sol. ann.	All	43
77	62Ni-22Mo-15Cr	Pipe & tube	B619		N10362	Sol. ann.	All	43
78	62Ni-22Mo-15Cr	Pipe & tube	B622		N10362	Sol. ann.	All	43
79	62Ni-22Mo-15Cr	Pipe & tube	B626		N10362	Sol. ann.	All	43
80	62Ni-28Mo-5Fe	Pipe & tube	B619	🔷	N10001	Sol. ann.		44
81	62Ni-28Mo-5Fe	Pipe & tube	B622		N10001	Sol. ann.		44
82	65Ni-28Mo-2Fe	Pipe & tube	B619		N10665	Sol. ann.		44
83	65Ni-28Mo-2Fe	Pipe & tube	B622	CO.	N10665	Sol. ann.		44
84	65Ni-29.5Mo-2Fe-2Cr	Pipe & tube	B619	<u></u>	N10675	Sol. ann.		44
85	65Ni-29.5Mo-2Fe-2Cr	Pipe & tube	B622		N10675	Sol. ann.		44
86	65Ni-29.5Mo-2Fe-2Cr	Pipe & tube	B626		N10675	Sol. ann.		44
		Pipe & tube						
87	60Ni-22Cr-9Mo-3.5Cb	Pipe & tube	B444	1	N06625	Annealed		43
88	60Ni-22Cr-9Mo-3.5Cb	Pipe & tube	B705	1	N06625	Annealed		43
89	57Ni-22Cr-14W-2Mo-La	Pipe & tube	B619		N06230	Sol. ann.		43
90	57Ni-22Cr-14W-2Mo-La		B622		N06230	Sol. ann.		43
91	57Ni-22Cr-14W-2Mo-La	Pipe & tube	B626		N06230	Sol. ann.		43
92	33Cr-31Ni-32Fe-1.5Mo-	Pipe	B619		R20033	Sol. ann.		45
	0.6Cu-N	100						
	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	Pipe & tube	B622		R20033	Sol. ann.		45
94	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	Tube	B626		R20033	Sol. ann.		45
95	99.0Ni-Low-C	Plate	B162		N02201	H.R. ann.		41
	99.0Ni-Low C	Plate	B162			H.R. as R.		41
	99.0Ni	Plate	B162			H.R. ann.		41
	99.0Ni	Plate	B162			H.R. as R.		41
	33Ni-42Fe-21Cr	Pl. & sht.	B409			Annealed	All	45
	33Ni-42Fe-21Cr-Al-Ti	Pl. & sht.	B409			Annealed	All	45
	26Ni-22Cr-5Mo-Ti	Pl. & sht.	B620		N08320	Sol. ann.	All	45
	67Ni-30Cu	Plate	B127		N04400	H.R. ann.		42
	47Ni-22Cr-19Fe-6Mo	Pl. & sht.	B582		N06007	Sol. ann.	>19	45
104	33Ni-42Fe-21Cr	Pl. & sht.	B409		N08800	Annealed	All	45

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	in Tarenthes	ses Refer to 1	Notes for A	ppenaix A	Basic Allo			MPa, at	Metal T				
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	[4b)] 150	175	200	225	250
68		-198	689	310	427	207	207	207	207	207	207	207	204	202
69		-198	586	241	427	161	161	161	161	161	161	154	149	144
70		-198	586	241	427	161	161	161	161	161	161		2 149	144
		-198	586	241	427	161	161	161	161	161	161	154	149	144
, -		1,0	500		127	101	101	101	101	101	n	\V.		
72		-198	689	310	427	207	207	207	207	207	207	207	207	206
73		-198	689	310	427	207	207	207	207	207	207	207	207	206
74		-198	689	310	427	207	207	207	207	207	207	207	207	200
75		-198	689	310	427	207	207	207	207	207	207	207	207	200
76		-198	689	310	427	207	207	207	207	207	207	207	207	200
77		-198	725	310	427	207	207	207	207	207	207	204	202	199
78		-198	725	310	427	207	207	207	207	207	207	204	202	199
79		-198	725	310	427	207	207	207	207	207	207	204	202	199
80		-198	689	310	427	207	207	207	207	207	207	207	207	207
81		-198	689	310	427	207	207	207	207	207	207	207	207	207
		-198	758	352	427	234	234	234	234	234	234	234	234	234
		-198	758	352	427	234	234	234	234	234	234	234	234	234
		-198	758	352	427	234	234	234	234	234	234	234	234	234
~ -		-198	758	352	427	234	234	234	234	234	234	234	234	234
86		-198	758	352	427	234	234	234	234	234	234	234	234	234
00		170	750	332	XO.	201	201	201	201	201	201	201	201	201
	(64)(70)	-198	827	414	649	276	276	276	274	273	272	270	269	267
88	(64)(70)	-198	827	414	649	276	276	276	274	273	272	270	269	267
89		-198	758	310	899	207	207	207	207	207	207	207	207	207
90		-198	758	310	899	207	207	207	207	207	207	207	207	207
91		-198	758	310	899	207	207	207	207	207	207	207	207	207
92		-198	Q50°	380	427	250	231	209	200	193	187	181	176	172
93		-198	750	380	427	250	231	209	200	193	187	181	176	172
94		-198	750	380	427	250	231	209	200	193	187	181	176	172
95	cM	-198	345	83	649	55.2	53.8	52.8	52.3	51.9	51.7	51.6	51.6	51.6
96	\(\sigma_{j}\)	-198	345	83	649	55.2	53.8	52.8	52.3	51.9	51.7	51.6	51.6	51.6
97		-198	379	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
		-198	379	138	316	91.9	91.9	91.9	91.9	91.9	91.9	91.9	91.9	91.9
99		-198	448	172	899	115	115	115	115	115	115	115	115	115
100		-198	448	172	899	115	115	115	115	115	115	115	115	115
200	•		1.0		0,,	110		110	_10		-10	-20	110	
101		-198	517	193	427	129	129	129	129	129	129	129	129	129
102		-198	483	193	482	129	119	112	108	105	103	102	101	101
103		-198	586	207	538	138	138	138	138	138	138	138	138	138
104		-198	517	207	816	138	138	138	138	138	138	138	138	138

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

									e, °C [Not				
Line No.	275	300	325	350	375	400	425	450	475	500	525	550	575
68	197	193	189	185	182	180	177	177					
69	140	137	135	133	132	131	129	128					
70	140	137	135	133	132	131	129	128					2
71	140	137	135	133	132	131	129	128				(0;
72	202	197	192	188	184	180	176	176				Y	
73	202	197	192	188	184	180	176	176				ري ساري	
74	194	188	184	180	177	175	174	173			/×		
75	194	188	184	180	177	175	174	173					
76	194	188	184	180	177	175	174	173		C			
77	197	193	190	188	186	184	182	180		ج			
78	197	193	190	188	186	184	182	180		0			
79	197	193	190	188	186	184	182	180					
80	207	207	207	207	207	207	206	206					
81	207	207	207	207	207	207	206	206					
82	234	234	234	234	234	234	234	234	7. "				
83	234	234	234	234	234	234	234	234					
84	234	234	234	234	234	233	231	230					
85	234	234	234	234	234	233	231	230					
86	234	234	234	234	234	233	231	230					
						×	0						
87	265	262	260	257	255	252	251	249	247	245	242	215	194
88	265	262	260	257	255	252	251	249	247	245	242	215	194
89	207	207	203	199	197 •	196	195	195	195	195	195	195	183
90	207	207	203	199	197	196	195	195	195	195	195	195	183
91	207	207	203	199 🦰	1 97	196	195	195	195	195	195	195	183
				()								
92	169	165	163	(161)	159	157	156	155					
93	169	165	163	161	159	157	156	155					
94	169	165	163	161	159	157	156	155					
		W.											
95	51.6	51.6	51.6	51.5	51.2	50.7	49.9	41.4	33.1	27.4	22.8	18.7	15.6
96	51.6	51.6	51.6	51.5	51.2	50.7	49.9	41.4	33.1	27.4	22.8	18.7	15.6
97	68.9	68.9	68.9										
98	91.9	91.9	91.9										
99	115	115	113	110	108	105	104	102	100	98.6	97.1	95.9	91.8
100	115	115	113	110	108	105	104	102	100	98.6	97.1	96.1	94.1
101	129	129	127	125	122	121	119	119					
102	101	101	101	101	100	99.6	98.6	79.7	59.9	55.2			
103	138	135	134	132	131	130	129	128	128	127	127	126	
104	138	138	138	138	138	138	138	138	138	138	138	136	107

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

-			Basic A	Allowable	Stress, S	, MPa, at	Metal Te	mperatur	e, °C [Not	es (1) an	d (4b)]		
Line No.	600	625	650	675	700	725	750	775	800	825	850	875	900
68													
69													
70												%	
71												JO,	
72				•••							~ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \)	
73											0,5		
74										(/			
75													
76										5			
77									<u>ç</u>				
78									, 0				
79													
80								0	>				
81													
82								<i>(1)</i> ,					
83							~e	,					
84							111.						
85							N						
86						11							
00				•••		×O							
87	156	136	91.0			F							
88	156	136	91.0		Silv								
89	153	128	107	89.7	• 74.7	61.9	50.8	 41.1	32.6	25.2	 18.9	13.8	10.2
90	153	128	107	89.7	74.7	61.9	50.8	41.1	32.6	25.2	18.9	13.8	10.2
91	153	128	107	89.7	74.7	61.9	50.8	41.1	32.6	25.2	18.9	13.8	10.2
91	133	120	- 107	C.	74.7	01.9	30.0	41.1	32.0	23.2	10.9	13.0	10.2
92			20										
93		2											
94		40,											
95	12.9	10.0	8.27										
96	12.9	10.0	8.27										
97	•												
98													
99	75.7	62.6	50.6	41.2	33.6	27.7	22.6	18.3	15.0	11.9	9.03	7.35	5.86
100	85.5	69.3	56.8	46.8	38.6	31.5	25.5	20.6	17.1	13.8	10.7	7.98	6.20
101													
102													
103													
104	83.8	63.9	44.7	29.8	15.5	11.7	8.68	7.20	6.25	5.11			

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.		Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
105	-	Pl. & sht.	B709			N08028	Sol. ann.	All	45
106	42Ni-21.5Cr-3Mo-2.3Cu	Plate	B424			N08825	Annealed		45
107	35Ni-35Fe-20Cr-Cb	Pl. & sht.	B463			N08020	Annealed	All	45
108	40Ni-29Cr-15Fe-5Mo	Pl. & sht.	B582			N06030	Sol. ann.	All	45
109	47Ni-22Cr-19Fe-6Mo	Pl. & sht.	B582			N06007	Sol. ann.	≤19	45
110	47Ni-22Cr-9Mo-18Fe	Pl. & sht.	B435			N06002	H.R sol. ann.	All	43
111	72Ni-15Cr-8Fe	Plate	B168			N06600	H.R. ann.		43
112	72Ni-15Cr-8Fe	Plate	B168			N06600	H.R. as R.		43
113	58Ni-29Cr-9Fe	Plate	B168			N06690	Annealed	≥5	43
114	58Ni-29Cr-9Fe	Sheet	B168			N06690	H.R. ann. or C.R. ann.	0.5 to 6	43
115	67Ni-30Cu	Plate	B127			N04400	H.R. as R.		42
116	37Ni-33Fe-25Cr	Pl. & sht.	B409		11/	N08120	Sol. ann.	All	45
117	31Ni-33Fe-27Cr-6.5Mo- Cu-N	Pl. & sht.	B625		FUI!	N08031	Annealed	All	45
118	61Ni-16Mo-16Cr	Pl. & sht.	B575	10,		N06455	Sol. ann.	All	43
119	54Ni-16Mo-15Cr	Pl. & sht.	B575			N10276	Sol. ann.	All	43
120	60Ni-22Cr-9Mo-3.5Cb	Plate	B443	1		N06625	Annealed	All	43
121	57Ni-22Cr-14W-2Mo-La	Pl. & sht.	B435			N06230	Sol. ann.	All	43
122	55Ni-21Cr-13.5Mo	Sheet	B575			N06022	Sol. ann.	<5	43
123	58Ni-33Cr-8Mo	Pl. & sht. Pl. & sht.	B575			N06035	Sol. ann.	All	43
124	46Fe-24Ni-21Cr-6Mo- Cu-N	Pl. & sht.	B688			N08367	Annealed	>5	45
125	46Fe-24Ni-21Cr-6Mo- Cu-N	Pl. & sht.	B688			N08367	Annealed	≤5	45
126	59Ni-23Cr-16Mo	Pl. & sht.	B575			N06059	Sol. ann.	All	43
	59Ni-23Cr-16Mo-1.6Cu	Pl. & sht.	B575			N06200	Sol. ann.	All	43
128	62Ni-22Mo-15Cr	Pl. & sht.	B575			N10362	Sol. ann.	All	43
129	62Ni-28Mo-5Fe	Plate	B333			N10001	Sol. ann.	≥5, ≤64	44
	62Ni-28Mo-5Fe	Sheet	B333			N10001	Sol. ann.	≤5	44
	65Ni-28Mo-2Fe	Pl. & sht.	B333			N10665	Sol. ann.	All	44
132	65Ni-29.5Mo-2Fe-2Cr	Pl. & sht.	B333			N10675	Sol. ann.	All	44
133	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	Pl. & sht.	B625			R20033	Sol. ann.		45
134	99.0Ni-Low C	Forg. & ftg.	B160			N02201	Annealed	All	41
	99.0Ni–Low C	Forg. & ftg.	B366				Annealed	All	41
136	99.0Ni	Forg. & ftg.	B366			N02200	Annealed	All	41
	99.0Ni	Forg. & ftg.	B564				Annealed	All	41
138	33Ni-42Fe-21Cr	Forg. & ftg.	B564			NU8810	Annealed		45

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	in Parentne	ses Refer to N	iotes for A	appenaix <i>A</i>		owable St		MPa, at					
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225	250
105		-198	505	215	454	143	143	143	143	143	143	143	143	143
106	(9)	-198	585	240	538	161	161	161	161	161	161	161	161	161
107		-198	552	241	427	161	161	161	161	161	161		2 161	161
108		-198	586	241	427	161	161	161	161	161	161	161	157	154
109		-198	621	241	538	161	161	161	161	161	161	161	161	161
110		-198	655	241	427	161	161	161	161	161	161	161	161	156
											3°			
111		-198	552	241	649	161	161	161	161	161	161	161	161	161
112		-198	586	241	649	161	161	161	161	161	161	161	161	161
113		-198	586	240	482	160	160	160	160	160	160	160	160	160
114		-198	586	240	482	160	160	160	160	160	160	160	160	160
								6) ,					
115		-198	517	276	482	172	172	172	171	170	168	165	164	162
116		-198	621	276	899	184	184	184	184	184	184	184	180	175
117		-198	648	276	427	184	184	184	184	184	177	171	166	162
118		-198	689	276	427	184	7 184	184	184	184	184	184	184	184
		-198	689	283	677	188	188	188	188	188	188	188	188	187
	(64)(70)	-198	758	379	649	253	253	253	251	250	249	248	247	245
121		-198	758	310	899	207	207	207	207	207	207	207	207	207
122		-198	689	310	427	207	207	207	207	207	207	207	204	202
123		-198	586	241	427	161	161	161	161	161	161	154	149	144
				C,										
124		-198	655	310	427	207	207	207	207	206	202	198	195	192
125		-198	689	310	427	207	207	207	207	207	207	206	199	193
126		-198	689	310	427	207	207	207	207	207	207	207	207	206
127		-198	689	310	427	207	207	207	207	207	207	207	207	200
128		-198	725	310	427	207	207	207	207	207	207	204	202	199
129		198	689	310	427	207	207	207	207	207	207	207	207	207
130		-198	793	345	427	230	230	230	230	230	230	230	230	230
131		-198	758	352	427	234	234	234	234	234	234	234	234	234
132	"SN.	-198	758	352	427	234	234	234	234	234	234	234	234	234
133		-198	750	380	427	250	231	209	200	193	187	181	176	172
134	(9)(9a)	-198	345	69	649	46.0	44.7	43.9	43.6	43.3	43.2	43.2	43.2	43.2
135	(32)(74)	-198	345	69	649	46.0	44.7	43.9	43.6	43.3	43.2	43.2	43.2	43.2
136	(32)(74)	-198	380	105	260	70.0	70.0	70.0	70.0	70.0	70.0	70.0	70.0	70.0
137		-198	379	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
138	(9)	-198	448	172	899	115	115	115	115	115	115	115	115	115

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						, MPa, at							
Line No.	275	300	325	350	375	400	425	450	475	500	525	550	575
105	140	137	133	130	125	122	119	116	113				
106	161	161	161	161	161	160	159	158	157	156	155	153	
107	161	161	161	161	161	160	157	156					2
108	151	148	146	143	141	138	136	136					0
109	160	158	156	154	153	152	151	150	149	136	132	130	
110	152	148	145	142	140	138	137	137					
												ල ` (ද	
111	161	161	161	161	161	161	161	161	161	84.8	58,4	39.7	27.0
112	161	161	161	161	161	161	161	161	161	84.8	58.4	39.7	27.0
113	160	160	160	160	160	160	160	160	160	160	5/2		
114	160	160	160	160	160	160	160	160	160	160			
									,	0			
115	161	160	159	158	156	136	102	63.8	33.5	27.6			
116	170	166	163	160	158	156	154	153	153	152	151	151	151
117	158	155	152	149	146	144	141	140	7. "				
								we.					
118	184	184	184	184	182	180	178	176					
119	183	177	172	169	165	162	159	157	156	155	154	143	118
120	243	241	238	236	233	231	230	228	227	225	222	215	194
121	207	207	203	199	197	196 🔪	195	195	195	195	195	195	183
122	197	193	189	185	182	180	177	177					
123	140	137	135	133	132	131	129	128		•••	•••		•••
						O.							
124	188	183	179	176	173	170	168	167					
405	100	100	450	456	O ₂₀	450	160	465					
125	188	183	179	176	173	170	168	167	•••	•••	•••		•••
126	202	197	192	188	184	180	176	176					
127	194	188	184	180	177	175	174	173					
128	197	193	190	188	186	184	182	180	•••	•••	•••		
129	207	207	207	207	207	207	206	206	•••	•••	•••	•••	•••
130	230	230	230	230	230	230	229	229					•••
131	234	234	234	234	234	234	234	234		•••			
131	234	234	234	234	234	233	231	230					
132	234	234	234	234	234	233	231	230		•••			
133	169	165	163	161	159	157	156	155					
133	109	103	103	101	139	137	130	133					
134	43.2	43.2	43.1	42.9	42.6	42.1	41.5	40.7	33.1	27.4	22.8	18.7	15.6
135	43.2	43.2	43.1	42.9	42.6	42.1	41.5	40.7	33.1	27.4	22.8	18.7	15.6
136	70.0												
137	68.9	68.9	68.9	•••						•••			
138	115	115	113	110	108	105	104	102	100	98.6	97.1	95.9	91.8

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			Basic A	Allowable	Stress, S	, MPa, at	Metal Te	mperatur	e, °C [<mark>Not</mark>	es (1) an	d (4b)]		
Line No.	600	625	650	675	700	725	750	775	800	825	850	875	900
105													
106													
107												1	
108												00	
109											O) V	
110													
111	19.2	15.0	13.8							(\(\)		
112	19.2	15.0	13.8							- RAIL			
113										S)			
114									4 01				
115) `				
116	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
117													
118							KLI						
119	99.1	81.6	67.0	54.6	42.2		N						
120	156	136	91.0										
121	153	128	107	89.7	74.7	61.9	50.8	41.1	32.6	25.2	18.9	13.8	10.2
122					>	F							
123	•••				Cill					•••			
124				N									
125				CO.									
126													
127			" O"										
128			71,										
129		.0											
130		4											
131	NY												
132	Simi			•••	•••								
133													
134	12.9	10.0	8.27										
135	12.9	10.0	8.27										
136													
137													
138	75.7	62.6	50.6	41.2	33.6	27.7	22.6	18.3	15.0	11.9	9.03	7.35	5.86

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						a		
Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
-	33Ni-42Fe-21Cr-Al-Ti	Forg. & ftg.	B564			Annealed		45
	33Ni-42Fe-21Cr	Fittings	B366			Annealed	All	45
	33Ni-42Fe-21Cr-Al-Ti	Fittings	B366			Annealed	All	45
	67Ni-30Cu	Forg. & ftg.	B564			Annealed	All	42
	67Ni-30Cu	Forg. & ftg.	B366		N04400	Annealed	- 411	42
143	0/NI-30Cu	rorg. & rtg.	Б300		N04400	Aimealeu	SAIIV	42
144	72Ni-15Cr-8Fe	Forg. & ftg.	B366		N06600	Annealed	All	43
	40Ni-29Cr-15Fe-5Mo	Forg. & ftg.	B366		N06030	Sol. ann.	All	45
	40Ni-29Cr-15Fe-5Mo	Forg. & ftg.	B462		N06030	Sol. ann.	All	45
	33Ni-42Fe-21Cr	Forg. & ftg.	B366			C.D. ann.	All	45
	33Ni-42Fe-21Cr	Forg. & ftg.	B564			Annealed		45
140	33NI-42I'E-21GI	rorg. & rtg.	D304		1100000	Aimeaieu		43
140	35Ni-35Fe-20Cr-Cb	Forg. & ftg.	B366		N08020	Annealed	All	45
	35Ni-35Fe-20Cr-Cb	Forg. & ftg.	B462		N08020	Annealed		45
	72Ni-15Cr-8Fe	Forg. & ftg.	B564	"	N06600	Annealed	 All	43
131	/2NI-13GI-0FE	roig. & itg.	D304	<i>(11)</i>	NUUUUU	Aimealeu	All	43
152	42Ni-21.5Cr-3Mo-2.3Cu	Fittings	B366	~e`	N08825	C.D. ann.	All	45
	42Ni-21.5Cr-3Mo-2.3Cu	Forgings	B564	7.	N08825	Annealed		45
	58Ni-29Cr-9Fe	Forgings	B564		N06690	Annealed	All	43
	37Ni-33Fe-25Cr	Fittings	B366		N08120	Sol. ann.	All	45
	37Ni-33Fe-25Cr	F :	NODE CA		N08120	Sol. ann.	All	45
150	37141 331 C 23G1	1 or grings	F 2301		1100120	301. 41111.	7111	15
157	47Ni-22Cr-9Mo-18Fe	Forg. & ftg. Forg. & ftg.	B366		N06002	Sol. ann.	All	43
	31Ni-33Fe-27Cr-6.5Mo-	Forg. & ftg.	B366			Sol. ann.	All	45
	Cu-N							
159	31Ni-33Fe-27Cr-6.5Mo-	Forg. & ftg.	B564	•••	N08031	Annealed	All	45
	Cu-N					H.W.		
	54Ni-16Mo-15Cr	Forg. & ftg.	B366		N10276		All	43
	54Ni-16Mo-15Cr	Forg. & ftg.	B462		N10276	Sol. ann.	All	43
162	54Ni-16Mo-15Cr	Forg. & ftg.	B564		N10276	Sol. ann.	All	43
163	62Ni-28Mo-5Fe	Forg. & ftg.	B366		N10001	Sol. ann.	All	44
	55Ni-21Cr-13.5Mo	Forg. & ftg.	B366			Sol. ann.	All	43
	55Ni-21Cr-13.5Mo	Forg. & ftg.	B462		N06022	Sol. ann.	All	43
	55Ni-21 C r-13.5Mo	Forg. & ftg.	B564		N06022	Sol. ann.	All	43
	58Ni-33Cr-8Mo	Forg. & ftg.	B366			Sol. ann.	All	43
	58Ni-33Cr-8Mo	Forg. & ftg.	B462			Sol. ann.	All	43
	58Ni-33Cr-8Mo	Forg. & ftg.	B564		N06035		All	43
	59Ni-23Cr-16Mo	Forg. & ftg.	B366		N06059	Sol. ann.	All	43
171	59Ni-23Cr-16Mo	Forg. & ftg.	B564		N06059	H.W. sol.	All	43
170	EON: 220m 16Ma 160	Forg 0 ftg	D266		NO(200	ann.	A 11	42
	59Ni-23Cr-16Mo-1.6Cu	Forg. & ftg.	B366		N06200	Sol. ann.	All	43
	59Ni-23Cr-16Mo-1.6Cu	Forg. & ftg.	B462		N06200	Sol. ann.	All	43
1/4	59Ni-23Cr-16Mo-1.6Cu	Forg. & ftg.	B564		NU6200	Sol. ann.	All	43

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	in r ar entire.	ses Reier to	votes for A	ррениіх л	Basic Allo			MPa, at	Metal T				
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	[4b)] 150	175	200	225	250
139	(9)	-198	448	172	899	115	115	115	115	115	115	115	115	115
	(9)(74)	-198	450	170	899	115	115	115	115	115	115	115	115	115
	(9)(74)	-198	450	170	899	115	115	115	115	115	115	115	2 15	115
142	(9)	-198	483	172	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4	90.4
	(32)(74)	-198	483	172	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4	90.4
											N.)		
144	(32)(74)	-198	517	172	649	115	115	115	115	115	115	115	115	115
145	(74)	-198	586	241	427	161	161	161	161	161	Q ₁₆₁	161	157	154
146		-198	586	241	427	161	161	161	161	161	161	161	157	154
147	(74)	-198	517	207	816	138	138	138	138	138	138	138	138	138
148	(9)	-198	517	207	816	138	138	138	138	138	138	138	138	138
								. (3)					
149	(74)	-198	552	241	427	161	161	161	161	161	161	161	161	161
150		-198	552	241	427	161	161		161	161	161	161	161	161
151	(9)	-198	552	241	649	161	161	161	161	161	161	161	161	161
							(1),							
152	(9)(74)	-198	585	240	538	161	161	161	161	161	161	161	161	161
153		-198	585	240	538	160	160	160	160	160	160	160	160	160
154		-198	586	241	482	2160	160	160	160	160	160	160	160	160
155		-198	621	276	899		184	184	184	184	184	184	180	175
156		-198	621	276	899	184	184	184	184	184	184	184	180	175
					Y- "									
157	(32)	-198	689	276	816	184	184	184	184	184	184	184	184	178
158	7 7	-198	648	276	427	184	184	184	184	184	177	171	166	162
	(-)			1										
159		-198	648	276	427	184	184	184	184	184	177	171	166	162
160	(74)	-198	689	283	677	188	188	188	188	188	188	188	188	187
161	(9)	-198	689	283	677	188	188	188	188	188	188	188	188	187
162	(9)	-198	689	283	677	188	188	188	188	188	188	188	188	187
163	(32)	-198	689	310	427	207	207	207	207	207	207	207	207	207
164	(32)(74)	-198	689	310	427	207	207	207	207	207	207	207	204	202
	(9)	-198	689	310	427	207	207	207	207	207	207	207	204	202
	(9)	-198	689	310	427	207	207	207	207	207	207	207	204	202
	(32)(74)	-198	586	241	427	161	161	161	161	161	161	154	149	144
168		-198	586	241	427	161	161	161	161	161	161	154	149	144
169		-198	586	241	427	161	161	161	161	161	161	154	149	144
	(74)	-198	689	310	427	207	207	207	207	207	207	207	207	206
171		-198	689	310	427	207	207	207	207	207	207	207	207	206
-/1		270	557	010	,	-57	-57	_0,	_0,	_,,	_3,	_0,	_0,	_50
172	(74)	-198	689	310	427	207	207	207	207	207	207	207	207	200
173		-198	689	310	427	207	207	207	207	207	207	207	207	200
174		-198	689	310	427	207	207	207	207	207	207	207	207	200

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						, MPa, at							
Line No.	275	300	325	350	375	400	425	450	475	500	525	550	575
139	115	115	113	110	108	105	104	102	100	98.7	97.1	96.1	94.1
140	115	115	113	110	108	105	104	102	100	98.6	97.1	95.9	91.8
141	115	115	113	110	108	105	104	102	100	98.7	97.1	96.1	941
142	90.4	90.4	90.4	90.4	89.8	89.0	88.0	79.7	59.9	55.2			0
143	90.4	90.4	90.4	90.4	89.8	89.0	88.0	79.7	59.9	55.2		0	
												~ N. J	
144	115	115	115	115	115	115	115	115	115	84.8	58.4	39.7	27.0
145	151	148	146	143	141	138	136	136			(7)		
146	151	148	146	143	141	138	136	136			N		
147	138	138	138	138	138	138	138	138	138	138	138	136	107
148	138	138	138	138	138	138	138	138	138	138	138	136	107
										`O.			
149	161	161	161	161	161	160	157	156	\sim				
150	161	161	161	161	161	160	157	156	$\langle Q \rangle$				
151	161	161	161	161	161	161	161	161	161	84.8	58.4	39.7	27.0
152	161	161	161	161	161	160	159	158	157	156	155	153	
153	160	160	160	160	160	159	158	157	156	156	154	151	
154	160	160	160	160	160	160	160	160	160	160			
155	170	166	163	160	158	156	154	153	153	152	 151	 151	 151
156	170	166	163	160	158	156	154	153	153	152	151	151	151
150	170	100	103	100	150	150	151	155	155	152	151	131	131
157	173	169	165	162	160	158	157	155	154	135	134	133	129
158	158	155	152	149	146	144	141	141					
					W.	•							
159	158	155	152	149	146	144	141	141					
160	183	177	172	169) 165	162	159	157	156	155	154	143	118
161	183	177	172	169	165	162	159	157	156	155	154	143	118
162	183	177	172	169	165	162	159	157	156	155	154	143	118
102	103	1//		107	103	102	137	137	130	155	154	143	110
163	207	207	207	207	207	207	206	206					
100	20.			20.	207	207	200	200					•••
164	197	193	189	185	182	180	177	177					
165	197	-1-1	189	185	182	180	177	177					
166	197	193	189	185	182	180	177	177					
167	140	137	135	133	132	131	129	128					
168	140	137	135	133	132	131	129	128					
169	140	137	135	133	132	131	129	128					
170	202	197	192	188	184	180	176	176					
171	202	197	192	188	184	180	176	176					
172	194	188	184	180	177	175	174	173					
173	194	188	184	180	177	175	174	173					
174	194	188	184	180	177	175	174	173					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

-			Basic A	Allowable	Stress, S	, MPa, at l	Metal Te	mperatur	e, °C [Not	es (1) an	d (4b)]		
Line No.	600	625	650	675	700	725	750	775	800	825	850	875	900
139	85.5	69.3	56.8	46.8	38.6	31.5	25.5	20.6	17.1	13.8	10.2	7.98	6.20
140	75.7	62.6	50.6	41.2	33.6	27.7	22.6	18.3	15.0	11.9	9.03	7.35	5.86
141	85.5	69.3	56.8	46.8	38.6	31.5	25.5	20.6	17.1	13.8	10.2	7.98	6.20
142												00,	
143											O	, <u>r</u>	
144	19.2	15.0	13.8								တ္သာ`		
145											,		
146										- MV			
147	83.8	63.9	44.7	29.8	15.5	11.7	8.68	7.20	6.25	511			
148	83.8	63.9	44.7	29.8	15.5	11.7	8.68	7.20	6.25	5.11			
149								(%				
150								Q `	/				
151	19.2	15.0	13.8					أللع					
152							w6						
153							10						
154						• . 0							
155	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
156	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
157	115	94.2	77.3	64.9	54,7	44.7	36.1	29.2	23.6	19.1			
158				1									
159				CO.,									
160	99.1	81.6	67.0	* 54.6	42.2								
161	99.1	81.6	67.0	54.6	42.2								
162	99.1	81.6	67.0	54.6	42.2								
163		40,											
164	W												
165	5												
166													
167													
168													
169													
170													
171													
172													
173													
174													

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
	62Ni-22Mo-15Cr	Fittings	B366		N10362	Sol. ann.	All	43
176	62Ni-22Mo-15Cr	Forgings	B462		N10362	Sol. ann.	All	43
	62Ni-22Mo-15Cr	Forgings	B564		N10362	Sol. ann.	All	43
	60Ni-22Cr-9Mo-3.5Cb	Forg. & ftg.	B564			Annealed	≤100	43
170	00111 2201 7110 0.000	1015. & 115.	D501		1100025	Timearca		15
179	65Ni-28Mo-2Fe	Forg. & ftg.	B366	•••	N10665	Sol. ann.	Ali	44
	65Ni-29.5Mo-2Fe-2Cr	Forg. & ftg.	B366		N10675	Sol. ann	All	44
	65Ni-29.5Mo-2Fe-2Cr	Forg. & ftg.	B462		N10675	Sol. ann.	All	44
	65Ni-29.5Mo-2Fe-2Cr	Forg. & ftg.	B564		N10675	Sol. ann.	All	44
	57Ni-22Cr-14W-2Mo-La	•	B564			Sol. ann.	All	43
	57Ni-22Cr-14W-2Mo-La	0 0	B366			Sol. ann.	All	43
104	5/NI-22CI-14VV-2MO-La	roig. & itg.	D300		NU0230	301. aiiii.	All	43
105	22C - 24N: 22E - 4 EM -	Pitting	D266		R20033	C-1		45
185	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	rittings	B366	···	K20033	Sol. ann.		45
186	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	Fittings	B462	elle	R20033	Sol. ann.		45
187	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	Forgings	B564	net	R20033	Sol. ann.		45
			N					
	99.0Ni	Rod & bar	B160			H.W.	All	41
189	99.0Ni	Rod & bar	B160		N02200	Annealed	All	41
		L						
190	67Ni-30Cu	Rod & bar	B164		N04400	Ann. forg.	All	42
		CV.						
191	33Ni-42Fe-21Cr	Rod & bar Rod & bar Rod & bar Rod & bar	B408		N08810	Sol. trt. or		45
400	00111 4017 046 41 111					ann.		
	33Ni-42Fe-21Cr-Al-Ti	Rod & bar	B408			Annealed		45
193	33Ni-42Fe-21Cr	Rod & bar	B408		N08800	Annealed		45
194	26Ni-22Cr-5Mo-Ti	Rod & bar	B621		N08320	Sol. ann.	All	45
	C C	Z_{i}						
	47Ni-22Cr-19Fe-6Mo	Rod & bar	B581		N06007	Sol. ann.	>19	45
	42Ni-21.5Cr-3Mo-2.3Cu		B425			Annealed		45
	58Ni-29Cr-9Fe	Rod & bar	B166		N06690	H.R.	>75	43
198	58Ni-29Cr-9Fe	Rod & bar	B166		N06690	H.R. ann. or C.D. ann.	All	43
199	47Ni-22Cr-19Fe-6Mo	Rod & bar	B581		N06007	Sol. ann.	≤19	45
200	40Ni-29Cr-15Fe-5Mo	Rod & bar	B581		N06030	Sol. ann.	All	45
201	31Ni-33Fe-27Cr-6.5Mo- Cu-N	Rod & bar	B649		N08031	Annealed	All	45
202	67Ni-30Cu	Rod & bar	B164		N04400	H.W.	All except hex >54	42
203	58Ni-33Cr-8Mo	Rod & bar	B574		N06035	Sol. ann.	All	43
204	37Ni-33Fe-25Cr	Rod & bar	B408		N08120	Sol. ann.	All	45
205	61Ni-16Mo-16Cr	Rod & bar	B574		N06455	Sol. ann.	All	43

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Numbers	in rarentic	ses Refer to N	iotes for A	ppenuix A	Basic Allo			MPa, at	Metal T				
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	[4b)] 150	175	200	225	250
175		-198	725	310	427	207	207	207	207	207	207	204	202	199
176		-198	725	310	427	207	207	207	207	207	207	204	202	199
177		-198	725	310	427	207	207	207	207	207	207	204	202	199
	(9)(64)	-198	827	414	649	276	276	276	274	273	272	270	269	267
1.0	(2)(0.1)	170	02.		017		2.0	270	-, 1	2,5		7	207	20,
179	(74)	-198	758	352	427	234	234	234	234	234	284	234	234	234
180	(74)	-198	758	352	427	234	234	234	234	234	234	234	234	234
181		-198	758	352	427	234	234	234	234	234	234	234	234	234
182		-198	758	352	427	234	234	234	234	234	234	234	234	234
183		-198	758	310	899	207	207	207	207	207	207	207	207	207
184	(74)	-198	758	310	899	207	207	207	207	207	207	207	207	207
185		-198	750	380	427	250	231	209	200	193	187	181	176	172
186		-198	750	380	427	250	231	209	200	193	187	181	176	172
187		-198	750	380	427	250	231	209	200	193	187	181	176	172
188	(9)	-198	414	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
189		-198	379	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
190	(13)	-198	483	172	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4	90.4
191	(9)	-198	450	170	899	115	115	115	115	115	115	115	115	115
192	(9)	-198	450	170	899	115	115	115	115	115	115	115	115	115
193	(9)	-198	515	205	816	138	138	138	138	138	138	138	138	138
194		-198	517	193	427	129	129	129	129	129	129	129	129	129
195		-198	586	207	538	138	138	138	138	138	138	138	138	138
196		198	585	240	538	161	161	161	161	161	161	161	161	161
197		-198	585	240	482	160	160	160	160	160	160	160	160	160
198	_ //	-198	586	240	482	160	160	160	160	160	160	160	160	160
199	\	-198	621	241	538	161	161	161	161	161	161	161	161	161
200		-198	586	241	427	161	161	161	161	161	161	161	157	154
201		-198	648	276	427	184	184	184	184	184	177	171	166	162
202		-198	552	276	510	184	182	177	174	171	168	165	164	162
203	(9)	-198	586	241	427	161	161	161	161	161	161	154	149	144
204		-198	621	276	899	184	184	184	184	184	184	184	180	175
205		-198	689	276	427	184	184	184	184	184	184	184	184	184

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				Allowable						es (1) an			
Line No.	275	300	325	350	375	400	425	450	475	500	525	550	575
175	197	193	190	188	186	184	182	180					
176	197	193	190	188	186	184	182	180					
177	197	193	190	188	186	184	182	180					2
178	265	262	260	257	255	252	251	249	247	245	242	215	194
179	234	234	234	234	234	234	234	234				ုက္ခ	
180	234	234	234	234	234	233	231	230				ر رس	
181	234	234	234	234	234	233	231	230			78)	
182	234	234	234	234	234	233	231	230					
183	207	207	203	199	197	196	195	195	 195	 195	195	 195	 183
184	207	207	203	199	197	196	195	195	195	195	195	195	183
104	207	207	203	199	197	190	173	193	193	0	173	193	103
185	169	165	163	161	159	157	156	155	20,				
186	169	165	163	161	159	157	156	155					
187	169	165	163	161	159	157	156	155					
400							10.	7					
188	68.9	68.9	68.9				1,10						
189	68.9	68.9	68.9			×	0						
190	90.4	90.4	90.4	90.4	89.8	89.0	88.0	79.7	59.9	55.2			
191	115	115	113	110	108	105	104	102	100	98.6	97.1	95.9	91.8
192	115	115	113	110	Q_{08}	105	104	102	100	98.7	97.1	96.1	94.1
193	138	138	138	138	138	138	138	138	138	138	137	131	108
173	150	130	150	Q.	130	130	130	150	150	150	137	151	100
194	129	129	127	125	122	121	119	119					
195	138	135	134	132	131	130	129	128	128	127	127	126	
196	161	161	161	161	161	160	159	158	157	156	155	153	
197	160	160	160	160	160	160	160	160	160	160			
198	160	160	160	160	160	160	160	160	160	160			
199	160	158	156	154	153	152	151	150	149	136	132	130	
200	151	148	146	143	141	138	136	136					
201	158	155	152	149	146	144	141	141					
202	161	160	159	158	156	136	102	63.8	33.5	17.0	13.0		
203	140	137	135	133	132	131	129	128					
204	170	166	163	160	158	156	154	153	153	152	151	151	151
205	184	184	184	184	182	180	178	178					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			Basic A	llowable	Stress, <i>S</i> ,	MPa, at	Metal Te	mperatur	e, °C [Not	es (1) an	d (4b)]		
Line No.	600	625	650	675	700	725	750	775	800	825	850	875	900
175													
176													
177												76	
178	156	136	91.0									JO,	
179)	
180											0,0		
181											.		
182													
183	153	128	107	89.7	74.7	61.9	50.8	41.1	32.6	25.2	18.9	13.8	10.2
184	153	128	107	89.7	74.7	61.9	50.8	41.1	32.6	25.2	18.9	13.8	10.2
185									5 ⁴				
186								الملك					
187							ine						
188						; <	Y						
189						×0.							
190					Cilici	F							
191	75.7	62.6	50.6	41.2	.33.6	27.7	22.6	18.3	15.0	11.9	9.03	7.35	5.86
192	85.5	69.3	56.8	46.8	38.6	31.5	25.5	20.6	17.1	13.8	10.2	7.98	6.20
193	85.0	64.4	44.8	30.0	15.5	11.3	8.82	6.98	6.43	5.00			
194													
195		OF											
196		7											
197	K												
198	SW.												
199													
200													
201													
202				•••									
203													
204	117	96.2	79.3	65.6	54.4	45.0	37.2	30.6	25.1	20.5	16.5	13.0	9.8
205													

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line			Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Nominal Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
206	54Ni-16Mo-15Cr	Rod & bar	B574		N10276	Sol. ann.	All	43
207	62Ni-22Mo-15Cr	Rod & bar	B574		N10362	Sol. ann.	All	43
208	60Ni-22Cr-9Mo-3.5Cb	Rod & bar	B446	1	N06625	Annealed	>100, ≤250	43
209	60Ni-22Cr-9Mo-3.5Cb	Rod & bar	B446	1	N06625	Annealed	≤100	43
210	57Ni-22Cr-14W-2Mo-La	Rod & bar	B572		N06230	Sol. ann.	All	43
211	59Ni-23Cr-16Mo	Rod & bar	B574		N06059	Sol. ann.	All	43
212	59Ni-23Cr-16Mo-1.6Cu	Rod & bar	B574		N06200	Sol. ann.	All	43
213	65Ni-29.5Mo-2Fe-2Cr	Rod & bar	B335		N10675	Sol. ann.	All	44
214	33Cr-31Ni-32Fe-1.5Mo- 0.6Cu-N	Rod	B649		R20033	Sol. ann.		45
215	53Ni-17Mo-16Cr-6Fe- 5W	Castings	A494	CW12MW	N30002			
216	56Ni-19Mo-18Cr-2Fe	Castings	A494	CW6M	N30107			
217	59Ni-22Cr-14Mo-4Fe- 3W	Castings	A494	CX2MW	N26022	Sol. ann.		43
	ASMENOR	Castings Castings Com. Click	o vie					

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			ses herer to r		PP	Basic All			MPa, at					
Line No.	Notes	Min. Temp., °C (6)	Min. Tensile Str., MPa	Min. Yield Str., MPa	Max. Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225	250
206		-198	689	283	677	188	188	188	188	188	188	188	188	187
207		-198 -198	725	310	427	207	207	207	207	207	207	204	202	199
	 (9)(64)(70)	-198	758	345	649	230	230	230	230	230	230		2 30	230
200	(3)(04)(70)	-190	730	343	049	230	230	230	230	230	230	230	230	230
209	(9)(64)(70)	-198	827	414	649	276	276	276	274	273	272	270	269	267
210		-198	758	310	899	207	207	207	207	207	207	207	207	207
											3)			
211		-198	689	310	427	207	207	207	207	207	207	207	207	206
212		-198	689	310	427	207	207	207	207	207	207	207	207	200
213		-198	758	352	427	234	234	234	234	234	234	234	234	234
									5 P					
214		-198	750	380	427	250	231	209 (200	193	187	181	176	172
								X						
045	(0) (4.4)	100	106	0.7.6	= 00				4.2			4.5	4.5	4.5
215	(9)(44)	-198	496	276	538	165	165	165	165	165	165	165	165	165
216	(9)	-198	496	276	538	165	165	165	165	165	165	165	165	165
217	(9)	-198	552	310	260	184	184	184	184	184	184	184	184	184
		NO RM	496 552	W. Cli	io vi									
	ASME													

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

		T ur circii						mperatur					
Line No.	275	300	325	350	375	400	425	450	475	500	525	550	575
206	183	177	172	169	165	162	159	157	156	155	154	143	118
207	197	193	190	188	186	184	182	180					
208	230	230	230	230	230	230	230	228	227	225	222	215	194
209	265	262	260	257	255	252	251	249	247	245	242	215	194
210	207	207	203	199	197	196	195	195	195	195	195	195	183
211	202	197	192	188	184	180	176	176			18))	
212	194	188	184	180	177	175	174	173					
213	234	234	234	234	234	233	231	230		0	2/4		
214	169	165	163	161	159	157	156	155		ON I			
215	165	165	165	165	165	165	165	165	165	165	165	157	
216	165	165	165	165	165	165	165	165	165	165	165	157	
217	184							KUE					
				30°.	ON	click	olies	165					
	P	SMEN	of										

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

206 99.1 81.6 67.0 54.6 42.2	-			Basic A	Allowable	Stress, S	, MPa, at	Metal Te	mperatur	e, °C [Not	es (1) and	l (4b)]		
207 .		600	625	650	675	700	725	750	775	800	825	850	875	900
208 156 136 91.0	206	99.1	81.6	67.0	54.6	42.2								
209 156 136 91.0	207													
210 153 128 107 89.7 74.7 61.9 50.8 41.1 32.6 25.2 18.9 13.8 10.2	208	156	136	91.0									1/2	
	209	156	136	91.0									P)	
211	210	153	128	107	89.7	74.7	61.9	50.8	41.1	32.6	25.2	18.9	13.8	10.2
212 213 214 215 216 217	211										/	\$		
214	212													
214	213										Silvi			
215	214									K OT				
216	215								III Pr	···				
217	216							0	(0)					
M. Click to view	217							NVE						
					12	. Clic	F, ON							
			R	MOC										
RIVIDE		4	\mathcal{A}_{O}											
I PORMIDE	-	SMI												
ASMENOR MIDE	١													
ASMENORMIDE														

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	P-No. (5)	Notes	Min. Temp., °C (6)	Min. Tensile Strength, MPa	Min. Yield Strength, MPa
1	Ti	Smls. & wld. tube	B338	1	R50250	Annealed	51		-59	240	138
	Ti	Smls. pipe	B861	1	R50250	Annealed	51		-59	240	138
	Ti	Wld. pipe	B862	1	R50250	Annealed	51		-59	240	138
		· · · · ·									0-
4	Ti	Smls. & wld. tube	B338	2	R50400	Annealed	51		-59	345	275
5	Ti	Smls. pipe	B861	2	R50400	Annealed	51		-59	345	275
6	Ti	Wld. pipe	B862	2	R50400	Annealed	51		-59	345	275
										2	
	Ti	Smls. & wld. tube	B338	3	R50550	Annealed	52		-59	450	380
		Smls. pipe	B861	3	R50550	Annealed	52		-59	450	380
9	Ti	Wld. pipe	B862	3	R50550	Annealed	52		1-59	450	380
10	Ti–Pd	Smls. & wld. tube	B338	7	R52400	Annealed	51	, D.	- 59	345	275
	Ti-Pd	Smls. wid. tube	B861	7	R52400	Annealed	51	8,	-59	345	275
	Ti-Pd	Wld. pipe	B862	7	R52400	Annealed	51	<i>y</i>	-59	345	275
	11 1 4	wa. pipe	D00 2	,	1102 100	Timicaica			37	515	273
13	Ti-0.3Mo-0.8Ni	Smls. & wld. tube	B338	12	R53400	Annealed <	52		-59	485	345
14	Ti-0.3Mo-0.8Ni	Smls. pipe	B861	12	R53400	Annealed	52		-59	485	345
15	Ti-0.3Mo-0.8Ni	Wld. pipe	B862	12	R53400	Annealed	52		-59	485	345
						KKI					
16		Plate, sheet, strip	B265	1		Annealed	51		-59	240	138
17	Ti	Plate, sheet, strip	B265	2	<i>1</i> ,	Annealed	51		-59	345	275
18	Ti	Plate, sheet, strip	B265	3	R50550	Annealed	52		-59	450	380
	Ti-Pd	Plate, sheet, strip	B265	7	R52400	Annealed	51		-59	345	275
20	Ti-0.3Mo-0.8Ni	Plate, sheet, strip	B265	12	R53400	Annealed	52		-59	485	345
21	Ti	Fittings	B363	WPT1	R50250	Annealed	51		-59	240	138
22	Ti	Forgings	B381	F-1	R50250	Annealed	51		-59	240	138
23	Ti	Fittings	B363	WPT2	R50400	Annealed	51		-59	345	275
24		Forgings	B381	F-2	R50400	Annealed	51		-59	345	275
25		Fittings	B363	WPT3	R50550	Annealed	52		-59	450	380
26		Forgings	B381	F-3	R50550	Annealed	52		-59	450	380
	Ti-Pd	Fittings	B363	WPT7	R52400	Annealed	51		-59	345	275
	Ti-Pd	Forgings	B381	F-7		Annealed	51		-59	345	275
	Ti-0.3Mo-0.8Ni		B363	WPT12		Annealed	52		-59	485	345
30	Ti-0.3Mo-0.8Ni	Forgings	B381	F-12	R53400	Annealed	52	•••	-59	485	345
31	Ti S	Dar	B348	1	DEUSEU	Annealed	51		-59	240	138
32	Y	Bar Bar	B348	1 2	R50400		51		-59	345	275
33		Bar	В348	3		Annealed	52		-59 -59	450	380
	Ti–Pd	Bar	В348	3 7		Annealed	51		-59 -59	345	275
	Ti-Pa Ti-0.3Mo-0.8Ni	Bar	B348	12		Annealed	52		-59 -59	345 485	345
33	11-0.51v10-0.0111	DαI	D340	14	NJJ400	Aimedieu	JZ		-37	703	343
36	Ti	Castings	B367	C-2	R52550		51	(14)(44)	-59	345	275
37		Castings	B367	C-3	R52550		52	(14)(44)	-59	450	380
38	Ti–Pd	Castings	B367	C-7	R52700		51	(14)(44)	-59	345	275

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Nu	mucis III Pa	arentheses I						Tempera					raieu
	Max. Use	Min.	Dasic 1	inowabic	Jul C33,	<i>5</i> , MI <i>a</i> , <i>c</i>	at Mctai	Tempera	iture, e	[Notes (r) and (rujj	
Line	Temp.,	Temp. to											
No.	°C	40	65	100	125	150	175	200	225	250	275	300	325
1	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
2	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
3	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
													. 92
4	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
5	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
6	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	58.7	54.7	50.7
7	316	149	139	124	113	102	93.3	84.7	77.7	70.7	66.2	61.7	<i>57.7</i>
8	316	149	139	124	113	102	93.3	84.7	77.7	70.7	66.2	61.7	<i>57.7</i>
9	316	149	139	124	113	102	93.3	84.7	77.7	70.7	66.2	61.7	<i>57.7</i>
	010		107		110	102	20.0	0	,	S	3.00.2	51.7	<i>57.17</i>
10	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
11	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
12	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
								<	\sim				
13	316	161	156	148	139	130	123	116	111	106	104	101	98.3
14	316	161	156	148	139	130	123	116	111	106	104	101	98.3
15	316	161	156	148	139	130	123	Ø 116	111	106	104	101	98.3
16	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
17	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	58.7	54.7	50.7
18	316	149	139	124	113	102	93.3	84.7	77.7	70.7	66.2	61.7	<i>57.7</i>
19	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	58.7	54.7	50.7
20	316	161	156	148	139	130	123	116	111	106	104	101	98.3
					Cili								
21	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
22	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
23	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
24	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
25	316	149	139	124	113	102	93.3	84.7	77.7	70.7	66.2	61.7	<i>57.7</i>
26	316	149	139	124	113	102	93.3	84.7	77.7	70.7	66.2	61.7	<i>57.7</i>
27	316	115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
28		115	108	98.3	90.7	83.0	77.5	72.0	67.3	62.7	<i>58.7</i>	54.7	50.7
29	316	161	156	148	139	130	123	116	111	106	104	101	98.3
30	316	161	156	148	139	130	123	116	111	106	104	101	98.3
21	212	00.2	72.0	(2.4		40.4	42.4	20.2	22.0	20.2	27.2	25.2	22.7
31	316	80.3	73.8	62.4	55.5	49.4	43.4	38.3	33.9	30.2	27.3	25.2	23.7
32	316 316	115 149	108 139	98.3 124	90.7 113	83.0 102	77.5 93.3	72.0 84.7	67.3 77.7	62.7 70.7	58.7	54.7 61.7	50.7 <i>57.7</i>
33						102					66.2		
34	316 316	115 161	108 156	98.3	90.7 139	83.0	77.5	72.0 116	67.3 111	62.7	58.7 104	54.7 101	50.7 98.3
35	310	161	156	148	139	130	123	116	111	106	104	101	70.3
36	260	115	106	92.7	85.3	78.0	72.2	66.3	61.5	56.7	52.0		
37	260	149	139	124	113	102	93.3	84.7	77.7	70.7	65.3		
38		115	106	92.7	85.3	78.0	72.2	66.3	61.5	56.7	52.0		
	•												

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	UNS No.	P-No. (5)	Notes	Min. Temp., °C (6)	Min. Tensile Strength, MPa	Min. Yield Strength, MPa	Max. Use Temp., °C
1	99.2Zr	Pipe & tube	B523	R60702	61		-59	379	207	371
	99.2Zr	Pipe & tube	B658	R60702	61		-59	379	207	371
3	95.5Zr + 2.5Cb	Pipe & tube	B523	R60705	62	(73)	-59	552	379	371
4	95.5Zr + 2.5Cb	Pipe & tube	B658	R60705	62	(73)	-59	552	379	371
5	99.2Zr	Plate & sheet	B551	R60702	61		-59	379	2075	371
6	95.5Zr + 2.5Cb	Plate & sheet	B551	R60705	62	(73)	-59	552	379	371
7	99.2Zr	Forgings & bar	B493	R60702	61		-59	379	207	371
8	99.2Zr	Forgings & bar	B550	R60702	61		-59	379 379	207	371
9	95.5Zr + 2.5Cb	Forgings & bar	B493	R60705	62	(73)	-59	483	379	371
10	95.5Zr + 2.5Cb	Forgings & bar	B550	R60705	62	(73)	150 P	552	379	371
	99.2Zr 95.5Zr + 2.5Cb 95.5Zr + 2.5Cb	ORMOC	COM	Click	olien	TILE				

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			Bas	ic Allowa	ble Stre	ss, S, MP	a, at Met	al Temp	erature,	°C [Notes	(1) and	(4b)]		
	Min.								•					
Line No.	Temp. to 40	65	100	125	150	175	200	225	250	275	300	325	350	375
1	126	119	103	92.4	82.5	73.6	65.7	58.8	52.8	47.8	43.7	40.4	37.8	36.1
2	126	119	103	92.4	82.5	73.6	65.7	58.8	52.8	47.8	43.7	40.4	37.8	36.1
3	184	169	149	139	130	123	116	111	106	101	97.6	94.6	92.4	91.0
4	184	169	149	139	130	123	116	111	106	101	97.6	94.6	92.4	91.0
5	126	119	103	92.4	82.5	73.6	65.7	58.8	52.8	47.8	43.7	40.4	37.8	36.1
6	184	169	149	139	130	123	116	111	106	101	97.6	94.6	92.4	91.0
											,	\$		
7	126	119	103	92.4	82.5	73.6	65.7	58.8	52.8	47.8	43.7	40.4	37.8	36.1
8		119	103	92.4	82.5	73.6	65.7	58.8	52.8	47.8	43.7	40.4	37.8	36.1
										7 5	~			
9	184	169	149	139	130	123	116	111	106	101	97.6	94.6	92.4	91.0
10	184	169	149	139	130	123	116	111	106	101	97.6	94.6	92.4	91.0
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Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line	Nominal		Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
1	Al-Mn-Cu	Smls. pipe & tube	B210	Alclad 3003	A83003	0		21
2	Al-Mn-Cu	Smls. pipe & tube	B210	Alclad 3003	A83003	H112		21
	Al-Mn-Cu	Smls. pipe & tube	B241	Alclad 3003	A83003	0		21
4	Al-Mn-Cu	Smls. pipe & tube	B241	Alclad 3003	A83003	H112		21
5	Al-Mn-Cu	Smls. pipe & tube	B210	Alclad 3003	A83003	H14	(21
6	Al-Mn-Cu	Smls. pipe & tube	B210	Alclad 3003	A83003	H18	٠. س	21
7	99.60Al	Smls. pipe & tube	B210	1060	A91060	0	6,5	21
8	99.60Al	Smls. pipe & tube	B210	1060	A91060	H112	,	21
9	99.60Al	Smls. pipe & tube	B210	1060	A91060	H113		21
10	99.60Al	Smls. pipe & tube	B241	1060	A91060	0		21
11	99.60Al	Smls. pipe & tube	B241	1060	A91060	H112		21
12	99.60Al	Smls. pipe & tube	B241	1060	A91060	H113		21
13	99.60Al	Smls. pipe & tube	B210	1060	A91060	H14		21
14	99.0Al-Cu	Smls. pipe & tube	B241	1100	A91100	0		21
15	99.0Al-Cu	Smls. pipe & tube	B241	1100	A91100	H112		21
16	99.0Al-Cu	Smls. pipe & tube	B210	1100	A91100	H113		21
17	99.0Al-Cu	Smls. pipe & tube	B210	1100	A91100	H14		21
				:107				
18	Al-Mn-Cu	Smls. pipe & tube	B210	3003	A93003	0		21
19	Al-Mn-Cu	Smls. pipe & tube	B210	3003	A93003	H112		21
20	Al-Mn-Cu	Smls. pipe & tube	B241	3003	A93003	0		21
21	Al-Mn-Cu	Smls. pipe & tube	B241	3003	A93003	H112		21
22	Al-Mn-Cu	Smls. pipe & tube	B491	3003	A93003	0		21
23	Al-Mn-Cu	Smls. pipe & tube	B491	3003	A93003	H112		21
		<u></u>)					
24	Al-Mn-Cu	Smls. pipe & tube	B210	3003	A93003	H14		21
25	Al-Mn-Cu	Smls. pipe & tube	B210	3003	A93003	H18		21
26	Al-Mn-Cu	Smls. pipe & tube	B241	3003	A93003	H18		21
		OM						
27	Al-2.5Mg	Smls. pipe & tube	B210	5052	A95052	0		22
28	Al-2.5Mg	Smls. pipe & tube	B241	5052	A95052	0		22
29	Al-2.5Mg	Smls. pipe & tube	B210	5052	A95052	H32		22
30	Al-2.5Mg	Smls. pipe & tube	B210	5052	A95052	H34		22
	P							
31	Al-4.4Mg-Mn	Smls. pipe & tube	B210	5083	A95083	0		25
32	Al-4.4Mg-Mn	Smls. pipe & tube	B210	5083	A95083	H112		25
33	Al-4.4Mg-Mn	Smls. pipe & tube	B241	5083	A95083	0		25
34	Al-4.4Mg-Mn	Smls. pipe & tube	B241	5083	A95083	H112		25
35	Al-4.0Mg-Mn	Smls. pipe & tube	B210	5086	A95086	0		25
36	Al-4.0Mg-Mn	Smls. pipe & tube	B210	5086	A95086	H112		25
37	Al-4.0Mg-Mn	Smls. pipe & tube	B241	5086	A95086	0		25
38	Al-4.0Mg-Mn	Smls. pipe & tube	B241	5086	A95086	H112		25

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

			Min.		-		-	able Stre		Pa, at Me	etal Tem	perature	
Line		Min. Temp.,	Tensile	Min. Yield Strength,	Max. Use Temp.,	Min. Temp.					,,		
No.	Notes	°C (6)	MPa	MPa	°C	to 40	65	100	125	150	175	200	225
1	(14)(33)	-269	90	31	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
2	(14)(33)	-269	90	31	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
3	(14)(33)	-269	90	31	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
4	(14)(33)	-269	90	31	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
5	(14)(33)	-269	131	110	204	43.7	43.7	43.7	41.7	29.0	21.1 (16.7	16.1
6	(14)(33)	-269	179	159	204	59.8	59.8	59.8	<i>57.0</i>	29.0	211	16.7	16.1
											27.		
7	(14)(33)	-269	59	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
8	(14)(33)	-269	59	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
9	(14)(33)	-269	59	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
10	(14)(33)	-269	59	17	204	11.5	11.5	10.9	9,8	8.8	7.5	5.8	5.5
11	(14)(33)	-269	59	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
12	(14)(33)	-269	59	17	204	11.5	11.5	10.9	09.8	8.8	7.5	5.8	5.5
13	(14)(33)	-269	83	69	204	27.6	27.6	27.6	26.6	18.1	12.7	8.4	7.8
								Q ~ _					
14	(14)(33)	-269	76	21	204	13.8	13.8	13.7	13.2	11.8	9.3	7.2	6.9
15	(14)(33)	-269	76	21	204	13.8	13.8	13.7	13.2	11.8	9.3	7.2	6.9
16	(14)(33)	-269	76	24	204	16.1	16.1	16.0	15.6	11.8	9.3	7.2	6.9
17	(14)(33)	-269	110	97	204	36.8	36.8	36.1	33.1	19.0	13.6	8.5	7.8
						107							
18	(14)(33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
19	(14)(33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
20	(14)(33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
	(14)(33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
	(14)(33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
	(14)(33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
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24	(14)(33)	-269	138	117	204	46.0	46.0	46.0	43.9	29.0	21.1	16.7	16.1
	(14)(33)	-269	186		204	62.1	62.1	60.3	52.1	36.1	24.5	18.0	17.0
	(14)(33)	-269	186		204	62.1	62.1	60.3	52.1	36.1	24.5	18.0	17.0
		ON!	/										
27	(14)	-269	172	69	204	46.0	46.0	46.0	45.9	41.6	28.8	17.6	16.1
	(14)	-269	172		204	46.0	46.0	46.0	45.9	41.6	28.8	17.6	16.1
	(14)(33)	-269	214		204	71.2	71.2	71.2	71.0	41.6	28.8	17.6	16.1
	(14)[33]	-269	234		204	78.1	78.1	78.1	78.1	41.6	28.8	17.6	16.1
	(2)												
31	(33)	-269	269	110	65	73.5	73.5						
	(33)	-269	269		65	73.5	73.5						
	(33)	-269	269		65	73.5	73.5						
	(33)	-269	269		65	73.5	73.5						
51	(30)	207	207	110		. 5.5	. 5.5						
35	(33)	-269	241	97	65	64.4	64.4						
	(33)	-269	241		65	64.4	64.4						
	(33)	-269	241		65	64.4	64.4						
	(33)	-269	241		65	64.4	64.4						
	18.20											•	-

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line	Nominal		Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
39	Al-4.0Mg-Mn	Smls. pipe & tube	B210	5086	A95086	H32		25
40	Al-4.0Mg-Mn	Smls. pipe & tube	B210	5086	A95086	H34		25
41	Al-3.5Mg	Smls. pipe & tube	B210	5154	A95154	0		22
42	Al-3.5Mg	Smls. pipe & tube	B210	5154	A95154	H34	(22
							\$3. \$3. \$6.	<i>V</i>
43	Al-2.7Mg-Mn	Smls. pipe & tube	B241	5454	A95454	0	0,	22
44	Al-2.7Mg-Mn	Smls. pipe & tube	B241	5454	A95454	H112	8)	22
45	Al-5.1Mg-Mn	Smls. pipe & tube	B210	5456	A95456	0		25
46	Al-5.1Mg-Mn	Smls. pipe & tube	B210	5456	A95456	H112		25
	Al-5.1Mg-Mn	Smls. pipe & tube	B241	5456	A95456			23
48	Al-5.1Mg-Mn	Smls. pipe & tube	B241	5456	A95456	H112		25
					_<	, 0		
	Al-Mg-Si-Cu	Smls. pipe & tube	B210	6061	A96061	T4 wld.		23
	Al-Mg-Si-Cu	Smls. pipe & tube	B210	6061	A96061	T6 wld.		23
	Al-Mg-Si-Cu	Smls. pipe & tube	B241	6061	A96061	T4 wld.		23
52	Al-Mg-Si-Cu	Smls. pipe & tube	B241	6061	A96061	T6 wld.		23
F 2	Al M. C. C	Cula dia O. I.	D2.44	(0(1	100001	TD 4		22
	Al-Mg-Si-Cu	Smls. pipe & tube	B241	6061	A96061	T4		23
	Al-Mg-Si-Cu	Smls. pipe & tube	B210	6061 6061	A96061	T4		23
	Al-Mg-Si-Cu	Smls. pipe & tube	B241 B210	6061	A96061	T6 T6		23 23
30	Al-Mg-Si-Cu	Smls. pipe & tube	D210	4001	A96061	10		23
57	Al-Mg-Si	Smls. pipe & tube	B210	6063	A96063	T4 wld.		23
	Al-Mg-Si	Smls. pipe & tube	B210	6063	A96063	T5 wld.		23
	Al-Mg-Si	Smls. pipe & tube	B210	6063	A96063	T6 wld.		23
	Al-Mg-Si	Smls. pipe & tube	B241	6063	A96063	T4 wld.		23
	Al-Mg-Si	Smls. pipe & tube	B241	6063	A96063	T5 wld.		23
	Al-Mg-Si	Smls. pipe & tube	B241	6063	A96063	T6 wld.		23
63	Al-Mg-Si	Smls. pipe & tube	B241	6063	A96063	T4	≤13	23
64	Al-Mg-Si	Smls. pipe & tube	B210	6063	A96063	T4		23
65	Al-Mg-Si	Smls. pipe & tube	B241	6063	A96063	T5	≤13	23
66	Al-Mg-Si	Smls. pipe & tube	B241	6063	A96063	T6		23
67	Al-Mg-Si	Smls. pipe & tube	B210	6063	A96063	Т6		23
68	Al-4.4Mg-Mn	Wld. pipe & tube	B547	5083	A95083	0		25
	•							
69	Al-Mn-Cu	Structural tube	B221	Alclad 3003	A83003	0		21
70	Al-Mn-Cu	Structural tube	B221	Alclad 3003	A83003	H112		21
	99.0Al	Structural tube	B221	1060	A91060	0		21
72	99.0Al	Structural tube	B221	1060	A91060	H112		21
	99.0Al-Cu	Structural tube	B221	1100	A91100	0		21
	99.0Al-Cu	Structural tube	B221	1100	A91100	H112		21
75	Al-Mn-Cu	Structural tube	B221	3003	A93003	0		21

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

N	lumbers in Pa	ar Chitheses	Min.	oces for Ap	Max.			able Stre	ess, S, MF lotes (1)	a, at Mo	etal Tem		
Line No.	Notes	Min. Temp., °C (6)	Tensile	Min. Yield Strength, MPa	Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225
39	(33)	-269	276		65	91.9	91.9						
40		-269	303		65	101.1	101.1						
	(00)												
41		-269	207	76	65	50.6	50.6					~ V.	
42	(33)	-269	269	200	65	89.6	89.6				(, O	
											3		
43	(33)	-269	214	83	204	55.2	55.2	55.2	48.9	37.5	28.6	21.7	20.7
44	(33)	-269	214	83	204	55.2	55.2	55.2	48.9	37.50	28.6	21.7	20.7
45	(33)	-269	283	131	65	87.3	87.3			(4)			
46	(33)	-269	283		65	87.3	87.3			11.			
47	. ,	-269	283		65	87.3	87.3						
48	(33)	-269	283	131	65	87.3	87.3		9/	•••			
49	(22)(63)	-269	165		204	55.2	55.2	55.2	54.3	52.0	46.3	35.3	34.8
50	(22)(63)	-269	165		204	<i>55.2</i>	55.2	55.2	54.3	52.0	46.3	35.3	34.8
51	(22)(63)	-269	165		204	<i>55.2</i>	55.2	55.2	54.3	52.0	46.3	35.3	34.8
52	(22)(63)	-269	165		204	55.2	55.2	55.2	54.3	52.0	46.3	35.3	34.8
53	(33)(63)	-269	179	110	204	59.8	59.8	59.8	58.9	56.3	50.2	38.3	35.9
	(33)	-269	207		204	68.9	68.9	68.9	67.8	64.8	<i>57.9</i>	40.2	35.9
	(33)(63)	-269	262	241	204	87.3	87.3	87.3	83.6	72.3	57.2	40.2	35.9
	(33)	-269	290	241	204	96.5	96.5	96.5	92.5	<i>79.9</i>	63.1	40.2	35.9
				ناء	CK								
57		-269	117		204	39.1	39.1	<i>37.9</i>	35.9	32.1	<i>25.7</i>	17.6	13.8
58		-269	117	_\	204	39.1	39.1	<i>37.9</i>	35.9	32.1	25.7	17.6	13.8
59		-269	117)/ ₄	204	39.1	39.1	37.9	35.9	32.1	25.7	17.6	13.8
60		-269	117		204	39.1	39.1	<i>37.9</i>	35.9	32.1	25.7	17.6	13.8
61 62		-269	117		204 204	39.1	39.1 39.1	<i>37.9</i> <i>37.9</i>	35.9 35.9	32.1	25.7 25.7	17.6 17.6	13.8
62		-269) 117		204	39.1	39.1	37.9	33.9	32.1	25.7	17.0	13.8
	(33)	-269	131		204	43.7	43.7	43.7	43.7	43.7	35.8	23.9	10.3
	(33)	-269	152		204	46.0	45.8	45.8	45.5	45.5	41.5	27.7	12.0
	(33)	-269	152		204	50.6	50.6	48.7	46.6	41.4	27.5	15.3	13.8
	(33)	-269	207		204	68.9	68.9	67.7	59.0	45.9	27.5	15.3	49.3
67	(33)	-269	228		204	75.8	75.8	74.8	64.0	49.2	27.5	15.3	13.8
68	\	-269	276	124	65	82.7	82.7						
	(33)(69)	-269	90		204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
	(33)(69)	-269	90		204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
	(33)(69)	-269	59		204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
72	(33)(69)	-269	59	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
	(33)(69)	-269	76		204	13.8	13.8	13.7	13.2	11.8	9.3	7.2	6.9
	(33)(69)	-269	76		204	13.8	13.8	13.7	13.2	11.8	9.3	7.2	6.9
75	(33)(69)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
	Al-Mn-Cu	Structural tube	B221	3003	A93003	H112		21
, 0	III IIII Gu	oti actarar taoc	<i>D</i> 22 1	3003	1170000			21
77	Al-2.5Mg	Structural tube	B221	5052	A95052	0		22
	Al-4.4Mg-Mn	Structural tube	B221	5083	A95083	0		9 2
	Al-4.0Mg-Mn	Structural tube	B221	5086	A95086	0	0	25
	Al-3.5Mg	Structural tube	B221	5154	A95154	0		22
	G						A.3	
81	Al-2.7Mg-Mn	Structural tube	B221	5454	A95454	0	0,5	22
82	Al-5.1Mg-Mn	Structural tube	B221	5456	A95456	0	,	25
						- Wr		
83	Al-Mg-Si-Cu	Structural tube	B221	6061	A96061	T4 wld.		23
84	Al-Mg-Si-Cu	Structural tube	B221	6061	A96061	T6 wld.		23
85	Al-Mg-Si-Cu	Structural tube	B221	6061	A96061	,T4		23
86	Al-Mg-Si-Cu	Structural tube	B221	6061	A96061	Т6		23
					76.			
87	Al-Mg-Si	Structural tube	B221	6063	A96063	T4 wld.		23
88	Al-Mg-Si	Structural tube	B221	6063	A96063	T5 wld.		23
89	Al-Mg-Si	Structural tube	B221	6063	A96063	T6 wld.		23
90	Al-Mg-Si	Structural tube	B221	6063	A96063	T4	≤13	23
91	Al-Mg-Si	Structural tube	B221	6063	A96063	T5	≤13	23
92	Al-Mg-Si	Structural tube	B221	6063	A96063	Т6		23
			•	L				
	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	0	≥0.15, <13	21
	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	0	≥13, ≤75	21
	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	H112	≥13, ≤50	21
	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	H12	≥0.43, <13	21
	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	H12	≥13, ≤50	21
	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	H14	≥0.23, <13	21
99	Al-Mn-Cu	Plate & sheet	B209	Alclad 3003	A83003	H14	≥13, ≤25	21
100	41.74.74		D200	41.1.1.2004	100001	0	.045 40	20
	Al-Mn-Mg	Plate & sheet	B209	Alclad 3004	A83004	0	≥0.15, <13	22
	Al-Mn-Mg	Plate & sheet	B209	Alclad 3004	A83004	0	≥13, ≤75	22
	Al-Mn-Mg	Plate & sheet	B209	Alclad 3004	A83004	H112	≥6, <13	22
	Al-Mn-Mg	Plate & sheet	B209	Alclad 3004	A83004	H112	≥13, ≤75	22
	Al-Mn-Mg Al-Mn-Mg	Plate & sheet	B209	Alclad 3004	A83004 A83004	H32	≥0.43, <13	22
	Al-Mn-Mg	Plate & sheet Plate & sheet	B209 B209	Alclad 3004 Alclad 3004	A83004 A83004	H32 H34	≥13, ≤50 ≥0.23, <13	22 22
	Al-Mn-Mg	Plate & sheet	B209	Alclad 3004	A83004 A83004	H34		22
107	M-MII-Mg	rate & sneet	D2U7	Aiciau 3004	A03004	1134	≥13, ≤25	44
102	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T4 wld.		23
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T6 wld.		23
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T4		23
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T451	 ≥6, <13	23
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T451	≥13, ≤75	23
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T6		23

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

N	umbers in Par	rentneses		otes for Ap		Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1) and (4b)]							
		Min.		Min. Yield	Max. Use	Min.		<u>[IN</u>	otes (1)	anu (40)	<u>, </u>		
Line No.	Notes	Temp., °C (6)	Strength, MPa	Strength, MPa	Temp., °C	Temp. to 40	65	100	125	150	175	200	225
	(33)(69)	-269	97		204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
77	(69)	-269	172	69	204	46.0	46.0	46.0	45.9	41.6	28.8	17.6	16.1
78	(69)	-269	269	110	65	73.5	73.5					~V	
79	(69)	-269	241	97	65	64.4	64.4				(10	
80	(69)	-269	207	76	65	50.6	50.6				ري.		
										(21.		
81	(69)	-269	214	83	204	55.2	55.2	55.2	48.9	37.5	28.6	21.7	20.7
82	(69)	-269	283	131	65	87.3	87.3			*			
									C	41.			
	(22)(63)(69)	-269	165		204	55.2	<i>55.2</i>	55.2	54.3	52.0	46.3	35.3	34.8
	(22)(63)(69)	-269	165		204	55.2	55.2	55.2	54.3	52.0	46.3	35.3	34.8
	(33)(63)(69)	-269	179		204	59.8	59.8	59.8	58.9	56.3	50.2	38.3	35.9
86	(33)(63)(69)	-269	262	241	204	87.3	87.3	87.3	83.6	72.3	57.2	40.2	35.9
0.7	((0)	260	117		204	20.1	20.1	27.0	25.0	22.1	25.7	17.0	12.0
	(69) (69)	-269 -269	117 117		204 204	39.1 39.1	39.1 39.1	37.9 37.9	35.9 35.9	32.1 32.1	25.7 25.7	17.6 17.6	13.8 13.8
	(69)	-269 -269	117		204	39.1 39.1	39.1	37.9 37.9	35.9 35.9	32.1 32.1	25.7 25.7	17.6 17.6	13.8
	(13)(33)(69)	-269	131		204	43.7	43.7	43.7	43.7	43.7	35.8	23.9	10.3
	(13)(33)(69)	-269	151		204	50.6	50.6	48.7	46.6	41.4	27.5	15.3	13.8
	(33)(69)	-269	207		204	68.9	68.9	67.7	59.0	45.9	27.5	15.3	49.3
72	(33)(07)	207	207	172		00.5	00.5	07.7	33.0	13.5	27.5	15.5	17.5
93	(66)	-269	90	31	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
	(68)	-269	97		204	23.0	22.2	21.3	20.4	18.2	13.6	10.9	10.5
	(33)(66)	-269	103	41.	204	27.6	26.6	25.6	24.4	18.2	13.6	10.9	10.5
96	(33)(66)	-269	110	76	204	36.8	36.8	35.9	33.7	29.0	21.1	16.7	16.1
97	(33)(68)	-269	117	83	204	39.1	39.1	39.1	39.1	29.0	21.1	16.7	16.1
98	(33)(66)	-269	131	110	204	43.7	43.7	43.7	41.7	29.0	21.1	16.7	16.1
99	(33)(68)	-269	138	117	204	46.0	46.0	46.0	43.9	29.0	21.1	16.7	16.1
		1/1											
100	(66)	-269	145	55	204	36.8	36.8	36.8	36.8	36.8	26.9	17.4	16.1
	(68)	-269	152	59	204	39.1	39.1	39.1	39.1	38.9	26.9	17.4	16.1
	(33)(66)	-269	152	59	204	39.1	39.1	39.1	39.1	38.9	26.9	17.4	16.1
	(33)(68)	-269	159		204	41.4	41.4	41.4	41.4	38.9	26.9	17.4	16.1
	(33)[66]	-269	186		204	62.1	62.1	62.1	60.4	38.9	26.9	17.4	16.1
	(33)(68)	-269	193		204	64.4	64.4	64.4	60.4	38.9	26.9	17.4	16.1
	(33)(66)	-269	214		204	71.2	71.2	71.2	71.2	38.9	26.9	17.4	16.1
107	(33)(68)	-269	221	172	204	73.5	73.5	73.5	73.5	38.9	26.9	17.4	16.1
	(00) (10)						-			g = -		07.	
	(22)(63)	-269	165		204	<i>55.2</i>	55.2	55.2	54.3	52.0	46.3	35.3	34.8
	(22)(63)	-269	165		204	55.2	55.2	55.2	54.3	52.0	46.3	35.3	34.8
	(33)(66)	-269	186		204	62.1	62.1	62.1	61.0	58.3	52.1	39.7	35.9
	(33)(66)	-269	186		204	62.1	62.1	62.1	61.0	58.3	52.1 57.0	39.7	35.9
	(33)(68)	-269	207		204	68.9	68.9	68.9	67.8	64.8	57.9	40.2	35.9
113	(33)(66)	-269	262	221	204	87.3	87.3	87.3	83.8	72.3	57.2	40.2	35.9

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size, mm	P-No. (5)
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T651	≥6, <13	23
	Al-Mg-Si-Cu	Plate & sheet	B209	Alclad 6061	A86061	T651	≥13, ≤100	23
116	99.60Al	Plate & sheet	B209	1060	A91060	0		S 27
	99.60Al	Plate & sheet	B209	1060	A91060	H112	≥13, ≤25	21
118	99.60Al	Plate & sheet	B209	1060	A91060	H12		21
	99.60Al	Plate & sheet	B209	1060	A91060	H14	~ N. J	21
							8,0	
	99.0Al-Cu	Plate & sheet	B209	1100	A91100	0		21
	99.0Al-Cu	Plate & sheet	B209	1100	A91100	H112	≥13, ≤50	21
	99.0Al-Cu	Plate & sheet	B209	1100	A91100	H12		21
123	99.0Al-Cu	Plate & sheet	B209	1100	A91100	H14	•••	21
124	Al-Mn-Cu	Plate & sheet	B209	3003	A93003	< 0		21
125	Al-Mn-Cu	Plate & sheet	B209	3003	A93003	H112	≥13, ≤50	21
126	Al-Mn-Cu	Plate & sheet	B209	3003	A93003	H12		21
127	Al-Mn-Cu	Plate & sheet	B209	3003	A93003	H14		21
128	Al-Mn-Mg	Plate & sheet	B209	3004	A93004	0		22
	Al-Mn-Mg	Plate & sheet	B209	3004	A93004	H112		22
	Al-Mn-Mg	Plate & sheet	B209	3004	A93004	H32		22
	Al-Mn-Mg	Plate & sheet	B209	3004	A93004	H34		22
101	in in ing	Thate & Sheet	5207	Ch 2001	1175001	110 1	•••	22
132	Al-1.5Mg	Plate & sheet	B209	5050	A95050	0		21
133	Al-1.5Mg	Plate & sheet	B209	5050	A95050	H112		21
134	Al-1.5Mg	Plate & sheet	B209	5050	A95050	H32		21
135	Al-1.5Mg	Plate & sheet	B209	5050	A95050	H34		21
136	Al-2.5Mg	Plate & sheet	B209	5052	A95052	0	•••	22
	Al-2.5Mg	Plate & sheet	B209	5052	A95052	H112	 ≥13, ≤75	22
	Al-2.5Mg	Plate & sheet	B209	5052	A95052	H32		22
	Al-2.5Mg	Plate & sheet	B209	5052	A95052	H34		22
	14	0						
140	Al-4.4Mg-Mn	Plate & sheet	B209	5083	A95083	0	≥1.3, ≤38	25
141	Al-4.4Mg=Mn	Plate & sheet	B209	5083	A95083	H32	≥5, ≤38	25
142	Al-4.0Mg-Mn	Plate & sheet	B209	5086	A95086	0		25
143	Al-4.0Mg-Mn	Plate & sheet	B209	5086	A95086	H112	≥13, ≤25	25
144	Al-4.0Mg-Mn	Plate & sheet	B209	5086	A95086	H32		25
145	Al-4.0Mg-Mn	Plate & sheet	B209	5086	A95086	H34		25
146	Al-3.5Mg	Plate & sheet	B209	5154	A95154	0	•••	22
	Al-3.5Mg	Plate & sheet	B209	5154	A95154	H112	≥13, ≤75	22
	Al-3.5Mg	Plate & sheet	B209	5154	A95154	Н32		22
	Al-3.5Mg	Plate & sheet	B209	5154	A95154	Н34		22

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

				occo for Ap		Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1) and (4b)]							
		Min.	Min. Tensile	Min. Yield	Max. Use	Min.		L.	(-)	(20	,		
Line		Temp.,		Strength,	Temp.,	Temp.							
No.	Notes	°C (6)	MPa	MPa	°C	to 40	65	100	125	150	175	200	225
	(33)(66)	-269	262		204	87.3	87.3	87.3	83.8	72.3	57.2	40.2	35.9
115	(33)(68)	-269	290	241	204	96.5	96.5	96.5	92.5	79.9	63.1	40.2	35.9
												. 92	
116		-269	55		204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
	(13)(33)	-269	69		204	23.0	21.8	19.1	17.0	15.0	11.8	7.5	5.9
	(33)	-269	76		204	25.3	25.3	23.1	21.0	18.1	12.7	8.4	7.8
119	(33)	-269	83	69	204	27.6	27.6	27.6	26.6	18.1	12.7	8.4	7.8
120		-269	76	24	204	16.1	16.1	16.0	15.6	11.8	9.3	7.2	6.9
	(13)(33)	-269	83		204	23.0	23.0	22.7	21.6	16.3	11.8	7.5	6.9
	(33)	-269	97		204	32.2	32.2	31.3	25.2	19.0	13.6	8.5	7.8
	(33)	-269	110		204	36.8	36.8	36.1	33.1	19.0	13.6	8.5	7.8
120	(00)	20)	110	,,	201	20.0	50.0	00.1	O S.I	1710	1010	Olb	710
124		-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
125	(13)(33)	-269	103	41	204	27.6	26.6	25.6	24.4	18.2	13.6	10.9	10.5
126	(33)	-269	117	83	204	39.1	39.1	38.1	35.8	29.0	21.1	16.7	16.1
127	(33)	-269	138	117	204	46.0	46.0	46.0	43.9	29.0	21.1	16.7	16.1
						14	6						
128		-269	152	59	204	39.1	39.1	39.1	39.0	38.9	26.9	17.4	16.1
129	(33)	-269	159	62	204	41.4	41.4	41.4	41.4	38.9	26.9	17.4	16.1
130	(33)	-269	193	145	204	64.4	64.4	64.4	60.4	38.9	26.9	17.4	16.1
131	(33)	-269	221	172	204	73.5	73.5	73.5	73.5	38.9	26.9	17.4	16.1
400		2.60	40.4	il au	$\mathcal{O}_{\mathcal{I}}$	07.6	0.7.6	0.5.5	0.5.5	0==	20.4	400	
132		-269	124		204	27.6	27.6	27.5	27.5	27.5	20.1	10.8	9.7
	(33)	-269	138		204	36.8	36.7	36.7	36.6	35.8	20.1	10.8	9.7
	(33)	-269	152	1,	204	50.6	50.6	50.6	50.6	35.8	20.1	10.8	9.7
135	(33)	-269	473	138	204	57.5	<i>57.5</i>	57.5	57.5	35.8	20.1	10.8	9.7
136		-269	172	65	204	43.7	43.7	43.7	43.6	41.6	28.8	17.6	16.1
	(13)(33)	-269	172		204	43.7	43.7	43.7	43.6	41.6	28.8	17.6	16.1
	(33)	-269	214		204	71.2	71.2	71.2	71.0	41.6	28.8	17.6	16.1
	(33)	269	234		204	78.1	78.1	78.1	78.1	41.6	28.8	17.6	16.1
	(2)	0 -0											
140	(13)	-269	276	124	65	82.7	82.7						
141	(13)[33]	-269	303	214	65	101.1	101.1						
142		-269	241	97	65	64.4	64.4						
143	(13)(33)	-269	241	110	65	73.5	73.5						
	(33)	-269	276	193	65	91.9	91.9						
145	(33)	-269	303	234	65	101.1	101.1						
146		-269	207		65	50.6	50.4						
	(13)(33)	-269	207		65	50.6	50.4						
	(33)	-269	248		65	82.7	82.7						
149	(33)	-269	269	200	65	89.6	89.6		•••		•••		
	l												

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

Line	Nominal		Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
150	Al-3.5Mg	Plate & sheet	B209	5254	A95254	0		22
151	Al-3.5Mg	Plate & sheet	B209	5254	A95254	H112	≥13, ≤75	22
152	Al-3.5Mg	Plate & sheet	B209	5254	A95254	H32		22
153	Al-3.5Mg	Plate & sheet	B209	5254	A95254	H34		22
							0	9.
154	Al-2.7Mg-Mn	Plate & sheet	B209	5454	A95454	0	ا ری	22
155	Al-2.7Mg-Mn	Plate & sheet	B209	5454	A95454	H112	≥13, ≤75	22
156	Al-2.7Mg-Mn	Plate & sheet	B209	5454	A95454	H32	Ø ₂	22
157	Al-2.7Mg-Mn	Plate & sheet	B209	5454	A95454	H34	, , ,	22
						CM.		
158	Al-5.1Mg-Mn	Plate & sheet	B209	5456	A95456	0	≥1.3, ≤38	25
159	Al-5.1Mg-Mn	Plate & sheet	B209	5456	A95456	H32	≥5, <13	25
					•	6 C		
160	Al-2.5Mg	Plate & sheet	B209	5652	A95652	0	•••	22
161	Al-2.5Mg	Plate & sheet	B209	5652	A95652	H112	≥13, ≤75	22
162	Al-2.5Mg	Plate & sheet	B209	5652	A95652	H32	•••	22
163	Al-2.5Mg	Plate & sheet	B209	5652	A95652	H34		22
				**				
	Al-Mg-Si-Cu	Plate & sheet	B209	6061	A96061	T4 wld.		23
	Al-Mg-Si-Cu	Plate & sheet	B209	6061	A96061	T6 wld.		23
	Al-Mg-Si-Cu	Plate & sheet	B209	6061	A96061	T4		23
	Al-Mg-Si-Cu	Plate & sheet	B209	6061	A96061	Т6		23
168	Al-Mg-Si-Cu	Plate & sheet	B209	6061	A96061	T651	≥6, ≤100	23
169	Al-Mn-Cu	Forgings & fittings	B361	WP Alclad 3003	A83003	0		21
170	Al-Mn-Cu	Forgings & fittings	B361	WP Alclad 3003	A83003	H112		21
171	99.60Al	Forgings & fittings	B361	WP1060	A91060	0		21
172	99.60Al	Forgings & fittings	B361	WP1060	A91060	H112		21
1,2	33.00TH	Torgange & reenigs	Bool	***1000	1171000	11112	•••	21
		OK						
173	99.0Al-Cu	Forgings & fittings	B361	WP1100	A91100	0		21
174	00.041 C-	Faurium 0 fittings	D2/1	WP1100	A01100	11112		21
1/4	99.0Al-Cu	Forgings & fittings	B361	WP1100	A91100	H112		21
175	Al-Mn-Cu	Forgings & fittings	B247	3003	A93003	H112		21
	Al-Mn-Cu	Forgings & fittings	B247	3003	A93003	H112 wld.		21
	Al-Mn-Cu	Forgings & fittings	B361	WP3003	A93003	0		21
	-							
178	Al-Mn-Cu	Forgings & fittings	B361	WP3003	A93003	H112	•••	21
170	Al-Mn-Cu	Forgings & fittings	B247	5083	A95083	0		25
	Al-Mn-Cu	Forgings & fittings	B247 B247	5083	A95083	H112	•••	25 25
	Al-Mn-Cu	Forgings & fittings	B247 B247	5083	A95083	H112 wld.	•••	25 25
101	in min ou	1 orgings & numgs	DLTI	5005	1175005	IIIIL WIU.		23

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	umbers in Fal	chilleses	Min.	occs for Ap	Max.	Basic Allowable Stress, S, MPa, at Metal Temperature, °C [Notes (1) and (4b)]							
Line No.	Notes	Min. Temp., °C (6)	Tensile	Min. Yield Strength, MPa	Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225
150		-269	207		65	50.6	50.4						
	(13)(33)	-269	207		65	50.6	50.4		•••			•••	
152		-269	248		65	82.7	82.7						
	(33)	-269	269		65	89.6	89.6					28	•••
133	(33)	207	20)	200	03	07.0	02.0		•••			0,,	
154		-269	214	83	204	55.2	55.2	55.2	48.9	37.5	286	21.7	20.7
	(13)(33)	-269	214		204	55.2	55.2	55.2	48.9	37.5	28.6	21.7	20.7
	(33)	-269	248		204	82.7	82.7	82.7	49.5	37.5	28.6	21.7	20.7
	(33)	-269	269		204	89.6	89.6	89.6	49.5	37.5	28.6	21.7	20.7
10.	(00)	207	-07	200	-0.	07.0	07.0	07.0	17.0	N.	_0.0		
158	(13)	-269	290	131	65	87.3	87.3						
	(13)(33)	-269	317		65	105.7	105.7		8 /				
								· · · · · · · · · · · · · · · · · · ·	0,				
160		-269	172	65	204	43.7	43.7	43.7	43.6	41.6	28.8	17.6	16.1
161	(13)(33)	-269	172	65	204	43.7	43.7	43.7	43.6	41.6	28.8	17.6	16.1
162	(33)	-269	214	159	204	71.2	71.2	71.2	71.0	41.6	28.8	17.6	16.1
163	(33)	-269	234	179	204	78.1	78.1	78.1	78.1	41.6	28.8	17.6	16.1
						×X	6						
164	(22)(63)	-269	165		204	55.2	<i>55.2</i>	<i>55.2</i>	54.3	52.0	46.3	35.3	34.8
165	(22)(63)	-269	165		204	55.2	55.2	55.2	54.3	52.0	46.3	35.3	34.8
166	(33)(63)	-269	207	110	204	68.9	68.9	68.9	67.8	64.8	57.9	40.2	35.9
167	(33)	-269	290	241	204	96.5	96.5	96.5	92.5	79.9	63.1	40.2	35.9
168	(13)(33)	-269	290	241	204	96.5	96.5	96.5	92.5	79.9	63.1	40.2	35.9
169	(13)(14)(32)	-269	90	31,	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
109	(33)(66)	-209	90	131	204	20.7	19.9	19.3	10.4	17.3	13.0	10.9	10.5
170	(13)(14)(32) (33)(66)	-269	_ &	31	204	20.7	19.9	19.3	18.4	17.3	13.6	10.9	10.5
171	(13)(14)(32) (33)	-269	OC*55	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
172	(13)(14)(32) (33)	-269	√ 55	17	204	11.5	11.5	10.9	9.8	8.8	7.5	5.8	5.5
173	(13)(14)(3 2) (33)	-269	76	21	204	13.8	13.8	13.7	13.2	11.8	9.3	7.2	6.9
	(13)(14)(32) (33)	-269	76	21	204	13.8	13.8	13.7	13.2	11.8	9.3	7.2	6.9
	(9)(45)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
	(9)(45)	-269	97		204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
177	(13)(14)(32) (33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
178	(13)(14)(32) (33)	-269	97	34	204	23.0	22.1	21.4	20.5	18.2	13.6	10.9	10.5
179	(9)(32)(33)	-269	268	110	65	73.5	73.5						
	(9)(32)(33)	-269	268	110	65	73.5	73.5						
	(9)(32)(33)	-269	268		65	73.5	73.5						

Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

						Class /		
Line	Nominal		Spec.	Type/		Class/ Condition/	Size,	P-No.
No.	Composition	Product Form	No.	Grade	UNS No.	Temper	mm	(5)
182	Al-4.4Mg-Mn	Forgings & fittings	B361	WP5083	A95083	0		25
183	Al-4.4Mg-Mn	Forgings & fittings	B361	WP5083	A95083	H112		25
								0
	Al-3.5Mg	Forgings & fittings	B361	WP5154	A95154	0		22
185	Al-3.5Mg	Forgings & fittings	B361	WP5154	A95154	H112	(22
							્ જે	•
	Al-Mg-Si-Cu	Forgings & fittings	B247	6061	A96061	T6 wld.	. C.	23
	Al-Mg-Si-Cu	Forgings & fittings	B361	WP6061	A96061	T4 wld.	&~	23
	Al-Mg-Si-Cu	Forgings & fittings	B361	WP6061	A96061	T6 wld.		23
189	Al-Mg-Si-Cu	Forgings & fittings	B361	WP6061	A96061	T4		23
190	Al-Mg-Si-Cu	Forgings & fittings	B247	6061	A96061	H112 T6 wld. T4 wld. T6 wld. T4		23
	Al-Mg-Si-Cu	Forgings & fittings	B361	WP6061	A96061	T6, T6		23
-7-	in hig or ou	r orgango er munigo	2001	0001	11,000	()		
) `		
192	Al-Mg-Si	Forgings & fittings	B361	WP6063	A96063	T4 wld.		23
193	Al-Mg-Si	Forgings & fittings	B361	WP6063	A96063	T6 wld.		23
194	Al-Mg-Si	Forgings & fittings	B361	WP6063	A96063	T4		23
195	Al-Mg-Si	Forgings & fittings	B361	WP6063	A96063	Т6		23
				:67				
	Al-Si-Mg	Castings	B26	356.0	A03560	T71		26
	Al-Si-Mg	Castings	B26	356.0	A03560	Т6		26
198	Al-Si	Castings	B26	443.0	A04430	F		
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Table A-1M Basic Allowable Stresses in Tension for Metals (SI Units) (Cont'd)

	Basic Allowable Stress, S, MPa, at Metal Temperature, °C Min. Max. [Notes (1) and (4b)]												
Line No.	Notes	Min. Temp., °C (6)	Tensile	Min. Yield Strength, MPa	Use Temp., °C	Min. Temp. to 40	65	100	125	150	175	200	225
	(13)(32)(33)	-269	269		65	73.5	73.5						
	(13)(32)(33)	-269	269		65	73.5	73.5						
	(==)(==)(==)												
184	(32)(33)	-269	207	76	65	50.6	50.6					W.00	
	(32)(33)	-269	207	76	65	50.6	50.6					0.	
											n	V	
186	(9)(22)	-269	165		204	55.2	<i>55.2</i>	<i>55.2</i>	54.3	52.0	46.3	35.3	34.8
187	(22)(32)(63)	-269	165		204	55.2	<i>55.2</i>	<i>55.2</i>	54.3	52.00	46.3	35.3	34.8
188	(22)(32)(63)	-269	165		204	55.2	<i>55.2</i>	<i>55.2</i>	54.3	52.0	46.3	35.3	34.8
189	(13)(32)(33) (63)	-269	179	110	204	59.8	59.8	59.8	58.9	56.3	50.2	38.3	35.9
190	(9)(33)	-269	262	241	204	87.3	87.3	87.3	83.6	72.3	<i>57.2</i>	40.2	35.9
191	(13)(32)(33)	-269	262	241	204	87.3	87.3	87.3	83.6	72.3	57.2	40.2	35.9
	(63)						•	o Ox					
192	(32)	-269	117	•••	204	39.1	39.1	37.6	36.0	32.0	24.7	15.3	13.8
	(32)	-269	117		204	39.1	39.1	37.6	36.0	32.0	24.7	15.3	13.8
194	(13)(32)(33)	-269	124	62	204	41.4	4 1.3	41.3	41.0	41.0	33.9	22.6	9.8
195	(13)(32)(33)	-269	207	172	204	68.9	68.9	67.7	59.0	45.9	27.5	15.3	13.8
196	(9)(43)	-269	172	124	204	57.5	<i>57.5</i>	<i>57.5</i>	55.0	49.8	38.6	18.9	16.5
197	(9)(43)	-269	207	138	121	68.9	68.9	68.9	<i>57.9</i>				
198	(9)(43)	-269	117	48	204	32.0	32.0	32.0	32.0	32.0	32.0	32.0	24.1
	ASMEN	ORM		48 ()									

Table A-1A Basic Casting Quality Factors, E_c

Spec. No.	Description	<i>E_c</i> [Note (2)]	Appendix A Notes
Iron			
A47	Malleable iron castings	1.00	(9)
A48	Gray iron castings	1.00	(9)
A126	Gray iron castings	1.00	(9)
A197	Cupola malleable iron castings	1.00	(9) _C
A278	Gray iron castings	1.00	(9)
A395	Ductile and ferritic ductile iron castings	0.80	(9), (40)
A536	Ductile iron castings	0.80	9 (9), (40)
A571	Austenitic ductile iron castings	0.80	(9), (40)
Carbon Steel	Austenitic ductile iron castings Carbon steel castings Ferritic steel castings Martensitic stainless and alloy castings Ferritic steel castings Centrifugally cast pipe Austenitic steel castings Centrifugally cast pipe Steel castings		
A216	Carbon steel castings	0.80	(9), (40)
A352	Ferritic steel castings	0.80	(9), (40)
Low and Intermediate Alloy Steel		401	
A217	Martensitic stainless and alloy castings	0.80	(9), (40)
A352	Ferritic steel castings	0.80	(9), (40)
A426	Centrifugally cast pipe	1.00	(10)
Stainless Steel	ine		
A351	Austenitic steel castings	0.80	(9), (40)
A451	Centrifugally cast pipe	0.90	(10), (40)
A487	Steel castings	0.80	(9), (40)
Copper and Copper Alloy	tick		
B61	Steam bronze castings	0.80	(9), (40)
B62	Composition bronze castings	0.80	(9), (40)
B148	Al-bronze and Si-Al-bronze castings	0.80	(9), (40)
B584	Copper alloy castings	0.80	(9), (40)
Nickel and Nickel Alloy	0.		
Nickel and Nickel Alloy A494 Aluminum Alloy	Nickel and nickel alloy castings	0.80	(9), (40)
Aluminum Alloy			
B26, Temper F	Aluminum alloy castings	1.00	(9), (10)
B26, Temper T6, T71	Aluminum alloy castings	0.80	(9), (40)
Titanium and Titanium Alloy			
B367	Titanium and titanium alloy castings	0.80	(9), (40)

(18) Table A-1B Basic Quality Factors for Longitudinal Weld Joints in Pipes and Tubes, E_i

Spec. No.	Class (or Type)	Description	<i>E_j</i> [Note (2)]	Appendix A Notes
Carbon Ste	eel			
API 5L		Seamless pipe	1.00	
		Electric fusion welded pipe, 100% radiographed	1.00	•••
		Electric resistance welded pipe	0.85	
		Electric fusion welded pipe, double butt seam	0.95	
		Continuous welded (furnace butt welded) pipe	0.60	
A53	Type S	Seamless pipe	1.00	
	Type E	Electric resistance welded pipe	0.85	
	Type F	Seamless pipe Electric resistance welded pipe Furnace butt welded pipe Seamless pipe	0.60	
A106		Seamless pipe	1.00	
A134		Electric fusion welded pipe, single butt, straight or spiral (helical) seam	0.80	
A135		Electric resistance welded pipe	0.85	•••
A139		Electric fusion welded pipe, straight or spiral (helical) seam	0.80	
A179		Seamless tube Seamless tube Seamless tube Seamless pipe Electric resistance welded pipe Seamless tube Seamless pipe	1.00	
A333		Seamless pipe	1.00	
		Electric resistance welded pipe	0.85	
A334		Seamless tube	1.00	
A369		Seamless pipe	1.00	
A381		Electric fusion welded pipe, 100% radiographed	1.00	
		Electric fusion welded pipe, spot radiographed	0.90	(19)
		Electric fusion welded pipe, as manufactured	0.85	
A524		Seamless pipe	1.00	
A587		Electric resistance welded pipe	0.85	
A671	12, 22, 32, 42, 52	Electric fusion welded pipe, 100% radiographed	1.00	
	13, 23, 33, 43, 53	Electric fusion welded pipe, double butt seam	0.85	
A672	12, 22, 32, 42, 52	Electric fusion welded pipe, 100% radiographed	1.00	
	13, 23, 33, 43, 53	Electric fusion welded pipe, double butt seam	0.85	
A691	12, 22, 32, 42, 52	Electric fusion welded pipe, 100% radiographed	1.00	
	13, 23, 33, 43, 53	Electric fusion welded pipe, double butt seam	0.85	
Low and I	ntermediate Alloy St	pel .		
A333		Seamless pipe	1.00	
11000	MIL	Electric resistance welded pipe	0.85	(78)
A334 💙	9 .	Seamless tube	1.00	
A335		Seamless pipe	1.00	
A369		Seamless pipe	1.00	
A671	12, 22, 32, 42, 52	Electric fusion welded pipe, 100% radiographed	1.00	
	13, 23, 33, 43, 53	Electric fusion welded pipe, double butt seam	0.85	(78)
A672	12, 22, 32, 42, 52	Electric fusion welded pipe, 100% radiographed	1.00	•••
	13, 23, 33, 43, 53	Electric fusion welded pipe, double butt seam	0.85	(78)
A691	12, 22, 32, 42, 52	Electric fusion welded pipe, 100% radiographed	1.00	
	13, 23, 33, 43, 53	Electric fusion welded pipe, double butt seam	0.85	(78)

Table A-1B Basic Quality Factors for Longitudinal Weld Joints in Pipes and Tubes, E_i (Cont'd)

Spec. No.	Class (or Type)	Description	<i>E_j</i> [Note (2)]	Appendix A Notes
Stainless S	Steel			
A249		Electric fusion welded tube, single butt seam	0.80	
A268		Seamless tube	1.00	
		Electric fusion welded tube, double butt seam	0.85	O
		Electric fusion welded tube, single butt seam	0.80	7/0
A269		Seamless tube	1.00 🦵	,
		Electric fusion welded tube, double butt seam	0.85	
		Electric fusion welded tube, single butt seam	0.80	
A270		Seamless tube	1.00	
		Electric fusion welded tube, double butt seam	0.85	
		Seamless tube Electric fusion welded tube, double butt seam Electric fusion welded tube, single butt seam Seamless pipe Electric fusion welded pipe, double butt seam Electric fusion welded pipe, single butt seam Electric fusion welded pipe, 100% radiographed Electric fusion welded pipe, 100% radiographed	0.80	
A312		Seamless pipe	1.00	
		Electric fusion welded pipe, double butt seam	0.85	
		Electric fusion welded pipe, single butt seam	0.80	
		Electric fusion welded pipe, 100% radiographed	1.00	(46)
A358	1, 3, 4	Electric fusion welded pipe, 100% radiographed	1.00	
	5	Electric fusion welded pipe, spot radiographed	0.90	
	2	Electric fusion welded pipe, double butt seam	0.85	
A376		Seamless pipe	1.00	
A409		Electric fusion welded pipe, double butt seam	0.85	
		Electric fusion welded pipe, single butt seam	0.80	
A789		Seamless tube	1.00	
		Electric fusion welded tube, 100% radiographed	1.00	
		Electric fusion welded tube, double butt	0.85	
		Electric fusion welded tube, single butt	0.80	
A790		Seamless pipe	1.00	
		Electric fusion welded pipe, 100% radiographed	1.00	
		Electric fusion welded pipe, double butt	0.85	
	o o	Electric fusion welded pipe, single butt	0.80	
A813	DW	Electric fusion welded pipe, double butt	0.85	
	SW	Electric fusion welded pipe, single butt	0.80	
A814	DW DW	Electric fusion welded pipe, double butt	0.85	
	SW	Electric fusion welded pipe, single butt	0.80	
A928	1, 3, 4	Electric fusion welded pipe, 100% radiographed	1.00	
	5	Electric fusion welded pipe, spot radiographed	0.90	
	2	Electric fusion welded pipe, double butt seam	0.85	
	d Copper Alloy			
B42		Seamless pipe	1.00	
B43		Seamless pipe	1.00	
B68		Seamless tube	1.00	
B75		Seamless tube	1.00	

Table A-1B Basic Quality Factors for Longitudinal Weld Joints in Pipes and Tubes, E_i (Cont'd)

Spec. No.	Class (or Type)	Description	<i>E_j</i> [Note (2)]	Appendix A Notes
Copper an	d Copper Alloy (Con	ıt'd)		
B88	•••	Seamless water tube	1.00	
B280		Seamless tube	1.00	
				6
B466		Seamless pipe and tube	1,00	
B467		Electric resistance welded pipe	0.85	
		Electric fusion welded pipe, double butt seam	0.85	
		Electric resistance welded pipe Electric fusion welded pipe, double butt seam Electric fusion welded pipe, single butt seam Seamless pipe and tube Welded pipe Welded pipe Welded pipe Welded pipe, 100% radiographed Electric fusion welded pipe double butt seam	0.80	
Nickel and	Nickel Alloy	ME		
B161		Seamless pipe and tube	1.00	
B163		Seamless tube	1.00	
B165		Seamless pipe and tube	1.00	
B167		Seamless pipe and tube	1.00	
B407		Seamless pipe and tube	1.00	
B444		Seamless pipe and tube	1.00	
B464		Welded pipe	0.80	
B474	1, 3, 4	Welded pipe, 100% radiographed	1.00	
	2	Electric fusion welded pipe, double butt seam	0.85	
B514		Welded pipe	0.80	
B515		Welded tube	0.80	
B619		Electric resistance welded pipe	0.85	•••
		Electric fusion welded pipe, double butt seam	0.85	
		Electric fusion welded pipe, single butt seam	0.80	
B622		Seamless pipe and tube	1.00	
B626	All	Electric resistance welded tube	0.85	
D020	All	Electric fusion welded tube, double butt seam	0.85	•••
		Electric fusion welded tube, single butt seam	0.80	•••
B668	All	Seamless pipe and tube	1.00	•••
B675	All	Welded pipe	0.80	
B690	All	Seamless pipe and tube	1.00	
B704	Shi	Welded tube	0.80	
B701		Welded pipe	0.80	
B725		Electric fusion welded pipe, double butt seam	0.85	
D7 20		Electric fusion welded pipe, single butt seam	0.80	
B729		Seamless pipe and tube	1.00	
D004	1 2 5	Walded vine 1000/ redience led	1.00	
B804	1, 3, 5	Welded pipe, 100% radiographed	1.00	
	2, 4	Welded pipe, double fusion welded	0.85	•••
	6	Welded pipe, single fusion welded	0.80	

Table A-1B Basic Quality Factors for Longitudinal Weld Joints in Pipes and Tubes, E_i (Cont'd)

Spec. No.	Class (or Type)	Description	<i>E_j</i> [Note (2)]	Appendix A Notes
Titanium a	and Titanium Alloy			
B338		Seamless tube	1.00	
		Electric fusion welded tube, 100% radiographed	1.00	
		Electric fusion welded tube, double butt seam	0.85	O
		Electric fusion welded tube, single butt seam	0.80	7/2
B861		Seamless pipe	1.00	9
B862		Electric fusion welded pipe, 100% radiographed	1.00	
		Electric fusion welded pipe, double butt seam	0.85	
		Electric fusion welded pipe, single butt seam	0.80	
Zirconium	and Zirconium Alloy	Electric fusion welded pipe, single butt seam Electric fusion welded pipe, single butt seam Seamless tube Electric fusion welded tube Seamless pipe Electric fusion welded pipe Seamless tube Seamless pipe and tube Welded pipe and tube, 100% radiographed		
B523		Seamless tube	1.00	
		Electric fusion welded tube	0.80	
B658		Seamless pipe	1.00	
		Electric fusion welded pipe	0.80	
		11/13		
Aluminum	•		4.00	
B210		Seamless tube	1.00	
B241		Seamless pipe and tube	1.00	
B547				
		Welded pipe, single butt seam	0.85 0.80	
	ASMENOR	Welded pipe, single butt seam Welded pipe, single butt seam W		

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Table A-2 Design Stress Values for Bolting Materials

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

		Class/						Specifie Strengt		Met	ign St al Te °F [N	mpe	ratur		
Nominal Compositio	Product n Form	Spec. No.		UNS No.	Class/ Condition/ Temper	Size Range, Dia., in.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300	400	500
	Bolts	A675	45	D40450			(8f)(8g)	-20	45	22.5	11.3	11.3	11.3	11.3	11.3
	Bolts	A675	50	D40500			(8f)(8g)	-20	50	25	12.5	12.5	12.5	12. 5	12.5
	Bolts	A675	55	D40550			(8f)(8g)	-20	55	27.5	13.8			. •	13.8
	Bolts	A307					(8f)(8g)	-20	60		15.0		_/ /		15.0
	Bolts	A675	60	D40600			(8f)(8g)	-20	60	30	15.0	\ \150	15.0	15.0	15.0
	Bolts	A675		D40650			(8g)	-20	65	32.5	12				16.3
	Bolts	A675		D40700			(8g)	-20	70		17.5				17.5
•••	Bolts	A675		D40800			(8g)	-20	80	40	20.0				20.0
	Bolts	F3125		K02706			(8g)	-20	120	92	23.0				23.0
	2016								4	_	20.0	20.0	20.0	20.0	20.0
	Nuts	A194		K01503			(42)	-20	` O;						
	Nuts	A194		K04002			(42)	-55							
	Nuts	A194	2H	K04002			(42)	-55							
	Nuts	A194		K04002			(42)	-55							
	Nuts,	A563	A	K05802			(42b)	-20							
	hvy. hex					sien	KLE								
Alloy Steel						W.S.									
Cr-½Mo	Bolts	A193	В7М	G41400		≤4 110		-55	100	80	20.0	20.0	20.0	20.0	20.0
Cr-½Mo	Bolts	A320		G41400		≥21/ ₂		-100	100	80	20.0				20.0
5Cr	Bolts	A193		S50100	X	≤4	(15)	-20	100	80	20.0				20.0
Cr-Mo-V	Bolts	A193		K14072	cjilo	>2 ¹ / ₂ , ≤4	(15)	-20	110	95	22.0				22.0
Alloy steel	Bolts	A354	D.C.	K04100	, · ·	>2 ¹ / ₂ , ≤4	(15)	0	115	99	23.0	22.0	22.0	22.0	23.0
Cr-Mo	Bolts	A193		G41400	7,	$>2^{1}/2, \le 4$ $>2^{1}/2, \le 4$	(15)	-40	115	95	23.0				23.0
Ni-Cr-Mo	Bolts	A320		G43400		>∠ / ₂ , ≤4 ≤4		-150	125	105	25.0				25.0
Cr-Mo	Bolts	A320		041400		≤4 ≤2 ¹ / ₂	(15) (15)	-150 -150	125	105	25.0				25.0
Cr-Mo	Bolts	A320	()	G40370		$\leq 2^{1/2}$	(15)	-150	125	105	25.0				25.0
Cr-Mo	Bolts	A320	()	G41370		$\leq 2^{1}/_{2}$	(15)	-150	125	105	25.0				25.0
Cr-Mo	Bolts	A320	7.	G87400		$\leq 2^{1}/_{2}$	(15)	-150	125	105	25.0				25.0
		Ο,					(-)								
Cr-Mo	Bolts	A193		G41400		≤2 ¹ / ₂		-55	125	105	25.0				25.0
Cr-Mo-V	Bolts	A193		K14072		≤2 ¹ / ₂	(15)	-20	125	105	25.0				25.0
Alloy steel	CBolts	A354		K04100		≤2 ¹ / ₂	(15)	0	125	109					25.0
Alloy steel	Bolts	A354	BD	K04100		≤4	(15)	-20	150	130	30.0	30.0	30.0	30.0	30.0
5Cr	Nuts	A194	3	S50100			(42)	-20							
C-Mo	Nuts	A194	4	K14510			(42)	-55							
C-Mo	Nuts	A194	4L	K14510			(42)	-150							
Cr-Mo	Nuts	A194	7	G41400			(42)	-55							
Cr-Mo	Nuts	A194	7L	G41400			(42)	-150							
Cr-Mo	Nuts	A194	7M	G41400			(42)	-55							
Cr-Mo	Nuts	A194	7ML	G41400			(42)	-100							

Table A-2 Design Stress Values for Bolting Materials

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

Design Stress, ksi, at Metal Temperature, °F [Note (1)]

600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
11.3	11.1	10.7	10.4	9.2	7.9	5.9	4.0												45	A675
12.5	12.4	11.9	10.7	9.2	7.9	5.9	4.0												50	A675
13.8	13.6	13.1	12.7	10.8	8.7	5.9	4.0												55	A675
																			B	A307
																		$^{\prime}$ $^{\circ}$) *	
	14.8						4.0											7,	60	A675
	16.1					6.3	4.0										<i>,</i> &	J	65	A675
	17.3			12.0	9.3	6.7	4.0												70	A675
	19.8															S			80	A675
23.0	23.0	23.0	•••											•••	/				A325	F3125
															Š	`			1	A194
																			2	A194
														Δ	٠				2H	A194
														X					2HM	A194
													(1)	·* 					A	A563
												Nike	ટ `							
												N.								
											110									y Steel
					16.3		8.5	4.5	2.4		"			•••					B7M	A193
					16.3		8.5	4.5	2.4										L7M	A320
					14.3		8.0	5.8	4.2	2.9	1.8	1.0	0.6						B5	A193
22.0	22.0	22.0	22.0	22.0	21.0	18.5	15.3	11.0	6.3	2.8	1.2			•••					B16	A193
23.0	23.0								• •										ВС	A354
			23.0	20.0	16.3	12.5	8.5	4.5	2.4										В7	A193
	25.0						C)											L43	A320
	25.0					(٠,١												L7	A320
	25.0					(O)													L7A	A320
	25.0				11.)													L7B	A320
	25.0				$\mathcal{I}_{\mathcal{I}_{\mathcal{I}}}$														L7C	A320
				\mathcal{O}'																
				.		17.0		8.5	4.5	2.4									B7	A193
		-	25.0	25.0	23.5	20.5	16.0	11.0	6.3	2.8	1.2								B16	A193
	25.0																		BC	A354
30.0	30.0																		BD	A354
																			3	A194
																			4	A194
																			4L	A194
																			7	A194
																			7L	A194
																			7M	A194
																			7ML	A194

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

								· · ·	Specifie Strengt			ign Stre tal Tem °F [Not	perat	ure,
Nominal Composition	Product Form	Spec. No.		UNS No.	Class/ Condition/ Temper	Size Range, Dia., in.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200 3	00 40	00 500
Stainless Steel														
16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2	>1½, ≤1½	(15)(60)	-325	90	50	18.8	17.3 1	5.6 14	.3 13.3
16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	90	50	18.8	17.3 1	5.6 14	3 13.3
18Cr-8Ni	Bolts	A193	B8	S30400	2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	100	50	18.8	16.7_1	5.0 13	.8 12.9
18Cr-8Ni	Bolts	A320	B8	S30400	2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	100	50	18.8	16.7 1	5 .0 13	.8 12.9
18Cr-10Ni-Cb	Bolts	A193	B8C		2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	100	50	18.8	17.9 1	6.5 15	5.5 15.0
18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	100	50	18.8	17.9 1	6.5 15	5.5 15.0
18Cr-10Ni-Ti	Bolts	A193	B8T	S32100	2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	100	50 🗸	18.8	17.8 1	6.5 15	.3 14.3
18Cr-10Ni-Ti	Bolts	A320	B8T	S32100	2	>1 ¹ / ₄ , ≤1 ¹ / ₂	(15)(60)	-325	100	50	18.8	17.8 1	6.5 15	.3 14.3
18Cr-9Ni	Bolts	A320	B8F	S30300	1		(8f)(15)	-325	75	C ₃₀	18.8	16.7 1	5.0 13	.8 12.9
							(39)		of P					
19Cr-9Ni	Bolts	A453	651B			>3	(15)(35)	-20	95	50	23.8	23.4 2	2.1 21	.3 20.8
19Cr-9Ni	Bolts		651B			≤3	(15)(35)	-20	95	60	23.8			.3 20.8
19Cr-9Ni	Bolts	A453	651A			>3	(15)(35)	-20	100	60	23.8	23.4 2	2.1 21	.3 20.8
19Cr-9Ni	Bolts		651A			≤3	(15)(35)	-20	100	70	23.8			.3 20.8
16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2	>1, ≤1 ¹ / ₄	(15)(60)	-325	105	65	18.8	17.3 1	6.3 16	.3 16.3
16Cr-12Ni-2Mo	Bolts	A320		S31600	2	>1, ≤1 ¹ / ₄	(15)(60)	-325	105	65	18.8			.3 16.3
18Cr-10Ni-Cb	Bolts	A193			2	>1, ≤1 ¹ / ₄	(15)(60)	-325	105	65	18.8			.3 16.3
18Cr-10Ni-Cb	Bolts	A320		S34700	2	≥10≤1 ¹ / ₄	(15)(60)		105	65	18.8			.3 16.3
18Cr-8Ni	Bolts	A193		S30400	2	>1, ≤1 ¹ / ₄	(15)(60)		105	65	18.8			.3 16.3
18Cr-8Ni	Bolts	A320		S30400	2/10	>1, ≤1 ¹ / ₄	(15)(60)		105	65	18.8			.3 16.3
18Cr-10Ni-Ti	Bolts	A193		S32100		>1, ≤1 ¹ / ₄	(15)(60)	-325	105	65	18.8			.3 16.3
18Cr-10Ni-Ti	Bolts	A320		S32100	2	>1, ≤1 ¹ / ₄	(15)(60)	-325	105	65	18.8			.3 16.3
					4.	, .4	(-)()							
18Cr-10Ni-Ti	Bolts	A193	В8Т	S32100	1		(8f)(15) (28)	-325	75	30	18.8	17.8 1	6.5 15	3.3 14.3
18Cr-8Ni	Bolts	A320	B8	S30400	1		(8f)(15) (28)	-425	75	30	18.8	16.7 1	5.0 13	.8 12.9
18Cr-10Ni-Cb	Bolts	A193	B8C		1		(8f)(15) (28)	-425	75	30	18.8	17.9 1	6.5 15	5.5 15.0
16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	1		(8f)(15) (28)	-325	75	30	18.8	17.3 1	5.6 14	.3 13.3
/	Mi													
16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2	>³/ ₄ , ≤1	(15)(60)		100	80	20.0	20.0 2	0.0 20	.0 20.0
16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	>³⁄₄, ≤1	(15)(60)	-325	100	80	20.0	20.0 2	0.0 20	.0 20.0
18Cr-10Ni-Cb	Bolts	A193	B8C		2	>³/ ₄ , ≤1	(15)(60)	-325	115	80	20.0	20.0 2	0.0 20	.0 20.0
18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	>³/ ₄ , ≤1	(15)(60)	-325	115	80	20.0	20.0 2	0.0 20	.0 20.0
18Cr-8Ni	Bolts	A193	B8	S30400	2	>³/ ₄ , ≤1	(15)(60)		115	80	20.0	20.0 2	0.0 20	.0 20.0
18Cr-8Ni	Bolts	A320	B8	S30400	2	>³/ ₄ , ≤1	(15)(60)	-325	115	80	20.0	20.0 2	0.0 20	.0 20.0
18Cr-10Ni-Ti	Bolts	A193	B8T	S32100	2	>³/ ₄ , ≤1	(15)(60)	-325	115	80	20.0	20.0 2	0.0 20	.0 20.0
18Cr-10Ni-Ti	Bolts	A320	B8T	S32100	2	>³⁄ ₄ , ≤1	(15)(60)	-325	115	80	20.0	20.0 2	0.0 20	.0 20.0
12Cr	Bolts	A437	B4C	S42200			(35)	-20	115	85	21.3	21.3 2	1.3 21	.3 21.3
13Cr	Bolts	A193	В6	S41000		≤4	(15)(35)	-20	110	85	21.3	21.3 2	1.3 21	.3 21.3

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

Design Stress, ksi, at Metal Temperature, °F [Note (1)]

600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
																			Stainles	s Steel
12.6	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5										B8M Cl. 2	
12.6	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5										B8M CL2	
							12.5		12.5										B8 Cl. 2	
12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5	12.5									O)	A320
								13.4	12.5									V.	B8C Cl. 2	
								13.4	12.5								(S))	B8C Cl. 2	
							12.5		12.5								⟨~;```		B8T Cl. 2	
							12.5	12.5	12.5							CN			B8T Cl. 2	
12.3	12.0	11.7	11.5	11.2	11.0										5	So.			B8F Cl. 1	A320
															1	Υ				
20.5	20.4	20.3	20.2	20.0	197	193	18.9	18 2	17.5					<	, O				651B	A453
							18.9		17.5					SO'					651B	A453
							18.9		17.5			•••		K.		•••			651A	A453
							18.9		17.5			•••	102			•••			651A	A453
20.5	20.1	20.0	20.2	20.0	17.7	17.0	10.7	10.2	17.0				2)				•••		00111	11100
16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3			R							B8M Cl. 2	A193
							16.3		16.3			7							B8M Cl. 2	
							16.3		16.3		ile								B8C Cl. 2	
16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	C)								B8C Cl. 2	A320
16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	1									B8 Cl. 2	A193
16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	C)									B8 Cl. 2	A320
16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3										B8T Cl. 2	A193
16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3	16.3										B8T Cl. 2	A320
							($O{L_{\mu}}$												
13.5	13.2	13.0	12.7	12.6	12.4	12.3	121	12.0	9.6	6.9	5.0	3.6	2.6	1.7	1.1	8.0	0.5	0.3	B8T Cl. 1	A193
							٠.													
12.3	12.0	11.7	11.5	11.2	11.0	10.8	10.6	10.4	10.1	9.8	7.7	6.1	4.7	3.7	2.9	2.3	1.8	1.4	B8 Cl. 1	A320
143	14.0	138	137	13 6	135	134	134	13.4	12.1	9.1	6.1	4.4	3.3	2.2	1.5	1.2	0.9	0.8	B8C Cl. 1	Δ193
11.5	11.0	15.0	15.7		14.5	13.1	15.1	13.1	12.1	7.1	0.1	1.1	5.5	2.2	1.5	1.2	0.5	0.0	DOG GI. I	11173
12.6	12.3	12.1	11.9	11.8	11.6	11.5	11.4	11.3	11.2	11.1	9.8	7.4	5.6	4.2	3.2	2.4	1.8	1.4	B8M Cl. 1	A193
		CA	7,																	
	· \							20.0	20.0										B8M Cl. 2	
							20.0		20.0										B8M Cl. 2	
							20.0		20.0										B8C Cl. 2	
							20.0		20.0										B8C Cl. 2	
							20.0		20.0										B8 Cl. 2	
							20.0		20.0										B8 Cl. 2	
							20.0		20.0										B8T Cl. 2	
20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0	20.0										B8T Cl. 2	A320
24.0	24.0	24.0	24.0																D4C	A 405
								•••									•••		B4C	A437
21.3	21.3	21.3	21.3	21.3	21.3	20.2	18.7												B6	A193

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

									Specifie Strengt		Met	ign Si al Te °F [N	mpe	ratur	
Nominal Composition	Product Form	Spec. No.		UNS No.		Size Range, Dia., in.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300	400	500
Stainless Steel															
14Cr-24Ni	Bolts	A453	660	S66286	Α		(15)(35)	-325	130	85	21.3	21.3	21.3	21.3	21.3
14Cr-24Ni	Bolts	A453	660	S66286	В		(15)(35)	-325	130	85	21.3	21.3	21.3	21.3	21.3
16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2	≤ ³ / ₄	(15)(60)	-325	110	95	22.0	22.0	22.0	22.0	22.0
16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	≤ ³ / ₄	(15)(60)	-325	110	95	22.0	22.0	22.0	22.0	22.0
18Cr-10Ni-Cb	Bolts	A193	B8C		2	≤3/4	(15)(60)	-325	125	100	25.0	25.0	25.0	25.0	25.0
18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	≤ ³ / ₄	(15)(60)	-325	125	100	25.0	25.0	25.0	25.0	25.0
18Cr-8Ni	Bolts	A193	B8	S30400	2	≤ ³ / ₄	(15)(60)	-325	125	100	25.0	25.0	25.0	25.0	25.0
18Cr-8Ni	Bolts	A320	B8	S30400	2	≤ ³ / ₄	(15)(60)	-325	125	100	25.0	25.0	25.0	25.0	25.0
18Cr-10Ni-Ti	Bolts	A193	B8T	S32100	2	≤ ³ / ₄	(15)(60)	-325	125	100	25.0	25.0	25.0	25.0	25.0
18Cr-10Ni-Ti	Bolts	A320	B8T	S32100	2	≤ ³ / ₄	(15)(60)	-325	125	100	25.0	25.0	25.0	25.0	25.0
12Cr	Bolts	A437	B4B	S42225			(35)	-20	145	105	26.3	26.3	26.3	26.3	26.3
12Cr	Nuts	A194	6	S41000			(35)(42)	-20							
18Cr-9Ni	Nuts	A194	8FA	S30300			(428)	-20							
16Cr-12Ni-2Mo	Nuts	A194	8MA	S31600		W	(42)	-325							
18Cr-10Ni-Ti	Nuts	A194	8TA	S32100		*O	(42)	-325							
18Cr-8Ni	Nuts	A194	8	S30400	×		(42)	-425							
18Cr-8Ni	Nuts	A194	8A	S30400	cillo		(42)	-425							
18Cr-10Ni-Cb	Nuts	A194	8CA	S34700			(42)	-425							
A.	MEN	ORING.	MOO	\$34700											

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

Design Stress, ksi, at Metal Temperature, °F [Note (1)]

600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	1,350	1,400	1,450	1,500	Type/ Grade	Spec. No.
																	S	tainles	s Steel (Cont'd)
21.3	21.3	21.3	21.3	21.3	21.3	21.3	21.3	21.3	21.3										660 Cl. A	A453
21.3	21.3	21.3	21.3	21.3	21.3	21.3	21.3	21.3	21.3										660 CLB	A453
																			0,	
22.0	22.0	22.0	22.0	22.0	22.0	22.0	22.0	22.0	22.0									0	B8M Cl. 2	A193
22.0	22.0	22.0	22.0	22.0	22.0	22.0	22.0	22.0	22.0									, N	B8M Cl. 2	A320
																	0	5		
24.6	24.5	24.5	24.5	24.5	24.5	24.4	24.2	23.9	23.5								<u>ر ب</u> ۷		B8C Cl. 2	A193
								23.9	23.5								Y		B8C Cl. 2	A320
25.0	25.0	25.0	25.0	25.0	25.0	25.0	24.7	23.9	22.9						,	(S)			B8 Cl. 2	A193
25.0	25.0	25.0	25.0	25.0	25.0	25.0	24.7	23.9	22.9						<u>k</u> \	Y			B8 Cl. 2	A320
25.0	25.0	25.0	25.0	25.0	25.0	25.0	25.0	25.0	25.0						`O,				B8T Cl. 2	A193
25.0	25.0	25.0	25.0	25.0	25.0	25.0	25.0	25.0	25.0										B8T Cl. 2	A320
														Q~						
26.3	26.3	26.3											11:5						B4B	A437
													YO.						6	A194
												30)						8FA	A194
											_	4								
											10								8MA	A194
											7.								8TA	A194
										" XC	,									
										3/2									8	A194
																			8A	A194
									·										8CA	A194

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

									Specifie Strengt		Tempe	at Me	tal e, °F
Nominal Composition	Product Form	Spec. No.		UNS No.	Class/ Condition/ Temper	Size Range, Dia., in.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300
Copper and Cop	per Alloy												
Naval brass	Bolts	B21		C46400	060		(8f)	-325	50	20	12.5	12.5	12.5
Naval brass	Bolts	B21		C48200	060		(8f)	-325	50	20	12.5		
Naval brass	Bolts	B21		C48500	060		(8f)	-325	50	20	12.5	12.5	12.5
Cu	Bolts	B187		C10200	060		(8f)	-325	30	10	6.7	5.4	5.0
Cu	Bolts	B187		C11000	060		(8f)	-325	30	100	6.7	5.4	5.0
Cu	Bolts	B187		C12000	060		(8f)	-325	30	10	6.7	5.4	5.0
Cu	Bolts	B187		C12200	060		(8f)	-325	30	10	6.7	5.4	5.0
Cu-Si	Bolts	B98		C65100	060	•••	(8f)(52)	-325 🐛	40	12	8.0	8.0	7.1
Cu-Si	Bolts	B98		C65500	060		(8f)(52)	-325	52	15	10.0	10.0	10.0
Cu-Si	Bolts	B98		C66100	060		(8f)(52)	-325	52	15	10.0	10.0	10.0
Cu-Si	Bolts	B98		C65500	H01		(8f) Q	-325	55	24	10.0	10.0	10.0
Cu-Si	Bolts	B98		C66100	H01		(8f)	-325	55	24	10.0	10.0	10.0
Cu-Si	Bolts	B98		C65500	H02	<2	0	-325	70	38	10.0	10.0	10.0
Cu-Si	Bolts	B98		C66100	H02	<2	, No.	-325	70	38	10.0	10.0	10.0
Cu-Si	Bolts	B98		C65100	H06	>1, <1½		-325	75	40	10.0	10.0	10.0
Cu-Si	Bolts	B98		C65100	H06	>¹⁄ ₂ ,∕≰1		-325	75	45	11.3	11.3	11.3
Cu-Si	Bolts	B98		C65100	H06	≥1/ ₂		-325	85	55	13.8	13.8	13.8
Al-Si-bronze	Bolts	B150		C64200	HR50	>1, ≤2		-325	80	42	16.7	13.9	13.4
Al-Si-bronze	Bolts	B150		C64200	HR50	>½, ≤1		-325	85	42	16.7	13.9	13.4
Al-Si-bronze	Bolts	B150		C64200	HR50	≤ ¹ / ₂		-325	90	42	16.7	13.9	13.4
Al-bronze	Bolts	B150		C61400	HR50	>1, ≤2		-325	70	32	17.5	17.5	17.5
Al-bronze	Bolts	B150		C61400	HR50	>¹/ ₂ , ≤1		-325	75	35	17.5	17.5	17.5
Al-bronze	Bolts	B150	C	C61400	HR50	≤1/2		-325	80	40	18.0	18.0	18.0
Al-bronze	Bolts	B150	\mathcal{O}_{m}	C63000	HR50	>2, ≤3		-325	85	42.5	21.3	21.3	21.0
Al-bronze	Bolts	B150		C63000	M20	>3, ≤4		-325	85	42.5	20.0	19.6	19.1
Al-bronze	Bolts	B150		C63000	HR50	>1, ≤2		-325	90	45	22.5	22.5	22.5
Al-bronze	Bolts	B150		C63000	HR50	≥1/2, ≤1		-325	100	50	22.5	22.5	22.5
Nickel and Nick	el Alloy												
Low C-Ni	Bolts	B160		N02201	Hot fin./ann.		(8f)	-325	50	10	6.7	6.4	6.3
Ni	Bolts	B160		N02200	Hot fin.		(8f)	-325	60	15	10.0	10.0	10.0
Ni	Bolts	B160		N02200	Annealed		(8f)	-325	55	15	10.0	10.0	10.0
Ni	Bolts	B160		N02200	Cold drawn			-325	65	40	10.0	10.0	10.0
Ni-Cu	Bolts	B164		N04400	C.D./str. rel.		(54)	-325	84	50	16.7	14.6	13.6
Ni-Cu	Bolts	B164		N04405	Cold drawn		(54)	-325	85	50	16.7	14.6	13.6
Ni-Cu	Bolts	B164		N04400	Cold drawn		(54)	-325	85	55	16.7	14.6	13.8
Ni-Cu	Bolts	B164		N04400	Annealed		(8f)	-325	70	25	16.7	14.6	13.6
Ni-Cu	Bolts	B164		N04405	Annealed		(8f)	-325	70	25	16.7	14.6	13.6

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

Design Stress, ksi, at Metal Temperature, °F [Note (1)]

400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	UNS No.	Spec. No.
																Copper	and Cop	per Alloy
																	C46400	B21 %
																	C48200	B21
																	C48500	B21
																	, S	
																	610200	B187
																- ".\ <u>\</u>	C11000	B187
																1	C12000	B187
															··· C		C12200	B187
															'P		C65100	B98
•••	•••		•••												O ⁿ		C65500	B98
			•••		•••									X			C66100	B98
•••			•••													•••	C65500	B98
																	C66100	
	•••				•••								101					B98
	•••		•••		•••) ^{3.}				C65500	B98
												11/1			•••	•••	C66100	B98
												7					C65100	B98
	•••				•••						ile						C65100	B98
											\circ						C65100	B98
10.8	5.2	1.7	1.2							1	,						C64200	B150
10.8	5.2	1.7	1.2		•••												C64200	B150
10.8	5.2	1.7	1.2		•••				\mathcal{C}								C64200	B150
10.0	3.2	1.7	1.2		•••				*								C04200	D130
17.2	16.0						(14									C61400	B150
17.2	16.0							<u>ر</u>									C61400	B150
17.7	16.4						<u>).i.</u>										C61400	B150
						O'												
20.7	19.4	12.0	8.6	6.0	4.2)											C63000	B150
18.8	17.6	12.0	8.6	6.0	4.2												C63000	B150
22.5	21.1	12.0	8.6	6,0	4.2												C63000	B150
22.5	21.1	12.0	8.6	6.0	4.2												C63000	B150
		~	\ \'															
		5	•													Nicke		ckel Alloy
	X	6.2			6.1	6.0	5.8	4.5	3.7	3.0	2.4	2.0	1.5	1.2	1.0		N02201	
		10.0														•••	N02200	
		10.0															N02200	
10.0	10.0	10.0	10.0														N02200	B160
12.2	121	191	191														NO4400	D164
13.2		13.1			•••										•••		N04400	
																•••	N04405	
13.8																•••	N04400	
							12.6		9.2							•••	N04400	
13.2	13.1	13.1	13.1	13.0	12.9	12./	12.6	12.5	9.2								N04405	в104

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

									Specifie Streng		Tempe	at Me	tal e, °F
Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size Range, Dia., in.	Notes	Min. Temp., °F (6)	Tensile	Yield	Min. Temp. to 100	200	300
Nickel and Nick	el Alloy												
Ni-Cu	Rod	B164		N04405	Hot fin.	≤3		-325	75	35	16.7	14.6	13.6
Ni-Cu	Hex	B164		N04400	Hot fin.	≥2 ¹ / ₈ , ≤4	(8f)	-325	75	30	16.7	14.6	13.6
Ni-Cu	All except hex	B164		N04400	Hot fin.	>21/8		-325	80	40	16.7	14.6	13.6
Ni-Cr-Fe	Rod	B166		N06600	Cold drawn	≤3	(41)(54)	-325	105	80 6	20.0	20.0	20.0
Ni-Cr-Fe	Rod	B166		N06600	Hot fin.	≤3		-325	90	40	16.7	15.9	15.2
Ni-Cr-Fe	Bolts	B166		N06600	Annealed			-325	80	35	16.7	15.9	15.2
Ni-Cr-Fe	Rod	B166		N06600	Hot fin.	>3		-325	85	35	16.7	15.9	15.2
Ni-Mo	Bolts	B335		N10001	Annealed			-325	100	46	25.0	25.0	25.0
Ni-Mo-Cr	Bolts	B574		N10276	Sol. ann.			-325	100	41	25.0	24.9	23.0
Aluminum Alloy	,						أال						
	Bolts	B211	6061	6061	T6, T651 wld.	≥1/8, ≤8	(8f)(43) (63)	-452	24		4.8	4.8	4.8
	Bolts	B211	6061	6061	T6, T651	≥1/8, ≤8	(43)(63)	-452	42	35	8.4	8.4	8.4
	Bolts	B211	2024	2024	T4	>6 ¹ / ₂ , ≤8	(43)(63)	-452	58	38	9.5	9.5	9.5
	Bolts	B211	2024	2024	T4	>4 ¹ / ₂ , ≤6 ¹ / ₂	(43)(63)	-452	62	40	10.0	10.0	10.0
	Bolts	B211	2024	2024	T4.	$\geq \frac{1}{2}$, $\leq 4\frac{1}{2}$	(43)(63)	-452	62	42	10.5	10.5	10.3
	Bolts	B211	2024	2024	T4	$\geq \frac{1}{8}$, $< \frac{1}{2}$	(43)(63)	-452	62	45	11.3	11.3	10.3
	Bolts	B211	2014	2014	T6, T651	≥1/8, ≤8	(43)(63)	-452	65	55	13.0	13.0	12.4
P	MEN	SRM	DOC	2014									

Table A-2 Design Stress Values for Bolting Materials (Cont'd)

Numbers in Parentheses Refer to Notes for Appendix A Tables; Specifications Are ASTM

Design Stress, ksi, at Metal Temperature, °F [Note (1)]

400	500	600	650	700	750	800	850	900	950	1,000	1,050	1,100	1,150	1,200	1,250	1,300	UNS No.	Spec. No.
															Nickel	and Nic	kel Alloy	(Cont'd)
13.2	13.1	13.1	13.1	13.0	12.9	12.7	12.6	12.5	9.2								N04405	B164
13.2	13.1	13.1	13.1	13.0	12.9	12.7	12.6	12.5	9.2								N04400	B164
13.2	13.1	13.1	13.1	13.0	12.9	12.7	12.6	12.5	9.2								N04400	B164
20.0	20.0															 , Q	N06600	B166
14.6	14.0	13.5	13.3	13.1	12.9	12.7	12.5	12.4	10.0	7.0	4.5	3.0	2.2	2.0	1.8		N06600	B166
14.6	14.0	13.5	13.3	13.1	12.9	12.7	12.5	12.4	9.2	7.0	4.5	3.0	2.2	2.0	1.8	U.	N06600	B166
14.6	14.0	13.5	13.3	13.1	12.9	12.7	12.5	12.4	9.2	7.0	4.5	3.0	2.2	2.0	1.8		N06600	B166
24.6	24.3	23.6	23.3	23.0	22.8	22.6	22.5							4	O.,		N10001	B335
21.3	19.9	18.7	18.2	17.8	17.4	17.1	16.9	16.7	16.6	16.5	16.5		<)(),			N10276	B574
													111				Alumin	um Alloy
3.6													FUII!				A96061	
4.8											110	N. C.					A96061	B211
4.2											7.						A92024	B211
4.5										~ ×	<i>y</i>						A92024	B211
4.5									<	CA							A92024	B211
4.5									C								A92024	B211
4.3									٠.								A92014	B211
	P	S	E	OR	In			O.	•									

(18)

Table A-2M Design Stress Values for Bolting Materials (SI Units)

				••				
Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size Range, Dia., mm	Notes
1	Carbon steel	Bolts	A675	45	D40450			(8f)(8g)
2	Carbon steel	Bolts	A675	50	D40500			(8f)(8g)
3	Carbon steel	Bolts	A675	55	D40550			(8f)(8g)
4	Carbon steel	Bolts	A307	В				(8f)(8g)
-	Coderated	n.h.	A 675	60	D40600		20	(00(0.)
		Bolts	A675	60	D40600		0 V	(8f)(8g)
6		Bolts	A675	65	D40650	•••	, S	(8g)
7	Carbon steel	Bolts	A675	70	D40700	•••	₹.	(8g)
8		Bolts	A675	80	D40800		, 💙	(8g)
9	Carbon steel	Bolts	F3125	A325	K02706	" all		(8g)
10	Carbon steel	Nuts	A194	1	K01503	" \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		(42)
11	Carbon steel	Nuts	A194	2, 2H	K04002	4,		(42)
12	Carbon steel	Nuts	A194	2HM	K04002	<u></u>		(42)
13	Carbon steel	Nuts	A563	A, hvy. hex	К05802			(42b)
1.1	Cr. 0.2Mo	Dolta	A102	D7M	C41400		~100	
	Cr-0.2Mo Cr-0.2Mo	Bolts Bolts	A193 A320	B7M	G41400 G41400		≤100 ≤64	
				L7M	,			(15)
	5Cr	Bolts	A193	B5	S50100	•••	≤100	(15)
17	Cr-Mo-V	Bolts	A193	B16	K14072		>64, ≤100	(15)
18	Alloy steel	Bolts	A354	BC			>64 , ≤100	(15)
19	Cr-Mo	Bolts	A193	B7	G41400		>64, ≤100	(15)
20	Ni-Cr-Mo	Bolts	A320	L43	G43400		≤100	(15)
21	Cr-Mo	Bolts	A320	L7	G41400		≤64	(15)
22	Cr-Mo	Bolts	• A320	L7A	G40370		≤64	(15)
23	Cr-Mo	Bolts	A320	L7B	G41370		≤64	(15)
24	Cr-Mo	Bolts	A320	L7C	G87400		≤64	(15)
25	Cr-Mo	Bolts	A193	В7	G41400		≤64	
	Cr-Mo-V	Bolts	A193	вл В16	K14072		≤64	
	Alloy steel	Bolts	A354	BC			≤64	(15) (15)
	_		A354	BD			≤04 ≤100	(15)
20	Alloy steel 5Cr	Dolls	A334	טט			2100	(13)
29	5Cr	Nuts	A194	3	S50100			(42)
	C-Mo	Nuts	A194	4	K14510			(42)
	C-Mo	Nuts	A194	4L	K14510			(42)
	Cr-Mo	Nuts	A194	7	G41400			(42)
33	Cr-Mo	Nuts	A194	7L	G41400			(42)
	Cr-Mo	Nuts	A194	7M	G41400			(42)
	Cr-Mo	Nuts	A194	7ML	G41400		•••	(42)
				P.01-		_	-	
	16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2	>32, ≤38	(15)(60)
	16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	>32, ≤38	(15)(60)
	18Cr-8Ni	Bolts	A193	B8	S30400	2	>32, ≤38	(15)(60)
39	18Cr-8Ni	Bolts	A320	B8	S30400	2	>32, ≤38	(15)(60)

Table A-2M Design Stress Values for Bolting Materials (SI Units)

	Min.	Min.	Min.				ess, MPa,				Note (1)	1
	Temp.,	Tensile	Yield	Max. Use	Min.					-		-
Line	°C	Strength,	Strength,	Temp.,	Temp.	. =	100	425	150	455	200	225
No.	(6)	MPa	MPa	°C	to 40	65	100	125	150	175	200	225
1	-29	310	155	482	77.6	77.6	77.6	77.6	77.6	77.6	77.6	77.6
2	-29	345	172	482	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2
3	-29	379	190	482	94.8	94.8	94.8	94.8	94.8	94.8	94.8	94.8
4	-29	414		260	103	103	103	103	103	103	103	103
5	-29	414	207	482	103	103	103	103	103	103 🤇	103	103
6	-29	448	224	538	112	112	112	112	112	112	112	112
7	-29	483	241	538	121	121	121	121	121	121	121	121
8	-29	552	276	343	138	138	138	138	138	138	138	138
9	-29	825	635	343	159	159	159	159	159	159	159	159
10	-29			40) `			
11	-48			40				& K				
12	-48			40			(,	Ο.				
13	-29			40			OOK					
14	-48	689	552	538	138	138	138	138	138	138	138	138
15	-73	689	552	538	138	138	138	138	138	138	138	138
16	-29	689	552	649	138	138	138	138	138	138	138	138
17	-29	758	655	593	152	152	152	152	152	152	152	152
18	-18	793	683	343	159	159	159	159	159	159	159	159
19	-40	793	655	538	159	159	159	159	159	159	159	159
20	-101	862	724	371	172	172	172	172	172	172	172	172
21	-101	862	724	371	172	172	172	172	172	172	172	172
22	-101	862	724	343	172	172	172	172	172	172	172	172
23	-101	862	724	343	172	172	172	172	172	172	172	172
24	-101	862	724	343	172	172	172	172	172	172	172	172
25	-48	862	724	538	172	172	172	172	172	172	172	172
26	-29	862	724	593	172	172	172	172	172	172	172	172
27	-18	862	752	343	172	172	172	172	172	172	172	172
28	-29	1034	896	343	207	207	207	207	207	207	207	207
29	-29	,* 	***	40								
30	C-48			593								
31	-101			593								
32	-48			593								
33	-101			593								
34	-48			593								
35	-73			593								
36	-198	621	345	538	129	126	118	112	107	103	99.1	95.8
37	-198	621	345	538	129	126	118	112	107	103	99.1	95.8
38	-198	689	345	538	129	123	113	108	103	99.0	95.6	92.7
39	-198	689	345	538	129	123	113	108	103	99.0	95.6	92.7

Table A-2M Design Stress Values for Bolting Materials (SI Units)

			ע	esign Stre	ess, MPa, a	t Metal Te	mperature	e, °C [Note	(1)]			
Line No.	250	275	300	325	350	375	400	425	450	475	500	525
1	77.6	77.6	77.6	77.6	76.0	73.7	71.5	64.0	55.8	43.9	31.7	
2	86.2	86.2	86.2	86.2	84.5	81.9	73.3	64.0	55.8	43.9	31.7	
3	94.8	94.8	94.8	94.8	92.9	90.1	87.4	75.3	62.1	45.0	31.7	
4	103	103										18
5	103	103	103	103	101	98.3	95.1	79.5	62.6	45.0	31.7	·
6	112	112	112	112	110	106	95.1	79.5	64.4	47.7	32.5	21.4
7	121	121	121	121	118	115	101	83.8	66.8	50.3	33.2	21.4
8	138	138	138	138	135					😯)	
9	159	159	159	159	159					ME		
10									7 5	9 . "		
11									, 0			
12	•••											
13		•••	•••					"SI)			
14	138	138	138	138	138	138	138	138	115	92.3	67.3	41.6
15	138	138	138	138	138	138	138 🕜	138	115	92.3	67.3	41.6
16	138	138	138	138	138	138	138	138	138	80.6	61.7	46.4
17	152	152	152	152	152	152	2 1 52	152	148	132	113	88.3
18	159	159	159	159	159	*0 7.						
19	159	159	159	159	159	159	159	159	116	92.3	67.3	41.6
20	172	172	172	172	172	172						
21	172	172	172	172	172	172						
22	172	172	172	172	172							
23	172	172	172	172	172							
24	172	172	172	172	172							
25	172	172	172	172	172	172	172	172	121	93.4	67.3	41.6
26	172	172	172	172	172	172	172	172	166	146	121	90.1
27	172	172	172	172	172							
28	207	207	207	207	207							
29		ME.										
30	0	···										
31												
32												
33												
34												
35												
36	92.8	90.3	88.1	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2
37	92.8	90.3	88.1	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2
38	90.1	87.9	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2
39	90.1	87.9	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2	86.2

Table A-2M Design Stress Values for Bolting Materials (SI Units)

				Design St	ress, MPa,	at Metal T	emperatur	e, °C [Note	(1)]			
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
1												
2			•••									
3												
4											18	
5											2	
6	14.2									, ;)	
7	14.2									~3)		
8										, V		
9	•••	•••							CM			
10									VS.			
11												
12								- X				
13								60,				
14	23.5						النب					
15	23.5						@·`					
16	34.7	25.5	17.8	11.4	6.7		<i>(</i>),					
17	59.3	33.0	15.9			NS;						
18					🔪	0						
19	23.5											
20					alio,							
21					O."							
22				15	•							
23				Ob								
24		•••		C.							***	
25	23.5											
26	59.3	33.0	15.9									
27		Q	7,									
28		CHO.										
29												
30	SI											
31	P											
32		•••										
33		•••										
34												
35												
36	86.2											
37	86.2											
38	86.2											
39	86.2											

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type Grac		Class/ Condition/ Temper	Size Range, Dia., mm	Notes
40	18Cr-10Ni-Cb	Bolts	A193	B8C		2	>32, ≤38	(15)(60)
41	18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	>32, ≤38	(15)(60)
42	18Cr-10Ni-Ti	Bolts	A193	B8T	S32100	2	>32, ≤38	(15)(60)
43	18Cr-10Ni-Ti	Bolts	A320	B8T	S32100	2	>32, ≤38	(15)(60)
44	18Cr-9Ni	Bolts	A320	B8F	S30300	1		(8f)(15) (39)
45	19Cr-9Ni	Bolts	A453	651B			>75	(15)(35)
46	19Cr-9Ni	Bolts	A453	651B			≥75	(15)(35)
47	19Cr-9Ni	Bolts	A453	651A			2>75	(15)(35)
48	19Cr-9Ni	Bolts	A453	651A			≤75	(15)(35)
49	16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2 5	>25, ≤32	(15)(60)
50	16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	>25, ≤32	(15)(60)
51	18Cr-10Ni-Cb	Bolts	A193	B8C	/,	2 `	>25, ≤32	(15)(60)
52	18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	>25, ≤32	(15)(60)
53	18Cr-8Ni	Bolts	A193	В8	\$30400	2	>25, ≤32	(15)(60)
54	18Cr-8Ni	Bolts	A320	В8	\$30400	2	>25, ≤32	(15)(60)
55	18Cr-10Ni-Ti	Bolts	A193	B8T	S32100	2	>25, ≤32	(15)(60)
56	18Cr-10Ni-Ti	Bolts	A320	ввт 🔾	. (/)	2	>25, ≤32	(15)(60)
57	18Cr-10Ni-Ti	Bolts	A193	BBT	S32100	1		(8f)(15) (28)
58	18Cr-8Ni	Bolts	A320	O _{B8}	S30400	1		(8f)(15) (28)
59	18Cr-10Ni-Cb	Bolts	A193	B8C		1		(8f)(15) (28)
60	16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	1		(8f)(15) (28)
61	16Cr-12Ni-2Mo	Bolts C	A193	B8M	S31600	2	>19, ≤25	(15)(60)
62	16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	>19, ≤25	(15)(60)
63	18Cr-10Ni-Cb	Bolts	A193	B8C		2	>19, ≤25	(15)(60)
	18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	>19, ≤25	(15)(60)
65	18Cr-8Ni	Bolts	A193	В8	S30400	2	>19, ≤25	(15)(60)
	18Cr-8Ni	Bolts	A320	В8	S30400	2	>19, ≤25	(15)(60)
	18Cr-10Ni-Ti	Bolts	A193	В8Т	S32100	2	>19, ≤25	(15)(60)
	18Cr-10Ni-Ti	Bolts	A320	B8T	S32100	2	>19, ≤25	(15)(60)
69	12Cr	Bolts	A437	B4C	S42200			(35)
70	13Cr	Bolts	A193	В6	S41000		≤100	(15)(35)
	14Cr-24Ni	Bolts	A453	660	S66286	A		(15)(35)
	14Cr-24Ni	Bolts	A453	660	S66286	В		(15)(35)
73	16Cr-12Ni-2Mo	Bolts	A193	B8M	S31600	2	≤19	(15)(60)
74	16Cr-12Ni-2Mo	Bolts	A320	B8M	S31600	2	≤19	(15)(60)
75	18Cr-10Ni-Cb	Bolts	A193	B8C		2	≤19	(15)(60)
	18Cr-10Ni-Cb	Bolts	A320	B8C	S34700	2	≤19	(15)(60)

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

Min. Min. Min. Design Stress, MPa, at Metal Temperatu								Note (1)]			
	Temp.,	Tensile	Yield	Max. Use	Min.							
Line No.	°C (6)	Strength, MPa	Strength, MPa	Temp., °C	Temp. to 40	65	100	125	150	175	200	225
40	-198	689	345	538	129	129	122	117	113	110	108	105
41	-198	689	345	538	129	129	122	117	113	110	108	105
42	-198	689	345	538	129	129	121	118	114	110	106	103
43	-198	689	345	538	129	129	121	118	114	110	106	103
44	-198	517	207	427	129	123	113	108	103	99.0	95.6	92.7
45	-29	655	345	538	164	164	160	156	152	149	147	145
46	-29	655	414	538	164	164	160	156	152	149	147	145
47	-29	689	414	538	164	164	160	156	152	149	147	145
48	-29	689	483	538	164	164	160	156	152	149	147	145
49	-198	724	448	538	129	126	118	112	112	112	112	112
50	-198	724	448	538	129	126	118	112	112	112	112	112
51	-198	724	448	538	129	129	122	Q ₁₇	113	112	112	112
52	-198	724	448	538	129	129	122	117	113	112	112	112
53	-198	724	448	538	129	123	113	112	112	112	112	112
54	-198	724	448	538	129	123	113	112	112	112	112	112
55	-198	724	448	538	129	129	121	118	114	112	112	112
56	-198	724	448	538	129	129	121	118	114	112	112	112
					New							
57	-198	517	207	816	129	129	121	118	114	110	106	103
58	-254	517	207	816	O 129	123	113	108	103	99.0	95.6	92.7
59	-254	517	207	816	129	129	122	117	113	110	108	105
60	-198	517	207	816	129	126	118	112	107	103	99.1	95.8
			رن ح	•								
61	-198	689	552	538	138	138	138	138	138	138	138	138
62	-198	689	552	538	138	138	138	138	138	138	138	138
63	-198	793	552	538	138	138	138	138	138	138	138	138
64	-198	793	552	538	138	138	138	138	138	138	138	138
65	-198	793	552	538	138	138	138	138	138	138	138	138
66	-198	793	552	538	138	138	138	138	138	138	138	138
67	-198	793	552	538	138	138	138	138	138	138	138	138
68	<i>E</i> 198	793	552	538	138	138	138	138	138	138	138	138
69	-29	793	586	371	147	147	147	147	147	147	147	147
70	-29	758	586	482	147	147	147	147	147	147	147	147
71	-198	896	586	538	147	147	147	147	147	147	147	147
72	-198	896	586	538	147	147	147	147	147	147	147	147
73	-198	758	655	538	152	152	152	152	152	152	152	152
74	-198	758	655	538	152	152	152	152	152	152	152	152
75	-198	862	689	538	172	172	172	172	172	172	172	172
76	-198	862	689	538	172	172	172	172	172	172	172	172

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

	Design Stress, MPa, at Metal Temperature, °C [Note (1)]											
Line No.	250	275	300	325	350	375	400	425	450	475	500	525
40	104	102	99.9	98.0	96.4	95.2	94.2	93.5	93.0	92.7	92.6	92.4
41	104	102	99.9	98.0	96.4	95.2	94.2	93.5	93.0	92.7	92.6	92.4
42	100	97.2	94.7	92.6	90.8	89.2	87.8	86.6	86.2	86.2	86.2	86.2
43	100	97.2	94.7	92.6	90.8	89.2	87.8	86.6	86.2	86.2	86.2	86.2
44	90.1	87.9	85.8	84.0	82.3	80.6	79.1	77.6	76.2			V0_
												2
45	144	143	142	141	141	140	139	138	136	134	134	128
46	144	143	142	141	141	140	139	138	136	134	131	128
47	144	143	142	141	141	140	139	138	136	134	2 131	128
48	144	143	142	141	141	140	139	138	136	134	131	128
										M		
49	112	112	112	112	112	112	112	112	112	112	112	112
50	112	112	112	112	112	112	112	112	112	112	112	112
51	112	112	112	112	112	112	112	112	112	112	112	112
52	112	112	112	112	112	112	112	112	112	112	112	112
53	112	112	112	112	112	112	112	112	112	112	112	112
54	112	112	112	112	112	112	112	112	112	112	112	112
55	112	112	112	112	112	112	112	112	112	112	112	112
56	112	112	112	112	112	112	112	112	112	112	112	112
							N					
57	99.9	97.2	94.7	92.6	90.8	89.2	87.8	86.6	85.6	84.7	84.0	83.2
58	90.1	87.9	85.8	84.0	82.3	80.6	79.1	77.6	76.2	74.8	73.4	72.1
59	104	102	99.9	98.0	96.4	95.2	94.2	93.5	93.0	92.7	92.6	92.4
60	92.8	90.3	88.1	86.2	84.6	83.3	82.2	81.2	80.4	79.7	79.0	78.4
				$C_{\mathcal{O}}$) *							
61	138	138	138	138	138	138	138	138	138	138	138	138
62	138	138	138	138	138	138	138	138	138	138	138	138
63	138	138	138	138	138	138	138	138	138	138	138	138
64	138	138	138	138	138	138	138	138	138	138	138	138
65	138	138	138	138	138	138	138	138	138	138	138	138
66	138	138	138	138	138	138	138	138	138	138	138	138
67	138	138	138	138	138	138	138	138	138	138	138	138
68	138	138	138	138	138	138	138	138	138	138	138	138
69	147	147	147	147	147	147						
			147		147	147						
70	147	147	147	147	147	147	147	147	147	141	133	
71	147	147	147	147	147	147	147	147	147	147	147	147
72	147	147	147	147	147	147	147	147	147	147	147	147
73	152	152	152	152	152	152	152	152	152	152	152	152
74	152	152	152	152	152	152	152	152	152	152	152	152
75 76	172	171	170	170	169	169	169	169	169	168	167	166
76	172	171	170	170	169	169	169	169	169	168	167	166

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

			ber3 III 1 ur					e, °C [Note				
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
40	92.2											
41	92.2											
42	86.2											
43	86.2										0	
44											0/2	
45	124									O	`	
46	124									01:		
47	124									<i>⇔</i>		
48	124											
49	112								SI			
50	112							\$	Y			
51	112							- Z C				
52	112							O_{k}				
53	112							Q Y				
54	112						1113					
55	112											
56	112					,	ille					
57	82.4	59.2	44.0	32.9	24.5	183	12.5	8.5	6.2	4.3	2.8	1.7
58	70.7	69.4	63.8	51.6	41.6	32.9	26.5	21.3	17.2	14.1	11.2	8.8
59	92.2	75.9	57.2	40.2	30.3	23.2	16.2	11.4	9.0	7.1	5.9	5.3
60	77.7	76.9	75.9	65.0	50.5	39.2	30.4	23.6	18.4	14.3	11.1	8.6
61	138		C	O								
62	138		\sim									
63	138		"(<u>)</u>									
64	138	🔿	<i>///</i>									
65	138	- X										
66	138	,40										
67	138	/										
68	138											
69	Y 											
70												
71	 147											
72	147											
73	152	•••	•••	•••	•••	•••	•••	•••			•••	•••
74	152	•••	•••	•••			•••	•••			•••	•••
75	164			•••				•••			•••	•••
76	164										•••	
76	104							•••			•••	

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

		In tarentheses Refer		PP				
Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size Range, Dia., mm	Notes
77	18Cr-8Ni	Bolts	A193	B8	S30400	2	≤19	(15)(60)
78	18Cr-8Ni	Bolts	A320	В8	S30400	2	≤19	(15)(60)
79	18Cr-10Ni-Ti	Bolts	A193	B8T	S32100	2	≤19	(15)(60)
80	18Cr-10Ni-Ti	Bolts	A320	B8T	S32100	2	≤19	(15)(60)
81	12Cr	Bolts	A437	B4B	S42225		83	(35)
82	12Cr	Nuts	A194	6	S41000		0	(35)(42)
83	18Cr-9Ni	Nuts	A194	8FA	S30300	•••	&	(42)
						4	,	
84	16Cr-12Ni-2Mo	Nuts	A194	8MA	S31600	··· collin		(42)
85	18Cr-10Ni-Ti	Nuts	A194	8TA	S32100	" VS.	•••	(42)
						& P		
86	18Cr-8Ni	Nuts	A194	8	S30400	Ö.		(42)
87	18Cr-8Ni	Nuts	A194	8A	S30400			(42)
	18Cr-10Ni-Cb	Nuts	A194	8CA	S34700	•••		(42)
								()
89	Naval brass	Bolts	B21	Jien the fil	C46400	060		(8f)
	Naval brass	Bolts	B21	*Kle	C48200	060		(8f)
91	Naval brass	Bolts	B21		C48500	060	•••	(8f)
92		Bolts	B187	10	C10200	060		(8f)
93		Bolts	B187	7.	C11000	060		(8f)
94		Bolts	B187) 	C12000	060		(8f)
95		Bolts	B187		C12200	060	•••	(8f)
								(-)
96	Cu-Si	Bolts	• B98		C65100	060		(8f)(52)
	Cu-Si	Bolts	B98		C65500	060	•••	(8f)(52)
	Cu-Si	Bolts	B98		C66100	060		(8f)(52)
	Cu-Si	Bolts (1)	B98		C65500	H01		(8f)
	Cu-Si	Bolts	B98		C66100	H01		(8f)
	Cu-Si	Bolts	B98		C65500	H02	≤50	
	Cu-Si	Bolts	B98		C66100	H02	≤50	
	Cu-Si	Bolts	B98		C65100	H06	>25, ≤38	
	Cu-Si	Bolts	B98	•••	C65100	Н06	>13, ≤25	
	Cu-Si Cu-Si	Bolts	B98		C65100	Н06	≤13	
106	Al-Si-bronze	Bolts	B150		C64200	HR50	>25, ≤50	
	Al-Si-bronze	Bolts	B150		C64200	HR50	>13, ≤25	
	Al-Si-bronze	Bolts	B150		C64200	HR50	≤13	
100	in or bronde	2010	2100		001200	111.00	_10	
109	Al-bronze	Bolts	B150	•••	C61400	HR50	>25, ≤50	
	Al-bronze	Bolts	B150		C61400	HR50	>13, ≤25	
	Al-bronze	Bolts	B150		C61400	HR50	≤13	
	· · · · ·		.= =					
112	Al-bronze	Bolts	B150		C63000	HR50	>50, ≤75	
	Al-bronze	Bolts	B150		C63000	M20	>75, ≤100	
	-					-	-,	

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

	Min.	Min.		be for Appendix A Tables; Specifications Are ASTM Design Stress, MPa, at Metal Temperature, °C [Note (1)]								
	Temp.,	Tensile	Min. Yield	Max. Use	Min.		, ,			•		<u> </u>
Line	°C	Strength,	Strength,	Temp.,	Temp.	- -	100	40=	4		200	
No.	(6)	MPa	MPa	°C	to 40	65	100	125	150	175	200	225
77	-198	862	689	538	172	172	172	172	172	172	172	172
78 7 0	-198	862	689	538	172	172	172	172	172	172	172	172
79	-198	862	689	538	172	172	172	172	172	172	172	172
80	-198	862	689	538	172	172	172	172	172	172	172	172
81	-29	1000	724	343	181	181	181	181	181	181) 1 ₈₁	181
01	-29	1000	724	343	101	101	101	101	101	101	101	101
82	-29			40						~ ~ . ~		
83	-29		•••	40	•••					C 5 "	•••	
03	2)		***	40								•••
84	-198			40				6	M			
85	-198			40)			
00	170		•••	10				5 /				
86	-254			40			🗸	O.				
87	-254			40			Ω_{k}					
88	-254			40			Q.V					
						6						
89	-198	345	138	149	86.2	86.2	86.2	86.2	86.2			
90	-198	345	138	149	86.2	86.2	86.2	86.2	86.2			
91	-198	345	138	149	86.2	86.2	86.2	86.2	86.2			
92	-198	207	69	149	46.0	38.8	37.2	36.5	34.2			
93	-198	207	69	149	46.0	38.8	37.2	36.5	34.2			
94	-198	207	69	149	46.0	38.8	37.2	36.5	34.2			
95	-198	207	69	149	46.0	38.8	37.2	36.5	34.2			
				, CV.								
96	-198	276	83	149	55.2	55.2	55.2	54.0	48.3			
97	-198	359	103	149	68.9	68.9	68.9	68.9	68.8			
98	-198	359	103	149	68.9	68.9	68.9	68.9	68.8			
99	-198	379	165	149	68.9	68.9	68.9	68.9	68.8			
100	-198	379	165	149	68.9	68.9	68.9	68.9	68.8			
101	-198	483	262	149	68.9	68.9	68.9	68.9	68.8			
102	-198	483	262	149	68.9	68.9	68.9	68.9	68.8			
103	-198	517	276	149	68.9	68.9	68.9	68.9	68.9			
104	-198	517	310	149	77.6	77.6	77.6	77.6	77.6			
105	-198	586	379	149	94.8	94.8	94.8	94.8	94.8			
	12°											
106	-198	552	290	316	115	100	95.2	93.6	92.1	89.1	76.9	57.7
107	-198	586	290	316	115	100	95.2	93.6	92.1	89.1	76.9	57.7
108	-198	621	290	316	115	100	95.2	93.6	92.1	89.1	76.9	57.7
400	100	400	201	0.00	404	404	101	404	404	101	440	
109	-198	483	221	260	121	121	121	121	121	121	119	115
110	-198	517	241	260	121	121	121	121	121	121	119	115
111	-198	552	276	260	124	124	124	124	124	124	122	118
112	100	E0 <i>6</i>	202	271	1.47	147	147	116	145	1 // /	1.49	140
112	-198	586	293	371 271	147	147	147	146	145	144	143	140
113	-198	586	293	371	138	137	134	133	132	131	130	128

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

Design Stress, MPa, at Metal Temperature, °C [Note (1)]													
Line													
No.	250	275	300	325	350	375	400	425	450	475	500	525	
77	172	172	172	172	172	172	172	172	172	172	172	168	
78	172	172	172	172	172	172	172	172	172	172	172	168	
79	172	172	172	172	172	172	172	172	172	172	172	172	
80	172	172	172	172	172	172	172	172	172	172	172	472	
81	181	181	181	181	181						 سار	2."	
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106	40.9	24.1	14.5	10.3									
107	40.9	24.1	14.5	10.3									
108	40.9	24.1	14.5	10.3									
109	111	109											
110	111	109											
111	115	112											
440	404	404	05.0	5 0.0	.	20.2							
112	136	126	97.2	73.9	54.4	39.3							
113	124	117	97.2	73.9	54.4	39.3							

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

				Design St	ress, MPa,	at Metal T	emperatur	e, °C [Note	(1)]			
Line No.	550	575	600	625	650	675	700	725	750	775	800	825
77	162	•••						•••			***	
78	162											
79	172											
80	172						•••				200	
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104 105												
106	B											
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108												
109												
110												
111												
112												
113												

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

Line No.	Nominal Composition	Product Form	Spec. No.	Type/ Grade	UNS No.	Class/ Condition/ Temper	Size Range, Dia., mm	Notes
114	Al-bronze	Bolts	B150		C63000	HR50	>25, ≤50	
115	Al-bronze	Bolts	B150		C63000	HR50	≥13, ≤25	
116	Low C-Ni	Bolts	B160		N02201	Hot fin./ ann.		8 0
117	Ni	Bolts	B160		N02200	Hot fin.	oo	(8f)
118	Ni	Bolts	B160		N02200	Annealed	C	(8f)
119	Ni	Bolts	B160		N02200	Cold drawn	01.	
120	Ni-Cu	Bolts	B164		N04400	C.D./str. rel.	^{დეე}	(54)
121	Ni-Cu	Bolts	B164		N04405	Cold drawn		(54)
122	Ni-Cu	Bolts	B164		N04400	Cold drawn		(54)
123	Ni-Cu	Bolts	B164		N04400	Annealed		(8f)
124	Ni-Cu	Bolts	B164		N04405	Annealed		(8f)
					4	Q.		
125	Ni-Cu	Rod	B164		N04405	Hot fin.	≤75	
126	Ni-Cu	Hex	B164		N04400	Hot fin.	≥54, ≤100	(8f)
127	Ni-Cu	All except hex	B164		N04400	Hot fin.	>54	
				Jien the fil				
128	Ni-Cr-Fe	Rod	B166	" Kle	N06600	Cold drawn	≤75	(41)(54)
129	Ni-Cr-Fe	Rod	B166	N	N06600	Hot fin.	≤75	
130	Ni-Cr-Fe	Bolts	B166		N06600	Annealed	•••	
131	Ni-Cr-Fe	Rod	B166		N06600	Hot fin.	>75	
132	Ni-Mo	Bolts	B335		N10001	Annealed	•••	
			<i>C</i>),					
133	Ni-Mo-Cr	Bolts	B574		N10276	Sol. ann.		
134	Aluminum alloy	Bolts Bolts	B211	6061	A96061	T6, T651 wld.	≥3, ≤200	(8f)(43) (63)
135	Aluminum alloy	Bolts	B211	6061	A96061	T6, T651	≥3, ≤200	(43)(63)
136	Aluminum alloy	Bolts	B211	2024	A92024	T4	>165, ≤200	(43)(63)
137	Aluminum alloy	Bolts	B211	2024	A92024	T4	>114, ≤165	(43)(63)
138	Aluminum alloy	Bolts	B211	2024	A92024	T4	>13, ≤114	(43)(63)
139	Aluminum alloy	Bolts	B211	2024	A92024	T4	≥3, <13	(43)(63)
140	Aluminum alloy	Bolts	B211	2014	A92014	T6, T651	≥3, ≤200	(43)(63)

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

Min. Min. Min. Min. Min. Max. Max. Max. Min. Temp. Temp.		N/:			s Refer to No	_		ess, MPa, a				Note (1)	1
114 -198 621 310 371 155 152 242 242 242 246 48.9 48.9<		Temp., °C	Tensile Strength,	Yield Strength,	Temp.,	Min. Temp.				•			
115 -198 689 345 371 155 155 155 155 155 155 155 155 155 155 155 155 155 155 155 155 155 155 153 153 148 148 140 43.6 43.3 43.1 43.9 43.0 117 -198 414 103 316 68.9													
116													
117 -198 414 103 316 68.9 68.													
118 -198 379 103 316 68.9 90.9 90.9 90.4 12.2 19.8 48.8 11.5 106 99.7 96.2 93.6 91.9	116	-198	345	69	649	46.0	44.8	44.0	43.6	43.3	43.1	43.0	43.0
119 -198 448 276 316 68.9 90.9 90.4 121 -198 586 345 260 115 106 99.7 96.2 93.6 91.9 90.9 90.4 122 -198 586 379 260 115 106 99.7 96.2 93.6 91.9 90.9 90.4 124 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 125 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127	117	-198	414	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
120 -198 579 345 316 115 106 99.7 96.2 93.6 91.9 90.9 90.4 121 -198 586 345 260 115 106 99.7 96.2 93.6 91.9 90.9 90.4 122 -198 586 379 260 115 106 99.7 96.2 93.6 91.9 90.9 90.4 123 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 124 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 125 -198 517 241 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9	118	-198	379	103	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
121 -198 586 345 260 115 106 99.7 96.2 93.6 91.9 90.9 90.4 122 -198 586 379 260 115 106 99.7 96.2 94.8	119	-198	448	276	316	68.9	68.9	68.9	68.9	68.9	68.9	68.9	68.9
122 -198 586 379 260 115 106 99.7 96.2 94.8 94.8 94.8 94.8 123 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 124 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 125 -198 517 241 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 138 138 138 138 138 <	120	-198	579	345	316	115	106	99.7	96.2	93.6	91.9	90.9	90.4
123 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 124 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 125 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 13	121	-198	586	345	260	115	106	99.7	96.2	93.6	91.9	90.9	90.4
124 -198 483 172 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 125 -198 517 241 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 188 138 <td>122</td> <td>-198</td> <td>586</td> <td>379</td> <td>260</td> <td>115</td> <td>106</td> <td>99.7</td> <td>96.2</td> <td>94.8</td> <td>94.8</td> <td>94.8</td> <td>94.8</td>	122	-198	586	379	260	115	106	99.7	96.2	94.8	94.8	94.8	94.8
125 -198 517 241 482 115 106 997 96.2 93.6 91.9 90.9 90.4 126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 <td< td=""><td>123</td><td>-198</td><td>483</td><td>172</td><td>482</td><td>115</td><td>106</td><td>99.7</td><td>96.2</td><td>93.6</td><td>91.9</td><td>90.9</td><td>90.4</td></td<>	123	-198	483	172	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4
126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 101 99.0 133 101 99.0 133 137 103 101 99.0 107	124	-198	483	172	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4
126 -198 517 207 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 101 99.0 133 101 99.0 133 137 103 101 99.0 107								6	O.				
127 -198 552 276 482 115 106 99.7 96.2 93.6 91.9 90.9 90.4 128 -198 724 552 260 138 148 143 1	125	-198	517	241	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4
128 -198 724 552 260 138 101 99.0 130 101 99.0 131 -198 586 241 649 115 112 109 107 105 103 101 99.0 131 -198 689 317 427 172 172 172 172 172 172 172 171 170 169 133 -198 689 283 538 172 172 170 164 158 153 148 143 134<	126	-198	517	207	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4
129 -198 621 276 649 115 112 109 107 105 103 101 99.0 130 -198 552 241 649 148 112 109 107 105 103 101 99.0 131 -198 586 241 649 115 112 109 107 105 103 101 99.0 132 -198 689 317 427 172 172 172 172 171 170 169 133 -198 689 283 538 172 172 170 164 158 153 148 143 134 -269 165 204 33.1 33.1 33.1 33.1 33.1 33.1 36.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5	127	-198	552	276	482	115	106	99.7	96.2	93.6	91.9	90.9	90.4
129 -198 621 276 649 115 112 109 107 105 103 101 99.0 130 -198 552 241 649 148 112 109 107 105 103 101 99.0 131 -198 586 241 649 115 112 109 107 105 103 101 99.0 132 -198 689 317 427 172 172 172 172 171 170 169 133 -198 689 283 538 172 172 170 164 158 153 148 143 134 -269 165 204 33.1 33.1 33.1 33.1 33.1 33.1 36.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5							.0						
130 -198 552 241 649 116 112 109 107 105 103 101 99.0 131 -198 586 241 649 115 112 109 107 105 103 101 99.0 132 -198 689 317 427 172 172 172 172 171 170 169 133 -198 689 283 538 172 172 170 164 158 153 148 143 134 -269 165 204 33.1 33.1 33.1 33.1 33.1 26.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137													
131 -198 586 241 649 115 112 109 107 105 103 101 99.0 132 -198 689 317 427 172 172 172 172 171 170 169 133 -198 689 283 538 172 172 170 164 158 153 148 143 134 -269 165 204 33.1 33.1 33.1 33.1 33.1 33.1 26.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2							•						
132 -198 689 317 427 172 172 172 172 172 171 170 169 133 -198 689 283 538 172 172 170 164 158 153 148 143 134 -269 165 204 33.1 33.1 33.1 33.1 33.1 33.1 26.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137 -269 427 276 204 68.9 68.9 68.9 68.9 68.9 46.1 31.3 31.3 138 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6 77.6													
133 -198 689 283 538 172 172 170 164 158 153 148 143 134 -269 165 204 33.1 33.1 33.1 33.1 33.1 33.1 36.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137 -269 427 276 204 68.9 68.9 68.9 68.9 68.9 46.1 31.3 31.3 138 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 77.6 <	131	-198	586	241	649	115	112	109	107	105	103	101	99.0
134 -269 165 204 33.1 33.1 33.1 33.1 33.1 33.1 33.1 33.1 26.4 16.1 135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137 -269 427 276 204 68.9 68.9 68.9 68.9 68.9 46.1 31.3 31.2 138 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6	132	-198	689	317	427	172	172	172	172	172	171	170	169
135 -269 290 241 204 57.9 57.9 57.9 57.9 57.9 47.3 34.9 21.1 136 -269 400 262 204 65.5 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137 -269 427 276 204 68.9 68.9 68.9 68.9 68.9 46.1 31.3 31.3 138 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6 77.6 77.6 77.6 70.2 46.2 31.2 31.2	133	-198	689	283	538	172	172	170	164	158	153	148	143
136 -269 400 262 204 65.5 65.5 65.5 65.5 65.5 43.1 29.3 29.3 137 -269 427 276 204 68.9 68.9 68.9 68.9 68.9 46.1 31.3 31.3 138 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6 77.6 77.6 77.6 70.2 46.2 31.2 31.2	134	-269	165		204	33.1	33.1	33.1	33.1	33.1	33.1	26.4	16.1
137 -269 427 276 204 68.9 68.9 68.9 68.9 68.9 46.1 31.3 31.3 138 -269 427 290 204 72.4 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6 77.6 77.6 77.6 70.2 46.2 31.2 31.2	135	-269	290	241	204	57.9	57.9	57.9	57.9	57.9	47.3	34.9	21.1
138 -269 427 290 204 72.4 72.4 72.4 70.2 46.2 31.2 31.2 139 -269 427 310 204 77.6 77.6 77.6 77.6 70.2 46.2 31.2 31.2	136	-269	400	262	204	65.5	65.5	65.5	65.5	65.5	43.1	29.3	29.3
139 -269 427 310 204 77.6 77.6 77.6 77.6 70.2 46.2 31.2 31.2	137	-269	427	276	204	68.9	68.9	68.9	68.9	68.9	46.1	31.3	31.3
139 -269 427 310 204 77.6 77.6 77.6 77.6 70.2 46.2 31.2 31.2			OK.										
	138	-269		290	204	72.4	72.4	72.4	72.4	70.2	46.2	31.2	31.2
140 269 448 379 204 89.6 89.6 89.6 89.6 84.2 46.9 26.2 20.2	139		427	310	204	77.6	77.6	77.6	77.6	70.2	46.2	31.2	31.2
	140	-269	448	379	204	89.6	89.6	89.6	89.6	84.2	46.9	26.2	20.2

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

			D	esign Stre	ess, MPa, a	t Metal Te	mperatur	e, °C [Note	(1)]			
Line No.	250	275	300	325	350	375	400	425	450	475	500	525
114	148	126	97.2	73.9	54.4	39.3						
115	148	126	97.2	73.9	54.4	39.3						
116	43.0	43.0	43.0	43.0	42.9	42.7	42.2	41.6	40.7	33.1	27.4	22.8
117	68.9	68.9	68.9	68.9							o	5
118	68.9	68.9	68.9	68.9							0) V	
119	68.9	68.9	68.9	68.9							7. N. J	
120	90.4	90.4	90.4	90.4						🗘	,O	
121	90.4	90.4								4,		
122	94.8	94.8								· Mr		
123	90.4	90.4	90.4	90.4	90.4	89.8	89.0	88.0	87.0	86.4	75.6	
124	90.4	90.4	90.4	90.4	90.4	89.8	89.0	88.0	87.0	86.4	75.6	
125	90.4	90.4	90.4	90.4	90.4	89.8	89.0	88.0	87.0	86.4	75.6	
126	90.4	90.4	90.4	90.4	90.4	89.8	89.0	88.0	87.0	86.4	75.6	
127	90.4	90.4	90.4	90.4	90.4	89.8	89.0	88.0	87.0	86.4	75.6	
128	138	138					200					
129	97.3	95.6	 94.0	 92.6	 91.2	 89.9	88.7	 87.7	 86.7	 85.8	 75.6	 58.4
130	97.3	95.6	94.0	92.6	91.2	89.9	88.7	87.7	86.7	85.8	75.6 75.6	58.4
131	97.3	95.6	94.0	92.6	91.2	89.9	88.7	87.7	86.7	85.8	75.6 75.6	58.4
131	97.3	73.0	94.0	92.0	91.2	1,20	00.7	67.7	00.7	03.0	73.0	30.4
132	168	166	164	162	160	158	157	156	155			
133	139	135	131	128	125	122	120	118	117	115	115	114
134				_ _C O								
135				℃								
136												
137			OWIL									
138		2) , "									
139												
140	🗡	Min										

Table A-2M Design Stress Values for Bolting Materials (SI Units) (Cont'd)

	Design Stress, MPa, at Metal Temperature, °C [Note (1)]												
Line No.	550	575	600	625	650	675	700	725	750	775	800	825	
114													
115													
116	18.7	15.6	12.9	10.0	8.2						8		
117											20,		
118										0) ···		
119										0,			
120										8			
121									<	, 			
122									CM.				
123									M.				
124								5	K				
125								ROK C					
126								Q Y					
127							the tril						
							0,						
128						5	(L)						
129	39.7	27.0	19.2	15.0	13.7	<i>u</i>							
130	39.7	27.0	19.2	15.0	13.7	10							
131	39.7	27.0	19.2	15.0	13.7	0							
132					13.7 Click								
133	114	•••			•								
134				CO.									
135) · 									
136	•••		"U										
137		0	MDO										
138		70,											
139	🗸												
140	and the												

APPENDIX B STRESS TABLES AND ALLOWABLE PRESSURE TABLES FOR **NONMETALS**

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ASME B31.3-2018

Specification Index for Appendix B

Spec. No.	Title [Note (1)]
ASTM	
C361	Reinforced Concrete Low-Head Pressure Pipe
C582	Contact-Molded Reinforced Thermosetting Plastic (RTP) Laminates for Corrosion Resistant Equipment
C599	Process Glass Pipe and Fittings
D1785	PVC Plastic Pipe, Schedules 40, 80, and 120
D2239	PE Plastic Pipe (SIDR-PR) Based on Controlled Inside Diameter
D2241	PVC Plastic Pressure-Rated Pipe (SDR Series)
D2447	PVC Plastic Pipe, Schedules 40, 80, and 120 PE Plastic Pipe (SIDR-PR) Based on Controlled Inside Diameter PVC Plastic Pressure-Rated Pipe (SDR Series) PE Plastic Pipe, Schedules 40 and 80, Based on Outside Diameter Thermoplastic Gas Pressure Pipe, Tubing and Fittings Reinforced Epoxy Resin Gas Pressure Pipe and Fittings PB Plastic Pipe (SDR-PR) PB Plastic Tubing Joints for IPS PVC Pipe Using Solvent Cement PE Plastic Tubing CPVC Plastic Hot- and Cold-Water Distribution Systems Filament-Wound Fiberglass RTR Pipe [Note (2)] Centrifugally Cast RTR Pipe [Note (2)] PB Plastic Pipe (SDR-PR) Based on Outside Diameter
D2513	Thermoplastic Gas Pressure Pipe, Tubing and Fittings
D2517	Reinforced Epoxy Resin Gas Pressure Pipe and Fittings
D2662	PB Plastic Pipe (SDR-PR)
D2666	PB Plastic Tubing
D2672	Joints for IPS PVC Pipe Using Solvent Cement
D2737	PE Plastic Tubing
D2846	CPVC Plastic Hot- and Cold-Water Distribution Systems
D2996	Filament-Wound Fiberglass RTR Pipe [Note (2)]
D2997	Centrifugally Cast RTR Pipe [Note (2)]
D3000	PB Plastic Pipe (SDR-PR) Based on Outside Diameter
D3035	PE Plastic Pipe (DR-PR) Based on Controlled Outside Diameter
D3309	PB Plastic Hot- and Cold-Water Distribution Systems
D3517	Fiberglass RTR Pressure Pipe [Note (2)]
D3754	Fiberglass RTR Sewer and Industrial Pressure Pipe [Note (2)]
F441	CPVC Plastic Pipe, Schedules 40 and 80
F442	CPVC Plastic Pipe (SDR-PR)
F2389	Pressure-Rated Polypropylene (PP) Piping Systems
F2788/F2788M	Metric and Inch-sized Crosslinked Polyethylene (PEX) Pipe
AWWA	
C300	Reinforced Concrete Pressure Pipe, Steel Cylinder Type, for Water and Other Liquids
C301	Prestressed Concrete Pressure Pipe, Steel Cylinder Type, for Water and Other Liquids
C302	Reinforced Concrete Pressure Pipe, Noncylinder Type
C950	Fiberglass Pressure Pipe

GENERAL NOTE: It is not practical to refer to a specific edition of each standard throughout the Code text. Instead, the approved edition references, along with the names and addresses of the sponsoring organizations, are shown in Appendix E.

NOTES:

(1) For names of plastics identified only by abbreviation, see para. A326.4.

- (2) The term fiberglass RTR takes the place of the ASTM designation "fiberglass" (glass-fiber-reinforced thermosetting resin).

Table B-1 Hydrostatic Design Stresses (HDS) and Recommended Temperature Limits for Thermoplastic Pipe

				Recom	mended	Hydrostati	c Design	Stress,	ksi, at
				Lim	erature its, °F				
ASTM Spec. No.	Pipe Designation	Material Designation	Cell Class	Minimum	(1), (2)] Maximum	_ 73°F [Note (3)]	100°F	180°F	200°F
	PR	ABS	43232	-40	176				
D2846	SDR11	CPVC4120	23447		180	2.0		0.5	
F441	Sch. 40	CPVC4120	23447	73	200	2.0		0.5	
F441	Sch. 80	CPVC4120	23447	73	200	2.0		0.5	b
F442	SDR-PR	CPVC4120	23447	73	200	2.0	1.64	0.5	
D3309	SDR11	PB2110		73	200	1.0	0. V.	0.5	
D2220	CIDD DD	DE1404		72		0.40	\$2		
D2239	SIDR-PR	PE1404		73 73	•••	0.40			
D2239	SIDR-PR	PE2305		73	•••	0.50 0.63			
D2239 D2239	SIDR-PR	PE2306 PE2406	•••	73 73	•••	0.63			
D2239 D2239	SIDR-PR SIDR-PR	PE3306	•••	73 73		0.63			
D2239 D2239	SIDR-PR	PE3406	•••	73 73		0.63			
D2239 D2239	SIDR-PR	PE3408	•••	73 73		0.80			
D2239	SIDK-FK	FE3400	•••	/3	Juli POF	0.00	•••		•••
D2447	Sch. 40 and 80	PE1404		73	,	0.40			
D2447	Sch. 40 and 80	PE2305		73		0.50			
D2447	Sch. 40 and 80	PE2306		73 73 73		0.63			
D2447	Sch. 40 and 80	PE2406		73		0.63			
D2447	Sch. 40 and 80	PE3306	🥎	73		0.63			
D2447	Sch. 40 and 80	PE3406	ick to	73		0.63			
D2737	SDR7.3, SDR9, SDR11	PE2305 (·lic,	73		0.50			
D2737	SDR7.3, SDR9, SDR11	PE2306	.	73		0.63			
D2737	SDR7.3, SDR9, SDR11	PE2406		73		0.63			
D2737	SDR7.3, SDR9, SDR11	PE3306		73		0.63			
D2737	SDR7.3, SDR9, SDR11	PE3406		73		0.63			
D2737	SDR7.3, SDR9, SDR11	PE3408		73		0.80			
D3035	DR-PR	PE1404		73		0.40			
D3035	DR-PR	PE2606	•••	73		0.40			•••
D3035	DR-PR	PE2708	•••	73	•••	0.80			•••
D3035	DR-PR	PE3608		73		0.80			
	SN								
D3035	DR-PR	PE3708		73	•••	0.80			
D3035	DR-PR	PE3710		73		1.00			
D3035	DR-PR	PE4608	•••	73	•••	0.80			
D3035	DR-PR	PE4708		73	•••	0.80			
D3035	DR-PR	PE4710	•••	73	***	1.00			
F714	SDR-PR	PE1404		73		0.40			
F714	SDR-PR	PE2606		73		0.63			
F714	SDR-PR	PE2708		73		0.80			
F714	SDR-PR	PE3608		73		0.80			

Table B-1 Hydrostatic Design Stresses (HDS) and Recommended Temperature Limits for Thermoplastic Pipe (Cont'd)

					mended	Hydrostati	c Design	Stress,	ksi, at
					erature its, °F				
ASTM		Material	Cell		(1), (2)]	_ 73°F			
Spec. No.	Pipe Designation	Designation	Class	Minimum	Maximum	[Note (3)]	100°F	180°F	200°F
F714	SDR-PR	PE3708		73	•••	0.80			
F714	SDR-PR	PE3710		73		1.00			
F714	SDR-PR	PE4608		73		0.80		8	
F714	SDR-PR	PE4708		73		0.80	20		
F714	SDR-PR	PE4710		73		1.00	3		
F2788/ F2788M	SDR/DR-PR	PEX0006		-58	230	0.63		0.40	0.31
F2788/ F2788M	SDR/DR-PR	PEX0008		-58	230	0.80		0.40	0.31
F2389	SDR6, SDR7.3, SDR11	PP		0	230	0.63	0.50	0.20	
D1785	Sch. 40, 80, 120	PVC1120	12454	73		2.00			
D1785	Sch. 40, 80, 120	PVC1220	12454	73		2.00			
D1785	Sch. 40, 80, 120	PVC2120	14333	73		2.00			
D1785	Sch. 40, 80, 120	PVC2116	14333	7 3		1.60			
D1785	Sch. 40, 80, 120	PVC2112	14333	73		1.25			
D1785	Sch. 40, 80, 120	PVC2110	14333	73		1.00			
D2241	PR (SDR series)	PVC1120	12454	73		2.00			
D2241	PR (SDR series)	PVC1220	12454	73		2.00			
D2241	PR (SDR series)	PVC2120	14333	73		2.00			
D2241	PR (SDR series)	PVC2116	14333	73		1.60			
D2241	PR (SDR series)	PVC2112	14333	73		1.25			
D2241	PR (SDR series)	PVC2110	14333	73		1.00			

NOTES:

⁽¹⁾ These recommended limits are for low pressure applications with water and other fluids that do not significantly affect the properties of the thermoplastic. The upper temperature limits are reduced at higher pressures, depending on the combination of fluid and expected service life. Lower temperature limits are affected more by the environment, safeguarding, and installation conditions than by strength.

⁽²⁾ These recommended limits apply only to materials listed. Manufacturers should be consulted for temperature limits on specific types and kinds of materials not listed.

⁽³⁾ Use these hydrostatic design stress (HDS) values at all lower temperatures.

Table B-1M Hydrostatic Design Stresses (HDS) and Recommended Temperature Limits for Thermoplastic Pipe (SI Units)

				Temperatu	mended re Limits, °C (1), (2)]	Hydrostatic	Design	Stress, I	MPa, at
ASTM Spec. No.	Pipe Designation	Material Designation	Cell Class	Minimum	Maximum	23°C [Note (3)]	38°C	82°C	93°C
	PR	ABS	43232	-40	80				
D2846	SDR11	CPVC4120	23447		82	13.8		3.45	
F441	Sch. 40	CPVC4120	23447	23	93.3	13.8		3.45	D
F441	Sch. 80	CPVC4120	23447	23	93.3	13.8		3.45	
F442	SDR-PR	CPVC4120	23447	23	93.3	13.8	11.3	3.45	
							0,		
D3309	SDR11	PB2110		23	93.3	6.9	\hat{S}_{2}	3.45	
D2239	SIDR-PR	PE1404		23		2.76			
D2239	SIDR-PR	PE2305		23		3.45			
D2239	SIDR-PR	PE2306		23		4.34			
D2239	SIDR-PR	PE2406		23		4.34			
D2239	SIDR-PR	PE3306		23	\sim	4.34			
D2239	SIDR-PR	PE3406		23	. Q.	4.34			
D2239	SIDR-PR	PE3408		23		5.51			
				0					
D2447	Sch. 40 and 80	PE1404		N23	•••	2.76			
D2447	Sch. 40 and 80	PE2305	,;c ⁺ ,c ⁻	23	•••	3.45			
D2447	Sch. 40 and 80	PE2306		23	•••	4.34			
D2447	Sch. 40 and 80	PE2406	_.	23	•••	4.34			
D2447	Sch. 40 and 80	PE3306		23	•••	4.34		•••	
D2447	Sch. 40 and 80	PE3406	IIC.	23	•••	4.34			
D2737	SDR7.3, SDR9, SDR11	PE2305	ر 	23		3.45			
D2737	SDR7.3, SDR9, SDR11	PE2306		23		4.34			
D2737	SDR7.3, SDR9, SDR11	PE2406		23		4.34			
D2737	SDR7.3, SDR9, SDR11	PE3306		23		4.34			
D2737	SDR7.3, SDR9, SDR11	PE3406		23		4.34			
D2737	SDR7.3, SDR9, SDR11	PE3408		23		5.51			
	SMI								
D3035	DR-PR	PE1404		23		2.76			
D3035	DR-PR	PE2606		23		4.34			
D3035	DR-PR	PE2708		23		5.51			
D3035	DR-PR	PE3608		23		5.51			
D3035	DR-PR	PE3708		23		5.51			
D3035	DR-PR	PE3710		23		6.89			
D3035	DR-PR	PE4608		23		5.51			
D3035	DR-PR	PE4708		23	•••	5.51			
D3035	DR-PR	PE4710		23		6.89			
F714	SDR-PR	PE1404		23		2.76			
F714	SDR-PR	PE2606		23		4.34			
F714	SDR-PR	PE2708	•••	23		5.51			
F714	SDR-PR	PE3608		23		5.51			

Table B-1M Hydrostatic Design Stresses (HDS) and Recommended Temperature Limits for Thermoplastic Pipe (SI Units) (Cont'd)

				Temperatu	mended re Limits, °C (1), (2)]	Hydrostatic	Design	Stress, I	MPa, at
ASTM Spec. No.	Pipe Designation	Material Designation	Cell Class	Minimum	Maximum	23°C [Note (3)]	38°C	82°C	93°C
F714	SDR-PR	PE3708	•••	23		5.51			
F714	SDR-PR	PE3710		23		6.89		8	
F714	SDR-PR	PE4608		23		5.51	200		
F714	SDR-PR	PE4708		23		5.51	CV		
F714	SDR-PR	PE4710		23		6.89			
F2788/ F2788M	SDR/DR-PR	PEX0006		-50	110	4.34		2.76	2.17
F2788/ F2788M	SDR/DR-PR	PEX0008		-50	110	5.51		2.76	2.17
F2389	SDR6, SDR7.3, SDR11	PP		-18	5699 P	4.34	3.45	1.38	
D1785	Sch. 40, 80, 120	PVC1120	12454	23	? ∼	13.8			
D1785	Sch. 40, 80, 120	PVC1220	12454	23		13.8			
D1785	Sch. 40, 80, 120	PVC2120	14333	23		13.8			
D1785	Sch. 40, 80, 120	PVC2116	14333	23		11.0			
D1785	Sch. 40, 80, 120	PVC2112	14333	23		8.6			
D1785	Sch. 40, 80, 120	PVC2110	14333	23		6.9			
			×O						
D2241	PR (SDR series)	PVC1120	12454	23		13.8			
D2241	PR (SDR series)	PVC1220	12454	23		13.8			
D2241	PR (SDR series)	PVC2120	14333	23		13.8			
D2241	PR (SDR series)	PVC2116	14333	23		11.0			
D2241	PR (SDR series)	PVC2112	14333	23		8.6			
D2241	PR (SDR series)	PVC2110	14333	23		6.9			

NOTES:

⁽¹⁾ These recommended limits are for low pressure applications with water and other fluids that do not significantly affect the properties of the thermoplastic. The upper temperature limits are reduced at higher pressures, depending on the combination of fluid and expected service life. Lower temperature limits are affected more by the environment, safeguarding, and installation conditions than by strength.

⁽²⁾ These recommended limits apply only to materials listed. Manufacturers should be consulted for temperature limits on specific types and kinds of materials not listed.

⁽³⁾ Use these hydrostatic design stress (HDS) values at all lower temperatures.

Table B-2 Listed Specifications for Laminated Reinforced Thermosetting Resin Pipe

Spec. No.	
ASTM C582	

GENERAL NOTE: The intent of listing in this Table is to include all the types, grades, classes, and hydrostatic design bases in the listed specifications.

Table B-3 Listed Specifications for Filament Wound and Centrifugally Cast Reinforced Thermosetting Resin and

	Spec. Nos. (ASTM Except as Noted)								
D2517	D2997	D3754							
D2996	D3517	AWWA C950							

GENERAL NOTE: The intent of listing in this Table is to include all the types, grades, classes, and hydrostatic design bases in the listed specifications.

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Table B-4 Allowable Pressures and Recommended Temperature Limits for Concrete Pipe

			Allowab	le Gage			d Tempe Note (1)]	
			Press	-	Minir	num	Maxi	mum
Spec. No.	Material	Class	kPa	psi	°C	°F	°C	°F
ASTM C361	Reinforced concrete	25	69	10				
		50	138	20				
		75	205	30				
		100	275	40				
		125	345	50			18	
AWWA C300	Reinforced concrete		1 795	260		<u></u>	7	
AWWA C301	Reinforced concrete	Lined cylinder	1 725	250		/,5		
		Embedded cylinder	2 415	350	400			
AWWA C302	Reinforced concrete		310	45	<i>//</i>			

NOTE: (1) These recommended limits apply only to materials listed. Manufacturers should be consumed for temperature limits on specific types and kinds of materials not listed.

Table B-5 Allowable Pressures and Recommended Temperature Limits for Borosilicate Glass Pipe

				Allo	wable	Temp		ımended Limits [Not	te (1)]
		Size Ran	ge 💉	Gage P	ressure	Mini	mum	Maxi	mum
ASTM Spec. No.	Material	DN	NPS	kPa	psi	°C	°F	°C	°F
C599	Borosilicate glass	8-15	1/4-1/2	690	100			232	450
		20	3/4	515	75			232	450
		25-80	1-3	345	50			232	450
		100	4	240	35			232	450
		150	6	138	20			232	450

NOTE: (1) These recommended limits apply only to materials listed. Manufacturers should be consulted for temperature limits on specific types and kinds of materials not listed.

Table B-6 Allowable Pressures and Recommended Temperature Limits for PEX-AL-PEX and PE-AL-PE Pipe

ASTM		Size	Range	Allowab Pres		Maxim Temperatur [Note (e Limits
Spec. No.	Material	mm	in.	kPa	psi	°C	°F
F1281	PEX-AL-PEX	9.12-60.75	3/8-21/2	1 379	200	23	73.4
				1 103	160	60	140
				862	125	82.2	180
F1282	PE-AL-PE	9.12-60.75	$\frac{3}{8} - 2\frac{1}{2}$	1 379	200	23	73.4
				1 103	160	60	0140
				862	100	82.2	180
F1974	Metal insert fittings for PEX-AL-PEX systems	12.16-25.32	1/2-1	862	125	82	180
	Metal insert fittings for	12.16-25.32	¹ / ₂ -1	1 103	160	60	140
	PE-AL-PE systems			862	125	82	180
	Metal insert fittings for PE-AL-PE systems hese recommended limits applifications and listed.	OM: Click	to lienty	Efulli			

APPENDIX C PHYSICAL PROPERTIES OF PIPING MATERIALS

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Data
Expansion
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Tab

	B = Lir	B = Linear Thermal Expansion, in./100ft	al Expans	ion, in./1	00 ft							•						
	5							Тел	Temperature Range 70°F to	re Rang	e 70°F t	0						
Material	Coefficient	(t -325	-150	-50	20	200	300	400	200	009	200	800	006	1,000	1,100	1,200	1,300	1,400
Group 1 carbon and low alloy	A	5.5	5.9	6.2	6.4	6.7	6.9	7.1	7.3	7.4	9.7	7.8	7.9	8.1	8.2	8.3	8.4	8.4
steels [Note (2)]	В	2	-1.6	6.0-	0	1.0	1.9	2.8	3.7	4.7	5.7	8.9	7.9	0.6	10.1	11.3	12.4	14.7
Group 2 low alloy steels [Note (3)]	Α	6.0	6,5	6.7	7.0	7.3	7.4	9.7	7.7	7.8	7.9	8.0	8.1	8.2	8.3	8.4	8.4	8.5
	В	-2.9	<u>-1</u>	-1.0	0	1.1	2.0	3.0	4.0	5.0	0.9	7.0	8.1	9.2	10.3	11.4	12.5	13.5
5Cr-1Mo steels	А	5.6	0.9	6.2	6.4	6.7	6.9	7.0	7.1	7.2	7.2	7.3	7.4	7.5	9.7	9.7	7.7	7.8
	В	-2.7	-1.6	0.0	0	1.0	1.9	2.8	3.7	4.6	5.5	6.4	7.4	8.4	9.3	10.3	11.4	12.4
9Cr-1Mo steels	Α	5.0	5.4	2.6	5.8	0.9	6.2	6.3	6.4	6.5	9.9	6.7	8.9	6.9	7.0	7.1	7.2	7.2
	В	-2.4	-1.4	-0.8	0	6.0	1.7	2.5	3.3	4.1	5.0	5.9	8.9	7.7	8.7	9.7	10.6	11.6
Straight chromium stainless steels						X 10												
12Cr to 13Cr steels	А	5.1	5.5	5.7	5.9	6.2	9	6.4	6.5	6.5	9.9	6.7	6.7	8.9	8.9	6.9	6.9	7.0
	В	-2.4	-1.5	-0.8	0	1.0	1.7%	2.5	3.3	4.2	5.0	5.8	6.7	9.7	8.5	9.4	10.2	11.1
15Cr to 17Cr steels	А	4.5	4.9	5.1	5.3	5.5	5.7	IN OR	5.9	0.9	6.1	6.2	6.2	6.3	6.4	6.4	6.5	6.5
	В	-2.1	-1.3	-0.7	0	6.0	1.6	2.3	3.0	3.8	4.6	5.4	6.2	7.0	7.9	8.7	9.5	10.4
27Cr steels	A	4.3	4.7	4.9	5.0	5.2	5.2	5.3	5.4	5.4	5.5	5.6	5.7	5.7	5.8	5.9	5.9	0.9
	В	-2.0	-1.2	-0.7	0	8.0	1.4	2.1	2.8	3.5	4.2	4.9	2.6	6.4	7.2	8.0	8.7	9.6
Austenitic stainless steels (304,	Α	7.5	8.0	8.2	8.5	8.9	9.2	9.5	9.7	Q .6	210.0	10.1	10.2	10.3	10.4	10.6	10.7	10.8
305, 316, 317, 321, 347, 348, 19-9DL, XM-15, etc.)	В	-3.6	-2.1	-1.2	0	1.4	2.5	3.8	5.0	6.3	65/1	8.8	10.2	11.5	12.9	14.3	15.8	17.2
Other austenitic stainless steels	Α	7.1	9.7	7.8	8.2	8.5	8.7	8.9	9.1	9.5	9.3	9.4	9.5	9.6	6.7	8.6	6.6	10.1
(309, 310, 315, XM-19, etc.)	В	-3.4	-2.0	-1.1	0	1.3	2.4	3.5	4.7	5.8	7.0	\$3 \$3	9.5	10.7	12.0	13.3	14.7	16.1
Gray iron	A	÷	:	:	:	2.8	5.9	6.1	6.3	6.5	6.7	8.9	<u>62</u> .	7.2	:	:	:	:
	В	:	:	:	0	6.0	1.6	2.4	3.2	4.1	5.0	0.9	7.0	98.0	÷	:	÷	÷
Ductile cast iron	А	÷	4.9	5.3	5.7	0.9	6.3	9.9	8.9	7.0	7.1	7.3	7.4	%	:	:	:	÷
	В	:	-1.3	-0.8	0	6.0	1.7	2.6	3.5	4.5	5.4	6.4	7.3	8.4	÷	:	÷	÷

Table C-1 Thermal Expansion Data (Cont'd)

Material Coefficient 150		B = Linear Thermal Expansion, in./100 ft	r Therma	l Expansi	Linear Thermal Expansion, in./100 ft	10 ft													
Coefficient 265 150 200 400 500 600 600 600 600 100 1100 1200 1200 1300 1300 1300 400 500 400 100 1100 </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Тет</th> <th>nperatu</th> <th>re Rang</th> <th>e 70°F</th> <th>to</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>									Тет	nperatu	re Rang	e 70°F	to						
A 58***Mea 72 72 81 83 85 87 88 89 89 90 91 91 91 92 93 93 94 <t< th=""><th>Material</th><th>Coefficient</th><th>-325</th><th>-150</th><th>-50</th><th>20</th><th>200</th><th>300</th><th>400</th><th>200</th><th>009</th><th>200</th><th>800</th><th>006</th><th>1,000</th><th>1,100</th><th>1,200</th><th>1,300</th><th>1,400</th></t<>	Material	Coefficient	-325	-150	-50	20	200	300	400	200	009	200	800	006	1,000	1,100	1,200	1,300	1,400
8 -27 48 -10 0 13 23 34 45 56 67 78 90 101 113 124 136 8 -27 -17 -60 11 21 21 21 45 56 67 75 77 79 80 82 83 84 85 86 87 88 84 85 86 87 88 89 81 85 86 87 88 87 86 87 87 88 87 86 87 <t< th=""><th>Monel (67Ni-30Cu) N04400</th><th>А</th><th>5.8</th><th>6.8</th><th>7.2</th><th>7.7</th><th>8.1</th><th>8.3</th><th>8.5</th><th>8.7</th><th>8.8</th><th>8.9</th><th>8.9</th><th>0.6</th><th>9.1</th><th>9.1</th><th>9.2</th><th>9.2</th><th>9.3</th></t<>	Monel (67Ni-30Cu) N04400	А	5.8	6.8	7.2	7.7	8.1	8.3	8.5	8.7	8.8	8.9	8.9	0.6	9.1	9.1	9.2	9.2	9.3
4 5.3 6.0 4.0 7.2 7.5 7.7 7.9 8.0 8.2 8.4 8.5 8.6 8.7 8.0 8 -2.7 -1.7 -1.0 0 1.1 2.1 3.1 4.1 5.1 6.2 7.3 8.4 9.5 10.7 11.8 13.0 8		В	-2.7	30)	-1.0	0	1.3	2.3	3.4	4.5	5.6	6.7	7.8	0.6	10.1	11.3	12.4	13.6	14.8
B -27 -170 0 11 21 41 51 62 73 84 95 107 118 130 4 60 61 62 70 70 72 73 84 95 107 118 130 8 0 111 120 20 70 72 73 75 86 98 110 110 110 20 70	Nickel alloys N02200 and	A	5.3	9.9	6:3	9.9	7.2	7.5	7.7	7.9	8.0	8.2	8.3	8.4	8.5	9.8	8.7	8.8	8.9
4 6.9 6.9 6.9 7.0 7.2 7.5 7.5 7.7 7.9 8.1 8.3 8.4 8.5 7.9 7.9 7.0	N02201	В	-2.7	-1.7	O'I-	0	1.1	2.1	3.1	4.1	5.1	6.2	7.3	8.4	9.5	10.7	11.8	13.0	14.2
B 0 11 19 27 36 45 54 64 75 86 98 110 12 A 55 61 64 68 44 73 75 76 78 79 80 82 84 86 87 A	Nickel alloy N06022	А	:	:		6.9	6.9	6.9	6.9	7.0	7.0	7.2	7.3	7.5	7.7	7.9	8.1	8.3	8.5
4 5.5 6.1 6.4 6.8 74 7.5 7.6 7.6 7.6 8.0		В	:	:	ŧ	.°	1.1	1.9	2.7	3.6	4.5	5.4	6.4	7.5	9.8	8.6	11.0	12.2	13.6
B -2.6 -1.6 -0.9 0 11.0 2.0 3.9 5.0 6.0 7.0 8.1 9.3 10.4 11.0 11.0 2.0 3.9 5.0 6.0 7.0 8.1 9.9 11.0 11.0 2.0 2.0 3.8 4.7 5.6 6.6 7.7 9.9 9.0 9.1 9.2 9.4 9.9 11.1 12.3 4.4 7.5 6.6 7.7 9.9 9.9 9.0 9.1 9.2 9.4 9.9 9.0 9.1 9.2 9.4 9.5 9.1 9.2 9.4 9.5 9.1 9.2 9.4 9.2 9.1 9.2	Nickel alloy N06600	A	5.5	6.1	6.4	8.9	老	7.3	7.5	9.7	7.8	7.9	8.0	8.2	8.3	8.4	9.8	8.7	8.9
4 6.7 7.1 7.2 7.3 7.4 7.5 7.6 7.7 7.9 8.0 8.2 8.4 7.5 7.6 6.6 7.7 7.9 8.0 9.0		В	-2.6	-1.6	-0.9	0	1.1	2.0	3.0	3.9	2.0	0.9	7.0	8.1	9.3	10.4	11.6	12.9	14.2
B 0 1.1 200 29 3.8 4.7 5.6 6.6 7.7 88 9.0 11.1 12.3 A 5.9 6.9 7.4 7.9 8.4 8.6 8.9 9.0 9.1 9.2 9.4 9.5 9.4 9.5 9.7 A -2.8 -1.7 -1.1 0 1.3 2.4 3.5 4.6 5.7 6.9 8.1 9.3 9.4 9.5 9.7 9.7 9.8 8.4 8.7 8.6 8.7 9.7 9.7 9.8 8.4 8.7 8.5 9.6 9.7	Nickel alloy N06625	А	:	:	i	6.7	7.1	120	7.3	7.4	7.4	7.5	9.7	7.7	7.9	8.0	8.2	8.4	8.5
4 5.9 6.9 6.9 9.1 9.2 9.2 9.3 9.4 9.6 9.7 9.2 9.3 9.4 9.6 9.7 9.2 9.3 9.4 9.5 9.7 9.3 9.4 9.5 9.4 9.5 9.4 9.5 9.7 9.7 9.8 8.4 8.7 8.9 8.1 8.3 8.4 8.5 9.6 1.1 1.4 1.4 1.4 1.5 1.5 1.4 1.4 1.5 1.5 1.4 1.4 1.5 1.5 1.4 1.4 1.5 1.5 1.4 8.7		В	:	:	i	0	1.1	2.07	5.9	3.8	4.7	2.6	9.9	7.7	8.8	6.6	11.1	12.3	13.6
B -2.8 -1.7 -1.1 0 1.3 2.4 3.5 4.6 5.7 6.9 8.1 9.3 10.5 11.8 13.0 14.4 A 7.2 7.5 7.7 7.9 8.0 8.4 8.5 8.6	Nickel alloys N08800 and	A	5.9	6.9	7.4	7.9	8.4	9.8	?	8.9	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	8.6
A 7.2 7.5 7.9 8.0 8.1 8.2 8.3 8.4 8.5 8.6 7.1 7.9 8.0 8.1 9.2 7.4 8.5 9.6	N08810	В	-2.8	-1.7	-1.1	0	1.3	2.4	3.5	4.6	5.7	6.9	8.1	9.3	10.5	11.8	13.0	14.4	15.7
B	Nickel alloy N08825	А	;	:	7.2	7.5	7.7	7.9	8.0	8.1	8.2	8.3	8.4	8.5	9.8	÷	;	i	;
4 6.0 6.3 6.5 6.7 7.0 7.0 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.9 7.9 7.0		В	:	:	-1.0	0	1.2	2.2	3.2	4.2	5.5	6.3	7.4	8.5	9.6	÷	:	÷	ŧ
B 0 1.0 1.8 2.7 6.4 7.5 6.4 7.5 8.5 9.5 10.7 A 7.7 8.7 9.0 9.3 9.6 9.7 9.8 9.9 10.0	Nickel alloy N10276	A	:	:	i	0.9	6.3	6.5	6.7	6.9	7.0	7.2	7.4	7.5	9.7	7.7	7.8	7.9	8.0
A 7.7 8.7 9.0 9.3 9.6 9.7 9.8 9.9 10.0		В	:	:	:	0	1.0	1.8	2.7	3.6	4.5	5.5	6.4	7.5	8.5	9.5	10.6	11.7	12.8
s	Copper alloys C1XXXX series	A	7.7	8.7	9.0	9.3	9.6	9.7	8.6	6.6	10.0	7	, č	÷	:	:	:	:	:
s A 8.8 8.9 9.2 9.6 10.0 10.1 10.2 10.3 10.4 10.5 10.6 40.7 10.8 10.9 11.0 B -4.0 -2.3 -1.3 0 1.6 2.8 4.0 5.3 6.6 8.0 9.3 10.7 12.1 13.5 14.9 A 8.2 8.5 9.0 9.3 9.8 10.0 10.2 10.5 10.7 10.9 11.2 11.4 0.1 13.5 14.9 B -3.9 -2.2 -1.3 0 1.5 2.8 4.1 5.4 6.8 8.2 9.8 11.4 13.0 14.7 16.4 B -3.2 -2.0 -1.1 0 1.3 2.4 3.5 4.7 5.8 7.0		В	-3.7	-2.3	-1.3	0	1.5	2.7	3.9	5.1	6.4	:	2	:	÷	:	:	:	÷
B -4.0 -2.3 -1.3 0 1.6 2.8 4.0 5.3 6.6 8.0 9.3 10.7 12.1 13.5 14.9 A 8.2 8.5 9.0 9.3 9.8 10.0 10.2 10.5 10.7 10.9 11.2 11.4 11.6 11.9 12.1 B -3.9 -2.2 -1.3 0 1.5 2.8 4.1 5.4 6.8 82 9.8 11.4 13.0 14.7 16.4 El (70Cu-30Ni) A 6.7 7.4 7.8 81 8.5 87 8.9 9.1 9.2 9.2	Bronze alloys	A	8.4	8.8	9.2	9.6	10.0	10.1	10.2	10.3	10.4	10.5	10.6	40.7	10.8	10.9	11.0	÷	÷
A 8.2 8.5 9.0 9.3 9.8 10.0 10.2 10.5 10.7 10.9 11.2 11.4 Ol.6 11.9 12.1 B -3.9 -2.2 -1.3 0 1.5 2.8 4.1 5.4 6.8 8.2 9.8 11.4 13.0 14.7 16.4 cel (70Cu-30Ni) A 6.7 7.4 7.8 8.1 8.5 8.7 8.9 9.1 9.2 9.2 B -3.2 -2.0 -1.1 0 1.3 2.4 3.5 4.7 5.8 7.0		В	-4.0	-2.3	-1.3	0	1.6	2.8	4.0	5.3	9.9	8.0	9.3	10.20	12.1	13.5	14.9	:	:
B -3.9 -2.2 -1.3 0 1.5 2.8 4.1 5.4 6.8 8.2 9.8 11.4 13.9 14.7 16.4 A 6.7 7.4 7.8 8.1 8.5 8.7 8.9 9.1 9.2 9.2 B -3.2 -2.0 -1.1 0 1.3 2.4 3.5 4.7 5.8 7.0	Brass alloys	A	8.2	8.5	9.0	9.3	8.6	10.0	10.2	10.5	10.7	10.9	11.2	12	11.6	11.9	12.1	:	:
A 6.7 7.4 7.8 8.1 8.5 8.7 8.9 9.1 9.2 9.2 9.2		В	-3.9	-2.2	-1.3	0	1.5	2.8	4.1	5.4	8.9	8.2	8.6	11.4	1390	14.7	16.4	:	:
-3.2 -2.0 -1.1 0 1.3 2.4 3.5 4.7 5.8 7.0	Copper-nickel (70Cu-30Ni)	A	6.7	7.4	7.8	8.1	8.5	8.7	8.9	9.1	9.2	9.2	:	÷	:	:	:	:	:
		В	-3.2	-2.0	-1.1	0	1.3	2.4	3.5	4.7	2.8	7.0	;	÷	:	:	:	:	:

Table C-1 Thermal Expansion Data (Cont'd)

	$A = \text{Mean Coefficient of Thermal Expansion, } 10^{-6} \text{ in./in./}^{\circ}\text{F}$ $B = \text{Linear Thermal Expansion, in./} 100 \text{ ft}$	efficient hermal E	of Therm xpansion	ıal Expans , in./ 100	sion, 10 ⁻ ft	-6 in./in	_	in Going	From 70	in Going From 70°F to Indicated Temperature [Note (1)]	licated T	emperat	ıre [Note	(1)]				
	N							Ter	nperatu	Temperature Range 70°F to	e 70°F	to						
Material	Coefficient	-322	-150 -	. 09-	70	200	300	400	200	009	200	800	006	1,000	1,100	1,200	1,300	1,400
Aluminum alloys) V	9,9	10.9	11.6 1	12.1	13.0	13.3	13.6	13.9	14.2	:	:	:	:	:	:	÷	:
	В -	4.7	-2.9	-1.7	0	2.0	3.7	5.4	7.2	0.6	:	:	÷	;	:	÷	:	÷
Titanium alloys (Grades 1, 2, 3, 7,	Α.	,	~	4.5	4.6	4.7	4.8	4.8	4.9	4.9	5.0	5.1	:	:	÷	:	÷	:
and 12)	В .		S	€0.6	0	0.7	1.3	1.9	2.5	3.1	3.8	4.5	÷	:	÷	;	ŧ	:
NOTES:			· :		-	:	-											
 I hese data are for information and it is not to be implied Group 1 alloys (by nominal composition): 	on and it is not t composition):	o be imj	plied tha	I that materials are suitable for all the temperature ranges shown.	als are s	uitable	tor all t	ne temp	erature	ranges s	hown.							
	Carbo	Carbon steels (C,	$\overline{}$	C-Si, C-Mn, and G-Mn-Si)	nd G-M	n-Si)	c	3Cr-1Mo										
	$C-\frac{1}{2}Mo$	0]					1,	$\frac{1}{2}Ni-\frac{1}{2}Mo-V$	N-0									
	$^{1}/_{2}$ Cr $^{-1}$	$\frac{1}{2}$ Cr- $\frac{1}{5}$ Mo-V			Ç	*	1,	$\frac{1}{2}Ni-\frac{1}{2}Cr-\frac{1}{4}Mo-V$	r-1/4Mo-	λ-								
	$\frac{1}{2}$ Cr- $\frac{1}{2}$	1/2Cr-1/4Mo-Si				×Ç	ω,	3 ₄ Ni $^{-1}$ ₂ Mo $^{-1}$ Cr $^{-1}$	o-Cr-V									
	$^{1}/_{2}Cr-^{1}/_{2}Mo$	½Mo)	(n)	$^{3}/_{4}Ni-^{1}/_{2}Mo-^{1}/_{3}Cr-V$	0-1/3Cr-	Λ-								
	$^{1/2}$ Cr $^{-1}$	$\frac{1}{2}Cr-\frac{1}{2}Ni-\frac{1}{4}Mo$	10				(S)	³ / ₄ Ni- ¹ / ₂ Cu-Mo	n-Mo									
	$^{3}_{4}\text{Cr}^{-1}$	$^{3}_{4}$ Cr- $^{1}_{2}$ Ni-Cu					R.	4Ni-1/2C	r-½Mo-	λ-								
	3 4Cr- 3	$\frac{3}{4}$ Cr- $\frac{3}{4}$ Ni-Cu-Al	-Al				ω,	34N-4Mo-34Cr	34Cr									
	$1\text{Cr}-\frac{1}{2}\text{Mo}$	₅ Mo					1	1Ni-1/2Cr-1/2Mo	¹ / ₂ Mo									
	1 Cr $^{-1}$ /	$1Cr-\frac{1}{5}Mo-Si$					1	$1\frac{1}{4}$ Ni– 1 Cr– $\frac{1}{2}$ Mo	r-1/2Mo									
	$1\text{Cr}-\frac{1}{2}\text{Mo}$	2Mo					1	$1\frac{3}{4}\text{Ni} - \frac{3}{4}\text{Cr} - \frac{1}{4}\text{Mo}$	$Cr-\frac{1}{4}M$	6								
	$1\mathrm{Cr}^{-1}$	$1Cr-\frac{1}{2}Mo-V$					2	$2Ni-\frac{3}{4}Cr-\frac{1}{4}Mo$	-1/4Mo	<								
	1^{1}_{4} Cr-	$1\frac{1}{4}Cr-\frac{1}{2}Mo$					2	$2Ni-\frac{3}{4}Cr-\frac{1}{3}Mo$	- ¹ / ₃ Mo	Ó								
	$1\frac{1}{4}$ Cr-	$1\frac{1}{4}Cr-\frac{1}{2}Mo-Si$	i				2	$2\frac{1}{2}Ni$		`	P							
	1%Cr-	1 ³ / ₄ Cr- ¹ / ₂ Mo-Cu	<u>, =</u>				3	$3\frac{1}{2}Ni$			5							
	$2Cr-\frac{1}{2}Mo$	2Mo					c	$3\frac{1}{2}Ni-1\frac{3}{4}Cr-\frac{1}{2}Mo-V$	$^{4}_{4}Cr-^{1}_{2}N$		71	. <						
	$2^{1}/_{4}Cr-1Mo$	-1Mo										2						
(3) Group 2 alloys (by nominal composition):	omposition):											2						
	Mn-V						~	$Mn^{-1}/_{2}Mo^{-1}/_{4}Ni$	-1/4Ni				က					
	$Mn-\frac{1}{4}Mo$	Mo					2	$Mn^{-1}/_2Mo^{-1}/_2Ni$	¹ / ₂ Ni				V	2				
	$Mn^{-1}/_2Mo$	Мо					2	Mn-½Mo-¾Ni	-3/4Ni					1 8				

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Table C-1M Thermal Expansion Data (SI Units)

 $A = \text{Mean Coefficient of Thermal Expansion, } 10^{-6} \text{ mm/mm/}^{\circ}\text{C}$ in Going From 20°C to Indicated Temperature Note [(1)] B = Linear Thermal Expansion, mm/m

						Т	emper	ature	Range	20°C	to				
Material	Coefficient	-200	-100	-50	20	50	75	100	125	150	175	200	225	250	275
Group 1 carbon and low alloy	A	9.9	10.7	11.1	11.5	11.8	11.9	12.1	12.3	12.4	12.6	12.7	12.9	13.0	13.2
steels [Note (2)]	В	-2.2	-1.3	-0.8	0	0.4	0.7	1.0	1.3	1.6	2.0	2.3	2.6	3.0	3.4
Group 2 low alloy steels	A	10.8	11.7	12.0	12.6	12.8	13.0	13.1	13.2	13.4	13.5	13.6	13.7	138	13.9
[Note (3)]	В	-2.4	-1.4	-0.8	0	0.4	0.7	1.0	1.4	1.7	2.1	2.4	2.8	3.2	3.6
5Cr-1Mo steels	A	10.1	10.8	11.2	11.5	11.8	12.0	12.1	12.3	12.4	12.5	12.6	12.6	12.7	12.8
	В	-2.2	-1.3	-0.8	0	0.4	0.7	1.0	1.3	1.6	1.9	(2.3)	2.6	2.9	3.3
9Cr-1Mo steels	A	9.0	9.8	10.1	10.5	10.6	10.7	10.9	11.0	11.1	11.2	11.3	11.4	11.5	11.6
	В	-2.0	-1.2	-0.7	0	0.3	0.6	0.9	1.2	1.4	1.7	2.0	2.3	2.6	3.0
Straight chromium stainless steels										KP.					
12Cr to 13Cr steels	A	9.1	9.9	10.2	10.6	10.9	11.0	11.1	11.3	11.4	11.4	11.5	11.6	11.6	11.7
	В	-2.0	-1.2	-0.7	0	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.4	2.7	3.0
15Cr to 17Cr steels	A	8.1	8.8	9.1	9.6	9.7	9.9	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7
	В	-1.8	-1.1	-0.6	0	0.3	0,5	0.8	1.1	1.3	1.6	1.9	2.2	2.4	2.7
27Cr steels	A	7.7	8.5	8.7	9.0	9.2	9.2	9.3	9.4	9.4	9.5	9.5	9.6	9.6	9.7
2761 566615	В	-1.7	-1.0	-0.6		0.3	0.5	0.7	1.0	1.2	1.5	1.7	2.0	2.2	2.5
Austenitic stainless steels (304,	Α	13.5	14.3	14.7	15.3	15.6	15.9	16.2	16.4	16.6	16.8	17.0	17.2	17.4	17.5
(305, 316, 317, 321, 347, 348, 19-9DL, XM-15, etc.)	В	-3.0	-1.7	710	0	0.5	0.9	1.3	1.7	2.2	2.6	3.1	3.5	4.0	4.5
Other austenitic stainless steels	A	12.8	13.6	14.1	14.7	15.0	15.2	15.4	15.6	15.7	15.9	16.0	16.1	16.3	16.4
(309, 310, 315, XM-19, etc.)	В	-2.8		-1.0	0	0.4	0.8	1.2	1.6	2.0	2.5	2.9	3.3	3.7	4.2
	(-O'	. 1.0	1.0											
Gray iron	$\frac{A}{B}$	J			9.8	10.1	10.2	10.4	10.5	10.7	10.8	11.0	11.1	11.2	11.4
					0	0.3	0.6	8.0	1.1	1.4	1.7	2.0	2.3	2.6	2.9
Ductile cast iron	N/A		8.8	9.5	10.3	10.5	10.7	10.9	11.1	11.3	11.6	11.8	12.0	12.2	12.4
· OP	В		-1.1	-0.7	0	0.3	0.6	0.9	1.2	1.5	1.8	2.1	2.5	2.8	3.1
Monel (67Ni-30Cu) N04400	A	10.4	12.2	13.0	13.8	14.1	14.4	14.6	14.8	15.0	15.1	15.3	15.4	15.5	15.6
CONFIN	В	-2.3	-1.5	-0.9	0	0.4	8.0	1.2	1.6	1.9	2.3	2.8	3.2	3.6	4.0
Nickel alloys N02200 and	A	9.6	10.8	11.4	11.9	12.4	12.7	13.0	13.3	13.5	13.7	13.9	14.0	14.2	14.3
N02201	В	-2.2	-1.4	-0.8	0	0.4	0.7	1.0	1.4	1.8	2.1	2.5	2.9	3.3	3.6
Nickel alloy N06022	A				12.4	12.4	12.4	12.4	12.4	12.4	12.4	12.4	12.5	12.5	12.6
·	В				0	0.4	0.7	1.0	1.3	1.6	1.9	2.2	2.6	2.9	3.2
Nickel alloy N06600	A	9.9	10.8	11.5	12.3	12.5	12.7	12.8	13.0	13.2	13.3	13.5	13.6	13.7	13.8
	В	-2.2	-1.3	-0.8	0	0.4	0.7	1.0	1.4	1.7	2.1	2.4	2.8	3.2	3.5
Nial al alla MOCCOS					100	10.4	10.6	100	100	100	10.4	10.0	100	100	100
Nickel alloy N06625	A				12.0	12.4	12.6	12.8	12.9	13.0	13.1	13.2	13.2	13.2	13.3
	В				0	0.4	0.7	1.0	1.4	1.7	2.0	2.4	2.7	3.0	3.4

Table C-1M Thermal Expansion Data (SI Units)

 $A = \text{Mean Coefficient of Thermal Expansion, } 10^{-6} \text{ mm/mm/}^{\circ}\text{C}$ B = Linear Thermal Expansion, mm/m in Going From 20°C to Indicated Temperature Note [(1)]

								Tem	peratu	re Rai	nge 20	°C to								
300	325	350	375	400	425	450	475		525	550	575	600	625	650	675	700	725	750	775	800
13.3	13.4	13.6	13.7	13.8	14.0	14.1	14.2	14.4	14.5	14.6	14.7	14.8	14.9	15.0	15.1	15.1	15.2	15.3	15.3	15.4
3.7	4.1	4.5	4.9	5.3	5.7	6.1	6.5	6.9	7.3	7.7	8.2	8.6	9.0	9.4	9.9	10.3	10.7	11.1	11.6	12.0
140	14.1	142	14.3	14.4	14.5	14.6	14.6	147	1/10	1/0	140	15.0	15.0	151	151	15 2	15 2	152	15.3	152
14.0 3.9	4.3	4.7	5.1	5.5	5.9	6.3	6.7	7.1	7.5	7.9	8.3	8.7	9.1	9.5					11.1	
0.7	1.0	1.,	5.1	0.0	0.7	0.5	0.7	,.1	7.0	7.5	0.0	0.7	,.1	7.0	,,,	10.5	10.7		41.1	11.0
12.8	12.9	13.0	13.0	13.1	13.2	13.2	13.3	13.4	13.4	13.5	13.6	13.6	13.7	13.7	13.8	13.9	13.9	14.0	14.0	14.1
3.6	3.9	4.3	4.6	5.0	5.3	5.7	6.1	6.4	6.8	7.2	7.5	7.9	8.3	8.7	9.0	9.4	9.8	10.2	10.6	11.0
11.7	11.8	11.9	11.9	12.0	12.1	12.2	12.3	12.3	12.4	12.5	12.6	12.7	12.7	12.8	12.9	13.0	13.1	13.3	13.4	13.6
3.3	3.6	3.9	4.2	4.6	4.9	5.2	5.6	5.9	6.3	6.6	7.0	7.3	7.7	8.1		8.9	9.3		10.1	
)				
														×	, k					
11.7	11.8	11.8	11.9	11.9	12.0	12.0	12.1	12.1	12.2	12.2	12.3	12.3	12.4	12.4	12.5	12.5	12.5	12.5	12.6	12.6
3.3	3.6	3.9	4.2	4.5	4.9	5.2	5.5	5.8	6.2	6.5	6.8		7.5	1 -	8.2	8.5	8.8	9.2	9.5	9.8
												- 3								
10.8	10.8	10.9										10	11.5						11.8	11.9
3.0	3.3	3.6	3.9	4.2	4.5	4.8	5.1	5.4	5.7	6.0	6.3	6.6	7.0	7.3	7.6	7.9	8.2	8.6	8.9	9.3
9.7	9.8	9.9	9.9	10.0	10.0	10.1	10.2	10.2	10.3	10.4	10.4	10.5	10.5	10.6	10.6	10.7	10.7	10.8	10.8	10.9
2.7	3.0	3.3	3.5	3.8	4.1	4.3	4.6	4.9	5.2	5.5	5.8	6.1	6.4	6.7	7.0	7.2	7.6	7.9	8.2	8.5
177	170	170	10.0	101	10.2	10.2	10.4	10.4	10 £	10.6	107	100	10.0	10.0	10.1	10.2	10.2	10.4	10.4	10.4
17.7 4.9	17.8 5.4	17.9 5.9	18.0 6.4	6.9	18.2 7.4	7.9	8.3												19.4 14.7	
4.7	5.4	3.7	0.4	0.7	7.4	7.5	0.5		٦.٦	7.7	10.4	10.7	11.7	12.0	12.5	13.1	13.0	14.1	14.7	13.2
16.5	166	16.6	167	16.8	16.9	170	17 1 *	172	172	173	17 <i>4</i>	175	176	177	17.8	179	18.0	18 1	18.2	183
4.6	5.0	5.5	5.9	6.4	6.8		7.8	8.2	8.7	9.2									13.7	
						C)`													
11.5	11.7	11.8	12.0	12.1		4.0	12.6		12.9	13.0										
3.2	3.6	3.9	4.2	4.6	5.0	5.3	5.7	6.1	6.5	6.9										
12.5	12.6	12.8	12.9	13.0	13.1	13.2	13.2	13.3	13.4	13.5										
3.5	3.9	4.2		4.9	5.3	5.7	6.0	6.4	6.8	7.2										
45.5	450	450	Ő	160	161	161	460	460	460	460	164	164	465	465	465	166	166	46.5	465	160
15.7	15.8	_ ()																		
4.4	4.8	134	5.7	0.1	6.5	6.9	7.4	7.0	0.2	0.0	9.1	9.5	10.0	10.4	10.0	11.5	11./	12.2	12.6	13.1
14.4	14.5	1 4.6	14.7	14.8	14.9	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.6	15.7	15.8	15.9	15.9	16.0	16.1	16.2
4.0	4.4	4.8	5.2	5.6	6.0	6.5	6.9	7.3	7.7	8.2	8.6	9.0	9.5	9.9	10.3	10.8	11.2	11.7	12.2	12.6
	12.7																			
3.5	3.9	4.2	4.6	5.0	5.3	5.7	6.1	6.5	7.0	7.4	7.8	8.3	8.7	9.2	9.7	10.1	10.6	11.1	11.6	12.1
14 0	14.1	14 2	143	144	145	146	147	148	149	15.0	151	15 2	153	154	15.6	157	15.8	159	161	162
	4.3																			
,				0		- 10			0			0	- 10					0		0
13.3	13.3	13.4	13.5	13.5	13.6	13.7	13.8	14.0	14.1	14.2	14.3	14.5	14.6	14.8	14.9	15.0	15.1	15.3	15.4	15.6
3.7	4.1	4.4	4.8	5.1	5.5	5.9	6.3	6.7	7.1	7.5	8.0	8.4	8.8	9.3	9.8	10.2	10.7	11.2	11.6	12.1

Table C-1M Thermal Expansion Data (SI Units) (Cont'd)

 $A = \text{Mean Coefficient of Thermal Expansion, } 10^{-6} \text{ mm/mm/}^{\circ}\text{C}$ B = Linear Thermal Expansion, mm/min Going From 20°C to Indicated Temperature Note [(1)]

						Т	emper	ature	Range	20°C	to				
Material	Coefficient	-200	-100	-50	20	50	75	100	125	150	175	200	225	250	275
Nickel alloys N08800 and	A	10.6	12.5	13.3	14.2	14.6	14.9	15.1	15.3	15.5	15.6	15.8	15.9	16.0	16.1
N08810	В	-2.3	-1.5	-0.9	0	0.4	0.8	1.2	1.6	2.0	2.4	2.8	3.3	3.7	4.1
Nickel alloy N08825	A			12.9	13.5	13.6	13.7	13.9	14.0	14.2	14.3	14.4	14.4	14.5	14.6
Š	В			-0.9	0	0.4	8.0	1.1	1.5	1.8	2.2	2.6	03 .0	3.3	3.7
Nickel alloy N10276	A				10.8	11.0	11.2	11.4	11.6	11.7	11.9	12.0	12.2	12.4	12.5
	В				0	0.3	0.6	0.9	1.2	1.5	1.8	2.2	2.5	2.8	3.2
Copper alloys C1XXXX series	A	13.9	15.7	16.2	16.7	17.0	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.8	17.9
	В	-3.1	-1.9	-1.1	0	0.5	0.9	1.4	1.8	2.3	2.7	3.2	3.6	4.1	4.6
Bronze alloys	A	15.1	15.8	16.4	17.2	17.6	17.9	18.0	18.2	18.2	18.3	18.4	18.5	18.5	18.6
	В	-3.3	-1.9	-1.1	0	0.5	1.0	14	1.9	2.4	2.8	3.3	3.8	4.3	4.7
Brass alloys	A	14.7	15.4	16.0	16.7	17.1	17.4	17.6	17.8	18.0	18.2	18.4	18.6	18.8	19.0
	В	-3.2	-1.9	-1.1	0	0.5	1.0	1.4	1.9	2.3	2.8	3.3	3.8	4.3	4.8
Copper-nickel (70Cu-30Ni)	A	11.9	13.4	14.0	14.5	214.9	15.2	15.3	15.5	15.7	15.8	16.0	16.1	16.3	16.4
	В	-2.6	-1.6	-1.0	001	0.4	8.0	1.2	1.6	2.0	2.5	2.9	3.3	3.7	4.2
Aluminum alloys	Α	18.0	19.7	20.8	21.7	22.6	23.1	23.4	23.7	23.9	24.2	24.4	24.7	25.0	25.2
	В	-4.0	-2.4	-1.5	0	0.7	1.3	1.9	2.5	3.1	3.7	4.4	5.1	5.7	6.4
Titanium alloys (Grades 1, 2, 3, 7,	Α	and the	<i>\</i>	8.2	8.3	8.4	8.5	8.5	8.6	8.6	8.6	8.7	8.7	8.7	8.8
and 12)	В	<u>ب</u> -		-0.6	0	0.3	0.5	0.7	0.9	1.1	1.3	1.6	1.8	2.0	2.2

Table C-1M Thermal Expansion Data (SI Units) (Cont'd)

 $A = \text{Mean Coefficient of Thermal Expansion, } 10^{-6} \text{ mm/mm/}^{\circ}\text{C}$ B = Linear Thermal Expansion, mm/m in Going From 20°C to Indicated Temperature Note [(1)]

								Temi	peratu	re Rai	nge 20)°C to								
300	325	350	375	400	425	450	475	500			575		625	650	675	700	725	750	775	800
'																				
16.2	16.3	16.4	16.5	16.5	16.6	16.7	16.8	16.8	16.9	17.0	17.1	17.2	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9
4.5	5.0	5.4	5.8	6.3	6.7	7.2	7.6	8.1	8.5	9.0	9.5	9.9	10.4	10.9	11.4	11.9	12.4	12.9	13.4	14.0
																			1/2)
14.7	14.8	14.9	15.0					15.4										<u>.</u>)	
4.1	4.5	4.9	5.3	5.7	6.1	6.5	7.0	7.4	7.8	8.3								ტ '		•••
12.6	12.0	12.0	120	12.1	122	122	12.4	12 5	12.6	127	12.0	12.0	140	111	112	142	درع	111	145	116
12.6 3.5	12.8 3.9	12.9 4.3	13.0 4.6	13.1	13.2 5.4	13.3 5.7	6.1	13.5 6.5	6.9	7.3	7.7	13.9 8.1	14.0 8.5	14.1 8.9	9.3	14.3 9.7	くノ		14.5 10.9	
3.3	3.9	4.5	4.0	5.0	5.4	5.7	0.1	0.5	6.9	7.3	7.7	0.1	0.5	0.9	9.3	18.	10.1	10.5	10.9	11.4
18.0	18.0														C	14.				
5.0	5.5													6	P					
														, 0						
18.7	18.8	18.9	19.0	19.0	19.1	19.2	19.3	19.4	19.4	19.5	19.6	19.7	19.7	19.8						
5.2	5.7	6.2	6.7	7.2	7.7	8.3	8.8	9.3	9.8	10.3	10.9	11.4	11.9	12.5						
												(1)								
19.2	19.3	19.5	19.6	19.8	20.1	20.3	20.5	20.7			(7.	21.6							
5.4	5.9	6.4	7.0	7.5	8.2	8.7	9.3	9.9	10.5	11.1	11.8	12.4	13.1	13.7						
											1/2									
16.5	16.5		16.6							in										
4.6	5.0	5.5	5.9	6.3					ΨC	7.										
25.5	25.6								1											
25.5 7.1	25.6 7.8							-ijc	٠											•••
7.1	7.0						•	O.												
8.8	8.8	8.9	8.9	9.0	9.2		1	•												
2.5	2.7	2.9	3.2	3.4	3.7),													
						\leftarrow														